

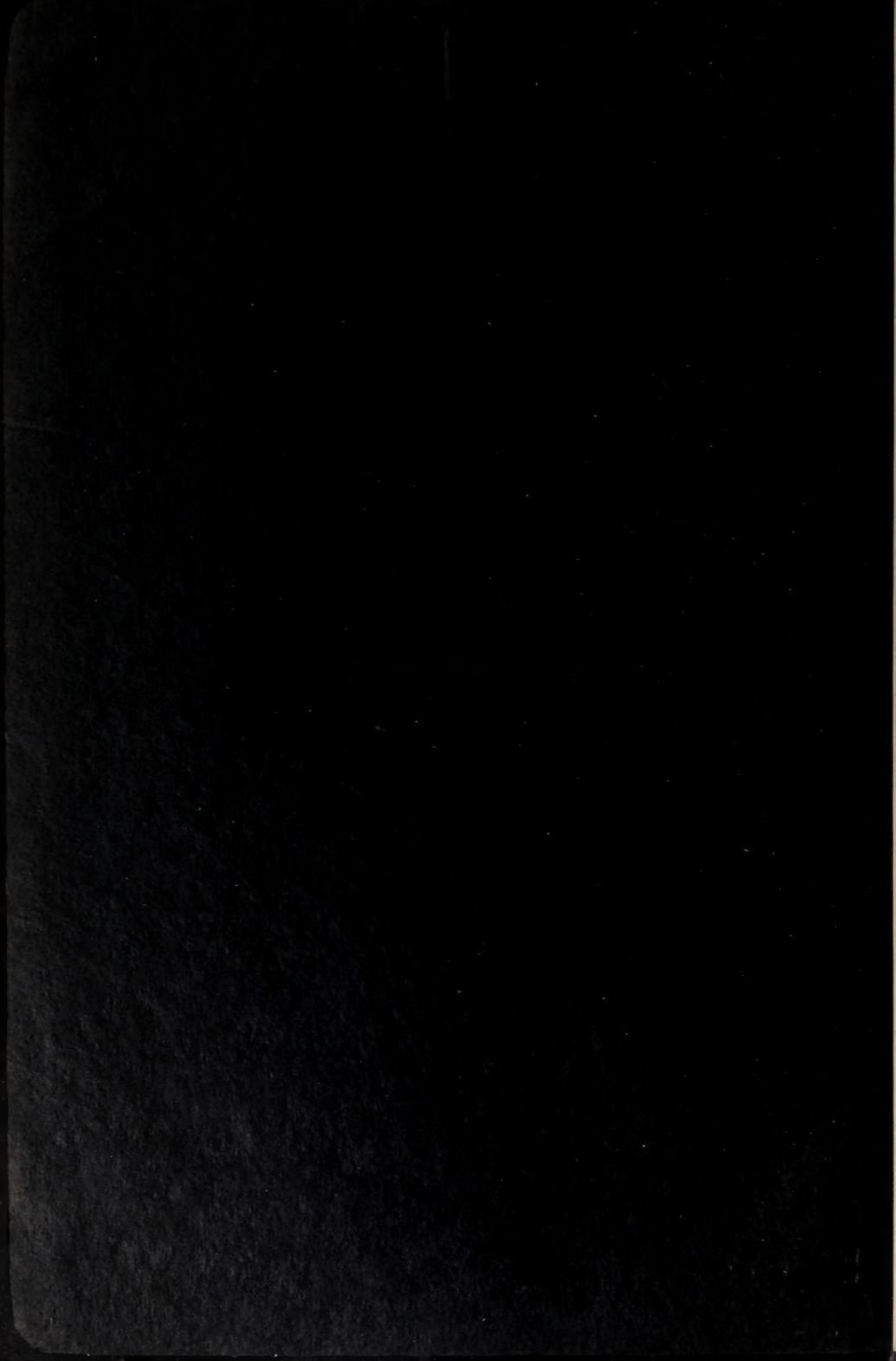
STEEL CONSTRUCTION



CONSOLIDATED STEEL CORPORATION, LTD.

AMERICAN INSTITUTE
OF
STEEL CONSTRUCTION
INC.





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STEEL CONSTRUCTION



First Edition
Eighth Printing
Eighty-fifth Thousand
December, 1930.

Lee H. Miller, Chief Engineer

**AMERICAN INSTITUTE
OF
STEEL CONSTRUCTION
INC.**

EXECUTIVE OFFICE:
200 MADISON AVENUE
NEW YORK, N. Y.

ENGINEERING OFFICE
1050 LEADER BUILDING
CLEVELAND, OHIO

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PREFACE

FIRST EDITION

THIS volume combines the information contained in our previous publications. Considerable new material has been added, and the data regarding the new sections recently produced by the various rolling mills is complete up to the date of publication.

We are also including, a Specification for Fireproofing, which has been prepared for us by a committee of well known engineers. This Specification together with the data derived from tests of insulating material will make possible the designing of the fireproofing for a structural steel frame on a rational basis and supplant the empirical procedure of the past.

New paragraphs have been added to our Code of Standard Practice, and other slight revisions made, which our experience indicates to have been desirable.

The general arrangement of the tabular information regarding the Dimensions, Functions, and Allowable Load for Structural Steel Shapes is now well known. It has been most favorably commented upon, particularly on account of the ease with which the desired information can be found. With this in mind, we have endeavored to design and group all the additional tabular data.

The arrangement of tables to provide the maximum convenience required related data to appear on opposite pages thus causing a few single blank pages. For the convenience of the user these pages have been ruled with cross section lines for notes and diagrams.

A list of General Contents appears on Page 4, and there is a complete index at the back of the book.

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Part I

Standard Specifications

Specification of the American Institute of Steel Construction, Inc. for the Design, Fabrication and Erection of Structural Steel for Buildings; adopted June 1st, 1923, revised Nov. 1st, 1928.

Specification of the American Society for Testing Materials for Structural Steel for Buildings.

Code of Standard Practice of the American Institute of Steel Construction, Inc.; adopted Oct. 1st, 1924, revised 1927; 1928.

Specification of the American Institute of Steel Construction, Inc., for the Fireproofing of Structural Steel for Buildings; adopted Oct. 8th, 1927.

Recommendations of the United States Department of Commerce for the Minimum Allowable Live Loads for Buildings.

The History of Steel and Iron



In 1923 the American Institute of Steel Construction undertook the work of promoting uniform practice in the industry, and in order that its efforts would not be interpreted as being unduly influenced by commercial interests it selected a committee from among the leading talent in the academic, engineering and architectural professions to prepare a Standard Specification on the Design, Fabrication, and Erection of Structural Steel. This committee represented a combined experience of approximately one hundred and fifty years in an industry which is not more than thirty-five years old. The personnel was as follows:

GEORGE F. SWAIN: M. Am Soc C E—M. Am Soc M E—M. Inst C E
M. A R E A—Past President, A S C E—Professor
of Civil Engineering, Harvard University

MILO S. KETCHUM: M. Am Soc C E—M. A R E A—Dean of the College
of Engineering, and Director of the Engineering
Experiment Station of the University of Illinois

E. R. GRAHAM: of Graham, Anderson, Probst & White, Architects,
Chicago, Ill.

W. J. THOMAS: M. Am Soc C E—Chief Engineer, Geo. B. Post &
Sons, Architects, N. Y.

WILBUR J. WATSON: M. Am Soc C E—M. A R E A—President, Watson
Engineering Company, Cleveland, Ohio



STANDARD SPECIFICATION

AMERICAN INSTITUTE OF STEEL CONSTRUCTION

Gentlemen:

After careful deliberation the Committee selected to prepare a Standard Specification for the design, fabrication and erection of structural steel for buildings, submit the accompanying Code for your adoption.

The present Specification contemplates that the inspection, is such that improper material containing defects which should cause rejection is not used. It is not intended to cover material salvaged from previous construction, which should not be used except under rigid supervision and inspection.

It is also understood that the proper loads are taken and that impact is allowed for in each case by adding a proper percentage to the stresses produced by static live loads so that the total stress found in any member is an equivalent static stress. This Specification does not attempt to state definitely what the live, dead, or wind loads should be, or what percentage should be added for impact, as these are factors which should receive the careful consideration of competent engineers for each case. The question of corrosion under unusual conditions should have careful consideration by the engineer.

The question of design is all-important. It necessarily presupposes that the design is good, made by and executed under the supervision of competent structural engineers; that proper provision is made for secondary stresses, eccentric loads, unequal distribution of stresses on rivets, etc.; that the details are suitable and that the workmanship is high grade.

It is recommended that the American Institute of Steel Construction maintain a Committee whose function shall be that of keeping such a Code as we submit consistent with the changing conditions of manufacture, design, and erection. Under these conditions, the Committee considers the unit stresses herein specified are proper.

Respectfully submitted by the Committee:

GEORGE F. SWAIN
MILO S. KETCHUM
E. R. GRAHAM
W. J. THOMAS
WILBUR J. WATSON

June 1st 1923

STANDARD SPECIFICATION FOR STRUCTURAL STEEL FOR BUILDINGS

As adopted by the
American Institute of Steel Construction

1. This Specification defines the practice adopted by the American Institute of Steel Construction for the design, fabrication, and erection of structural steel for buildings.

2. GENERAL

To obtain a satisfactory structure, the following major requirements must be fulfilled.

(a) The material used must be suitable, of uniform quality, and without defects affecting the strength or service of the structure.

(b) Proper loads and conditions must be assumed in the design.

(c) The unit stresses must be suitable for the material used.

(d) The workmanship must be good, so that defects or injuries are not produced in the manufacture.

(e) The computations and design must be properly made so that the unit stresses specified shall not be exceeded, and the structure and its details shall possess the requisite strength and rigidity.

3. MATERIAL

Structural steel shall conform to the Standard Specifications of the American Society for Testing Materials for Structural Steel for Buildings, Serial Designation A 9-21, as amended to date.

4. LOADING

(a) Steel structures shall be designed to sustain the dead weight imposed upon them, including the weight of the steel frame itself, and, in addition, the maximum live load as specified in each particular case. Proper provision shall be made for temporary stresses caused by erection.

(b) In cases where live loads have the effect of producing impact or vibration, a proper percentage shall be added to the static live load stresses to provide for such influences, so that the total stress found in any member is an equivalent static stress.

(c) Proper provision shall be made for stresses caused by wind both during erection and after completion of the building. The wind pressure is dependent upon the conditions of exposure, but the allowable stresses specified in section five (5), paragraphs (f) and (g), are based upon the steel frame being designed to carry a wind pressure of not less than twenty (20) pounds

per square foot on the vertical projection of exposed surfaces during erection, and fifteen (15) pounds per square foot on the vertical projection of the finished structure.

(d) Proper provision shall be made to securely fasten the reaction points of all steel construction and transmit the stresses to the foundations of the structure.

5. ALLOWABLE STRESSES

All parts of the structure shall be so proportioned that the sum of the maximum static stresses in pounds per sq. in. shall not exceed the following:

(a) *Tension.

Rolled Steel, on net section 18000

On the area of the nominal diameter of rivets under the limitations defined in Section 13, Paragraph e 13500

(b) Compression.

Rolled Steel, on short lengths or where lateral deflection is prevented. 18000

On gross section of columns,

$$18000$$

$$1 + \frac{l^2}{18000r^2}$$

with a maximum of 15000

in which l is the unsupported length of the column, and r is the corresponding least radius of gyration of the section, both in inches.

For main compression members, the ratio l/r shall not exceed 120, and for bracing and other secondary members, 200.

(c) Bending.

On extreme fibres of rolled shapes, and built up sections, net section, if lateral deflection is prevented 18000

When the unsupported length l exceeds 15 times b , the width of the compression flange, the stress in pounds per sq. in. in the latter shall not exceed

$$20000$$

$$1 + \frac{l^2}{2000b^2}$$

The laterally unsupported length of beams and girders shall not exceed 40 times b the width of the compression flange.

On extreme fibres of pins, when the forces are assumed as acting at the center of gravity of the pieces 27000

(d) Shearing.

On pins 13500

On power-driven rivets 13500

On turned bolts in reamed holes with a clearance of not more than 1/50 of an inch 13500

On hand-driven rivets 10000

On unfinished bolts 10000

*revised Nov. 1st, 1928.

On the gross area of the webs of beams and girders, where h , the height between flanges in inches, is not more than 60 times t , the thickness of the web in inches.....12000

On the gross area of the webs of beams and girders if the web is not stiffened where h , the height between flanges in inches, is more than 60 times t , the thickness of the web, the maximum shear per square inch, $\frac{V}{A}$ shall not exceed

$$1 + \frac{18000}{7200 t^2}$$

In Which V is the total shear, and A is gross area of web in square inches.

(e) Bearing.

	Double Shear	Single Shear
On pins.....	30000	24000
On power-driven rivets.....	30000	24000
On turned bolts in reamed holes.....	30000	24000
On hand-driven rivets.....	20000	16000
On unfinished bolts.....	20000	16000
On expansion rollers per lineal inch 600 times the diameter of the roller in inches.		

(f) Combined Stresses. For combined stresses due to wind and other loads, the permissible working stress may be increased $33\frac{1}{3}\%$, provided the section thus found is not less than that required by the dead and live loads alone.

(g) Members Carrying Wind Only.

For members carrying wind stresses only, the permissible working stresses may be increased $33\frac{1}{3}\%$.

6. SYMMETRICAL MEMBERS.

Sections shall preferably be symmetrical.

7. BEAMS AND GIRDERS.

(a) Rolled beams shall be proportioned by the moment of inertia of their net section. Plate girders with webs fully spliced for tension and compression shall be so proportioned that the unit stress on the net section does not exceed the stresses specified in section five (5) as determined by the moment of inertia of the net section.

(b) Plate girder webs shall have a thickness of not less than 1-160 of the unsupported distance between the flanges.

(c) Web splices shall consist of a plate on each side of the web capable of transmitting the full stress through the splice rivets.

(d) **Stiffeners.** Stiffeners shall be required on the webs of rolled beams and plate girders at the ends and at points of concentrated loads, and at other points where h the clear distance between flanges is greater than $85t\sqrt{18000(A/V)-1}$, in which t is the thickness of the web. When stiffeners are required, the distance in inches between them shall not be greater than $85t\sqrt{18000(A/V)-1}$, or not greater than 6 feet. When h is greater than 60 times t the thickness of the web of a plate girder, stiffeners shall be required at distances not greater than 6 feet apart. Stiffeners under or over concentrated loads shall be proportioned to distribute such loads into the web.

Plate girder stiffeners shall generally be in pairs, one on each side of the web, and shall have a close bearing against the flange angles at points of concentrated loading; stiffeners over the end bearings shall be on plate fillers. The pitch of rivet in stiffeners shall not exceed 6".

(e) **Flange plates** of all girders shall be limited in width so as not to extend more than 6" or more than 12 times the thickness of thinnest plate beyond the outer row of rivets connecting them to the angles.

(f) **Crane runway girders** and the supporting framework shall be proportioned to resist the greatest horizontal stresses caused by the operation of the cranes.

(g) **Rivets** connecting the flanges to the web at points of direct load on the flange between stiffeners shall be proportioned to carry the resultant of the longitudinal and transverse shears.

(h) **Rivets** connecting the flanges to the webs of plate girders and of columns subjected to bending shall be so spaced as to carry the increment of the flange stress between the rivets.

8. COLUMN BASES.

(a) Proper provision shall be made to distribute the column loads on the footings and foundations.

(b) The top surface of all column bases shall be planed for the column bearing.

(c) Column bases shall be set true and level, with full bearing on the masonry, and be properly secured to the footings.

9. EXCENTRIC LOADING.

Full provision shall be made for stresses caused by excentric loads.

10. COMBINED STRESSES.

(a) Members subject to both direct and bending stresses shall be so proportioned that the greatest combined stresses shall not exceed the allowed limits.

(b) All members and their connections which are subject to stresses of both tension and compression due to the action of live loads shall be designed

to sustain stress giving the largest section, with 50% of the smaller stress added to it. If the reversal of stress is due to the action of wind, the member shall be designed for the stress giving the largest section and the connections proportioned for the largest stress.

11. ABUTTING JOINTS.

Compression members when faced for bearings shall be spliced sufficiently to hold the connecting members accurately in place. Other joints in riveted work, whether in tension or compression, shall be fully spliced.

12. NET SECTIONS.

(a) In calculating tension members, the net section shall be used, and in deducting the rivet holes they shall be taken $\frac{1}{8}$ inch greater in diameter than the nominal diameter of the rivets.

(b) Pin-connected tension members shall have the section through the pinhole 25% in excess of the net section of the member, and a net section back of the pin hole equal to 75% of that required through the pin hole.

13. RIVETS AND BOLTS.

(a) In proportioning rivets, the nominal diameter of the rivet shall be used.

(b) Rivets carrying calculated stresses, and whose grip exceeds five diameters, shall have their number increased 1% for each additional $\frac{1}{10}$ inch in the rivet grip. Special care shall be used in heating and driving such rivets.

(c) Rivets shall be used for the connections of main members carrying live loads which produce impact, and for connections subject to reversal of stresses.

(d) Finished bolts in reamed holes may be used in shop or field work where it is impracticable to obtain satisfactory power-driven rivets. The finished shank shall be long enough to provide full bearing, and washers used under the nuts to give full grip when turned tight.

Unfinished bolts may be used in shop or field work for connections in small structures used for shelters, and for secondary members of all structures such as purlins, girts, door and window framing, alignment bracing and secondary beams in floor.

*(e) The end reaction stresses of trusses, girders, or beams, and the axial stresses of tension or compression members which are carried on rivets, shall have such stresses developed by the shearing and bearing values of the rivets; but where rivets are used for shelf or bracket supports or for connections that also provide rigidity to the structure, the rivets may in addition to their shearing and bearing stresses, carry tension as defined in Sec. 5 (a).

14. RIVET SPACING.

(a) The minimum distance between centers of rivet holes shall be three diameters of the rivet; but the distance shall preferably be not less than $4\frac{1}{2}$

*revised Nov. 1st, 1928.

inches for $1\frac{1}{4}$ inch rivets, 4 inches for $1\frac{3}{8}$ inch rivets, $3\frac{1}{2}$ inches for 1 inch rivets, 3 inches for $\frac{7}{8}$ inch rivets, $2\frac{1}{2}$ inches for $\frac{3}{4}$ inch rivets, 2 inches for $\frac{5}{8}$ inch rivets, and $1\frac{3}{4}$ inches for $\frac{1}{2}$ inch rivets. The maximum pitch in the line of stress of compression members composed of plates and shapes shall not exceed 16 times the thinnest outside plate or shape, nor 20 times the thinnest enclosed plate or shape with a maximum of 12 inches, and at right angles to the direction of stress the distance between lines of rivets shall not exceed 30 times the thinnest plate or shape. For angles in built sections with two gage lines, with rivets staggered, the maximum pitch in the line of stress in each gage line shall not exceed 24 times the thinnest plate with a maximum of 18 inches.

(b) In tension members composed of two angles, a pitch of 3'-6" will be allowed, and in compression members, 2'-0", but the ratio l/r for each angle between rivets shall not be more than $\frac{3}{4}$ of that for the whole member.

(c) The pitch of rivets at the ends of built compression members shall not exceed four diameters of the rivets for a length equal to $1\frac{1}{2}$ times the maximum width of the member.

(d) The minimum distance from the center of any rivet hole to a sheared edge shall be $2\frac{1}{4}$ inches for $1\frac{1}{4}$ inch rivets, 2 inches for $1\frac{3}{8}$ inch rivets, $1\frac{3}{4}$ inches for 1 inch rivets, $1\frac{1}{2}$ inches for $\frac{7}{8}$ inch rivets, $1\frac{1}{4}$ inches for $\frac{3}{4}$ inch rivets, $1\frac{1}{8}$ inches for $\frac{5}{8}$ inch rivets, and 1 inch for $\frac{1}{2}$ inch rivets. The maximum distance from any edge shall be 12 times the thickness of the plate, but shall not exceed 6 inches.

15. CONNECTIONS.

(a) Connections carrying calculated stresses except for lacing, sag bars, or angles, hand rails, or beam connections, shall not have less than 2 rivets; or for field connections not less than 3 rivets.

(b) Members meeting at a joint shall have their lines of center of gravity meet at a point if practicable; if not, provision shall be made for any excentricity.

(c) The rivets at the ends of any member transmitting the stresses into that member should have their centers of gravity in the line of the center of gravity of the member; if not, provision shall be made for the effect of the resulting excentricity. Pins may be so placed as to counteract the effect of bending due to dead load.

(d) When a beam or girder "A" is connected to another member in such a manner that "A" acts as a continuous or fixed end beam, proper provision shall be made for the bending moments at such a connection.

(e) Where stress is transmitted from one piece to another, through a loose filler, the number of rivets shall be properly increased; tight-fitting fillers shall be preferred.

16. LATTICE.

(a) The open sides of compression members shall be provided with lattice having tie plates at each end and at intermediate points if the lattice is

interrupted. Tie plates shall be as near the ends as practicable. In main members carrying calculated stresses the end tie plates shall have a length of not less than the distance between the lines of rivets connecting them to the flanges, and intermediate ones of not less than one-half of this distance. The thickness of tie plates shall not be less than one-fiftieth of the distance between the lines of rivets connecting them to the segments of the members, and the rivet pitch shall not be more than four diameters. Tie plates shall be sufficient in size and number to equalize the stress in the parts of the members.

(b) Lattice bars shall have neatly finished ends. The thickness of lattice bars shall be not less than one-fortieth for single lattice and one-sixtieth for double lattice of the distance between end rivets; their minimum width shall be as follows:

For 15" channels, or built sections with 3½" and 4" angles—2¼" (¾" rivets), or 2½" (⅞" rivets).

For 12", 10", and 9" channels, or built sections with 3" angles—2¼" (¾" rivets).

For 8" and 7" channels, or built sections with 2½" angles—2" (⅝" rivets), or 2¼" (¾" rivets)

For 6" and 5" channels, or built sections with 2" angles—1½" (½" rivets), or 1¾" (⅝" rivets).

(c) The inclination of lattice bars to the axis of the members shall generally be not less than 45° but when the distance between the rivet lines in the flanges is more than 15 inches, the lattice shall be double and riveted at the intersection if bars are used, or else shall be made of angles.

(d) Lattice bars shall be so spaced that the ratio l/r of the flange included between their connections shall be not over ¾ of that of the member as a whole.

17. EXPANSION.

Proper provision shall be made for expansion and contraction.

18. MINIMUM THICKNESS.

No steel less than $\frac{5}{16}$ inch thick shall be used for exterior construction, nor less than ¼ inch for interior construction, except for linings or fillers and rolled structural shapes.

These provisions do not apply to light structures such as skylights, marquees, fire-escapes, light one-story buildings, or light miscellaneous steel work.

For trusses having end reactions of 35000 pounds or over, the Gusset Plates shall be not less than ⅜ inch thick.

19. ADJUSTABLE MEMBERS.

The initial stress in adjustable members shall be assumed as not less than 5000 lbs.

20. WORKMANSHIP.

(a) All workmanship shall be equal to the best practice in modern structural shops.

(b) Drifting to enlarge unfair holes shall not be permitted.

(c) The several pieces forming built sections shall be straight and fit close together; and finished members shall be free from twists, bends, or open joints.

(d) Rolled sections, except for minor details, shall not be heated.

(e) Wherever steel castings are used, they shall be properly annealed.

(f) **Punching.** Material may be punched $\frac{1}{16}$ inch larger than the nominal diameter of the rivets, whenever the thickness of the metal is equal to or less than the diameter of the rivets, plus $\frac{1}{8}$ inch. When the metal is thicker than the diameter of the rivet, plus $\frac{1}{8}$ inch, the holes shall be drilled, or sub-punched and reamed.

*(g) Rivets are to be driven hot, and wherever practicable, by power. Rivet heads shall be of hemispherical shape and uniform size throughout the work for the same size rivet, full, neatly finished, and concentric with the holes. Rivets, after driving, shall be tight, completely filling the holes, and with heads in full contact with the surface. Rivets shall be heated uniformly and their temperature before driving should not exceed 1950° F. which is a light yellow color. A gun should not be used for driving after the temperature is below 1000° F., which is a blood red color.

(h) Compression joints depending upon contact bearing shall have the bearing surfaces truly faced after the members are riveted. All other joints shall be cut or dressed true and straight, especially where exposed to view.

*(i) The use of a cutting torch is permissible if the metal being cut is not carrying stresses during the operation. Stresses shall not be transmitted through a flame cut surface. The radius of re-entrant flame cut fillets shall be as large as possible, but never less than 1". To determine the net area of members so cut, $\frac{1}{8}$ " shall be deducted from the flame cut edges.

21. PAINTING.

*(a) Parts not in contact, but inaccessible after assembling, shall be properly protected by paint. Surfaces to be riveted in contact shall not be painted.

(b) All steel work, except where encased in concrete, shall be thoroughly cleaned and given one coat of acceptable metal protection well worked into the joints and open spaces.

(c) Machine finished surfaces shall be protected against corrosion.

(d) Field painting is a phase of maintenance, but it is important that unless otherwise properly protected, all steel work shall after erection be protected by a field coat of good paint applied by a competent painter.

*revised Nov. 1st, 1928.

22. ERECTION.

(a) The frame of all steel skeleton buildings shall be carried up true and plumb, and temporary bracing shall be introduced wherever necessary to take care of all loads to which the structure may be subjected, including erection equipment, and the operation of same. Such bracing shall be left in place as long as may be required for safety.

(b) As erection progresses the work shall be securely bolted up to take care of all dead load, wind and erection stresses.

(c) Wherever piles of material, erection equipment, or other loads are carried during erection, proper provision shall be made to take care of stresses resulting from the same.

(d) No riveting shall be done until the structure has been properly aligned.

(e) Rivets driven in the field shall be heated and driven with the same care as those driven in the shop.

23. INSPECTION.

(a) Material and workmanship at all times shall be subject to the inspection of experienced engineers representing the purchaser.

(b) Material or workmanship not conforming to the provisions of this Specification shall be rejected at any time defects are found during the progress of the work.

(c) The Contractor furnishing such material or doing such work shall promptly replace the same.

(d) All inspection as far as possible shall be made at the place of manufacture, and the Contractor or Manufacturer shall co-operate with the Inspector, permitting access for inspection to all places where work is being done.

AMERICAN SOCIETY FOR TESTING MATERIALS

1315 Spruce Street, Philadelphia, Pa.

STANDARD SPECIFICATIONS FOR STRUCTURAL STEEL FOR BUILDINGS

Serial Designation: A9-29

These specifications are issued under the fixed designation A 9; the final number indicates the year of original adoption as standard or, in the case of revision, the year of last revision.

Adopted, 1901; Revised, 1909, 1913, 1914, 1916, 1921, 1924, 1929.

I. MANUFACTURE**Process**

1. (a) Structural steel, except as noted in Paragraph (b), shall be made by either or both the following processes: Bessemer or open-hearth.

(b) Rivet steel, and steel for plates or angles over $\frac{3}{4}$ in. in thickness which are to be punched, shall be made by the open-hearth process.

II. CHEMICAL PROPERTIES AND TESTS**Chemical Composition**

2. The steel shall conform to the following requirements as to chemical composition:

	Structural Steel	Rivet Steel
Phosphorus	<div> <div>{ Bessemer.....</div> <div>{ Open-hearth.....</div> </div>	<div> <div>not over 0.10 per cent.....</div> <div>not over 0.06 per cent.....</div> </div>
Sulfur.....	not over 0.06 per cent.....	not over 0.06 per cent
Copper, when copper steel is specified.....	not over 0.045 per cent	not over 0.045 per cent
	not under 0.20 per cent.....	not under 0.20 per cent

Ladle Analyses

3. (a) A carbon determination, and a copper determination, when copper steel is specified shall be made of each melt of bessemer steel, and determinations for manganese, phosphorus and sulfur representing the average of the melts applied for each 12-hour period.

(b) An analysis of each melt of open-hearth steel shall be made to determine carbon, manganese, phosphorus and sulfur; also copper when copper steel is specified.

(c) These analyses shall be made by the manufacturer from test ingots taken during the pouring of each melt. The chemical composition thus determined shall be reported to the purchaser or his representative and the percentages of phosphorus and sulfur and also copper when copper steel is specified shall conform to the requirements specified in Section 2.

Check Analyses

4. Analyses may be made by the purchaser from finished material representing each melt. The phosphorus and sulfur content thus determined shall not exceed that specified in Section 2 by more than 25 per cent.

III. PHYSICAL PROPERTIES AND TESTS

Tension Tests

5. (a) The material shall conform to the following requirements as to tensile properties:

Properties Considered	Structural Steel	Rivet Steel
Tensile strength, lb. per sq. in. . . .	55,000—65,000	46,000—56,000
Yield point, min., per sq. in.	0.5 tens. str.	0.5 tens. str.
but in no case less than	30,000	25,000
Elongation in 8 in., min., per cent	<u>1,400,000^a</u> Tens. str.	<u>1,400,000</u> Tens. str.
Elongation in 2 in., min., per cent	22

^aSee Section 6.

(b) The yield point shall be determined by the drop of the beam of the testing machine.

Modifications in Elongation

6. (a) For structural steel over $\frac{3}{4}$ in. in thickness, a deduction from the percentage of elongation in 8 in. specified in Section 5 (a) of 0.25 per cent shall be made for each increase of $\frac{3}{32}$ in. of the specified thickness above $\frac{3}{4}$ in., to a minimum of 18 per cent.

(b) For structural steel under $\frac{5}{16}$ in. in thickness, a deduction from the percentage of elongation in 8 in. specified in Section 5 (a) of 1.25 per cent shall be made for each decrease of $\frac{3}{32}$ in. of the specified thickness below $\frac{5}{16}$ in.

Bend Tests

7. (a) Bend test specimens, except as specified in Paragraph (b), shall stand being bent cold through 180 deg. without cracking on the outside of the bent portion, as follows: For material $\frac{3}{4}$ in. or under in thickness, flat on itself; for material over $\frac{3}{4}$ in. to and including $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to the thickness of the specimen; and for material over $1\frac{1}{4}$ in. in thickness, around a pin the diameter of which is equal to twice the thickness of the specimen.

(b) Bend test specimens for rivet steel shall stand being bent cold through 180 deg. flat on themselves without cracking on the outside of the bent portion.

Test Specimens

8. (a) Test specimens shall be prepared for testing from the material in its rolled or forged condition, except as specified in Paragraphs (b) and (c).

(b) Test specimens for annealed material shall be prepared from the material as annealed for use, or from a short length of a full section similarly treated.

(c) Test specimens for rivet bars which have been cold-drawn shall be normalized before testing.

(*u*) Test specimens shall be taken longitudinally and, except as specified in Paragraphs (*f*), (*g*), and (*h*), shall be of the full thickness or section of material as rolled.

(*e*) Test specimens for plates, shapes and flats may be machined to the form and dimensions shown in Fig. 1, or with both edges parallel.

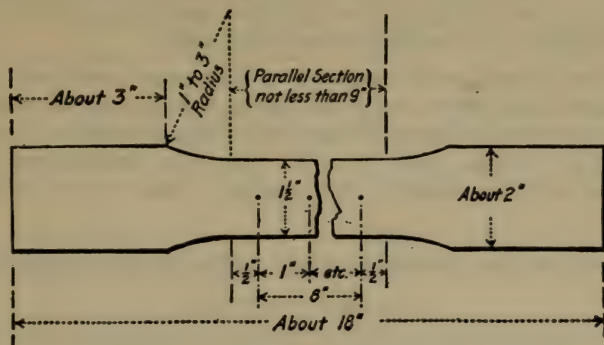
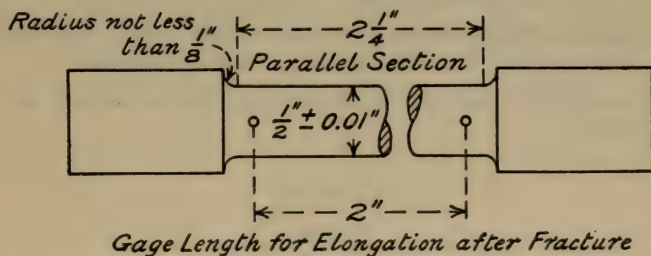


FIG. 1.

(*f*) Tension test specimens for material over $1\frac{1}{2}$ in. in thickness or diameter, except pins and rollers, may be machined to a thickness or diameter of at least $\frac{3}{4}$ in. for a length of at least 9 in., or they may conform to the dimensions shown in Fig. 2.



Note:—The Gauge Length, Parallel Section, and Fillets shall be as Shown, but the Ends may be of any Shape to fit the Holders of the Testing Machine in such a Way that the Load shall be axial.

FIG. 2.

(*g*) Bend test specimens for material over $1\frac{1}{2}$ in. in thickness or diameter, except pins and rollers, may be machined to a thickness or diameter of at least $\frac{3}{4}$ in. or to 1 by $\frac{1}{2}$ in. in section.

(*h*) Tension test specimens for pins and rollers shall conform to the dimensions shown in Fig. 2, and bend test specimens shall be 1 by $\frac{1}{2}$ in. in section.

(*i*) Test specimens for pins and rollers shall be taken so that the axis is 1 in. from the surface.

(*j*) The machined sides of rectangular bend test specimens may have the corners rounded to a radius not over $\frac{1}{16}$ in.

Number of Tests

9. (a) One tension and one bend test shall be made from each melt; except that if material from one melt differs $\frac{3}{8}$ in. or more in thickness, one tension and one bend test shall be made from both the thickest and the thinnest material rolled.

(b) If any test specimen shows defective machining or develops flaws, it may be discarded and another specimen substituted.

(c) If the percentage of elongation of any tension test specimen is less than that specified in Section 5 (a) and any part of the fracture is more than $\frac{3}{4}$ in. from the center of the gage length of a 2-in. specimen or is outside the middle third of the gage length of an 8-in. specimen, as indicated by scribe scratches marked on the specimen before testing, a retest shall be allowed.

IV. PERMISSIBLE VARIATIONS IN WEIGHT AND THICKNESS

Permissible Variations

10. (a) The cross-section or weight of each piece of steel shall not vary more than 2.5 per cent from that specified; except in the case of sheared plates, which shall be covered by the permissible variations specified in Paragraphs (b) and (c). (One cubic inch of rolled steel is assumed to weigh 0.2833 lb.)

(b) **Sheared Plates, When Ordered to Weight per Square Foot:** The weight of each lot¹ in each shipment shall not vary from the weight ordered more than the amount given in Table I.

(c) **Sheared Plates, When Ordered to Thickness:** The thickness of each plate shall not vary more than 0.01 in. under that ordered.

The overweight of each lot¹ in each shipment shall not exceed the amount given in Table II.

V. FINISH

Finish

11. The finished material shall be free from injurious defects and shall have a workmanlike finish.

VI. MARKING

Marking

12. The name or brand of the manufacturer and the melt number shall be legibly stamped or rolled on all finished material, except that rivet and lattice bars and other small sections shall, when loaded for shipment, be properly separated and marked for identification. The identification marks shall be legibly stamped on the end of each pin and roller. The melt number shall be legibly marked, by stamping if practicable, on each test specimen.

¹The term "lot" as applied to Table I means all of the plates of each group width and group weight; as applied to Table II, it means all of the plates of each group width and group thickness.

VII. INSPECTION AND REJECTION

Inspection

13. The inspector representing the purchaser shall have free entry, at all times while work on the contract of the purchaser is being performed, to all parts of the manufacturer's works which concern the manufacture of the material ordered. The manufacturer shall afford the inspector, without charge, all reasonable facilities to satisfy him that the material is being furnished in accordance with these specifications. All tests (except check analyses) and inspection shall be made at the place of manufacture prior to shipment, unless otherwise specified, and shall be so conducted as not to interfere unnecessarily with the operation of the works.

Rejection

14. (a) Unless otherwise specified, any rejection based on tests made in accordance with Section 4 shall be reported within five working days from the receipt of samples.

(b) Material which shows injurious defects subsequent to its acceptance at the manufacturer's works will be rejected, and the manufacturer shall be notified.

Rehearing

15. Samples tested in accordance with Section 4, which represent rejected material, shall be preserved for two weeks from the date of the test report. In case of dissatisfaction with the results of the tests, the manufacturer may make claim for a rehearing within that time.

Table I.—Permissible Variations of Rectangular Plates Ordered to Weight.

Permissible Variations in Average Weights per Square Foot of Plates for Widths Given, Expressed in Percentages of Ordered Weights																	
Ordered Weight, Lb. per Sq. Ft.	Under 48 in.,		48 to 60 in.,		60 to 72 in.,		72 to 84 in.,		84 to 96 in.,		96 to 108 in.,		108 to 120 in.,		120 to 132 in.,		Ordered Weight, Lb. per Sq. Ft.
	Over	Under	Over	Under	Over	Under	Over	Under	Over	Under	Over	Under	Over	Under	Over	Under	
Under 5	5	3	5.5	3	6	3	7	3	7.5	3	8	3	8.5	3	9	3	Under 5
5 to 7.5 excl.	4.5	3	5	3	5.5	3	6	3	6.5	3	7	3	7.5	3	8	3	5 to 7.5 excl.
7.5 to 10 "	4	3	4.5	3	5	3	5.5	3	6	3	6.5	3	7	3	7.5	3	7.5 to 10 "
10 to 12.5 "	3.5	2.5	4	3	4.5	3	5	3	5.5	3	6	3	6.5	3	7	3	10 to 12.5 "
12.5 to 15 "	3	2.5	3.5	2.5	4	3	4.5	3	5	3	5.5	3	6	3	6.5	3	12.5 to 15 "
15 to 17.5 "	2.5	2.5	3	2.5	3.5	2.5	4	3	4.5	3	5	3	5.5	3	6	3	15 to 17.5 "
17.5 to 20 "	2.5	2	2.5	2.5	3	2.5	3.5	2.5	4	3	4.5	3	5	3	5.5	3	17.5 to 20 "
20 to 25 "	2	2	2.5	2	2.5	2.5	3	2.5	3.5	2.5	4	3	4.5	3	5	3	20 to 25 "
25 to 30 "	2	2	2	2	2.5	2.5	2.5	2.5	3	2.5	3.5	2.5	4	3	4.5	3	25 to 30 "
30 to 40 "	2	2	2	2	2	2	2.5	2.5	2.5	3	2.5	3.5	3	4	3	4.5	30 to 40 "
40 or over	2	2	2	2	2	2	2	2	2.5	2	2.5	2.5	3	2.5	3	4	40 or over

Note.—The weight per square foot of individual plates shall not vary from the ordered weight by more than $1\frac{1}{3}$ times the amount given in this table.

Table II.—Permissible Overweights of Rectangular Plates Ordered to Thickness

Ordered Thickness, In.	Permissible Excess in Average Weights per Square Foot of Plates for Widths Given, Expressed in Percentages of Nominal Weights								Ordered Thickness, In.
	Under 48 in.	48 to 60 in., excl.	60 to 72 in., excl.	72 to 84 in., excl.	84 to 96 in., excl.	96 to 108 in., excl.	108 to 120 in., excl.	120 to 132 in., excl.	132 in. or over
Under $\frac{1}{8}$	9	10	12	14	12	12	14	16	19
$\frac{1}{8}$ to $\frac{1}{16}$ excl.	8	9	10	12	10	10	12	14	17
$\frac{1}{16}$ to $\frac{1}{4}$ "	7	8	9	10	9	9	10	12	15
$\frac{1}{4}$ to $\frac{3}{8}$ "	6	7	8	9	8	8	9	10	13
$\frac{3}{8}$ to $\frac{1}{2}$ "	5	6	7	8	7	7	8	9	11
$\frac{1}{2}$ to $\frac{5}{8}$ "	4.5	5	6	7	6	6	7	8	9
$\frac{5}{8}$ to 1 "	4	4.5	5	6	5	5	6	7	8
1 to $1\frac{1}{4}$ "	3.5	4	4.5	5	4.5	4.5	5	6	7
$1\frac{1}{4}$ to $1\frac{3}{4}$ "	3	3.5	4	4.5	4	4	5	6	7
$1\frac{3}{4}$ to 2 "	2.5	3	3.5	4	3.5	3.5	4	5	6
2 or over	2.5	2.5	3	3.5	4	4.5	5	6	7

Ordered Thickness, In.

Under $\frac{1}{8}$

$\frac{1}{8}$ to $\frac{1}{16}$ excl.

$\frac{1}{16}$ to $\frac{1}{4}$ "

$\frac{1}{4}$ to $\frac{3}{8}$ "

$\frac{3}{8}$ to $\frac{1}{2}$ "

$\frac{1}{2}$ to $\frac{5}{8}$ "

$\frac{5}{8}$ to 1 "

1 to $1\frac{1}{4}$ "

$1\frac{1}{4}$ to $1\frac{3}{4}$ "

$1\frac{3}{4}$ to 2 "

2 or over

CODE OF STANDARD PRACTICE

PREFACE

Since the use of structural steel came into existence about 1890, there has developed an industry engaged in the fabrication and erection of this material. At the present time this industry is furnishing annually over \$300,000,000 worth of material to the public.

During this period of evolution it is obvious that many inconsistent practices should have come into existence, and the American Institute of Steel Construction, representing the industry between the rolling mills and the buying public, have undertaken the codifying of the various conditions, with a view of establishing uniform practice.

The Institute's Specification on the design, fabrication, and erection of structural steel has been received with wide spread approval, and this Code of Standard Practice is now being issued to cover conditions not touched in the Specification.

CODE OF STANDARD PRACTICE

As adopted by the
American Institute of Steel Construction, Inc.

SECTION 1. GENERAL

(a) Scope.

The rules and practices hereinafter defined are adopted by the American Institute of Steel Construction as standard for the industry and shall govern all conditions where the contract between the buyer and seller does not specify otherwise and where they do not conflict with local or state requirements.

(b) Design.

Unless otherwise specified or required, the design, fabrication and erection of structural steel shall conform to the Standard Specification of the American Institute of Steel Construction for buildings, dated June 1, 1923, or as amended to date.

(c) Plans and Specifications for bidding.

The plans shall show a complete design with sizes, sections and the relative location of various members with floor levels, column centers and offsets figured, and shall show the character of the work to be performed with sufficient dimensions to permit the making of an accurate estimate of cost. Plans shall be made to scale not less than $\frac{1}{8}$ " to the foot, and large enough to convey the information adequately.

Wind bracing and special details when required shall be shown in sufficient detail regarding rivets and construction to permit an accurate estimate of cost.

(d) Responsibility of Design and Erection.

If the design, plans and specifications are prepared by the Buyer, the Seller shall not be responsible for the suitability, strength, rigidity or the practicability of erection.

SECTION 2. CLASSIFICATION

The Steel and iron items entering into the construction of a structure are divided into the following classes:

CLASS "A"—Structural Steel and Iron

CLASS "B"—Ornamental Steel and Iron

CLASS "C"—Steel Floor Joists

CLASS "D"—Miscellaneous Steel and Iron

In contracting to furnish the material for a structure where the material to be furnished is designated as structural steel and iron, ornamental steel and iron, steel floor joists, or miscellaneous steel and iron, the Seller will furnish only such items under each classification as are listed below, and no other items will be included unless by special agreement. In cases where materials in excess of minimum requirements are furnished to provide for waste or loss, all unused material remaining after completion of work shall be the property of the Seller and returned to him.

Unless specifically agreed to in the contract, the Seller of the structural steel "Class A" will not provide field connections or field holes for the ornamental steel and iron "Class B," the miscellaneous steel and iron "Class D," nor the materials for any other trades.

(a) Class "A" Structural Steel and Iron.

Contracts taken to furnish the structural steel and iron for a building are based on furnishing the following items only:

- Anchors for structural steel only
- Bases of steel or iron only
- Beams of rolled structural steel
- Bearing plates for structural steel
- Brackets made of structural steel shapes
- Channels of rolled structural steel
- Channels and angle supports only for suspended ceilings where they attach to structural steel, but not including small channel or angle furring
- Columns, structural steel, cast iron and pipe
- Girders of structural steel
- Grillage beams and girders—structural steel
- Hangers of structural steel
- Lintels as shown or enumerated
- Marquise (structural frame only)
- Rivets and bolts for field connections, as follows:
 1. The Seller shall furnish sufficient rivets of suitable size, plus at least 10% to cover waste for all field connections of steel to steel which are designated as riveted field connections.
 2. The Seller shall furnish sufficient bolts of suitable size, plus 5% to cover waste for all field connections of steel to steel which are designated to be bolted.
 3. No fitting up bolts or washers will be included unless specifically called for.
- Separators, angles, tees, clips, bracing and detail fittings in connection with structural steel frame
- Tie rods
- Trusses of structural steel

(b) Class "B" Ornamental Steel and Iron.

Contracts taken to furnish the ornamental steel and iron for a building are based on furnishing the following items only:

- All bronze and brass work, except hardware fittings
- Balconies
- Cast iron cornices
- Curtain guides
- Elevator fronts and enclosures
- Grilles and gratings
- Iron store fronts
- Lamp standards and brackets
- Marquise (steel or iron, except frame) see Class "A"

- Ornamental brackets, steel or iron
- Ornamental inside stairs, steel or iron
- Ornamental outside steel or iron stairs, including fire escapes
- Safety treads
- Railings (gas pipe, ornamental or brass)
- Sills and thresholds (brass, steel or iron)
- Spiral stairs, steel or iron
- Window sills and frames, steel or iron
- Wire work, ornamental steel or iron

(c) Class "C" Steel Floor Joists.

Contracts taken to furnish the steel floor joists for a building are based on furnishing the following items only:

- Steel joists which are not a part of the structural steel frame for the building, and which are devised to carry the floor or roof panels.
- Bracing and bridging for floor joists; clips for fastening floor joists
- Stirrup and hanger for floor joists
- Ties for floor joists

(d) Class "D" Miscellaneous Steel and Iron.

The nature and character of the material of this classification makes it impossible to cover all items and it is recommended that the Seller taking the contract to furnish the miscellaneous steel and iron work for a building specify all items in detail which it is intended to furnish. The general list of items under this classification is as follows:

- Area gratings
- Cast iron cover and frames
- Cast iron rainwater receivers
- Cast iron downspout shoes
- Cleanouts
- Coal chutes
- Column guards
- Door frames and bucks
- Foot scrapers
- Furnace or fireplace dampers
- Flag pole
- Ladders
- Pin rails
- Sidewalk doors
- Sills and curb angles, and anchors for same
- Special bolts or anchors where distinctly shown on the plans
- Stairs made of plain structural steel—not including treads of other materials
- Stacks
- Steel and cast iron platforms
- Steel or iron chimney caps
- Thimbles
- Wall plate anchors

Wheel guards

Window guards

Wire screens for partitions, door and window guards (this does not include fly screens)

(e) Materials not classed under above headings.

The following items are not covered by classifications A-B-C and D and will in no case be furnished by the Seller unless specifically agreed to and mentioned in the contract. It is not possible to designate every detail and the list is typical of material not included in classifications A-B-C and D. It is shown here to assist the Architect and Engineer in avoiding confusion.

Ash hoists

Awning boxes

Boilers

Elevators or accessories

Elevator guides or sheave beams

Expanded metal

Furring

Glass for any purpose whatever

Hollow metal doors or frames

Hoppers

Mail chute

Metal lockers

Miscellaneous carpenter or masonry bolts for connecting wood to wood
steel to wood, or wood to stone, etc.

Name plates

Patented devices

Pilot and driving nuts

Reinforcing steel

Rolling doors

Sheet metal work or corrugated sidings and roofing

Sidewalk lights

Steel sash and steel sash partitions

Spiral slides

Suspended ceiling, except as noted under Class "A"

Tanks and pans

Toilet partitions

Treads, except steel or iron

Vault doors

Ventilating brick

Wall, ceiling and floor registers

Wood handrails

Wood handrail brackets

And all other material not mentioned

SECTION 3. INVOICING

When conditions make it possible to award contracts on a lump sum basis the confusion of determining weights will be avoided. Scale weights involve a variation which frequently lead to a compromise based on calculated weights.

The rules hereinafter established, while not giving exact weights, are the basis upon which the Seller must make a lump sum or a pound price bid and they eliminate the necessity of increased cost of shop drawings and other refinements of manufacture which would very materially increase costs if exact weights were required.

(a) **Weights.**

Structural steel and iron sold at a unit price per pound, hundred weight (100 #) or ton (2000 #) shall be invoiced on the calculated weights of shapes, plates, bars, castings, rivets and bolts, based on the detailed shop drawings and shop bills of material which show actual dimensions of materials used as follows:

Dimensions:—

The weight will be figured on the basis of rectangular dimensions for all plates, and ordered overall lengths for all structural shapes and with no deductions for copes, clips, sheared edges, punchings, borings, milling or planing. When parts can be economically cut in multiples from material of larger dimension, the calculated weight shall be taken as that of the material from which the parts are cut.

Over-run, as follows:—

1. To the nominal theoretical weight of all universal mill and sheared plates or slabs will be added one-half the allowance for variation or over-weight in accordance with the specifications of the American Society for Testing Materials. All plates less than 5 feet in length shall be subject to the variation or over-weight given for sheared plates. (See table in A. S. T. M. Specification).
2. Reinforcing bars when not sold on a basis of scale weights shall be invoiced by the Seller at the theoretical weights plus $1\frac{1}{2}\%$ to allow for over-run weight of deformations, etc.
3. The calculated weights of castings shall be the weights determined from the detail drawings of the pieces including standard fillets for such pieces. To this an average over-run of 10% shall be added.

Rivets, as follows:—

1. The weight of shop rivets will be based on the weights shown in the following table:

Rivets $\frac{1}{2}$ " in diameter	20 #	per 100 rivets
Rivets $\frac{5}{8}$ " in diameter	30 #	per 100 rivets
Rivets $\frac{3}{4}$ " in diameter	50 #	per 100 rivets
Rivets $\frac{7}{8}$ " in diameter	100 #	per 100 rivets
Rivets 1" in diameter	150 #	per 100 rivets
Rivets $1\frac{1}{8}$ " in diameter	250 #	per 100 rivets
Rivets $1\frac{1}{4}$ " in diameter	325 #	per 100 rivets
2. Field rivets and bolts shall be invoiced at their actual weight.

Paint:—

One-half of 1% of the theoretical weights of the material painted will be added for each coat of paint. For work oiled, one-fourth of 1% for each coat will be added.

SECTION 4. DRAWINGS AND SPECIFICATIONS

(a) The Buyer shall furnish the Seller within a time agreed to in the contract a survey of the lot lines, together with a complete and full design of the structural steel frame definitely locating all openings, levels, etc.; and showing all material to be furnished by the Seller with such information as may be necessary for the completion of the shop drawings by the Seller. All such information and drawings shall be consistent with the original drawings and specifications.

(b) In case of discrepancies between the drawings and the specifications prepared by either the Seller or the Buyer, the specification shall govern; and in case of discrepancies between the scaled dimensions on the drawings and the figures written on them, the figures shall govern.

Should the Seller in the execution of his work find discrepancies in the information furnished by the Buyer, he shall refer such discrepancies to the Buyer before proceeding further with work which would be affected.

(c) Shop Drawings shall be made and submitted to the representative of the Buyer, who shall examine the same and return them approved with such corrections as he finds necessary. They shall be corrected by the Seller if necessary and returned for the Buyer's file as finally approved. The Seller may proceed with shop work, but in so doing he shall assume responsibility for having properly made the corrections indicated by the Buyer.

In addition to the set of blue prints of approved shop drawings for the Buyer's file as above referred to, the Buyer may require the Seller to furnish without cost to the Buyer, one additional set of shop drawing blue prints, but any further additional sets shall be paid for by the Buyer at cost, plus overhead and a fixed per cent for profit. All drawings or tracings made by the Seller for the execution of his work shall remain his property unless otherwise specifically agreed to.

(d) Shop Drawings prepared by the Seller and approved by a representative of the Buyer shall be deemed the correct interpretation of the work to be done, but does not relieve the Seller of responsibility for the accuracy of details.

(e) After the plans and shop drawings have been "approved" or "approved as noted" by the authority designated in the contract, any further changes required shall be made at the expense of the Buyer.

(f) When detailed shop drawings are furnished by the Buyer no responsibility for misfits due to errors in the drawings will be assumed by the Seller.

SECTION 5. GOOD WORKMANSHIP AND STANDARD PRACTICE

Good workmanship and standard practice in a modern structural shop is defined as follows:

(a) Material.

Stock material shall be of a quality substantially equal to that called for by the specifications of the American Society for Testing Materials for the classifications covering its intended use; and mill test reports shall constitute sufficient record as to the quality of material carried in stock. It is obviously

impossible for the Seller to maintain records of heat or blow numbers of every piece of material in his stock, and the same shall not be required if all his stock purchases are made under an established specification as to grade and quality.

Whenever a shop maintains such a practice in carrying a stock of material, it is deemed good practice to permit the use of such stock material in its fabricating operations whenever the shop desires to do so, instead of ordering items from the mill for a specific operation. Stock materials bought under no particular specifications, or under specifications materially less rigid than those mentioned above, or stock material which has not been subject to mill or other recognized test reports, shall not be used, except as noted below, without the approval of the Buyer and under rigid inspection.

It is permitted to use unidentified stock material free from surface imperfections for short sections of minor importance or for small unimportant details, where the quality of the material could not affect the strength of the structure.

(b) Straightening and Cleaning.

All material shall be clean and straight, and if straightening or flattening is necessary, it shall be done by a process that will not injure the material. Sharp kinks or bends shall be cause for rejection.

(c) Punching.

The punch shall be $\frac{1}{16}$ " larger than the nominal diameter of the rivet, and the die opening not more than $\frac{1}{8}$ " larger than the diameter of the punch. The thickness of the material in punched work shall not be greater than nominal diameter of the rivet, plus $\frac{1}{8}$ ". The accuracy of the punching shall be such that for any group of holes when assembled, 75% shall admit a rod equal to the diameter of the cold rivet at right angles to the plane of the connection, otherwise the holes shall be reamed.

Likewise, when work is assembled, all holes which will not admit a rod $\frac{1}{8}$ " smaller than the nominal diameter of the cold rivet shall be reamed.

(d) Reaming.

Reamed or drilled holes shall not be required unless specifically agreed to in the contract. When specifications require that work shall be sub-punched and reamed the die used for punching shall be $\frac{1}{16}$ " smaller than the nominal diameter of the rivet, and the assembled holes shall be reamed to a diameter of $\frac{1}{16}$ " larger than the nominal diameter of the rivet.

(e) Planing.

Planing or finishing of sheared plates or shapes will not be required unless specifically called for by the specifications or drawings.

(f) Assembling.

All parts of riveted members shall be well pinned or bolted and rigidly held together while riveting. Drifting done during assembling shall not distort the metal to enlarge the hole on the side on which the die was used in punching.

Finished members shall be true to line and free from twists, bends and open joints. It is not the function of fitting up bolts to bring improperly straightened material into place, thus causing a strain on the rivets in the finished work.

Compression members shall not have a lateral variation greater than 1 to 1000 of the axial length between the points which are to be laterally supported.

An allowable variation of $\frac{1}{32}$ " is permissible in the over all length of members with both ends milled.

Members without milled ends which are to be assembled to other steel parts of the structure shall not have an error greater than $\frac{1}{16}$ " for members 30 feet or less in length, and not more than $\frac{1}{8}$ " for members over 30 feet in length.

(g) *Riveting.

Rivets shall be heated uniformly and their temperature before driving should not exceed 1950° F. which is a light yellow color. A gun should not be used for driving after the temperature is below 1000° F., which is a blood red color. Rivets shall be driven and the heads formed with a proper sized die while hot. When heated and ready for driving, rivets shall be free from slag scale and carbon deposits. When driven they shall completely fill the holes.

Loose, burned or otherwise defective rivets shall be replaced. After driving, the rivet heads shall be full, neatly made, concentric with the rivet hole, and in full contact with the surface of the member. Caulking the rivet head shall not be permitted.

***(h) Cutting Torch.**

The use of a cutting torch is permissible if the metal being cut is not carrying stresses during the operation. Stresses shall not be transmitted through a flame cut surface. The radius of re-entrant flame cut fillets shall be as large as possible, but never less than 1". To determine the net area of members so cut, $\frac{1}{8}$ " shall be deducted from the flame cut edges.

SECTION 6. INSPECTION AND DELIVERY

(a) Inspection.

The Seller's shop service includes inspection by his own inspectors, and shop or mill inspection other than this shall be paid for by the Buyer.

(b) Acceptance of Materials.

When material is inspected by a representative of the Buyer at the Shop, the acceptance of such material by the Buyer's representative shall be considered the Buyer's final approval; but the Seller shall be responsible for the accuracy of the work and for defective material or workmanship which may be discovered before the completion of the structure.

(c) Order of Delivery.

Unless the order or sequence of delivery is specifically arranged for before the work is undertaken, it will be at the convenience of the Seller.

(d) Materials sold delivered.

When material is sold delivered on cars or trucks at the site of the structure, all unloading shall be done by the Buyer, and all responsibility to persons or property during such unloading shall be at the Buyer's risk.

*Revised 1928.

(e) Loss in shipment where material is sold fabricated only.

The quantity of material shown by the shipping statement will in all cases govern settlements unless notice of shortage is immediately reported to the agent of the delivering carrier, and his signed verification obtained, and like notice sent to the Seller within 48 hours after receipt of the shipment, in order that the alleged shortage may be investigated by the Seller.

(f) Storage of Material.

Where conditions make it necessary that material be stored for any length of time, and the contract does not provide for such storage, payments are to come due and be payable the same as if the material had been delivered at the building site; and the Seller shall be compensated for handling, storage, and other increased expenses that may result from such conditions.

SECTION 7. ERECTION

(a) Foundations.

The Seller or erector shall not be responsible for the strength or suitability of the foundations.

(b) Building Lines and Bench Marks.

Building lines and bench marks at the site of the structure shall be accurately located by the Buyer, and carefully shown or described by him or his representative to the steel erector or his engineer.

(c) Steel and Cast Iron Bases.

All steel grillage, steel slabs, cast iron, or steel bases, or steel columns with bases fabricated as an integral part of the column shall be set and wedged or shimmed by the seller or steel erector to grade or level lines, which are determined and fixed by the buyer, who shall grout all such parts in place. Before grouting the buyer shall check the grades and levels of the parts to be grouted, and shall be responsible for the accuracy of the same.

(d) Anchor Bolts.

All anchor or foundation bolts shall be set by the Buyer.

(e) Working Room.

The erection contractor shall be entitled to sufficient space at the site of the structure at a place convenient to him to place his derricks and other equipment necessary for erection. When conditions at the site provide working space not occupied by the structure, the erection contractor shall be entitled to storage space for sufficient material to keep his working force in continuous operation.

(f) Plumbing Up.

The temporary guys and braces shall be the property of the Seller, and if after the steel has been plumbed and leveled, the work of completing the structure by other contractors is suspended or delayed the owner of the temporary guys and braces shall receive reasonable compensation for their use. The guys shall be removed by the Buyer at his expense, and returned to the Seller in as good condition as when placed in the building with a reasonable depreciation.

Immediately upon completion by the steel erector, the Buyer shall assure himself by whatever agencies he may elect, that the steel erector's work is plumb and level, and properly guyed. If it is not, he should immediately notify the erector and direct him to perfect his work. After the steel erector has guyed and plumbed the work once to the satisfaction of the Buyer, his responsibility ceases. Any further work in gying or plumbing shall be performed entirely at the Buyer's expense.

In the setting or erecting of structural steel work, the individual pieces shall be considered plumb or level where the error does not exceed 1 to 500.

For exterior columns and columns adjacent to elevator shafts of multiple story buildings, the error from plumb shall not exceed 1 to 1000 for the total height of the column.

(g) Opportunity to Investigate Errors.

Correction of minor misfits and a reasonable amount of reaming and cutting of excess stock from rivets will be considered as a legitimate part of erection. Any error in shop work which prevents the proper assembling and fitting up of parts by the moderate use of drift pins, or a moderate amount of reaming and slight chipping or cutting, shall immediately be reported to the Seller and his approval of the method of correction obtained.

(h) Wall Plates.

All loose masonry bearing plates for beams, lintels, trusses or columns shall be set and grouted to grade and line by the Buyer ready for the steel erector to set his work.

(i) Loose Lintels.

Loose lintels or pieces of all kinds and descriptions required by the design of a building to carry brick work over openings, and which lintels or pieces are not attached in any way to the rest of the steel structure, and cannot be placed except as the masonry work advances, will not be erected by the steel erector unless by special agreement.

(j) Ornamental Iron and Bronze.

Fine ornamental iron and bronze work is considered as finishing material, and shall not be set in a building until after the marble, plaster, and other work, except decorating, is in place.

(k) Elevator Framing.

The setting or erection of guides, cars, machinery, cables, sheaves, pans, etc., for elevators, is not to be required of the steel erector.

(l) Field Assembling.

The size of assembled pieces of structural steel is fixed by the permissible weight and clearance dimensions of transportation. Unless such conditions are provided for by the Buyer or his engineer, the Seller shall provide for such field connections as will require the least field work; and such field connections shall be a part of the erection work.

(m) Cutting and Patching.

The Seller shall not be required to cut or patch any work, except his own,

unless particularly specified, and will not alter his own work required by changes or inaccuracies in the building without being reimbursed for the expense of such changes.

(n) Insurance.

The erector shall indemnify and save harmless the Buyer from all claims and costs arising from any damages to person or property occurring in the performance of his work due to any act or neglect of his employees or agents.

(o) Temporary Floors.

The Buyer shall provide plank, and cover all floors required by municipal or state laws, excepting the floor upon which the erecting derricks are located. This floor will be covered by the steel erector for working purposes.

(p) Field Paint.

Unless specifically agreed to in the contract, field paint shall be considered a phase of maintenance, and such protection as is necessary shall be provided for by the Buyer.

SECTION 8. DELAYS IN PROSECUTION OF WORK

(a) Causes not controlled by Seller or Buyer.

Neither Seller nor Buyer shall be responsible for delays in performance caused by delays at rolling mills, or in transportation, or due to strikes, fires, floods, storms, or other circumstances beyond their reasonable control whether related or unrelated, or similar or dissimilar to any of the foregoing. In case of delay to work due to any of the above causes, a reasonable extension of time shall be given for the completion of the work.

(b) Delays caused by the Seller.

Should the Seller at any time, except as provided in the preceding paragraphs, refuse or neglect to supply enough workmen of proper skill or material of proper quality, or to carry on the work with promptness and diligence, the Buyer, if not in default, may give the Seller ten days written notice, and at the end of that time if the Seller continues to neglect the work, the Buyer may provide such labor or materials and deduct the cost from any money due or to become due the Seller under the contract, or may terminate the employment of the Seller under the agreement and take possession of the premises and of all materials, tools, and appliances thereon and employ any other person to finish the work. In the latter case, the Seller shall receive no further payment until the work be finished; then if the unpaid balance that would be due under the contract exceeds the cost to the Buyer of finishing the work, such excess shall be paid to the Seller; but if such cost exceeds unpaid balance, the Seller shall pay the excess to the Buyer.

(c) Delays caused by the Buyer.

The Buyer shall be responsible for delays resulting from lack of complete data and from changes or revisions or the tardy approval of drawings. Information given later than the date fixed in the contract for the delivery of complete

information shall not be cause for a claim by the Seller unless such delay affects Seller's costs or manufacturing operations. When such delays increase costs or compel changes in the Seller's manufacturing operations he shall be recompensed for the damage resulting.

If information is available for the Seller to manufacture or erect the material in accordance with the conditions of the contract, and if he is prevented from the orderly and continuous prosecution of such work by any act or a neglect of the Buyer, the Seller may continue his work and may place fabricated material in storage at his own plant or elsewhere and the Buyer shall, upon tender of transfer of title, pay for said material as if it had been delivered under the terms of the contract. The Buyer shall also recompense the Seller for all expense incurred in the storing, caring for, or re-handling of said material; and for damage resulting from changed manufacturing operations. On erection work the Seller shall be recompensed for any extra expense incurred in wages and in the transportation of men or equipment to and from the site and their maintenance at the site during the period of delay, also for extra expense resulting from overtime made necessary by such delay.

If for more than one month at any time, any act or neglect of the Buyer, or any legal proceeding taken against him, prevents the starting or continuous prosecution of the work, the Seller may give the Buyer ten days written notice, and at the end of that time, if the Buyer continues at fault or the legal proceeding continues effective, the Seller may terminate his obligations under the contract; in which case the Buyer shall at once pay the Seller for the work done and material provided, and all damages the Seller may sustain, including damages resulting from changed shop operations.

SECTION 9. EXTRA WORK

(a) General.

Charges for extra work, or work not covered by the contract, shall be made on a basis that is definitely and mutually understood between the Buyer and the Seller at the time the occasion for such extra expense arises.

In the absence of such an understanding between the Buyer and Seller, the following is listed as proper expenses.

(b) Material.

All extra material required shall be invoiced out at current warehouse prices, plus cost of fabrication, including regular overhead costs, plus transportation costs, and an agreed per cent for profit.

(c) Drafting Labor.

All extra labor in the drafting room shall be invoiced out at cost plus overhead, plus an agreed per cent for profit.

(d) Shop Work.

All extra shop labor shall be charged at actual cost as shown by the time cards; to this shall be added the overhead expense, and the use of equipment and power. The sum of these charges shall be considered the actual cost of the shop, to which shall be added an agreed per cent for profit.

(e) Field Work.

All extra labor required in the erection of structural steel shall be invoiced as follows:

The actual labor cost shall be that shown by the time cards, to which shall be added the actual cost of insurance, the cost of labor transportation when necessary, and an additional allowance for overhead expense. The sum of these shall be considered the actual cost, to which shall be added an agreed per cent of profit.

Should the buyer or his agent or other trades engaged in the erection of other work connected with the structure require the use of materials or equipment belonging to the Seller, the Seller shall receive compensation for such extra service together with depreciation of equipment and an agreed per cent for profit.

(f) Miscellaneous.

Any additional cost, such as hauling, painting, crating, freight, etc., shall be charged at actual cost, plus overhead, plus insurance, plus an agreed per cent for profit.

(g) Overtime.

On contract work where the Seller has not agreed to work overtime, he shall not be required to do so without being paid for his extra expense and a profit.

(h) Extra Cleaning.

If because of continued storage, or for any other reason not the fault of the Seller, it should be necessary to clean and repaint the steel work, the cost of this additional cleaning and painting should be paid for as an extra, including regular overhead charges as specified for extra work elsewhere in this section.

SECTION 10. PROPOSALS AND CONTRACTS

(a) Direct Contracts.

It is recommended that in all cases where the structural steel frame of a building is self supporting, and also in all such other cases where the structural steel and iron items entering into the construction of a building can easily be separated from the other materials of construction, that all contracts for such structural steel or iron be made separately by the owner or his representative with the steel contractor.

(b) Conflicts.

In the event of a conflict between the terms and conditions of the proposal, and the terms and conditions stated in the plans and specifications, the terms of the proposal shall govern.

(c) Price for additions or deductions.

The Seller is not to be required nor expected to make the same unit price for additions to as for deductions from the list of material required for a structure. The contract, may however, specify a certain other unit price for such materials as may be deducted from the quantity of material as originally contemplated by the contract.

(d) Material not shown or called for.

Clauses in the specification to the effect that all steel and iron items necessary to complete the structure shall be furnished by the Seller, whether or not they are shown on the plans or called for in the specifications, being obviously unfair, will not be recognized or subscribed to. The Seller shall, however, furnish all material and labor for details that may be required for such steel and iron work as is shown on the drawings or called for in the specification, although such details may themselves not be shown or called for.

(e) Items not to be furnished.

Unless specifically mentioned in the request for bids, or specifically agreed to, the bidders do not estimate or include the following items in their proposals:

Any charges for surety bonds or insurance not required by law, or any other general charge such as building permits, license fees or taxes for permission to work in city or state, engineering fees, removal of rubbish, patching or repairing of plaster or masonry work, office or telephone service, light, heat, fire insurance, or the erection of temporary structures, enclosures or stairs.

(f) Terms.

The following terms of payment are adopted as standard and will govern in all cases, except when otherwise agreed to in the contract.

1. All payments shall be made in funds current at par in the city in which the Seller furnishing the material is located.

2. All materials for export, net cash in exchange for shipping documents will be required.

3. For all materials to be erected by the Seller, the Buyer shall on the 10th day of each month pay an amount equal to not less than 90% of the contract value of all materials shipped, stored or ready for shipment; and not less than 90% of the contract value of the erection performed during the preceding month; and shall pay the remainder within 10 days after the completion of the steel contract; but the amount reserved by the Buyer shall at no time exceed double the contract value of the work remaining yet to be done.

4. When the material which is not to be erected by the Seller is sold to a Buyer whose credit has been established with the Seller, terms net cash for contract value of each shipment. Payments to be made on the 10th day of the month following shipments.

5. Unless otherwise agreed to, when material is sold delivered at, or freight is allowed to destination, the Buyer shall pay freight charges and the Seller shall accept receipted freight bills as cash to apply on matured payments due on or after arrival at destination of materials covered by such freight expense bills.

6. Payments shall all be considered to be due and shall be paid at the time specified, regardless of the final settlement for the building as a whole, or for the work of any other trade; and when the contract is with a general contractor the payment for steel shall not be delayed by such general contractor pending his receiving estimates of payments from the owner.

7. Amounts past due shall bear interest at the maximum lawful rate.

STANDARD FORM OF PROPOSAL

The Seller for the consideration of.....
 hereby agrees to furnish all the materials and to perform all of the labor in
 accordance with the conditions of the Code of Standard Practice of the Amer-
 ican Institute of Steel Construction dated October 1st, 1924, for furnishing
 and erecting the.....
 for.....
 located at.....
 as shown on the drawings.....
 and as mentioned in the specifications for.....
 pages.....

Terms of payment shall be in accordance with the above mentioned Code
 of practice, except as follows.....

The Seller further agrees to furnish such material and complete such labor
 within the following time.....

The Buyer shall furnish complete information within.....
 days to enable the Seller to complete all necessary shop drawings.

Extra materials and labor furnished by the Seller shall be invoiced to the
 Buyer at their full cost plus a profit of.....
 per cent.

Inasmuch as materials are subject to prior sale, this proposal is made for
 acceptance on or before.....and the price is subject to
 change without notice.

Accepted By:

.....

Herein designated as the Buyer
 or his authorized agent

Date of Acceptance:

.....

Witnessed By:

.....

SIGNED BY

.....

.....

.....

Herein designated as Seller

.....

Date.....

REALIZING that the existing empirical methods of considering fire hazards and fire protection have been unsatisfactory to the construction industries, the American Institute of Steel Construction, Inc., asked a committee of prominent engineers to undertake the preparation of a Specification that would deal with these questions from a rational standpoint.

The resulting specification, we believe, constitutes a most important development to the construction industry.

The personnel of this committee is as follows:

H. G. BALCOM—

Mem. American Society of Civil Engineers
Mem. American Society for Testing Materials
Consulting Engineer, New York City

FRANK BURTON—Chairman of Committee

Past President, Building Officials Conference
Past President, Detroit Engineering Society
Mem. American Chemical Society
Consulting Engineer, Detroit, Mich.

A. R. ELLIS—

Mem. American Society for Testing Materials
Mem. American Society of Municipal Engineers
Mem. American Welding Society
Mem. Engineers Society of Western Pennsylvania
Mem. National Electric Light Association
General Manager, Pittsburgh Testing Laboratory, Pittsburgh, Pa.

S. H. INGBERG—

Mem. Western Society of Engineers
Mem. American Society for Testing Materials
Mem. American Concrete Institute
Mem. National Fire Protection Association
Assoc. Mem. Building Officials Conference
Senior Engineer, United States Bureau of Standards

RUDOLPH P. MILLER—

Mem. American Institute of Consulting Engineers
Mem. American Society of Civil Engineers
Mem. American Society for Testing Materials
Past President, Building Officials Conference
Past President, National Fire Protection Association
Mem. United States Department of Commerce Building Code Committee
Consulting Engineer, New York City

F. E. TURNEAURE—C. E., D. Eng.

Mem. American Association for Advancement of Science
Mem. Western Society of Engineers
Mem. American Railway Engineering Association
Mem. American Society of Civil Engineers
Mem. Society for Promotion of Engineering Education
Dean, College of Mechanics & Engineering, University of Wisconsin, Madison, Wis.

STANDARD SPECIFICATION FOR FIRE- PROOFING STRUCTURAL STEEL BUILDINGS

October 8th, 1927

Foreword

The Specification of the American Engineering Standards Committee for Fire Tests of Building Construction and Materials as published by the American Society for Testing Materials, serial designation C-19-26T, shall apply so far as it defines test procedure. The present specification provides an alternate method of defining the end point of the tests which is based on the maximum temperatures at which the structural steel is permitted to carry the stresses used in the design.

It is not intended that this specification will cover fire hazards that may occur during construction.

It is contemplated that the exterior and interior walls and the floor or roof slabs of the building will confine the fire to its place of origin without protection by automatic sprinklers or manual fire protection.

Such data regarding the fire resistance of structural steel members, and the insulating properties of materials, as have been derived in accordance with the specification C-19-26T, and that are found applicable to types of building members treated in this specification, may be used.

Data of this nature regarding columns were developed in a co-operative series of fire tests by The Associated Factory Mutual Laboratory, The Underwriters' Laboratories, and the Bureau of Standards, the results of which are given in the publication "Fire Tests of Building Columns," obtainable from the Underwriters' Laboratories, Chicago, Ill., or the Superintendent of Documents, Washington, D. C.

Since this specification deals with the question of fire protection from a relatively new standpoint, it has been considered advisable to incorporate some data that is informative, which if attached as notes or appendix might be overlooked.

STANDARD SPECIFICATION FOR FIRE- PROOFING STRUCTURAL STEEL BUILDINGS

October 8th, 1927



SECTION 1. PURPOSE AND SCOPE

The purpose and scope of this specification is:—

(a) To define basic conditions relative to the insulation necessary to protect structural steel when exposed to fire hazards, and thus enable engineers to design and classify steel structures for temperature resistance.

(b) To provide data that will enable the classification of fire hazards, and to rate them on the basis of their relative intensity and duration as compared to an established standard time-temperature hazard.

(c) To define the physical characteristics of structural steel within the temperature range that it is capable of carrying the working stresses used in designing, thus making possible the substitution of temperature determinations for the loading of test specimens during fire tests.

(d) To define fire test procedure that will give data on a uniform basis regarding the insulating properties of different fire resistive insulators.

SECTION 2. FIRES

(a) The intensity and duration of fires is variable, but for the purpose of this specification all fires shall be classified, with regard to their intensity and duration, on the basis of the average time-temperature definitions as set forth in the tentative specification for fire tests on building construction and materials as prepared by the sectional committee on Fire Test Specifications under the joint sponsorship of the United States Bureau of Standards, the American Engineering Standards Committee Fire Test Group, and the American Society for Testing Materials, in accordance with the procedure of the American Engineering Standards Committee, and published by the American Society for Testing Materials under serial designation C-19-26T.

(b) The time-temperature definition of the above referred to specification is given by the accompanying table and shown by the curve in Fig. No. 1.

1000° F.	at 5 minutes duration
1300° F.	at 10 minutes duration
1550° F.	at 30 minutes duration
1700° F.	at 1 hour duration
1792° F.	at 1 hour and 30 minutes duration
1850° F.	at 2 hours duration
1925° F.	at 3 hours duration
2000° F.	at 4 hours duration
2075° F.	at 5 hours duration
2150° F.	at 6 hours duration
2225° F.	at 7 hours duration
2300° F.	at 8 hours duration

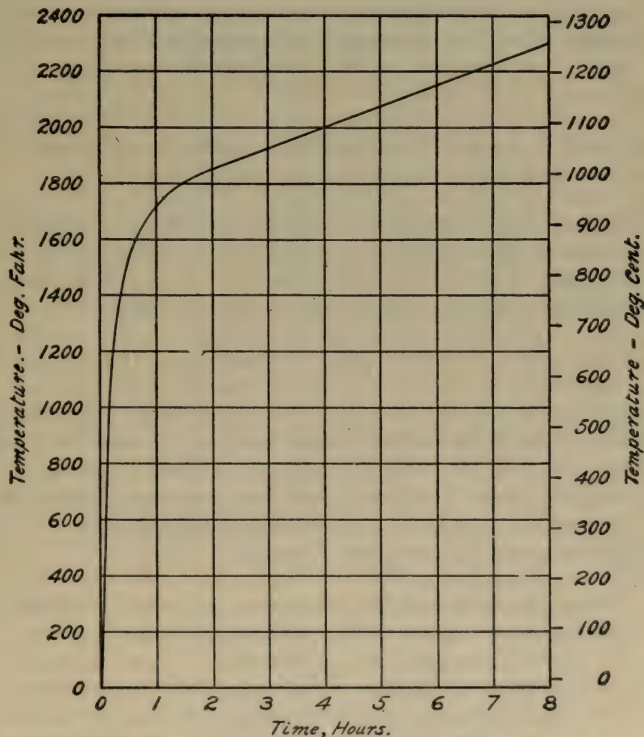


Fig. 1. Time Temperature Curve.

(c) The temperature in the combustion chamber fixed by the curve shall be deemed the average obtained from the readings of several thermo-couples (not less than three) symmetrically located to show the temperature near all parts

of the specimen being tested, the thermo-couples being enclosed and sealed in standard porcelain tubes $\frac{3}{4}$ inch outside diameter, and with walls $\frac{1}{8}$ inch thick. The exposed length of the thermo-couples and porcelain tubes shall extend not less than 12 inches into the combustion test chamber. Pyrometers or thermo-couple protecting tubes which are not standard may be used if under test conditions they give readings that are within the limits of accuracy that apply for furnace-temperature measurements. Other conditions defining the control of fire tests shall be as fixed by the above referred to specifications.

SECTION 3. FIRE HAZARDS

(a) For the purpose of this specification fire hazards shall be classified in accordance with the nature and combustibility of the materials which the buildings contain.

(b) Fire resistive buildings shall be rated as to fire hazards due to interior fires on the basis of the temperature which their combustible contents will produce, and the time that is necessary to complete the burning of the combustible contents as compared to the standard time-temperature definition above given.

(c) The steel in the exterior walls of buildings shall be adequately protected against existing or probable maximum future exterior fire hazards.

(d) The occupancy rating of the fire hazards of fire resistive buildings or parts thereof, shall be based upon the quantity of combustible contents per square foot of floor, and the equivalent intensity of fire which the contents will produce as compared to the standard time-temperature curve.

(e) All fire resistive buildings, together with such parts as are used for the storage or handling of extra quantities of combustible materials, shall be fire-proofed to protect them against maximum fire hazards within any section having fire separation from the remainder of the building, in accordance with the measured quantities of contained combustible materials including wood floor covering and wood trim. The burning out tests conducted by the Bureau of Standards with office occupancy and record storage, indicate the following equivalent fire hazard will approximately apply:

10 pounds per square foot constitutes a 1	hour fire hazard
15 pounds per square foot constitutes a $1\frac{1}{2}$	hour fire hazard
20 pounds per square foot constitutes a 2	hour fire hazard
30 pounds per square foot constitutes a 3	hour fire hazard
40 pounds per square foot constitutes a $4\frac{1}{2}$	hour fire hazard
50 pounds per square foot constitutes a 6	hour fire hazard
60 pounds per square foot constitutes a $7\frac{1}{2}$	hour fire hazard

The maximum fire hazard based on the weight of combustible materials shall be determined from the floor area of any one bay of the building or fire division thereof.

The above classification when applied to office equipment is based upon the use of wood furniture and shelving. Other burning out tests of offices equipped with metal furniture and shelving, and with papers exposed by opened drawers, show a very substantial reduction of the fire hazard.

The combustible contents of some fire resistive buildings may weigh less than 10 pounds per square foot of floor, but for the purpose of this specification no building shall be considered fire resistive that is not constructed to resist a fire of at least one hour standard duration with the pertaining safety factor.

SECTION 4. STEEL

(a) The occasion for fireproofing structural steel is to insulate it against a rise of temperature that would seriously impair its ability to sustain the loads at the unit stresses used in the design.

(b) This specification applies only to steel of the quality defined by the A. S. T. M. Standard Specification for Structural Steel for Buildings.

(c) The maximum working stresses for structural steel shall be those fixed by the Standard Specification for Structural Steel for Buildings of the American Institute of Steel Construction, dated June 1st, 1923.

(d) Under the conditions of this specification the structural steel shall carry the entire load, except that beams, girders, or trusses, may have wall bearing supports, and no stress shall be assumed as carried by the fireproofing materials, when subjected to a fire. In cases where the original design considers a part of the compression stresses as carried by some of the material used for fireproofing, a corresponding percentage of the stress may be considered as carried by the fireproofing material during a fire.

(e) In steel frame buildings or in buildings with part wall bearing, the skeleton frame shall be considered as the columns, and the girders, beams, trusses and spandrels having direct connections to the column. The secondary members of floor or roof panels are those which have no direct connections to the columns of the building. Supplementary steel members shall be those members used in connection with openings in outside wall or interior partitions, and which do not transmit the loads which they may carry through direct connections to the skeleton frame or secondary members. Masonry bearing lintels spanning openings greater than six feet shall be considered secondary members.

(f) The strength of structural steel at approximately 550° F. is about 25% greater than its normal temperature strength, and at 800° F. its strength is approximately the same as its normal temperature strength.

At a temperature of 1000° F. the compression strength of steel is approximately the same as the maximum permissible working stress in columns, and under a rare hazard of fire it shall be permissible for insulated steel columns to carry their working stresses when the average temperature at any critical cross

section does not exceed 1000° F., or when the maximum temperature at the critical cross section does not exceed 1200° F.

If the maximum working stress in tension or compression is 18,000 pounds per square inch in any member or critical flange of a member resisting bending moments, it shall be permissible for the member to carry its maximum working stress if the average temperature does not exceed 1000° F., or the maximum does not exceed 1200° F. at any cross section of the member, or its critical flange. If higher working stresses are used, proper consideration shall be given to extra insulation against temperature.

(g) If structural steel of special manufacture is used at higher working stresses than those fixed by this specification, its strength as compared to the steel of this specification at high temperatures shall be determined, and it shall be insulated against a rise of temperature that will leave its strength proportionately above the working stress.

(h) The average coefficient of expansion for structural steel between the temperatures of 200° F. and 1100° F. is given by the formula

$$C = .0000061 + .000000022 t$$

in which C is the coefficient of expansion for each degree F., and t is the temperature Fahr.

From 1100° F. to 1400° F. there is a slight variation in the coefficient, and below 200° F. the variation is less than that at the higher temperatures.

(i) Structural steel maintained at various constant temperatures has a uniform coefficient of elasticity up to the elastic limit stress, but between the elastic limit stress and the yield point stress, the rate of deformation with stress is a variable. If a member is subject to bending which produces stresses in the extreme fibre above the elastic limit it results in the extreme fiber and a portion of the adjacent fibers nearer the neutral axis carrying approximately the same stresses, and accounts for yield points determined by flexure being sometimes considerably higher than yield points determined by axial tension.

The coefficient of elasticity of steel decreases as the temperature increases, and the initial or tangent coefficient of elasticity for temperatures between 200° F. and 1300° F. is given approximately by the formula

$$E = 32400000 - 17000 t$$

in which E is the initial or tangent coefficient of elasticity, and t is the temperature Fahr. Between room temperature and 200° F. there is a smaller variation in E .

The formula $E = 32400000 - 17000 t$ does not apply for stresses above the elastic or proportional limit which varies with the temperature approximately as follows:

200° F. Elastic Limit	= 33000 # per sq. inch
300° F. Elastic Limit	= 28000 # per sq. inch
500° F. Elastic Limit	= 16000 # per sq. inch
700° F. Elastic Limit	= 12000 # per sq. inch
900° F. Elastic Limit	= 8000 # per sq. inch
1100° F. Elastic Limit	= 5000 # per sq. inch
1300° F. Elastic Limit	= 2000 # per sq. inch

SECTION 5. FIREPROOFING MATERIALS

(a) The insulating material used shall be so applied that the difference in temperature of the steel in any cross section shall not set up serious internal or buckling stresses, and so that such variation as exists will be symmetrical about the axes of compression members.

(b) Fire resisting insulating material shall continue to function within the temperature range of its use, and shall be so applied that it will not crack, spall, or buckle to seriously expose the steel to direct heat from fire.

(c) If the insulating of columns contemplates the use of air spaces between the steel and the insulator, there shall be fire stops placed at the floor levels.

SECTION 6. TESTS

(a) In lieu of the test procedure described in C-19-26T the following procedure may be employed in the preparation of data regarding the fire resistive properties of insulating materials that are used under the conditions of this specification.

(b) If the insulation contemplates the use of air spaces between the steel and the insulator, the ends of the test specimen shall be thoroughly fire-stopped to prevent the escape of heat from the air spaces.

(c) Temperature reading of all thermo-couples both in the combustion chamber and on the steel shall be made every five minutes during the first hour of the test, but may be read at 15 minute intervals thereafter.

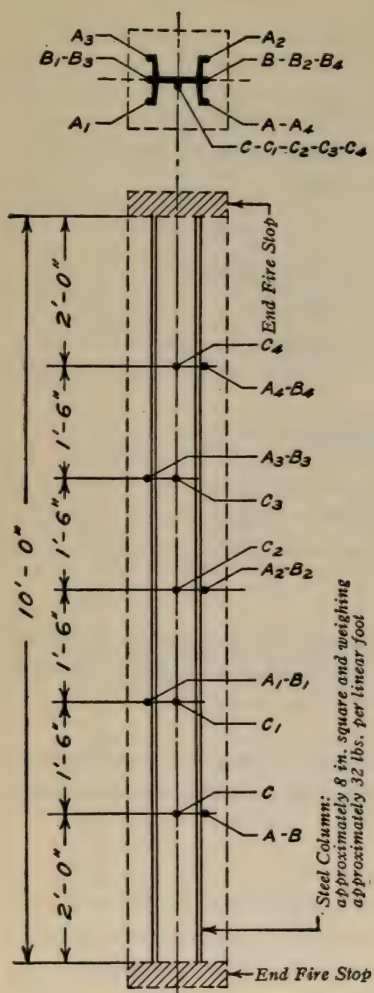


Fig. 2 Column Fireproofing Test

(d) Test specimens for columns shall consist of a rolled steel H section 10 feet long with not less than 15 thermo-couples arranged as shown in figure #2. The steel H section shall be approximately 8" square and weigh approximately 32 pounds per linear foot. The thermo-couples A, B, C — A₁, B₁, C₁, — A₂, B₂, C₂, — A₃, B₃, C₃, — A₄, B₄, C₄, shall be placed against or in the steel in the positions shown to give the temperature of the steel whether the fireproofing is solid or includes an air space. Column tests shall be conducted with the test specimen in a vertical position. The average temperature of the steel at different cross sections as found by the readings of thermo-couples A, B, C, — A₁, B₁, C₁, etc., shall not exceed 1000° F., and the maximum reading for any thermo-couple shall not exceed 1200° F. The average temperature of the steel as found for any cross section by the reading of A, B, C, — A₁, B₁, C₁, etc., will be obtained for this test specimen by the following formula:

$$\text{Average} = .39 \times A (\text{reading}) + .5 \times B (\text{reading}) + .11 \times C (\text{reading})$$

Example: If A reading is 1200° F., B reading is 1100° F., and C reading is 1000° F., the average for the area is $.39 \times 1200 + .5 \times 1100 + .11 \times 1000 = 1128^\circ \text{ F.}$

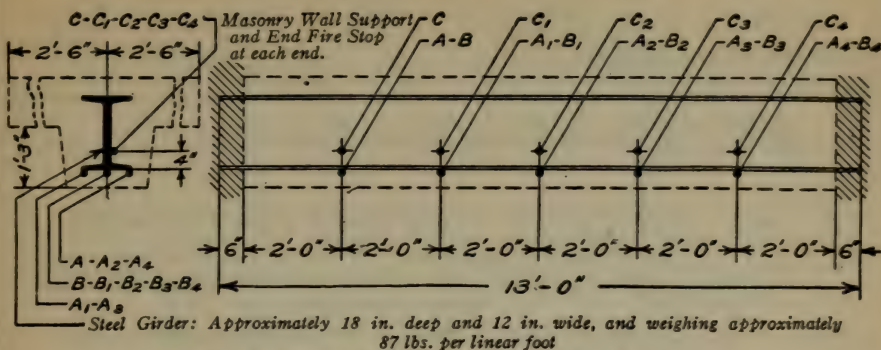


Fig. 3. Girder Fireproofing Test for Paneled Ceiling

(e) The test specimen for girders in paneled ceiling construction shall consist of a rolled steel girder 13 feet long with not less than 15 thermo-couples arranged as shown in Fig. No. 3. The steel girder section shall be approximately 18" deep with a flange approximately 12" wide and weigh approximately 87 pounds per linear foot. The panel projection below the ceiling shall be about 1'-3", and the thermo-couples A,B,C, — A₁, B₁, C₁, etc., shall be placed against or in the steel in the position shown to give the temperature of the steel whether the fireproofing is solid or includes an air space. The specimen shall be tested in a horizontal position. The average temperature of the steel of the flange as found from the readings of thermo-couples A,B,C, — A₁, B₁, C₁, — A₂, B₂, C₂, etc., shall not exceed 1000° F., and the maximum reading for any thermo-couple shall not exceed 1200° F. The average temperature of the steel of any flange cross section as found from the reading of A, B, C, — A₁, B₁, C₁, etc., will be obtained for this test specimen by the following formula:

$$\text{Average} = .43 \times A (\text{reading}) + .5 \times B (\text{reading}) + .07 \times C (\text{reading})$$



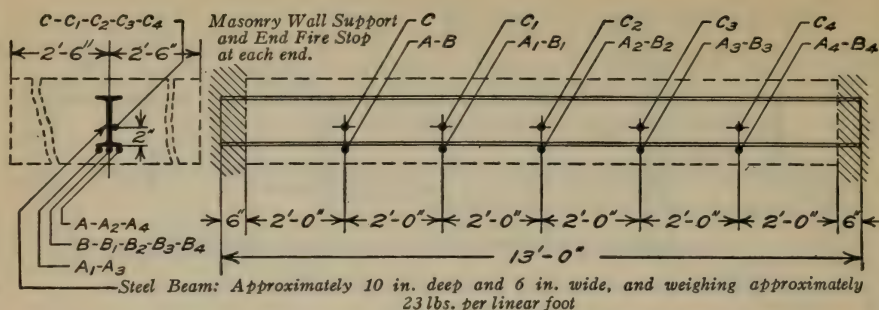


Fig. 4. Beam Fireproofing Test for Flush Ceiling

(f) The test specimen for flush ceiling floor construction shall consist of a rolled steel beam 13 feet long with not less than 15 thermo-couples arranged as shown in Fig. No. 4. The steel beam shall be approximately 10" deep with a flange approximately $5\frac{3}{4}$ " or 6" wide, and shall weigh approximately 23 pounds per linear foot. The thermo-couples A,B,C, — A₁, B₁, C₁, etc., shall be placed against or in the steel in the position shown to give the temperature of the steel whether the fireproofing is solid or includes an air space. The specimen shall be tested in a horizontal position. The average temperature of the steel of the flange as found from the readings of thermo-couples A,B,C, — A₁, B₁, C₁, etc., shall not exceed 1000° F., and the maximum reading for any thermo-couple shall not exceed 1200° F. The average temperature of the steel of any flange cross section as found from the reading of A,B,C, — A₁, B₁, C₁, etc., will be obtained for this test specimen by the following formula:

$$\text{Average} = .43 \times A (\text{reading}) + .5 \times B (\text{reading}) + .07 \times C (\text{reading})$$



SECTION 7. SAFETY FACTOR

(a) Steel buildings whose condition of exterior exposure and whose contents under fire hazards will not produce a temperature greater than 800° F. in the steel, shall be considered fire resistive without insulating protection for the steel.

(b) If the steel work has an insulating protection, the safety factor shall be based on the fireproofing material providing protection for a greater period of time than the combustible contents of the building will burn as shown in Section 3, Par. e. of this specification. The safety factor for all skeleton frame and secondary members shall be 1½. For example: if a building contains 10 pounds of combustible material per square foot of floor, and has a fire hazard of one hour duration, the steel work shall be protected against the temperatures defined in this specification for 1½ hours.

Supplementary members shall not require insulating protection.

The following tabulated data is not a part of the fireproofing specification but is given here to aid the engineer in a fuller understanding of the conditions relating to the subject. It has been compiled from a careful study of all the available literature that has appeared since about 1890 and is in substantial agreement with the research findings of Dr. Albert Sauveur, who is the Gordon McKay Professor of Metallurgy and Metallography of Harvard University.

The tangent elastic limit is the stress per square inch at which the stress-strain curve ceases to be a straight line. It will be noted that at high temperatures the spread between the tangent elastic limit and the yield point is greater than at normal temperatures.

Temp. Fahr.	Ultimate Strength in Pounds per Sq. In.	Yield Point in Pounds per Sq. In.	Tangent Elastic Limit in Pounds per Sq. In.	Modulus of Elasticity Below Tangent Elastic Limit	Per Cent of Elongation	Per Cent of Reduction of Area
100	54000	39000	36000	30 700 000	48	63
200	56000	43000	33000	29 000 000	43	66
300	58000	46000	28000	27 300 000	39	65
400	60000	47000	22000	25 600 000	37	64
500	63000	46000	16000	23 900 000	37	64
600	66000	44000	14000	22 200 000	40	66
700	60000	40000	12000	20 500 000	44	68
800	52000	37000	10000	18 800 000	49	76
900	43000	32000	8000	17 100 000	55	84
1000	34000	27000	7500	15 400 000	60	90
1100	25000	21000	5000	13 700 000	64	94
1200	19000	17000	3500	12 000 000	68	96
1300	14000	13000	2000	10 300 000	72	98

MINIMUM LIVE LOADS ALLOWABLE FOR USE IN THE DESIGN OF BUILDINGS

As recommended by the
Building Code Committee of the Bureau of Standards,
United States Department of Commerce

1. Definitions.

1. *Dead Load*.—The dead load in a building includes the weight of walls, permanent partitions, framing, floors, roofs, and all other permanent stationary construction entering into a building.

2. *Live Load*.—The live load includes all loads except dead loads.

2. General.

Buildings and all parts thereof shall be of sufficient strength to support safely their imposed loads, live and dead, in addition to their own proper dead load; provided, however, that no building or part of a building shall be designed for live loads less than those specified in the following sections.

3. Human Occupancy.

1. For rooms of private dwellings, hospital rooms and wards, guest rooms in hotels, lodging and tenement houses, and for similar occupancies, the minimum live load shall be taken as 40 pounds per square foot uniformly distributed, except that where floors of one and two family dwellings are of monolithic type or of solid or ribbed slabs the live load may be taken as 30 pounds per square foot.

2. For floors for office purposes and for rooms with fixed seats, as in churches, school classrooms, reading rooms, museums, art galleries, and theaters, the minimum live load shall be taken as 50 pounds per square foot uniformly distributed. Provision shall be made, however, in designing office floors for a load of 2,000 pounds placed upon any space $2\frac{1}{2}$ feet square wherever this load upon an otherwise unloaded floor would produce stresses greater than the 50-pound distributed load.

3. For aisles, corridors, lobbies, public spaces in hotels and public buildings, banquet rooms, assembly halls without fixed seats, grandstands, theater stages, gymnasiums, stairways, fire escapes or exit passageways, and other spaces where crowds of people are likely to assemble, the minimum live load shall be taken as 100 pounds per square foot uniformly distributed. This requirement shall not apply, however, to such spaces in private dwellings, for which the minimum live load shall be taken as in paragraph 1 of this section.

4. Industrial or Commercial Occupancy.

In designing floors used for industrial or commercial purposes, or purposes other than previously mentioned, the live load shall be assumed as the maximum caused by the use which the building or part of the building is to serve. The following loads shall be taken as the minimum live loads permissible for the occupancies listed, and loads at least equal shall be assumed for uses similar in nature to those listed in this section.

Floors used for:	Minimum Live Load in lbs. per sq. ft.
Storage purposes (general)	250
Storage purposes (special)	100
Manufacturing (light)	75
Printing plants	100
Wholesale stores (light merchandise)	100
Retail salesrooms (light merchandise)	75
Stables	75
Garages	
All types of vehicles	100
Passenger cars only	80
Sidewalks—250 or 800 pounds concentrated, which ever gives the largest moment or shear.	

5. Roof Loads.

Roofs having a rise of 4 inches or less per foot of horizontal projection shall be proportioned for a vertical live load of 30 pounds per square foot of horizontal projection applied to any or all slopes. With a rise of more than 4 inches and not more than 12 inches per foot a vertical live load of 20 pounds on the horizontal projection shall be assumed. If the rise exceeds 12 inches per foot no vertical live load need be assumed, but provision shall be made for a wind force acting normal to the roof surface (on one slope at a time) of 20 pounds per square foot of such surface.

6. Allowance for Movable Partition Loads.

Floors in office and public buildings and in other buildings subject to shifting of partitions without reference to arrangement of floor beams or girders shall be designed to support, in addition to other loads, a single partition of the type used in the building, placed in any possible position.

7. Reductions in Live Loads.

Except in buildings for storage purposes the following reductions in assumed total floor live loads are permissible in designing all columns, piers or walls, foundations, trusses, and girders.

<i>Reduction of total live loads carried</i>	<i>Per cent</i>
Carrying one floor	0
Carrying two floors	10
Carrying three floors	20
Carrying four floors	30
Carrying five floors	40
Carrying six floors	45
Carrying seven or more floors	50

For determining the area of footings the full dead loads plus the live loads, with reductions figured as permitted above, shall be taken; except that in buildings for human occupancy, listed in section 3, a further reduction of one-half the live load as permitted above may be used.

The Historical Development
of
S T E E L
and
I R O N

The two words, Steel and Iron, have been used so extensively to indicate the same thing that it is uncertain what should be the proper distinction between the two materials. However, the popular conception is that steel means a more refined state than the word iron.

Under modern conditions of production, the first state of iron after refinement from the ore is usually known as cast iron, and a continued refinement of cast iron is usually called steel; and it is the popular conception that a further refinement of the steel produces wrought iron. As a matter of fact, in the early production wrought iron was developed directly from the ore in a plastic condition and it was only after many centuries that the iron could be produced from the ore in a molten condition, which permitted it being poured into molds to form castings.

Next to oxygen, silicon and aluminum, iron is the most widely distributed and largest part of the solid material in the earth, and is about $4\frac{1}{8}\%$ of the solid earth crust.

For many years steel has been considered the index of the commercial activities of the country, but in a broader sense, it has from the beginning of history, been an accurate measure of the progress of civilization since it is the medium through which all of our attainments are possible, and without it we must have continued in a savage state. It is the only substance that

can be hardened to form the tools by which all of our necessities are made, including wood work, machinery, transportation, in all forms, agricultural implements, steam engines, and since it alone possesses magnetic properties, all our electrical devices and developments depend upon it.

It is doubtful whether iron was known when the pyramids were made some 6000 years ago, but it was used by the Hebrews, Assyrians, Phoenicians, Greeks, and by the Romans, who found it being used by the Britains at the time of Caesar's invasion. Through all of this time, and up to about 1400 A. D. iron was produced in very small quantities, and in a shallow saucer shaped forge in which the ore and charcoal were mixed and from which the iron was thus separated. It would therefore seem natural that up to this time iron would be used largely for weapons of combat and for small tools.

About 1400 A. D. the first masonry furnace resembling the principles of the modern blast furnace was made in Europe, and about one hundred years later, it was introduced into England. Previous to this all of the refining was accomplished by hand puddling, and forging, and it was only after the furnace method was developed, that quantities could be made large enough to use for castings. In fact it was impossible up to this time to develop temperatures that would melt the material.

Following this and for nearly three hundred and fifty years the methods of refinement were limited to puddling in a small reverberatory furnace from which the product was removed, as a puddle ball, and subjected to forging. The next outstanding accomplishment was the Bessemer converter developed between 1850 and 1860 in England by Henry Bessemer, and in America by William Kelly of Eddyville, Ky. Bessemer's financial strength enabled him to absorb his American contemporary and the process has since born his name. Briefly, the Bessemer process consists in passing air through a melted cast iron which contains combustible impurities in such quantities that chemical reaction is generated to raise the temperature to such a point that undesirable impurities are removed from the molten mass. This process is accomplished in about fifteen minutes, but its application is limited to iron which contains combustible materials in quantities that make the process workable.

While Bessemer was developing his converter, William Seimens was working on the open hearth process, and built the first gas burning furnace of this type in 1861. The success of the Bessemer even with its limitations as fixed by the nature of the ores required, and the resulting product, established that an almost unlimited market existed for an economically produced steel. This resulted in the vigorous development of the open hearth which was not so restricted as to the materials used, and while the process is longer than the Bessemer, the product is more uniform in chemical and physical properties, and soon outstripped its rival for public favor. Both processes made possible the casting of large ingots from which various shapes could be rolled, and by 1892 had practically eliminated sections of wrought iron which had to be made by welding small bars together through a re-

rolling process such as is still used for stay bolt iron and chain iron. As the development of steel progressed, the sky line of our cities changed rapidly. The electric furnace is following the open hearth and is capable of producing a material of almost any preconceived chemical analysis, but so far at a cost that prevents its entering into competition with the Bessemer or the open hearth for ordinary structural grade steel. The remarkable precision of chemical and physical properties that are uniformly attained by these processes is unknown to any other industry, and is illustrated by the fact that the chemical properties are expressed in hundredths of a per cent, and it is doubtful whether drops from a medicine dropper used in filling prescriptions are closer than 5% of each other. Throughout all of the processes of treating the ore and finishing through the Bessemer, the open hearth, or the electric furnace, great care is used in the selection of the fluxes, and the furnace linings by means of which the chemical properties of the material are determined.

In all of these processes, the method of refining involves the treatment of molten material, but it has been found commercially practicable to refine certain grades of cast iron, and change it from a crystalline to a malleable structure without heating it to the melting point.

Remaury in 1722 described the production of ductile castings by processes which removed the carbon from white grey iron by heating it in an oxide. This process is still used in Europe but in America it has been supplanted by the Boyden process, which was introduced in 1826. The Boyden process results in what is called malleable cast iron, which resembles the ordinary grey cast iron, only in that both are cast in molds.

Grey iron castings contain about 2½% graphite, which exists as flat flakes of free carbon and gives the fractured material a granular appearance. By subjecting certain grades of grey iron castings for about three days to a temperature of approximately 1300° F. but not higher than 1700° F. a part of the carbon is removed, and the remaining graphite flakes are converted into small carbon nodules which are scattered throughout the material. This results in a dead soft malleable iron.

Malleable cast iron (A. S. T. M. Specifications) is required to have a tensile strength, as measured in a test specimen of prescribed form, of 50,000 lbs. per square inch, and a minimum elongation of 10%. The point at which a test specimen of malleable iron will elongate about .01" in 2" is sometimes spoken of as the yield point, which is about 35,000 lbs. per square inch. The shearing strength is about 45,000 lbs. per square inch.

The material flows under compression at stresses above the yield point, and its ultimate strength by fracture in compression is therefore not determinable. The coefficient of elasticity or Young's modulus in tension or compression is about 25,000,000.

The following table is reproduced from a volume entitled "The Making, Shaping and Treating of Steel,"* and illustrates the approximate chemical properties which distinguishes pig iron, plain steel, and wrought iron.

Chemical Relations of Pig Iron, Wrought Iron and Plain Steel

Name	PER CENT. OF					
	Iron	Carbon	Manganese	Sulphur	Phosphorus	Silicon
Pig Iron	91 — 94	3.50—4.50	.50—2.50	.018—.100	.030—1.00	.25—3.50
Plain Steel	98.1—99.5	.07—1.30	.30—1.00 (.03—.10 as cast)	.020—.060 (.120)	.002—.100	.005—.50
Wrought Iron	99.0—99.8	.05—.25	.01—.10	.020—.100	.050—.20	.02—.20

** Note.—“The making, shaping and treating of steel” is published by the Carnegie Steel Co. and should be read by every person interested in steel. It can be obtained from the Bureau of Instructions of the Carnegie Steel Co. at Pittsburgh, Pa. Price \$7.50.*

Physical Properties of Steel and Iron

IRON

Pure iron is almost unknown commercially. It is a grayish white color and soft compared with carbon steel. It is malleable, ductile, and magnetic. It is 7.78 times heavier than water, and in its commercial forms melts at about 1520°C. or about 2770°F.

The presence of the various elements which are combined with iron in its commercial forms lowers this melting point very rapidly. The ultimate strength is approximately 38,000 pounds per square inch and the elastic limit about 20,000 pounds per square inch.

STRUCTURAL STEEL

Structural steel weighs .2833 pounds per cubic inch or 490 pounds per cubic foot. It is therefore about 7.85 times heavier than water.

ELASTICITY

Structural steel is perfectly elastic below the stress per square inch which is called the yield point, and beyond this yield point there will be permanent set or deformation when the load is removed. Just below the yield point, and usually within 1000 pounds per square inch of it is the elastic limit, below which the elongation or deformation is always exactly proportional to the stress per square inch. The ratio of elongation to the stress per square inch is called the coefficient of elasticity, the modulus of elasticity, or sometimes Young's Modulus. It may otherwise be defined as that stress per square inch, which in tension would double the length of a test specimen assuming that uniform elasticity were possible throughout the experiment. For structural grades of steel, the coefficient of elasticity is 29,000,000 pounds; that is, a bar 1 square inch in area will stretch one twenty-nine millionth (1/29,000,000) of an inch for each inch of length and for each pound of stress. It has been found by innumerable experiments that the physical properties of steel cannot be changed regardless of the number of times a load may be applied to it so long as the stresses produced do not exceed the elastic limit. It has also been found that when steel is loaded to produce stresses beyond its yield point, and therefore producing permanent set, that the material will have a higher elastic limit and yield point if the original stresses are

removed. It is this principle that is used in the manufacture of cold rolled, or cold drawn steel.

The following diagram is reproduced from "The Making, Shaping, and Treating of Steel," and graphically illustrates the performance of the material within the various ranges of its strength.

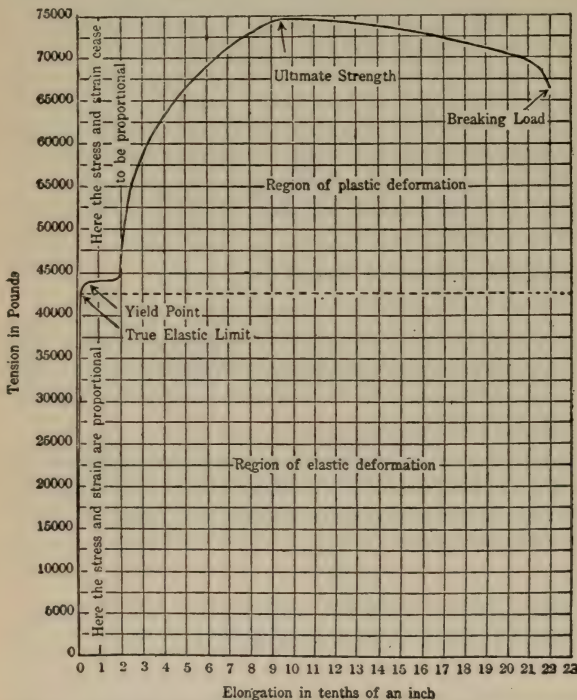


FIG. 46. Graph Representing the Pulling of a Structural Steel Test Piece.

The chart represents a specimen whose dimensions before pulling were as follows:

Length.....8"

Width.....1.41"

Thickness... .86"

Area in sq. in.1.213

The elastic limit per square inch was 36770 lbs.

The ultimate strength per square inch was 61500 lbs.

The elongation in 8" was 27.5%.

The reduction in area was 50.5%.

The elastic limit and ultimate strength of steel depend not only upon the chemical composition of the material, but also upon the amount of work done on the material in producing it, and the temperature at which the work is finished. While there may exist among engineers a division of opinion as to the importance of the percentage of elongation and the reduction of area, there is no difference regarding the importance of the elastic limit and the ultimate strength.

The effect of carbon on the ultimate strength and elastic limit is to increase them, but at the same time it also results in a harder steel, and for that reason in ordinary structural grades it is usually below .25%. Manganese also has the effect of increasing the elastic limit and ultimate strength, but not to the extent produced by carbon. In large quantities it has the effect of producing a material very difficult to manufacture. One of the important effects of manganese, however, is that it neutralizes the evil effects of sulphur. Sulphur up to 0.1% has little or no influence on the ductility or strength of steel at ordinary temperatures. It does, however, have the effect of producing what is known as the red short conditions which means that the material is difficult to work at a red heat.

Phosphorus for many years has been considered responsible for steel at ordinary temperatures being brittle or technically termed, cold short, but it is doubtful whether quantities less than .1% have any very marked influence. It does increase the hardness and the tensile strength of the steel and reduces the ductility. Some experimenters have found that the evils produced by phosphorus are not the same, and have found that under apparently similar conditions the effect is entirely different, which indicates that it should be considered as a treacherous element. Some users refuse to accept steel which contains a higher percentage than .04%.

Silicon is now considered beneficial up to .75%, and up to this point it increases the elastic limit and the ultimate strength of the material without interfering with its ductility.

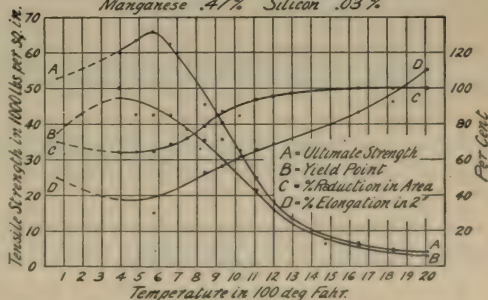
The Effect of Temperature on Structural Steel

Steel in a liquid form is melted iron which contains carbon and other elements in solution. The percentage of carbon has an important effect on the physical properties of the steel when it reaches normal temperatures. For tool steels the amount of carbon is sometimes as high as 1.50%, but for structural grades of steel the percentage is usually below .25%, which is sufficient to have important bearing on the properties. As the steel changes from liquid to solid, and as the solid cools, there is a tendency for the carbon to segregate from the solution. The extent to which this segregation takes place depends to some extent upon the rapidity with which the cooling process takes place.

In the manufacture of structural steel the temperature conditions of cooling through the soaking pit process are carefully controlled so as to produce a fine uniform structure. It has been found that a fine grained structure in the steel has greater strength and more desirable physical properties than a structure which is coarse and granular. The carbon in structural steel at normal temperatures is almost completely in solution, and is visible under the microscope only as small dots.

*Physical Properties of Steel at High Temperatures.
Carbon .15% Sulphur .027% Phosphorus .027%
Manganese .47% Silicon .03%*

This diagram is reproduced from the National Tube Company's Handbook of 1924, with the exception that the temperature readings are given on the Fahrenheit instead of the Centigrade scale.



The effect of temperature on the physical properties of steel is shown by the accompanying chart. These curves are based on tension tests of steel having about the same chemical analysis as structural steel. As the temperature is increased both the ultimate strength and the yield point increase until a temperature of 500° to 600° F. is reached, where both the ultimate strength and the yield point are approximately 25% above the normal temperature values. It will be

noted that at this range of temperature, the ductility of the steel, as represented by the percentage of reduction of area and percentage of elongation, decreases indicating a brittle range. At approximately 800° F. all of the physical properties are nearly the same as the normal temperature values, and at a temperature of approximately 1200° F., the yield point and the ultimate strength are almost the same, and the ultimate strength is about one-third of its normal temperature value. At a temperature of approximately 1350° F. there is what is known as the critical temperature.

The temperature and color chart reproduced from the Standard Handbook of Steel Construction shows the relation between temperature and color of steel, and summarizes the effect of temperature on steel.

Above 2100° F. the color is white, but as it cools it darkens in color and gradually decreases in volume by shrinking. During this cooling process there are a few seconds of time at the critical temperature, in which the color becomes brighter, and expansion in volume takes place. Above this temperature steel has lost its magnetic properties, and below it it gradually recovers them. Apparently a molecular reconstruction takes place accompanied by the absorption or release of heat, depending upon whether the temperature is ascending or descending through the critical temperature. At both the critical temperature and the temperature of maximum strength (near 600° F.) there takes place some rearrangement of the internal structure of the material, and during such rearrangement it may be reasonable to assume that stresses caused by shrinking should be very materially relieved.

As steel reaches the temperature of white heat, that is about 2100° F., the carbon is forced out of solution and segregated into flakes resembling those seen in the fracture of cast iron. This condition is sometimes described as burned steel, but in reality it is merely a segregation of the carbon from its condition of solution into one of intergranular flakes, which materially reduces the effective section of the steel and weakens it. It is, of course, possible by a proper annealing process, to reconstruct overheated steel, but the process requires considerable time and it is doubtful whether it should be undertaken without the supervision of experienced men.

It is therefore important that proper precautions be taken to prevent overheating either in the manufacture of rivets or in the heating of them for driving.

The above discussion leads to the following practical suggestions. Careful observation of these suggestions in the fabrication and erection of structural steel is highly important and will eliminate a great amount of trouble.

Rivets should be subjected to a soaking heat, and their temperature before driving should not exceed 1950° F., which is a light yellow color.

A pneumatic or vibrating rivet gun should not be used on rivets after the temperature is below 1000° F., which is a blood red color. Below this temperature is the brittle range, and vibrating impact will loosen the rivet instead of tightening it.

Do not use a flame cutting torch on steel which is carrying stresses.

Caulking should not be done until the temperature is below 200° F.

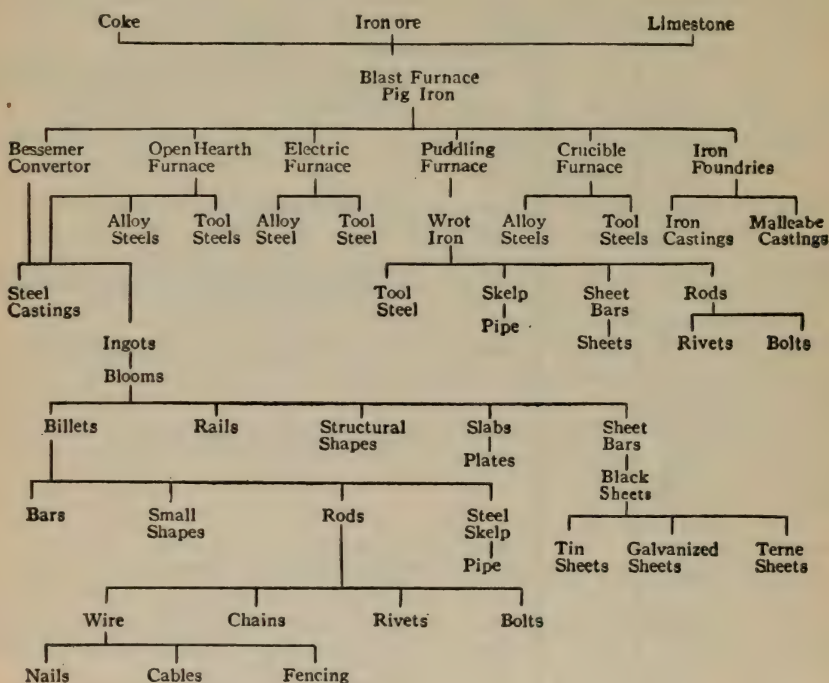
TEMPERATURE CHART

Working Temperature and Colour Chart for Iron and Steel

Conversion Formulae $F^{\circ} = \frac{9}{5} C + 32^{\circ}$
 $C^{\circ} = \frac{5}{9} (F - 32^{\circ})$

	Fahr.	Cent.	Fahr.	
	2770		2770	— Approximate melting point of pure iron.
	2700		2700	{ Melting point of steels, depending on carbon and other contents which reduce the melting point as their percentage increases.
	2600	1426.5	2600	
	2500	1371	2500	
	2400	1315.5	2400	
	2300	1260	2300	— Approximate melting point for Cast Iron.
White	2200	1204	2200	{ Distortion of microscopic intergranular structure of rivets starts, resulting in intergranular rupture after driving.
	2100	1149	2100	
	2000	1093	2000	— Rivets start to spit.
Light Yellow	1975	1065.5	1950	— Do not exceed this temperature in heating rivets.
	1900	1038	1900	
Lemon	1825			
	1800	982	1800	
	1725			— Proper temperature for driving rivets.
Orange	1700	926	1700	
Salmon	1650			
	1600	872	1600	
Bright Red	1550		1550	— Scaling starts.
	1500	816	1500	{ Range of temperatures for refining grey iron castings into malleable iron castings.
	1400	760	1400	
Cherry Red	1375		1350	{ Approximate critical temperature of tool steels. Colour brightens when cooling past this temperature and expansion takes place. A magnet reacts below but not at or above this temperature.
	1300	704	1300	
Medium Cherry	1250			Heat above here for quenching treatment.
	1200	648.5	1200	
Dark Cherry	1175			
	1100	593	1100	
Blood Red	1050			{ Maximum temperature at which fireproofed structural steel may carry A. I. S. C. designing stresses.
	1000	537.8	1000	
Dark Red	900	482.2	900	— Do not use gun on Rivet below this temperature.
	800	426.7	800	
	700	371.1	700	{ Ultimate Strength approximately equal to normal temperature strength of structural grade steel.
Blue Heat	600	315.6	600	
	500		500	{ At this temperature steel is in brittle condition. Ultimate Strength is 25% to 30% greater than normal temperature strength of structural grade steel.
	400	204.4	400	
	300		300	
	200	93.3	200	— Do no calking above this temperature.
	100	37.8	100	
	32	0	32	

Chart showing the sequence of manufacture of steel and iron products



In connection with the above chart showing the sequence of manufacture, it is practically impossible for a layman to appreciate the innumerable details and conditions that must be fulfilled in every process of manufacture. When however, it is understood that between the blast furnace producing the pig iron, and the rolling mill producing the structural shapes, there is a loss of production amounting to in many cases as much as 25 or 30%, the layman will understand to some degree what is involved when a special analysis of steel is required. It is also of interest to note that for every ton of finished rolled steel that is shipped from a steel plant approximately six tons of ore, fuel, fluxes, refractories, lubricants, etc. must be shipped into the mill. There is every reason to expect that the manufacturers of steel will continue to improve their metallurgical processes and increase the uniformity of the product.

Recently there has been work done on the development of a steel carrying a higher percentage of silicon which has the effect of increasing both the ultimate strength and elastic limit without interfering with the ductility of the product.

Part II

General Mathematical Tables

Stresses:—Elementary Discussion

Properties of Sections

Moments of Inertia of Rectangles

Moments of Inertia of Four Angles

Areas of Rectangles

Weights of Rectangular Bars

Wire Gauges

Areas and Weights of Round and Square Bars

Beam Loading Formulae

Coopers E 10 Engine Loading

Deflection

Functions of Numbers .001 to 1000

Trigonometrical Formulae

Trigonometrical Tables

Lengths of Circular Arcs

An Elementary Discussion of the Relation of External Loads and Internal Stresses

There is probably nothing so dangerous to safe construction as the blind use of empirical formulae. A formula is empirical so far as the user is concerned unless he understands it, and the fact that someone else may understand it does not change its empirical standing to the one who lacks the understanding.

Every engineer and architect now recognizes that an understanding of the relation of external loads to internal stresses in the materials which sustains the loads, is the basis of safety in the design of all structures. The necessity of such an understanding may be looked upon as almost an emergency with the present generation, due to the rapid transition from the "Iron Age" to the "Steel Age" which took place between 1885 and 1893 following the development of temperatures which enabled production of steel ingots from which all our steel products are manufactured. It has resulted in revolution of existing industrial conditions, and the evolution of new ones which mark a new era in human history. The industrial changes of the last forty or fifty years have been greater than those of all previous history. The development and distribution of technical information essential to such rapid progress has naturally been combined with much that seems mysterious and difficult for the uninitiated to understand.

It is the purpose of this discussion to place before the reader in elementary form and free from the difficult mathematical treatment it usually involves, one of the subjects on which much of our construction design depends.

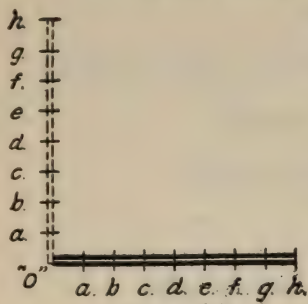


Figure (1)

Consider a steel bar eight feet long in a horizontal position shown in Figure 1, and assume that at each of the points, *a, b, c, d*, etc., there is one pound of material. If this bar is rotated to a vertical position as shown dotted, we know that work has been done. "*a*" has been lifted one foot and on it one foot pound of work was done. "*d*" has been lifted four feet and four foot pounds of work was done. "*h*" has been lifted eight feet and eight foot pounds of work was done. All of the work was done in the same time and we see at once, since the units

each weighed a pound, there must have been a different force acting on each of them, and that this force must be proportional to the distance from the axis of rotation "*O*". That is, the force acting on "*a*" was one pound, on "*d*" four pounds, and on "*h*" eight pounds. In other words, the force representing the capacity of any body to resist being rotated about an axis is directly proportional to its distance from that axis. *Note clearly that this is not the moment of a force, but is the measure of the force itself.* The force acting on "*h*" is eight pounds, and since it is eight feet from the axis of rotation "*O*", the moment of the force will be $8 \times 8'$ or $64'$. This establishes that the moment of resistance to rotation about the axis "*O*" is proportional to the square of the distance from the axis. An understanding of this will enable us to remove the mystery from the so called fourth dimension and make it rational.

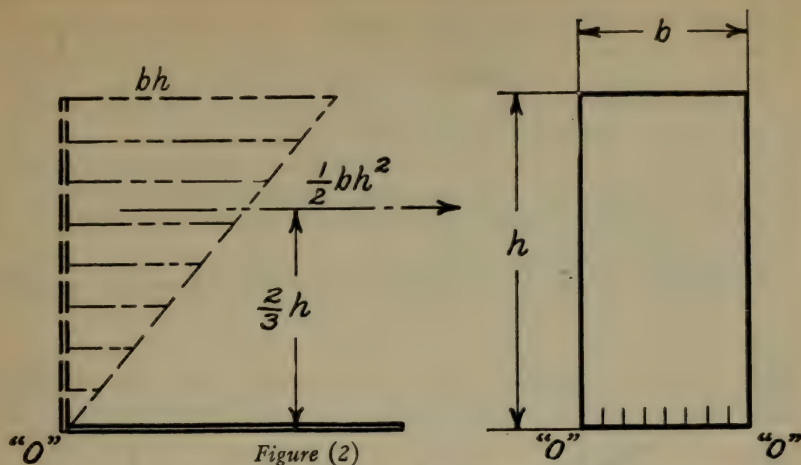


Figure (2)

If instead of a bar as in figure (1) we take several adjacent bars as shown in figure (2), we get a plate or rectangle whose height is h and whose breadth is b , and we again consider rotation about the axis $O - O$.

For each unit of breadth the force at a distance h from the axis will be h pounds and for b units of width the force is $b \times h$ pounds. This is represented graphically as bh in the figure (2). Similarly, the various horizontal lines in the triangle represent forces proportional to their distance from O and the area of the triangle will be the total of all the forces. The area of the triangle is $\frac{1}{2} (bh \times h) = \frac{1}{2} bh^2$. This force $\frac{1}{2} bh^2$ is the inertia of the rectangle whose height is h and breadth b when it is resisting rotation about the axis $O - O$. The force $\frac{1}{2} bh^2$ may be properly considered as concentrated at its center of gravity which is also the center of gravity of the triangle, and is $\frac{2}{3} h$ from the axis $O - O$.

The moment about the axis $O - O$ of the force $\frac{1}{2} bh^2$ is $\frac{1}{2} bh^2 \times \frac{2}{3} h$, or $\frac{1}{3} bh^3$, and is a fourth dimension quantity since it is $\frac{1}{3}$ the area of the rectangle bh multiplied by the square of h the height of the rectangle.

The quantity $\frac{1}{3} bh^3$ is the moment of inertia of the rectangle about the axis $O - O$ which is its base.

It is, however, usual in the analysis of stress in material that the rotation of a given cross section takes place about the center of gravity of the cross section instead of about its base O above found. This condition is shown in figure (3) where the axis of rotation is $X - X$. In such a case we have the equivalent of two rectangles each rotating about their base,

and in which h of figure (2) becomes $h/2$. The moment of inertia in this case is therefore $2 \times \frac{1}{3} b (h/2)^3 = \frac{1}{12} bh^3$.

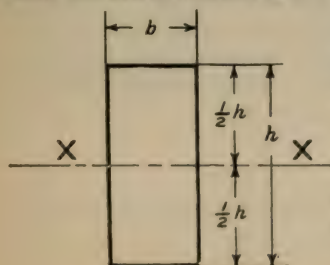


Figure (3)

The stresses which act in the materials of construction are classified as tension, compression or bearing, and shear. The action of pure tension is to elongate the material and reduce its area as it stretches. The action of compression is to shorten the specimen and

increase the area as it is compressed. The action of shear is to force the material on one side of a plane to slide along the material adjacent to it. One of the most familiar cases of shear is the punching of holes in a plate. Shear also exists in beams and girders, which also have tension and compression combined to form a couple to resist bending. It exists also in torsion where material is twisted as a shaft, and when a compression specimen is long enough shear acts along a plane at an angle to the axis of the specimen. Inasmuch as shear in the webs of beams and girders as well as in columns is combined with bearing or compression, the action is more properly described as one of crippling.

Consideration will now be given to the tension and compression stresses which form a couple to resist bending.

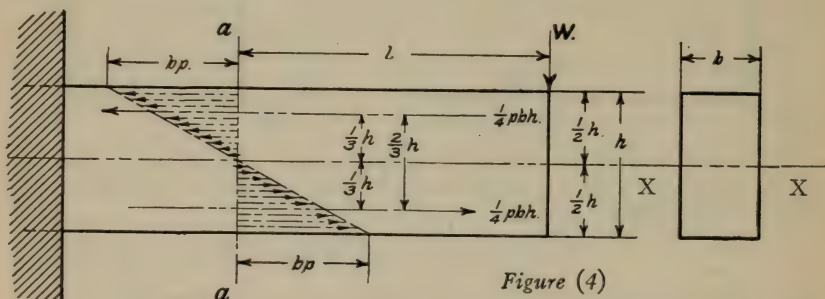


Figure (4)

Figure (4) represents a cantilever beam whose height is h and breadth b , and with a load W at a distance l from the cross section $a-a$. The maximum stress per square inch in tension or compression is p pounds.

The effect of the load W is to cause the section $a-a$ to rotate in the direction of a clock about the axis $X-X$. The only thing to prevent $a-a$ from rotating is the tension and compression stresses in the material. Above the center of the beam the fibres are in tension, and below the center they are in compression. The condition is similar to figure (3) and the intensity of the stresses will be directly proportional to their distance from the center. The maximum allowable intensity is, however, fixed as p pounds per square inch, and the total stress in the extreme fibre will be $b \times p$. The total stress for all fibres in tension or compression will be the area of the triangle, whose height is $h/2$ and whose breadth is bp .

This is $\frac{1}{2} bp \times h/2 = \frac{1}{4} bph$.

The effect of the tension and compression fibre stresses will be the same as if they were concentrated at the centers of gravity of the two triangles, and they will form a couple which balances the external bending moment. This balancing couple will therefore act opposite to the clock. The distance between the centers of gravity of the two triangles is $\frac{2}{3} h$ and the moment of the couple will be $\frac{1}{4} bph \times \frac{2}{3} h = \frac{1}{6} bph^2$ which is the moment of the internal stresses.

The moment of the external stresses M is $W \times l$.

From this we have the external moment $M = p \times \frac{1}{6} bh^2$.

In this we recognize the quantity $\frac{1}{6} bh^2$ as the section modulus of the rectangle bh , and the basic principle that the external moment M is equal to the stress per square inch in the extreme fibre multiplied by the section modulus (which is usually designated S .)

If we examine the value of the Section modulus we find that if it is multiplied by half the depth of the beam, or $h/2$ we get $\frac{1}{6}bh^2 \times h/2 = \frac{1}{12}bh^3$ which is the moment of inertia of the rectangle bh .

In other words, if we divide the moment of inertia by half the depth we get the section modulus, and the section modulus multiplied by the stress in the extreme fibre is the external moment.

In some text books half the depth $h/2$ is called y , and in others c , but as these are sometimes used in other connections in this discussion, v will indicate $h/2$.

Starting from the equation $M = p \times \frac{1}{6}bh^2$ and multiplying both sides by the same quantity, or rather the left side by v , and the right by $h/2$ we get $M \times v = p \times \frac{1}{6}bh^2 \times h/2 = p \times \frac{1}{12}bh^3$ or $Mv = pI$.

The fundamental principle involved in this elementary discussion extends into almost every phase of construction, and a clear understanding of it will contribute much to the elimination of empirical solution, and to the establishing of rational analysis.

It has been the purpose in the foregoing discussion to present the subject in concrete practical form without complicating it with the development of general formulae. The rectangular cross-section has been used because it permits of the simplest mathematical analysis of a basic principle from which further development may proceed. While the design of structural steel seldom involves the use of a single rectangular cross section, it is usually possible to subdivide the section used into a number of rectangles or triangles, some of which will have to resist rotation about an axis which is neither at the base nor center of gravity of the rectangle. For this reason, it becomes necessary to have a formula for the moment of inertia of an area about an axis at a given distance from the center of gravity of the cross-section, and the development of this is given in connection with figure (5).

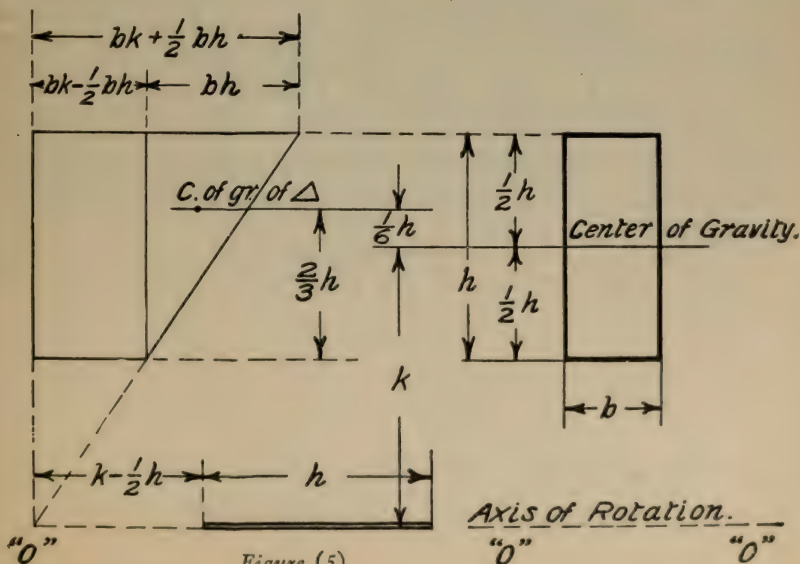


Figure (5)

This figure shows a rectangle with height h and breadth b rotating about an axis $O - O$ which is a distance k from the center of gravity of the rectangle.

The distance from the axis $O - O$ to the top of the rectangle is $k + h/2$ and from previous developed data the force for each unit of breadth is proportional to this distance, and therefore $k + h/2$. For b units of width, it will be b times this or $b(k + h/2) = bk + bh/2$. This is shown graphically in the diagram. Similarly the force for b units of width at the bottom of the rectangle or nearest the axis is $b k - bh/2$ which is also shown graphically. The total inertia or force resisting rotation about the axis $O - O$ will be the area of the figure made up of the rectangle whose height is h , and breadth $b k - bh/2$ together with the triangle whose height is h and breadth $b h$. The center of gravity of the rectangle is a distance k from the axis, and that of the triangle a distance of $k + h/6$. The moment of inertia about the axis will be the areas of the rectangle and triangle multiplied by their respective distances. That is, the moment of inertia about axis $O - O =$ area of rectangle $\times k +$ area of triangle $\times (k + h/6)$

$$\begin{aligned}
 &= (b k - bh/2) h \times k + \frac{1}{2} b h^2 (k + h/6) \\
 &= b h k^2 - bh^2 k/2 + bh^2 k/2 + \frac{1}{12} b h^3 \\
 &= b h k^2 + \frac{1}{12} b h^3 = \text{Area} \times k^2 + I
 \end{aligned}$$

Therefore, the moment of inertia of a rectangle about any axis is its moment of inertia about its center of gravity increased by the area of the rectangle multiplied by the square of the distance between the axis and the center of gravity.

In the analysis of the stresses in columns which fail by flexure the moment of inertia is used in a modified form which is called radius of gyration. The term "radius of gyration" is the distance from the axis of rotation at which, if the entire area were concentrated, it would have the same moment of inertia as the distributed area has. The formula for the moment of inertia of a rectangle about an axis through its center of gravity is

$$I = \frac{1}{12} b h^3 = b h \times \frac{1}{12} h^2$$

using A to equal the area $A = b h$ and substituting

$$I = A \times \frac{1}{12} h^2 = A h^2/12 = A (h/\sqrt{12})^2$$

In this equation $h/\sqrt{12}$ is the distance from the center of gravity that the entire area must be concentrated to give the same moment of inertia as the distributed area and $h/\sqrt{12}$ is called the radius of gyration which is designated r

Substituting r for $h/\sqrt{12}$

$$I = A r^2 \quad \text{or} \quad r^2 = I/A \quad \text{and} \quad r = \sqrt{I/A}$$

Nomenclature

I	=	Moment of Inertia
S	=	Section Modulus
r	=	Radius of Gyration
h	=	height or depth
b	=	breadth
A	=	Area
X-X	=	Horizontal Axis
Y-Y	=	Vertical Axis
x	=	distance along Horizontal Axis
y	=	distance along Vertical Axis
W	=	Total Load
W, W₁, etc.	=	Concentrated Loads
R, R₁, etc.	=	Reactions at the Supports
M	=	Bending Moment
M¹	=	Negative Bending Moment
E	=	Modulus of Elasticity
V	=	Vertical Shear
D	=	Deflection

Any deviation from the above nomenclature is
clearly noted at place of exception.

PROPERTIES OF VARIOUS SECTIONS

Section	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	a^2	$y = \frac{a}{2}$	$\frac{a^4}{12}$	$\frac{a^3}{6}$	$\frac{a}{\sqrt{12}} = .289 a$
	a^2	$y = a$	$\frac{a^4}{3}$	$\frac{a^3}{3}$	$\frac{a}{\sqrt{3}} = .577 a$
	a^2	$y = \frac{a}{\sqrt{2}} = .707 a$	$\frac{a^4}{12}$	$\frac{a^3}{6\sqrt{2}} = .118 a^3$	$\frac{a}{\sqrt{12}} = .289 a$
	$a^2 - a_1^2$	$y = \frac{a}{2}$	$\frac{a^4 - a_1^4}{12}$	$\frac{a^4 - a_1^4}{6 a}$	$\sqrt{\frac{a^2 + a_1^2}{12}}$
	$a^2 - a_1^2$	$y = a$	$\frac{a^4 - a_1^4}{3}$	$\frac{a^4 - a_1^4}{3 a}$	$\sqrt{\frac{a^2 + a_1^2}{3}}$
	$a^2 - a_1^2$	$y = \frac{a}{\sqrt{2}} = .707 a$	$\frac{a^4 - a_1^4}{12}$	$\frac{(a^4 - a_1^4)\sqrt{2}}{12 a} = .118 \frac{a^4 - a_1^4}{a}$	$\sqrt{\frac{a^2 + a_1^2}{12}} = .289 \sqrt{a^2 + a_1^2}$





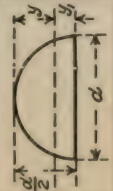
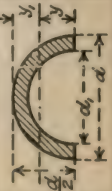
PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	bh	$y = \frac{h}{2}$	$\frac{bh^3}{12}$	$\frac{bh^2}{6}$	$\frac{h}{\sqrt{12}} = .289 h$
	bh	$y = h$	$\frac{bh^3}{3}$	$\frac{bh^2}{3}$	$\frac{h}{\sqrt{3}} = .577 h$
	bh	$y = \frac{bh}{\sqrt{b^2 + h^2}}$	$\frac{b^3 h^3}{6 (b^2 + h^2)}$	$\frac{b^2 h^2}{6 \sqrt{b^2 + h^2}}$	$\frac{bh}{\sqrt{6 (b^2 + h^2)}}$
	bh	$y = \frac{h \cos \alpha + b \sin \alpha}{2}$	$\frac{bh}{12} (h^2 \cos^2 \alpha + b^2 \sin^2 \alpha)$	$\frac{bh}{6} \left(\frac{h^2 \cos^2 \alpha + b^2 \sin^2 \alpha}{h \cos \alpha + b \sin \alpha} \right)$	$\sqrt{\frac{h^2 \cos^2 \alpha + b^2 \sin^2 \alpha}{12}}$
	$bh - b_1 h_1$	$y = \frac{h}{2}$	$\frac{bh^3 - b_1 h_1^3}{12}$	$\frac{bh^3 - b_1 h_1^3}{6h}$	$\sqrt{\frac{bh^3 - b_1 h_1^3}{12 (bh - b_1 h_1)}}$
	$b (h - h_1)$	$y = \frac{h}{2}$	$\frac{b (h^3 - h_1^3)}{12}$	$\frac{b (h^3 - h_1^3)}{6h}$	$\sqrt{\frac{h^3 - h_1^3}{12 (h - h_1)}}$

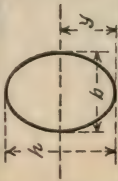
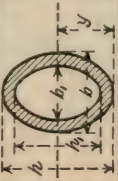
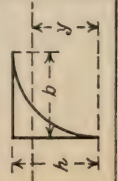
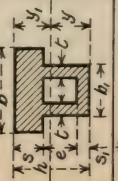

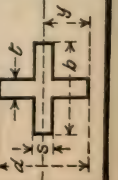
PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$\frac{3}{2} h^2 \tan 30^\circ = .866 h^2$	$y = \frac{h}{2}$	$\frac{A}{12} \left[\frac{h^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ $= .06 h^4$	$\frac{A}{6} \left[\frac{h (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ $= .12 h^3$	$\frac{h}{4 \cos 30^\circ} \sqrt{\frac{1 + 2 \cos^2 30^\circ}{3}}$ $= .264 h$
	$\frac{3}{2} h^2 \tan 30^\circ = .866 h^2$	$y = \frac{h}{2 \cos 30^\circ} = .577 h$	$\frac{A}{12} \left[\frac{h^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ $= .06 h^4$	$\frac{A}{6} \left[\frac{h (1 + 2 \cos^2 30^\circ)}{4 \cos 30^\circ} \right]$ $= .104 h^3$	$\frac{h}{4 \cos 30^\circ} \sqrt{\frac{1 + 2 \cos^2 30^\circ}{3}}$ $= .264 h$
	$2 h^2 \tan 22\frac{1}{2}^\circ = .828 h^2$	$y = \frac{h}{2}$	$\frac{A}{12} \left[\frac{h^2 (1 + 2 \cos^2 22\frac{1}{2}^\circ)}{4 \cos^2 22\frac{1}{2}^\circ} \right]$ $= .055 h^4$	$\frac{A}{6} \left[\frac{h (1 + 2 \cos^2 22\frac{1}{2}^\circ)}{4 \cos 22\frac{1}{2}^\circ} \right]$ $= .109 h^3$	$\frac{h}{4 \cos 22\frac{1}{2}^\circ} \sqrt{\frac{1 + 2 \cos^2 22\frac{1}{2}^\circ}{3}}$ $= .257 h$
	$n = \text{Number of Sides}$ $A = \frac{1}{4} n a^2 \cot . \text{OC}$ $= \frac{1}{2} n y^2 \sin . 2 \text{OC}$ $= n y_1^2 \tan . \text{OC}$	$y = \frac{a}{2 \sin . \text{OC}}$ $y_1 = \frac{a}{2 \tan . \text{OC}}$	$I_{1-1} = \frac{A (6 y^2 - a^2)}{24}$ $I_{2-2} = \frac{A (12 y_1^2 + a^2)}{48}$	$S_{1-1} = \frac{A (6 y^2 - a^2)}{24 y}$ $S_{2-2} = \frac{A (12 y_1^2 + a^2)}{48 y_1}$	$r_{1-1} = \sqrt{\frac{6 y^2 - a^2}{24}}$ $r_{2-2} = \sqrt{\frac{12 y_1^2 + a^2}{48}}$
	$\frac{h (b + b_1)}{2}$	$y = \frac{h (b_1 + b)}{3 (b + b_1)}$ $y_1 = \frac{h (b + 2 b_1)}{3 (b + b_1)}$	$\frac{h^3 (b^2 + 4 b b_1 + b_1^2)}{36 (b + b_1)}$	$\frac{h^2 (b^2 + 4 b b_1 + b_1^2)}{12 (b_1 + 2 b)}$	$\frac{h}{6 (b + b_1)} \sqrt{2 (b^2 + 4 b b_1 + b_1^2)}$
	$\frac{h (b + b_1)}{2}$	$y = h$	$\frac{h^3 (b + 3 b_1)}{12}$	$\frac{h^2 (b + 3 b_1)}{12}$	$\frac{h}{\sqrt{6}} \sqrt{\frac{b + 3 b_1}{b + b_1}}$

PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$\frac{bh}{2}$	$y = \frac{2h}{3}$ $y_1 = \frac{h}{3}$	$\frac{bh^3}{36}$	$\frac{bh^2}{24}$	$\frac{h}{\sqrt{18}} = .235702 \frac{h}{\sqrt{18}}$
	$\frac{bh}{2}$	$y = h$	$\frac{bh^3}{12}$	$\frac{bh^2}{12}$	$\frac{h}{\sqrt{6}} = .408248 \frac{h}{\sqrt{6}}$
	$\frac{\pi d^2}{4} = .785398 d^2$	$y = \frac{d}{2}$	$\frac{\pi d^4}{64} = .049087 d^4$	$\frac{\pi d^3}{32} = .098175 d^3$	$\frac{d}{4}$
	$\frac{\pi (d^2 - d_1^2)}{4}$ $= .785398 (d^2 - d_1^2)$	$y = \frac{d}{2}$	$\frac{\pi (d^4 - d_1^4)}{64} = .09087 (d^4 - d_1^4)$	$\frac{\pi (d^4 - d_1^4)}{32 d}$ $= .098175 \frac{d^4 - d_1^4}{d}$	$\frac{\sqrt{d^2 + d_1^2}}{4}$
	$\frac{\pi d^2}{8} = .392699 d^2$	$y = \frac{d(3\pi - 4)}{6\pi} = .287793 d$ $y_1 = \frac{2d}{3\pi} = .212207 d$	$\frac{d^4 (9\pi^2 - 64)}{1152\pi} = .006860 d^4$	$\frac{d^3 (9\pi^2 - 64)}{192 (3\pi - 4)}$ $= .023836 d^3$	$\frac{d \sqrt{9\pi^2 - 64}}{12\pi}$ $= .132168 d$
	$\frac{\pi (d^2 - d_1^2)}{8}$ $= .392699 (d^2 - d_1^2)$	$y = \frac{2 (d^3 - d_1^3)}{3\pi (d^2 - d_1^2)}$ $y_1 = \frac{3\pi d (d^2 - d_1^2) - 4 (d^3 - d_1^3)}{6\pi (d^2 - d_1^2)}$	$\frac{9\pi^2 (d^4 - d_1^4) (d^2 - d_1^2) - 64 (d^3 - d_1^3)^2}{1152\pi (d^2 - d_1^2)}$	$\frac{I}{y}$ if $y > y_1$ $\frac{I}{y_1}$ if $y_1 > y$	$\sqrt{\frac{I}{A}}$


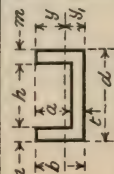
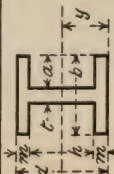

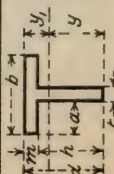

PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$\frac{\pi b h}{4} = .785 b h$	$\frac{h}{2}$	$\frac{\pi b h^3}{64} = .049 b h^3$	$\frac{\pi b h^2}{32} = .098 b h^2$	$\frac{h}{4}$
	$\frac{\pi (b h - b_1 h_1)}{4}$ $= .785 (b h - b_1 h_1)$	$\frac{h}{2}$	$\frac{\pi (b h^3 - b_1 h_1^3)}{64}$ $= .049 (b h^3 - b_1 h_1^3)$	$\frac{\pi (b h^2 - b_1 h_1^2)}{32}$ $= \frac{\pi (b h^3 - b_1 h_1^3)}{32 h}$	$\frac{1}{4} \sqrt{\frac{b h^3 - b_1 h_1^3}{b h - b_1 h_1}}$
	$(b = h = r)$ $\frac{\pi r^2}{4}$ $= .2146 r^2$	r $6 \left(1 - \frac{\pi}{4} \right)$ $= .7767 r$	$r^4 \left(\frac{1}{3} - \frac{\pi}{16} - \frac{1}{36 - 9\pi} \right)$ $= .0075 r^4$	$\frac{I}{y}$ $= .00966 r^3$	$\sqrt{.03494 r^2}$ $= .18693 r$
	$b s + 2 e t + b_1 s_1$	$y = \frac{2 t h^2 + (b_1 - 2 t) s_1^2 + (b - 2 t) (2 h - s) s}{2 A}$ $y_1 = h - y$	$\frac{b y_1^3 + b y_1^3 - (b_1 - 2 t) (y - s_1)^3}{3}$ $-\frac{(b - 2 t) (y_1 - s)^3}{3}$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$b m + h t + b_1 m$	$y = d - y_1$ $y_1 = \frac{t d^2 + m^2 (b - t) + m (b_1 - t) (2 d - m)}{2 A}$	$\frac{b y_1^3 + b_1 y^3 - (b - t) (y_1 - m)^3}{3}$ $-\frac{(b_1 - t) (y - m)^3}{3}$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$t d + s (b - t)$	$\frac{d}{2}$	$\frac{t d^3 + s^3 (b - t)}{12}$	$\frac{t d^3 + s^3 (b - t)}{6 d}$	$\sqrt{\frac{t d^3 + s^3 (b - t)}{12 [t d + s (b - t)]}}$

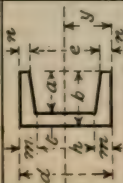
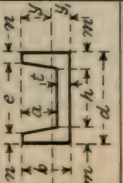

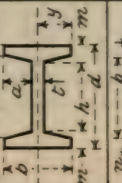


PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$t(2a - t)$	$y = a - \frac{a^2 + at - t^2}{2(2a - t)}$ $y_1 = \frac{a^2 + at - t^2}{2(2a - t)}$	$\frac{1}{3} \left[ty^3 + a(a-y)^3 - (a-t)(a-y-t)^3 \right]$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$t(2a - t)$	$y = \frac{a^2 + at - t^2}{2(2a - t)} \cos 45^\circ$ $y_1 = \sin 45^\circ (a + t) - y = .70711(a + t) - y$	When $x = a^2 + at - t^2 + 2(2a - t)$ $\frac{1}{3} \left[2x^4 - 2(x-t)^4 + t \left[a - \left(2x - \frac{t}{2} \right) \right]^3 \right]$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$t(b + h - t)$	$y = h - \frac{t(b + 2c) + c^2}{2(b + c)}$ $y_1 = \frac{t(b + 2c) + c^2}{2(b + c)}$	$\frac{1}{3} \left[t(h - y_1)^3 + by_1^3 - e(y_1 - t)^3 \right]$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$t(b + h - t)$	$y = h - \frac{t(h + 2e) + e^2}{2(h + e)}$ $y_1 = \frac{t(h + 2e) + e^2}{2(h + e)}$	$\frac{1}{3} \left[t(b - y_1)^3 + hy_1^3 - e(y_1 - t)^3 \right]$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$t(h + 2e)$	$y = \frac{h}{2}$	$\frac{1}{12} \left[bh^3 - e(h - 2t)^3 \right]$	$\frac{bh^3 - e(h - 2t)^3}{6h}$	$\sqrt{\frac{bh^3 - e(h - 2t)^3}{12t(h + 2e)}}$
	$t(h + 2e)$	$y = \frac{2b - t}{2}$	$\frac{1}{12} \left[h(b + e)^3 - 2e^3c - 6eb^2c \right]$	$\frac{h(b + e)^3 - 2e^3c - 6eb^2c}{6(2b - t)}$	$\sqrt{\frac{h(b + e)^3 - 2e^3c - 6eb^2c}{6(2b - t)}}$

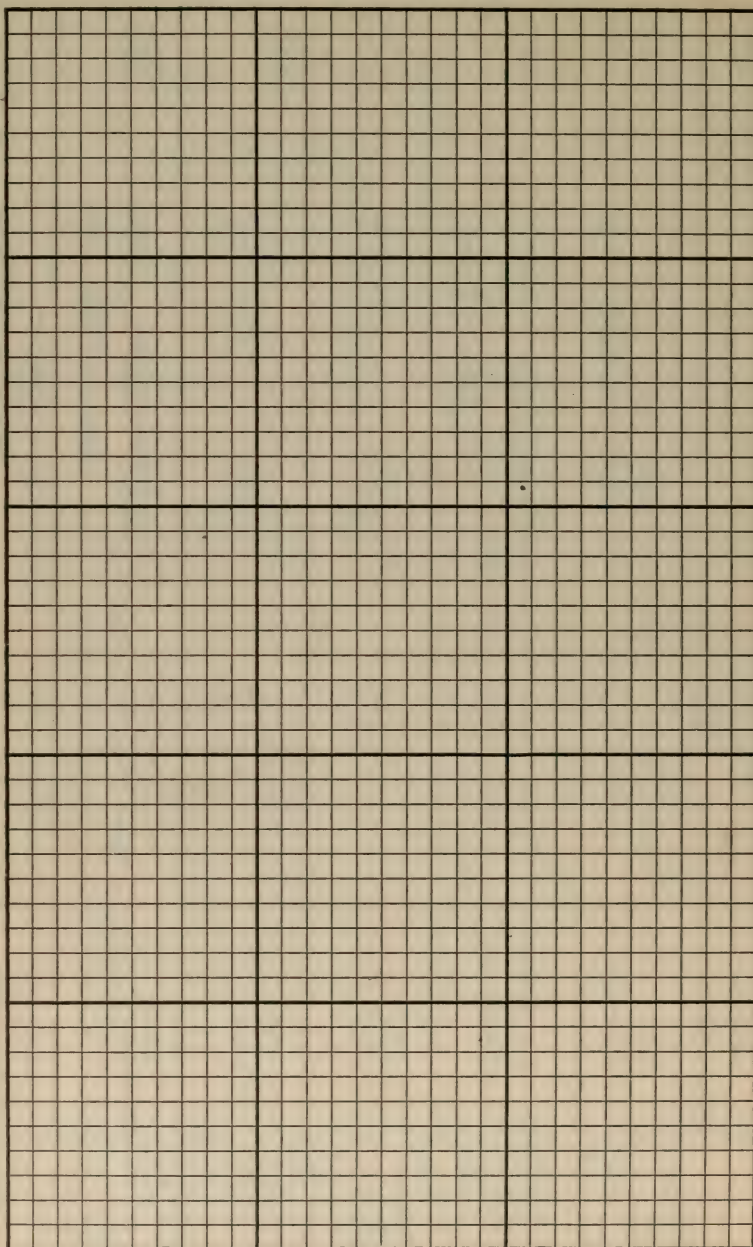
PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$bd - ah$	$y = \frac{d}{2}$	$\frac{1}{12} (bd^3 - ah^3)$	$\frac{bd^3 - ah^3}{6d}$	$\sqrt{\frac{bd^3 - ah^3}{12(bd - ah)}}$
	$bd - ah$	$y = \frac{b - y_1}{2}$ $y_1 = \frac{2b^2m + ht^2}{2A}$	$\frac{1}{3} (2mb^3 + ht^3) - Ay_1^2$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$bd - 2ah$	$y = \frac{d}{2}$	$\frac{1}{12} (bd^3 - 2ah^3)$	$\frac{bd^3 - 2ah^3}{6d}$	$\sqrt{\frac{I}{A}}$
	$bd - 2ah$	$y = \frac{b}{2}$	$\frac{1}{12} (2mb^3 + ht^3)$	$\frac{2mb^3 + ht^3}{6b}$	$\sqrt{\frac{I}{A}}$
	$bm + ht$	$y = \frac{d - y_1}{2}$ $y_1 = \frac{d^2t + m^2(b - t)}{2A}$	$\frac{1}{3} (ty^3 + by_1^3 - 2a(y_1 - m)^3)$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$bm + ht$	$y = \frac{b}{2}$	$\frac{1}{12} (mb^3 + ht^3)$	$\frac{mb^3 + ht^3}{6b}$	$\sqrt{\frac{I}{A}}$

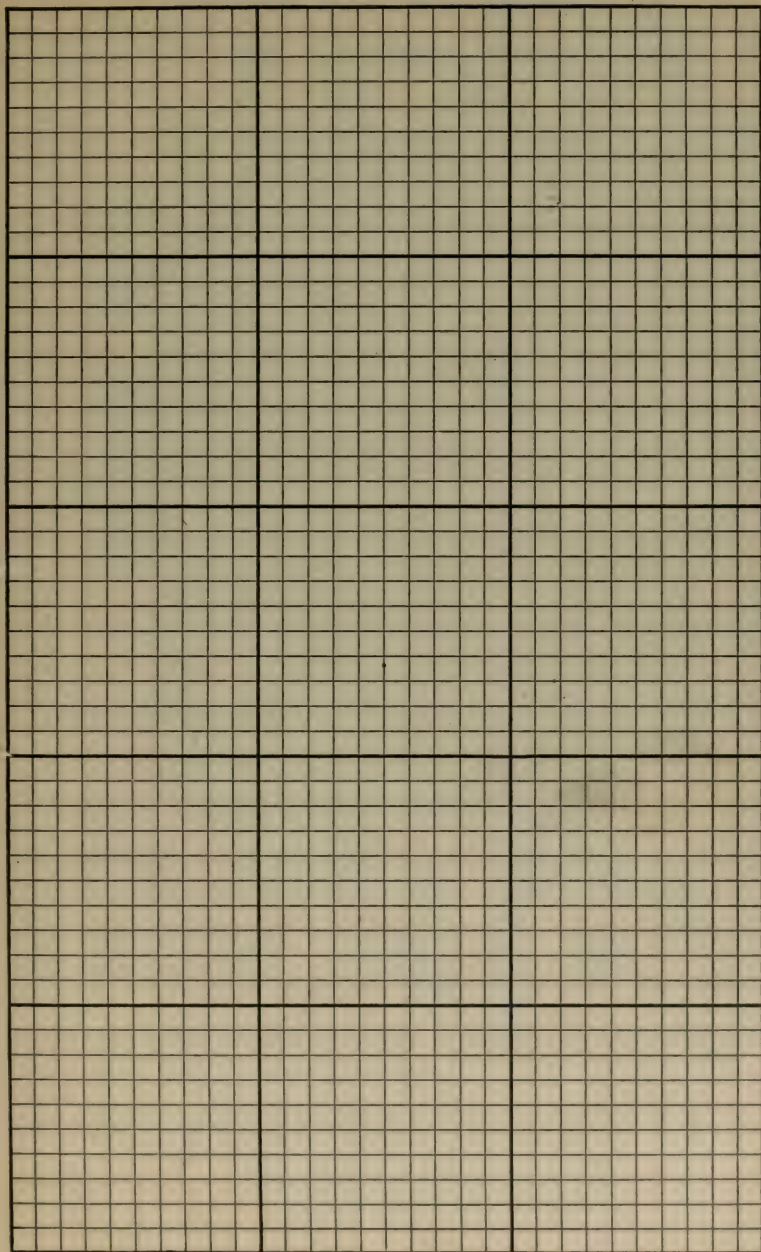
PROPERTIES OF VARIOUS SECTIONS

Sections	Area of Section A	Distance from Axis to Extremities of Section y and y_1	Moment of Inertia I	Section Modulus $S = \frac{I}{y}$	Radius of Gyration $r = \sqrt{\frac{I}{A}}$
	$td + a(m+n)$	$y = \frac{d}{2}$	$\frac{1}{12} \left[bd^3 - \frac{a}{8(m-n)}(e^4 - h^4) \right]$	$\frac{2I}{d}$	$\sqrt{\frac{I}{A}}$
	$td + a(m+n)$	$y = \frac{b-y_1}{2} + \frac{a(m-n)}{3} \left(\frac{b+2t}{A} \right)$	$\frac{1}{3} \left[2nb^3 + ht^3 + \frac{m-n}{2a}(b^4 - t^4) \right] - Ay_1^2$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$td + 2a(m+n)$	$y = \frac{d}{2}$	$\frac{1}{12} \left[bd^3 - \frac{a}{4(m-n)}(e^4 - h^4) \right]$	$\frac{2I}{d}$	$\sqrt{\frac{I}{A}}$
	$td + 2a(m+n)$	$y = \frac{b}{2}$	$\frac{1}{12} \left[2nb^3 + ht^3 + \frac{m-n}{4a}(b^4 - t^4) \right]$	$\frac{2I}{b}$	$\sqrt{\frac{I}{A}}$
	$\frac{e(t+u)}{2} + tm + a(m+n)$	$y = h - y_1$ $y_1 = \left[\frac{6an^2 + 2a(m-n)(m+2n) + 3td^2}{-e(t-u)(3d-e)} \right] + 6A$	$\frac{1}{12} \left[e^3(3u+t) + 4bm^3 - 2a(m-n)^3 \right] - A(y_1 - m)^2$	$\frac{I}{y}$	$\sqrt{\frac{I}{A}}$
	$\frac{e(t+u)}{2} + tm + a(m+n)$	$y = \frac{b}{2}$	$\frac{nb^3 + (m-n)^3 + eu^3}{12} + \frac{a(m-n)}{36} [2a^2 + (2a+3t)^2] + \frac{e(t-u)[(t-u)^2 + 2(t+2u)]}{144}$	$\frac{2I}{b}$	$\sqrt{\frac{I}{A}}$

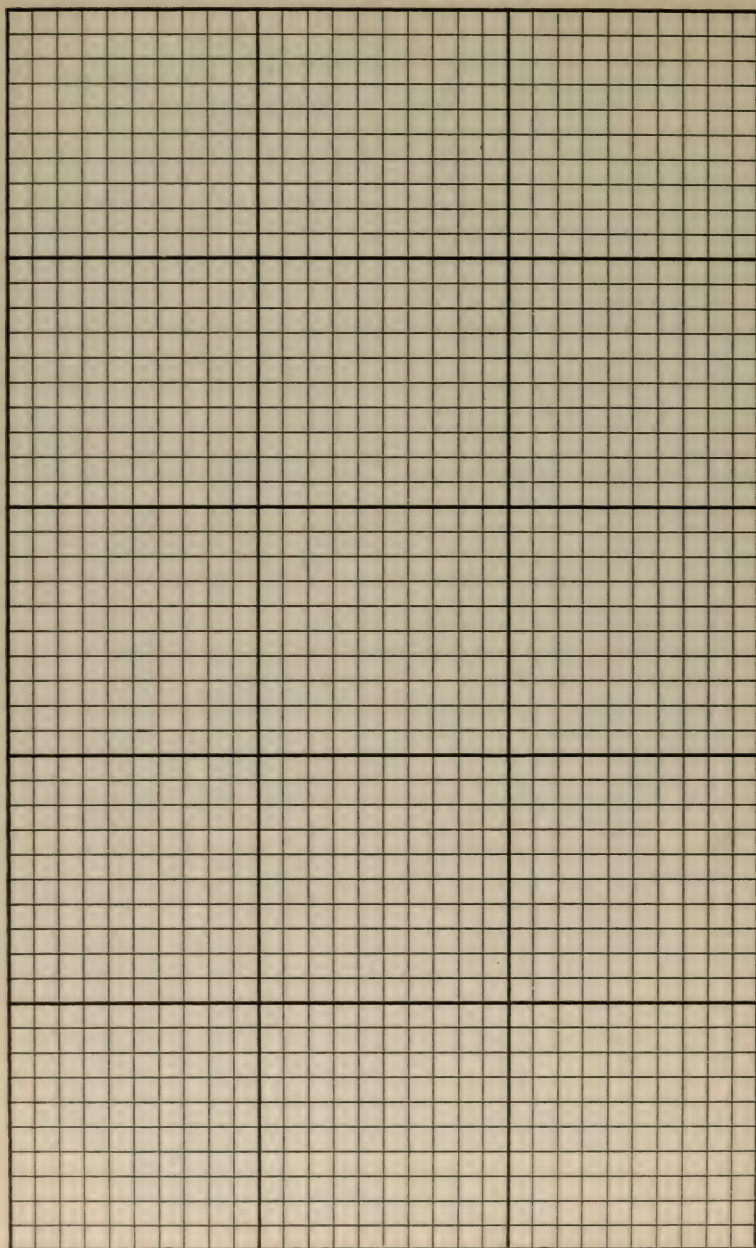
NOTES and DIAGRAMS



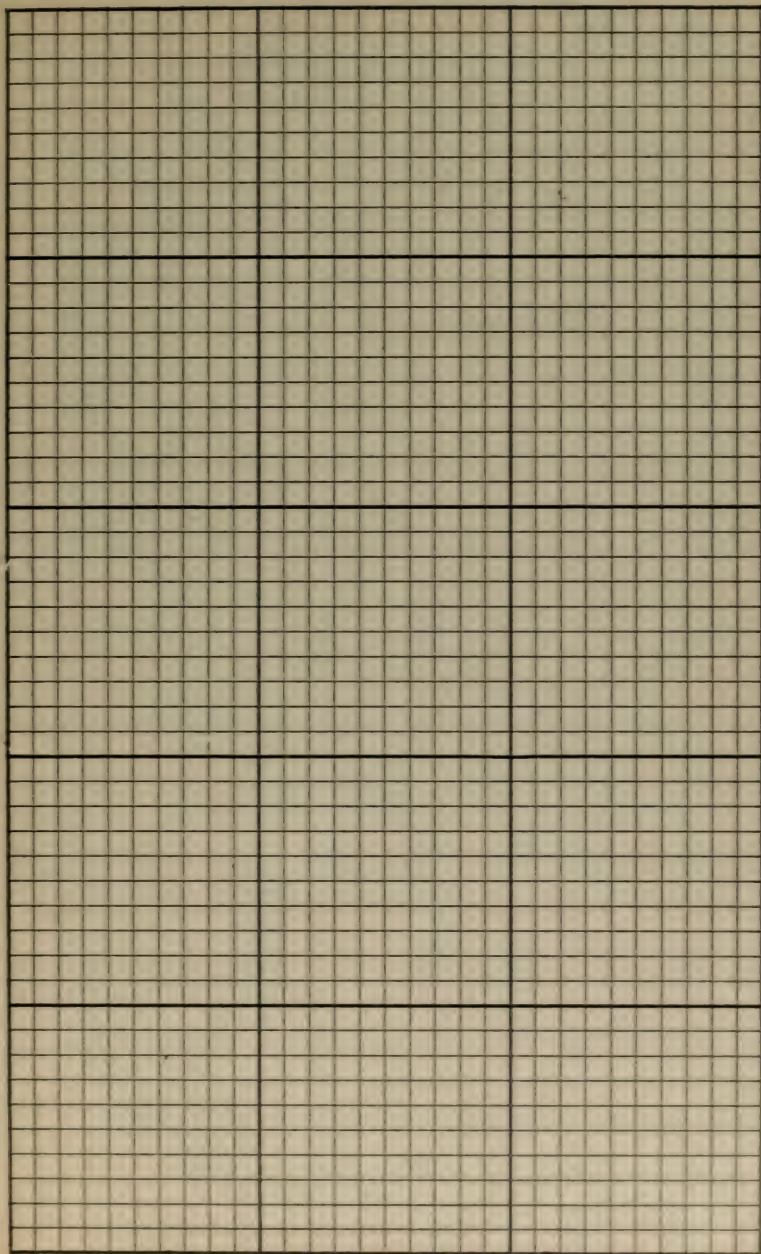
NOTES and DIAGRAMS



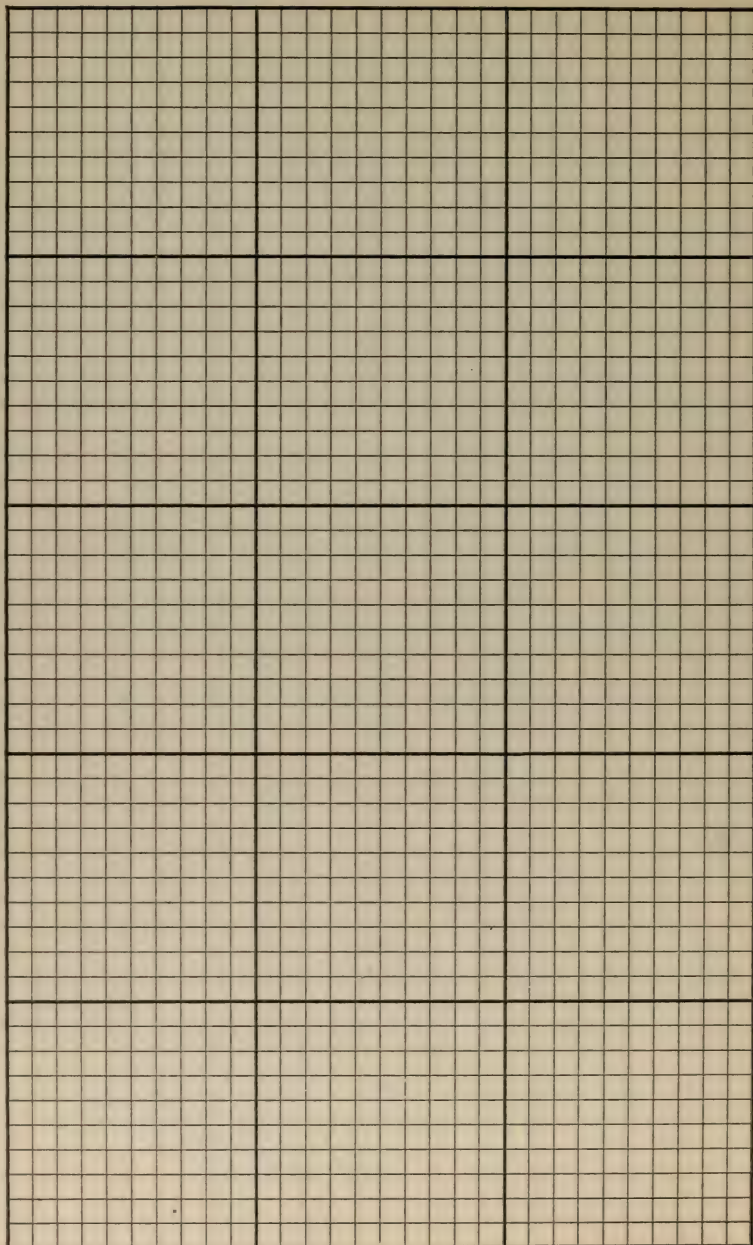
NOTES and DIAGRAMS



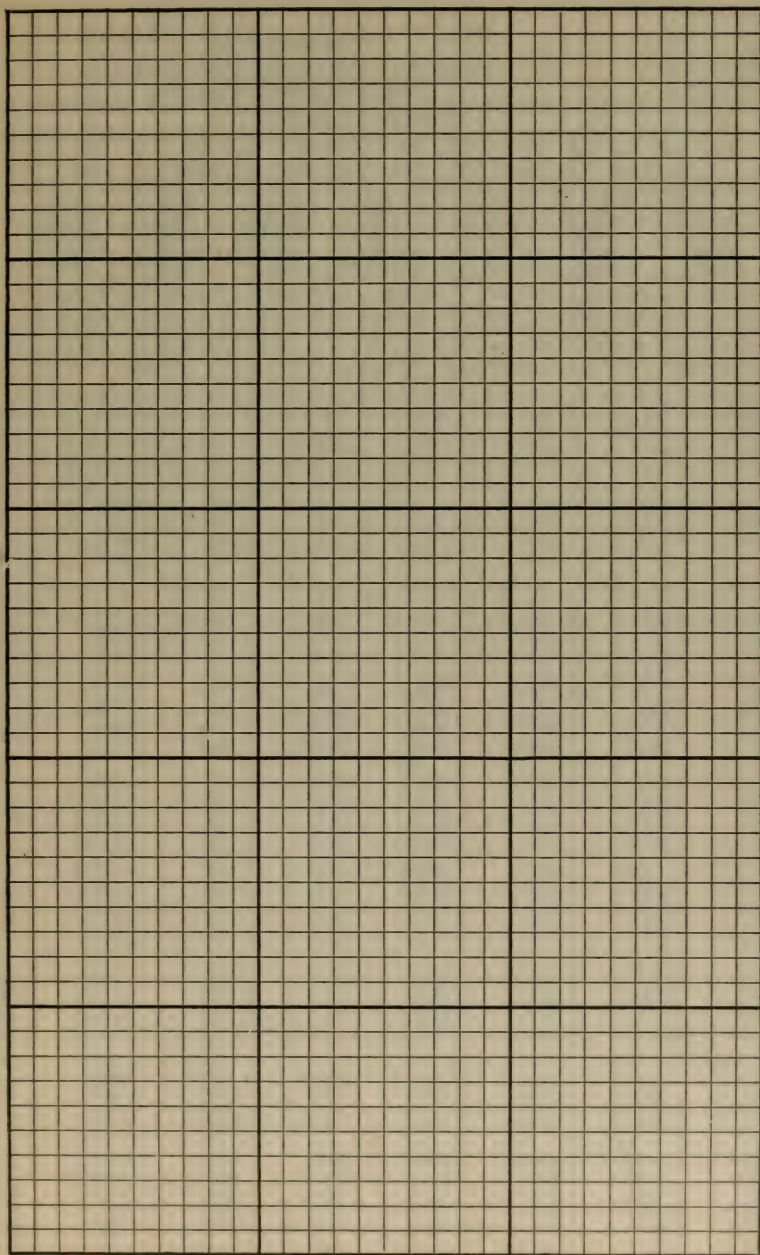
NOTES and DIAGRAMS



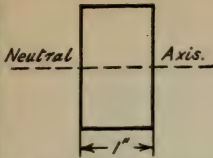
NOTES and DIAGRAMS



NOTES and DIAGRAMS



MOMENTS OF INERTIA OF RECTANGLES ABOUT THE NEUTRAL AXIS



Values given are the Moments of Inertia for Rectangles
ONE INCH WIDE

The value for any width rectangle may be obtained from
value given by direct multiplication

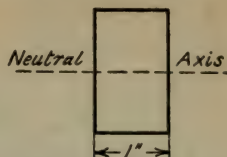
h in Inches	Additional Height h.							
	0	1/16	1/8	3/16	1/4	5/16	3/8	7/16
000002	.00016	.00055	.00130	.00254	.00439	.00698
1	.08333	.09995	.11865	.13955	.16276	.18842	.21663	.24754
2	.66667	.73114	.79964	.87229	.94922	1.0305	1.1164	1.2068
3	2.2500	2.3936	2.5431	2.6988	2.8607	3.0289	3.2036	3.3849
4	5.3333	5.5873	5.8491	6.1190	6.3971	6.6802	6.9783	7.2817
5	10.417	10.812	11.218	11.633	12.059	12.494	12.941	13.397
6	18.000	18.568	19.149	19.741	20.345	20.961	21.590	22.232
7	28.583	29.356	30.142	30.942	31.757	32.585	33.428	34.285
8	42.667	43.674	44.698	45.737	46.793	47.864	48.952	50.056
9	60.750	62.024	63.317	64.626	65.954	67.300	68.665	70.047
10	83.333	84.906	86.498	88.109	89.741	91.392	93.064	94.756
11	110.92	112.82	114.74	116.69	118.65	120.64	122.65	124.68
12	144.00	146.26	148.55	150.86	153.19	155.55	157.93	160.33
13	183.08	185.74	188.42	191.12	193.85	196.61	199.39	202.20
14	228.67	231.74	234.85	237.98	241.14	244.32	247.54	250.78
15	281.25	284.78	288.34	291.93	295.55	299.20	302.87	306.58
16	341.33	345.35	349.40	353.47	357.58	361.73	365.90	370.11
17	409.42	413.95	418.52	423.11	427.75	432.41	437.11	441.85
18	486.00	491.41	496.20	501.35	506.53	511.75	517.01	522.31
19	571.58	577.24	582.94	588.67	594.44	600.25	606.10	611.98
20	666.67	672.94	679.24	685.59	691.84	698.41	704.87	711.38
21	771.75	778.66	785.61	792.61	799.65	806.72	813.84	821.00
22	887.33	894.92	902.54	910.21	917.93	925.68	933.49	941.33
23	1013.9	1022.2	1030.5	1038.9	1047.3	1055.8	1064.3	1072.9
24	1152.0	1161.0	1170.1	1178.4	1188.4	1197.6	1206.8	1216.2
25	1302.1	1311.9	1321.7	1331.6	1341.5	1351.5	1361.6	1371.6
26	1464.7	1475.3	1485.9	1496.6	1507.3	1518.1	1529.0	1539.9
27	1640.2	1651.7	1663.1	1674.7	1686.2	1697.9	1709.5	1721.3
28	1829.3	1841.6	1853.9	1866.3	1878.8	1891.3	1903.8	1916.4
29	2032.4	2045.6	2058.8	2072.1	2085.4	2098.8	2112.3	2125.8
30	2250.0	2264.1	2278.2	2292.4	2306.7	2321.0	2335.4	2349.9
31	2482.6	2497.6	2512.7	2527.9	2543.1	2558.4	2573.8	2589.2
32	2730.7	2746.7	2762.8	2778.9	2795.2	2811.4	2827.8	2844.2
33	2994.7	3011.8	3028.9	3046.1	3063.3	3080.4	3098.0	3115.4
34	3275.3	3293.4	3311.6	3329.8	3348.1	3366.5	3384.9	3403.4
35	3572.9	3592.0	3611.3	3630.6	3650.0	3669.5	3689.0	3708.6
36	3888.0	3908.3	3928.6	3949.1	3969.6	3990.1	4010.8	4031.5
37	4221.1	4242.5	4264.0	4285.6	4307.3	4328.9	4350.7	4372.6
38	4572.7	4595.3	4617.9	4640.7	4663.5	4686.4	4719.4	4732.4
39	4943.3	4967.0	4990.9	5014.9	5038.9	5063.0	5087.2	5111.5
40	5333.3	5358.4	5383.5	5408.7	5433.9	5459.3	5484.7	5510.2
41	5743.4	5769.7	5796.1	5822.6	5849.1	5875.7	5902.5	5929.2
42	6174.0	6201.6	6229.3	6257.1	6284.9	6312.8	6340.9	6368.9
43	6625.6	6654.5	6683.5	6703.5	6741.8	6771.1	6800.4	6829.9
44	7098.7	7129.0	7159.3	7189.0	7220.3	7251.0	7281.7	7312.5
45	7593.8	7625.4	7657.2	7689.1	7721.0	7753.0	7785.2	7817.4
46	8111.3	8144.7	8177.6	8210.9	8244.3	8277.8	8311.3	8345.0
47	8651.9	8686.5	8721.1	8755.9	8790.7	8825.6	8860.7	8895.8
48	9216.0	9252.0	9288.2	9324.4	9360.7	9397.2	9433.7	9470.3
49	9804.1	9841.6	9879.3	9833.7	9954.9	9992.9	10031	10071
50	10417	10456	10495	10534	10574	10613	10653	10692
51	11054	11095	11136	11177	11218	11259	11300	11341
52	11717	11760	11802	11845	11887	11930	11973	12016
53	12406	12450	12494	12539	12583	12627	12672	12716
54	13122	13168	13213	13259	13305	13351	13397	13444
55	13865	13912	13959	14007	14055	14102	14150	14198
56	14635	14684	14733	14782	14832	14881	14931	14980
57	15433	15484	15535	15586	15637	15688	15739	15791
58	16259	16312	16365	16418	16470	16524	16577	16630
59	17115	17169	17224	17279	17333	17388	17443	17498

MOMENTS OF INERTIA OF RECTANGLES

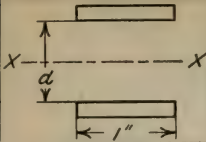
ABOUT THE NEUTRAL AXIS

Values given are the Moments of Inertia for Rectangles
ONE INCH WIDE

The value for any width rectangle may be obtained from
value given by direct multiplication



h in Inches	Additional Height h.							
	1/2 .500	3/16 .5625	5/8 .625	11/16 .6875	3/4 .750	13/16 .8125	7/8 .875	15/16 .9375
0	.01041	.01483	.02034	.02708	.03516	.04469	.05583	.06866
1	.28125	.31789	.35758	.40045	.44661	.49620	.54932	.60610
2	1.3021	1.4022	1.5073	1.6176	1.7331	1.8539	1.9803	2.1123
3	3.5729	3.7678	3.9696	4.1784	4.3945	4.6179	4.8488	5.0872
4	7.5937	7.9146	8.2443	8.5831	8.9310	9.2882	9.6548	10.031
5	13.865	14.343	14.832	15.331	15.843	16.365	16.898	17.443
6	22.885	23.552	24.231	24.924	25.629	26.347	27.079	27.825
7	35.156	36.043	36.944	37.859	38.790	39.736	40.698	41.674
8	51.177	52.314	53.468	54.639	55.827	57.032	58.254	59.493
9	71.448	72.867	74.305	75.762	77.238	78.733	80.247	81.780
10	96.469	98.202	99.955	101.73	103.52	105.34	107.18	109.04
11	126.74	128.82	130.92	133.04	135.19	137.35	139.55	141.76
12	162.76	165.21	167.69	170.19	172.72	175.27	177.85	180.46
13	205.03	207.89	210.78	213.69	216.63	219.60	222.60	225.62
14	254.05	257.35	260.68	264.04	267.42	270.83	274.28	277.75
15	310.32	314.09	317.89	321.72	325.58	329.47	333.40	337.35
16	374.34	378.61	382.92	387.25	391.62	396.02	400.45	404.92
17	446.61	451.42	456.25	461.12	466.03	470.97	475.94	480.95
18	527.63	533.00	538.40	543.84	549.32	554.83	560.38	565.96
19	617.91	623.87	629.87	635.90	641.98	648.09	654.24	660.44
20	717.93	724.51	731.14	737.81	744.51	751.26	758.05	764.88
21	828.20	835.44	842.73	850.05	857.43	864.84	872.29	879.79
22	949.22	957.15	965.13	973.15	981.21	989.32	997.47	1005.7
23	1081.5	1090.1	1098.8	1107.6	1116.4	1125.2	1134.1	1143.0
24	1225.5	1234.9	1244.4	1253.9	1263.4	1273.0	1282.6	1292.3
25	1381.8	1392.0	1402.2	1412.5	1422.8	1433.2	1443.6	1454.1
26	1550.8	1561.8	1572.8	1584.0	1595.1	1606.3	1617.6	1628.9
27	1733.1	1744.9	1756.8	1768.8	1780.8	1792.8	1804.9	1817.1
28	1929.1	1941.8	1954.6	1967.4	1980.3	1993.2	2006.2	2019.3
29	2149.4	2153.0	2166.7	2180.4	2194.2	2208.1	2222.0	2236.0
30	2364.4	2378.9	2393.6	2408.3	2423.0	2437.8	2452.7	2467.6
31	2604.7	2620.2	2635.8	2651.4	2667.2	2682.9	2698.8	2714.7
32	2860.7	2877.2	2893.8	2910.5	2927.2	2944.0	2960.8	2977.8
33	3132.9	3150.5	3168.1	3185.8	3203.6	3221.4	3239.3	3257.3
34	3422.0	3440.6	3459.3	3478.1	3496.9	3515.8	3534.8	3553.8
35	3728.2	3748.0	3767.8	3787.6	3807.6	3827.6	3847.6	3867.8
36	4052.3	4073.1	4094.0	4115.0	4136.1	4157.2	4178.4	4199.7
37	4394.5	4416.5	4438.6	4460.8	4483.0	4505.3	4527.7	4550.1
38	4755.5	4778.7	4802.0	4825.4	4848.8	4872.3	4895.9	4919.5
39	5135.8	5160.2	5184.7	5209.3	5239.6	5265.3	5285.5	5308.4
40	5535.8	5561.5	5587.3	5613.1	5639.0	5665.0	5691.0	5717.2
41	5956.1	5983.1	6010.1	6037.0	6064.4	6091.7	6119.0	6146.5
42	6397.1	6425.4	6453.7	6482.2	6510.7	6539.3	6568.0	6596.7
43	6867.7	6889.0	6918.7	6948.5	6978.3	7008.3	7038.3	7068.5
44	7343.4	7374.4	7405.5	7436.6	7467.9	7499.2	7530.6	7562.1
45	7849.7	7882.1	7914.6	7947.1	7979.8	8012.5	8045.4	8078.3
46	8378.7	8412.5	8446.5	8480.5	8514.6	8548.8	8583.1	8617.4
47	8931.0	8966.3	9001.7	9037.2	9072.7	9108.4	9144.2	9180.0
48	9507.0	9544.1	9580.7	9617.7	9654.8	9692.0	9729.2	9766.6
49	10107	10146	10184	10223	10261	10300	10339	10378
50	10732	10772	10812	10852	10892	10933	10973	11014
51	11383	11424	11466	11507	11549	11591	11633	11675
52	12059	12102	12145	12188	12232	12275	12319	12363
53	12761	12806	12851	12896	12941	12986	13031	13076
54	13490	13536	13583	13630	13676	13723	13770	13817
55	14246	14294	14343	14391	14440	14488	14537	14586
56	15030	15080	15130	15180	15231	15281	15331	15382
57	15842	15894	15946	15998	16050	16102	16154	16207
58	16683	16737	16791	16844	16898	16952	17006	17061
59	17554	17609	17665	17720	17776	17832	17888	17944



MOMENTS OF INERTIA OF TWO PLATES

Moments of Inertia of Two Plates ONE INCH WIDE About Axis X-X.
Depths measured between Plates.

To obtain the Moment of Inertia of two plates of any desired width multiply the Tabular Value given for the correct thickness and depth between plates by the net width.

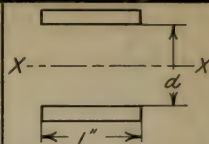
d Ins.	Thickness in Inches															
	1/8	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"		
6	2.3	4.9	6.2	7.6	9.1	10.6	12.1	13.8	15.4	17.2	18.9	20.7	22.7	24.7		
6 1/2	2.7	5.7	7.3	8.9	10.5	12.3	14.1	15.9	17.8	19.8	21.8	23.9	26.1	28.3		
7	3.2	6.6	8.4	10.2	12.1	14.1	16.1	18.2	20.4	22.6	24.9	27.2	29.7	32.2		
7 1/2	3.6	7.5	9.5	11.6	13.8	16.0	18.3	20.7	23.1	25.6	28.2	30.8	33.5	36.3		
8	4.1	8.5	10.8	13.2	15.6	18.1	20.6	23.3	26.0	28.8	31.6	34.6	37.6	40.7		
8 1/2	4.6	9.6	12.1	14.8	17.5	20.3	23.1	26.1	29.1	32.2	35.3	38.6	41.9	45.3		
9	5.2	10.7	13.6	16.5	19.5	22.6	25.7	29.0	32.3	35.7	39.2	42.8	46.4	50.2		
9 1/2	5.8	11.9	15.0	18.3	21.6	25.0	28.5	32.1	35.7	39.5	43.3	47.2	51.2	55.3		
10	6.4	13.1	16.6	20.2	23.8	27.6	31.4	35.3	39.3	43.4	47.6	51.9	56.2	60.7		
10 1/2	7.1	14.5	18.3	22.2	26.2	30.3	34.5	38.7	43.1	47.5	52.1	56.7	61.5	66.3		
12	9.2	18.8	23.7	28.7	33.9	39.1	44.2	49.8	55.4	61.0	66.8	72.6	78.6	84.7		
12 1/2	10.0	20.3	25.7	31.1	36.6	42.3	48.0	53.9	59.8	65.9	72.1	78.4	84.8	91.3		
14	12.5	25.4	32.0	38.8	45.6	52.6	59.7	66.9	74.2	81.7	89.2	96.9	104.7	112.7		
14 1/2	13.4	27.2	34.3	41.5	48.8	56.3	63.8	71.5	79.4	87.3	95.3	103.5	111.9	120.3		
15	14.3	29.1	36.7	44.3	52.1	60.1	68.1	76.3	84.7	93.1	101.7	110.4	119.2	128.2		
16	16.2	33.0	41.6	50.2	59.1	68.1	77.2	86.4	95.8	105.3	114.9	124.7	134.6	144.7		
16 1/2	17.3	35.1	44.2	53.4	62.8	72.3	81.9	91.7	101.6	111.7	121.9	132.2	142.7	153.3		
18	20.5	41.6	52.4	63.3	74.4	85.6	96.9	108.4	120.1	131.9	143.9	156.0	168.2	180.7		
18 1/2	21.7	43.9	55.3	66.8	78.5	90.3	102.2	114.3	126.6	139.0	151.6	164.3	177.2	190.3		
20	25.3	51.3	64.5	77.8	91.4	105.1	118.9	133.0	147.2	161.5	176.1	190.8	205.6	220.7		
20 1/2	26.6	53.8	67.7	81.7	95.9	110.3	124.8	139.5	154.4	169.4	184.6	200.1	215.6	231.3		
21	27.9	56.4	71.0	85.7	100.5	115.6	130.8	146.2	161.7	177.5	193.4	209.5	225.7	242.2		
22	30.6	61.9	77.8	93.9	110.1	126.6	143.2	160.0	177.0	194.2	211.5	229.0	246.8	264.7		
22 1/2	32.0	64.7	81.3	98.1	115.1	132.3	149.6	167.2	184.9	202.8	220.9	239.2	257.6	276.3		
24	36.4	73.5	92.4	111.4	130.6	150.1	169.7	189.5	209.6	229.8	250.2	270.8	291.6	312.7		
24 1/2	37.9	76.6	96.2	116.0	136.0	156.3	176.7	197.3	218.1	239.2	260.4	281.8	303.5	325.3		
26	42.7	86.1	108.2	130.4	152.9	175.6	198.5	221.6	244.9	268.4	292.1	316.1	340.3	364.7		
26 1/2	44.3	89.4	112.3	135.4	158.7	182.3	206.0	230.0	254.1	278.5	303.1	328.0	353.0	378.3		
27	46.0	92.8	116.6	140.5	164.7	189.1	213.7	238.5	263.6	288.8	314.3	340.1	366.0	392.2		
28	49.4	99.8	125.3	151.0	176.9	203.1	229.5	256.1	283.0	310.0	337.3	364.9	392.7	420.7		
28 1/2	51.2	103.3	129.7	156.3	183.2	210.3	237.6	265.1	292.9	320.9	349.2	377.6	406.3	435.3		
30	56.7	114.4	143.6	173.0	202.7	232.6	262.7	293.1	323.8	354.7	385.8	417.2	448.8	480.7		
30 1/2	58.6	118.2	148.4	178.7	209.4	240.3	271.4	302.8	334.4	366.3	398.4	430.8	463.4	496.3		
32 1/2	66.5	134.1	168.2	202.7	237.3	272.3	307.5	342.9	378.7	414.7	450.9	487.4	524.2	561.3		
33	68.6	138.2	173.4	208.9	244.6	280.6	316.8	353.4	390.2	427.2	464.5	502.1	540.0	578.2		
34 1/2	74.9	150.9	189.4	228.1	267.0	306.3	345.8	385.6	425.7	466.0	506.7	547.6	588.8	630.3		
36	81.6	164.3	206.0	248.1	290.4	333.1	376.0	419.2	462.7	506.5	550.6	595.0	639.7	684.7		
36 1/2	83.8	168.8	211.7	255.0	298.5	342.3	386.4	430.7	475.4	520.4	565.7	611.2	657.1	703.3		
38 1/2	93.2	187.7	235.4	283.4	331.7	380.3	429.2	478.4	527.9	577.8	627.9	678.4	729.2	780.3		
40 1/2	103.1	207.6	260.3	313.3	366.6	420.3	474.3	528.6	583.2	638.2	693.4	749.1	805.0	861.3		
42 1/2	113.6	228.4	286.4	344.7	403.3	462.3	521.6	581.2	641.2	701.5	762.2	823.2	884.6	946.3		
44 1/2	124.6	250.3	313.8	377.6	441.7	506.3	571.1	636.4	702.0	767.9	834.2	900.9	967.9	1035.3		
46 1/2	135.9	273.2	342.4	412.0	481.9	552.3	623.0	694.0	765.5	837.3	909.5	982.0	1055.0	1128.3		
48 1/2	147.8	297.1	372.3	447.9	523.9	600.3	677.0	754.2	831.7	909.7	988.0	1066.7	1145.8	1225.3		
50 1/2	160.2	321.9	403.4	485.3	567.6	650.3	733.4	816.9	900.7	985.0	1069.7	1154.8	1240.4	1326.3		
52 1/2	173.1	347.8	435.8	524.2	613.0	702.3	791.9	882.0	972.5	1063.4	1154.7	1246.5	1338.7	1431.3		
54 1/2	186.5	374.7	469.4	564.6	662.2	756.3	852.7	949.7	1047.0	1144.8	1243.0	1341.7	1440.8	1540.3		
56 1/2	200.4	402.6	504.3	606.5	709.2	812.3	915.8	1019.8	1124.3	1229.2	1334.5	1440.3	1546.6	1653.3		
58 1/2	214.8	431.4	540.5	649.9	759.9	870.3	981.1	1092.5	1204.3	1316.5	1429.3	1542.5	1656.1	1770.3		
60 1/2	229.7	461.3	577.8	694.8	812.3	930.3	1048.7	1167.6	1287.0	1406.9	1527.3	1648.1	1769.5	1891.3		
62 1/2	245.1	492.2	616.5	741.2	866.5	992.3	1118.5	1245.3	1372.5	1500.3	1628.5	1757.3	1886.5	2016.3		
64 1/2	261.0	524.1	656.4	789.1	922.4	1056.3	1190.6	1325.4	1460.8	1596.7	1733.0	1869.9	2007.4	2145.3		
66 1/2	277.4	556.9	697.5	838.6	980.1	1122.3	1264.9	1408.1	1551.8	1696.0	1840.8	1986.1	2131.9	2278.3		
68 1/2	294.3	590.8	739.9	889.5	1039.6	1190.3	1341.5	1493.2	1645.6	1798.4	1951.8	2105.7	2260.2	2415.3		
70 1/2	311.7	625.7	783.5	941.9	1100.8	1260.3	1420.3	1580.9	1742.1	1903.8	2066.1	2228.9	2392.3	2556.3		
72 1/2	329.6	661.6	828.4	995.8	1163.7	1332.3	1501.4	1671.1	1841.3	2012.2	2183.6	2355.5	2528.1	2701.3		
74 1/2	348.0	698.4	874.5	1051.2	1228.4	1406.3	1584.7	1763.7	1943.3	2123.5	2304.3	2485.7	2667.7	2850.3		
76 1/2	367.0	736.3	921.9	1108.1	1294.9	1482.3	1670.3	1858.9	2048.1	2237.9	2428.3	2619.4	2811.0	3003.3		
78 1/2	386.4	775.2	970.5	1166.5	1363.1	1560.3	1758.1	1956.5	2155.6	2355.3	2555.6	2756.5	2958.1	3160.3		
80 1/2	406.3	815.1	1020.4	1226.4	1433.0	1640.3	1848.2	2056.7	2265.9	2475.7	2686.1	2897.2	3108.9	3321.3		
82 1/2	426.7	855.9	1071.6	1287.8	1504.7	1722.3	1940.5	2159.3	2378.9	2599.0	2819.9	3041.3	3263.5	3486.3		
84 1/2	447.6	897.8	1123.9	1350.7	1578.1	1806.3	2035.0	2264.5	2494.6	2725.4	2956.9	3189.0	3421.8	3655.3		
90 1/2	513.3	1029.4	1288.6	1548.4	1809.0	2070.3	2332.3	2595.0	2858.4	3122.5	3387.4	3653.0	3919.3	4186.3		
96 1/2	583.5	1170.1	1464.5	1759.6	2055.6	2352.3	2649.7	2947.9	3246.9	3546.7	3847.2	4148.4	4450.5	4753.3		
102 1/2	658.2	1319.7	1651.6	1984.4	2317.9	2652.3	2987.4	3323.4	3660.2	3997.8	4336.2	4675.4	5015.4	5356.3		
108 1/2	737.5	1478.3	1850.0	2222.6	2596.0	2970.3	3345.4	3721.4	4098.2	4475.9	4854.5	5233.9	5614.1	5995.3		
114 1/2	821.2	1645.9	2059.7	2474.3	2889.8	3306.3	3723.6	4141.8	4561.0	4981.0	5402.0	5823.8	6246.6	6670.3		
120 1/2	909.4	1822.6	2280.6	2739.5	3199.4	3660.3	4122.1	4584.8	5048.5	5513.2	5978.8	6445.3	6912.8	7381.3		

MOMENTS OF INERTIA OF TWO PLATES

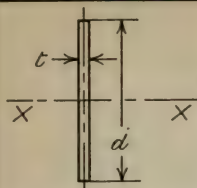
Moments of Inertia of Two Plates ONE INCH WIDE About Axis X—X

Depths measured between Plates.

To obtain the Moment of Inertia of two plates of any desired width multiply the Tabular Value given for the correct thickness and depth between plates by the net width.



d Ins.	Thickness in Inches													
	1/8	1/4	3/8	1/2	5/8	3/4	7/8	2	2 1/4	2 1/2	2 3/4	3	3 1/2	4
6	28.8	33.2	37.8	42.8										
6 1/2	32.9	37.9	43.1	48.6										
7	37.4	42.9	48.7	54.8										
7 1/2	42.1	48.2	54.6	61.3										
8	47.1	53.8	60.9	68.3										
8 1/2	52.3	59.7	67.5	75.6										
9	57.9	66.0	74.4	83.3	92.4	102.0								
9 1/2	63.7	72.6	81.7	91.3	101.3	111.6								
10	69.9	79.4	89.4	99.8	110.5	121.7								
10 1/2	76.3	86.6	97.4	108.6	120.2	132.2								
12	97.1	110.1	123.4	137.3	151.5	166.3	181.6	197.3						
12 1/2	104.7	118.5	132.8	147.6	162.8	178.6	194.8	211.6						
14	128.9	145.7	163.0	180.8	199.1	217.9	237.4	257.3	299.0	342.9	389.2	438.0		
14 1/2	137.6	155.4	173.7	192.6	212.0	231.9	252.5	273.6	317.5	363.9	412.6	463.9		
15	146.5	165.4	184.8	204.8	225.3	246.4	268.1	290.3	336.7	385.4	436.7	490.5	606.1	732.7
16	165.2	186.3	208.0	230.3	253.1	276.6	300.6	325.3	376.6	430.4	486.9	546.0	672.6	810.7
16 1/2	175.0	197.2	220.1	243.6	267.6	292.3	317.6	343.6	397.4	453.9	513.0	574.9	707.1	851.2
18	206.0	231.9	258.5	285.8	313.6	342.2	371.4	401.3	463.2	527.9	595.5	666.0	816.1	978.7
18 1/2	216.9	244.1	272.0	300.6	329.8	359.7	390.3	421.6	486.3	553.9	624.4	697.9	854.1	1023.2
20	251.3	282.6	314.5	347.3	380.7	414.8	449.7	485.3	558.9	635.4	715.1	798.0	973.6	1162.7
20 1/2	263.3	296.0	329.4	363.6	398.4	434.1	470.4	507.6	584.2	663.9	746.7	832.9	1015.1	1211.2
21	275.6	309.7	344.6	380.3	416.6	453.8	491.7	530.3	610.0	692.9	779.1	868.5	1057.6	1260.7
22	301.0	338.2	376.1	414.8	454.2	494.4	535.5	577.3	663.5	752.9	845.7	942.0	1145.1	1362.7
22 1/2	314.2	352.9	392.3	432.6	473.6	515.4	558.1	601.6	691.0	783.9	880.1	979.9	1190.1	1415.2
24	355.3	398.8	443.1	488.3	534.2	581.1	628.8	677.3	771.7	880.4	987.4	1098.0	1330.6	1578.7
24 1/2	369.6	414.7	460.7	507.6	555.3	603.8	653.3	703.6	806.9	913.9	1024.5	1138.9	1379.1	1635.2
26	414.1	464.4	515.6	567.8	620.7	674.7	729.6	785.3	899.7	1017.9	1140.0	1266.0	1530.1	1810.7
26 1/2	429.5	481.6	534.6	588.6	643.4	699.2	755.9	813.6	931.8	1053.9	1180.0	1309.9	1582.1	1871.2
27	445.2	499.1	554.0	609.8	666.5	724.1	782.8	842.3	964.4	1090.4	1220.4	1354.5	1635.1	1932.7
28	477.4	535.1	593.7	653.3	713.8	775.3	837.8	901.3	1031.3	1165.4	1303.6	1446.0	1743.6	2058.7
28 1/2	493.9	553.5	614.0	675.6	738.1	801.6	866.1	931.6	1065.7	1203.9	1346.2	1492.9	1799.1	2123.2
30	545.2	610.7	677.2	744.8	813.3	882.9	953.6	1025.3	1172.0	1322.9	1478.2	1638.0	1971.1	2322.7
30 1/2	562.8	630.4	698.9	768.6	839.2	910.9	983.7	1057.6	1208.5	1363.9	1523.6	1687.9	2030.1	2391.2
32 1/2	636.2	712.2	789.4	867.6	946.9	1027.3	1108.9	1191.6	1360.4	1533.9	1712.0	1894.9	2275.1	2675.2
33	655.3	733.5	812.8	893.3	974.8	1057.5	1141.3	1226.3	1399.8	1577.7	1760.8	1948.5	2338.6	2748.7
34 1/2	744.1	799.1	885.3	972.6	1061.0	1150.7	1241.5	1333.6	1521.3	1713.9	1911.4	2113.9	2534.1	2975.2
36	775.5	867.6	960.8	1055.3	1150.9	1247.8	1346.0	1445.3	1647.8	1855.4	2068.1	2286.0	2737.6	3210.7
36 1/2	796.5	891.0	986.7	1083.6	1181.7	1281.1	1381.7	1483.6	1691.2	1903.9	2121.7	2344.9	2807.1	3291.2
38 1/2	883.4	987.9	1093.6	1200.6	1308.9	1418.4	1529.4	1641.6	1870.0	2103.9	2343.1	2587.9	3094.1	3623.2
40 1/2	974.8	1089.7	1206.0	1323.6	1442.5	1562.8	1684.5	1807.6	2057.9	2313.9	2575.5	2842.9	3395.1	3971.2
42 1/2	1070.8	1196.6	1323.9	1452.6	1582.7	1714.2	1847.2	1981.6	2254.8	2533.9	2818.9	3099.1	3710.1	4335.2
44 1/2	1171.2	1308.5	1447.3	1587.6	1729.3	1872.6	2017.3	2163.6	2460.7	2763.9	3073.2	3388.9	4039.1	4715.2
46 1/2	1276.1	1425.4	1576.2	1728.6	1882.5	2037.9	2195.0	2353.6	2679.5	3003.9	3338.6	3679.9	4382.1	5111.2
48 1/2	1385.5	1547.2	1710.6	1875.6	2042.1	2210.3	2380.1	2551.6	2898.4	3253.9	3615.0	3982.9	4739.1	5523.2
50 1/2	1499.4	1674.1	1850.5	2028.6	2208.3	2389.7	2572.8	2757.6	3132.3	3513.9	3902.4	4297.9	5110.1	5951.2
52 1/2	1617.8	1806.0	1995.9	2187.6	2380.9	2576.1	2772.9	2971.6	3374.2	3783.9	4200.7	4624.9	5495.1	6395.2
54 1/2	1740.7	1942.9	2146.8	2352.6	2560.1	2769.4	2980.6	3193.6	3625.0	4063.9	4510.1	4963.9	5894.1	6855.2
56 1/2	1868.1	2084.7	2303.2	2523.6	2745.8	2969.8	3195.8	3423.6	3884.9	4353.9	4830.5	5314.9	6307.1	7331.2
58 1/2	2000.0	2231.6	2465.1	2700.6	2937.9	3177.2	3418.4	3661.6	4153.8	4653.9	5161.9	5677.9	6734.1	7823.2
60 1/2	2136.4	2383.5	2632.5	2883.6	3136.6	3391.6	3648.6	3907.6	4431.7	4963.9	5504.2	6052.9	7175.1	8331.2
62 1/2	2277.3	2540.4	2805.4	3072.6	3341.7	3612.9	3886.2	4161.6	4718.5	5283.9	5857.6	6439.9	7630.1	8855.2
64 1/2	2422.7	2702.2	2983.9	3267.6	3553.4	3841.3	4131.4	4423.6	5014.4	5613.9	6222.0	6838.9	8099.1	9395.2
66 1/2	2572.6	2869.1	3167.8	3468.6	3771.5	4076.7	4384.0	4693.6	5319.3	5953.9	6597.4	7249.9	8582.1	9951.2
68 1/2	2727.0	3041.0	3357.2	3675.6	3996.2	4319.1	4644.2	4971.6	5633.2	6303.9	6983.7	7672.9	9079.1	10523.2
70 1/2	2885.9	3217.9	3552.1	3888.6	4227.4	4568.4	4911.9	5257.6	5956.0	6663.9	7381.1	8107.9	9590.1	11111.2
72 1/2	3049.3	3399.7	3752.5	4107.6	4465.0	4824.8	5187.0	5551.6	6287.9	7033.9	7789.5	8554.9	10115.1	11715.2
74 1/2	3217.3	3586.6	3958.4	4332.6	4709.2	5088.2	5469.7	5853.6	6628.8	7413.9	8208.9	9013.9	10654.1	12335.2
76 1/2	3389.7	3778.5	4169.8	4563.6	4959.8	5358.8	5759.8	6163.6	6978.7	7803.9	8639.2	9484.9	11207.1	12971.2
78 1/2	3566.6	3975.4	4386.8	4800.6	5217.0	5635.9	6057.5	6481.6	7337.5	8203.9	9080.6	9967.9	11774.1	13623.2
80 1/2	3748.0	4177.2	4609.1	5043.6	5480.6	5920.3	6362.6	6807.6	7705.4	8613.9	9533.0	10463.1	12355.1	14291.2
82 1/2	3933.9	4384.1	4837.0	5292.6	5750.8	6211.7	6675.3	7141.6	8082.3	9033.9	9996.4	10970.1	12950.1	14975.2
84 1/2	4124.3	4596.0	5070.4	5547.6	6027.4	6510.1	6995.4	7483.6	8468.2	9463.9	10471.1	11489.1	13559.1	15675.2
90 1/2	4722.5	5261.6	5803.6	6348.6	6896.4	7447.2	8000.9	8557.6	9679.9	10814.1	11960.1	13118.1	15470.1	17871.2
96 1/2	5361.2	5972.2	6586.4	7203.6	7823.9	8447.3	9073.9	9704.6	10972.1	12254.1	13548.1	14855.1	17507.1	20211.2
102 1/2	6040.4	6727.9	7418.6	8112.6	8809.9	9510.4	10214.1	10922.1	12346.1	13784.1	15235.1	16700.1	19670.1	22695.2
108 1/2	6760.2	7528.5	8300.3	9075.6	9854.3	10637.1	11422.1	12212.1	13801.1	15404.1	17021.1	18653.1	21959.1	25323.2
114 1/2	7520.4	8374.1	9231.5	10093.1	10957.1	11826.1	12698.1	13574.1	15346.1	17114.1	18906.1	20714.1	24374.1	28895.2
120 1/2	8321.1	9264.7	10212.1	11164.1	12119.1	13078.1	14041.1	15008.1	16953.1	18914.1	20890.1	22883.1	26915.1	31011.2



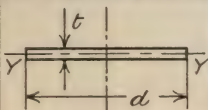
MOMENTS OF INERTIA OF ONE PLATE

MOMENT OF INERTIA OF ONE PLATE ABOUT AXIS X - X

Various depths and thicknesses
as used for Web Plates for built up Columns or Girders.

To obtain the Moment of Inertia for any thickness of Plate not listed below, multiply the Tabular Value given for the correct depth and one inch thick by the desired thickness.

d	Thickness in Inches														
Ins.	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1		
6	4.5	5.6	6.7	7.9	9.0	10.1	11.2	12.4	13.5	14.6	15.7	16.9	18.0		
7	7.1	8.9	10.7	12.5	14.3	16.1	17.9	19.7	21.4	23.2	25.0	26.8	28.6		
8	10.7	13.3	16.0	18.7	21.3	24.0	26.7	29.3	32.0	34.7	37.3	40.0	42.7		
9	15.2	19.0	22.8	26.6	30.4	34.2	38.0	41.8	45.6	49.4	53.2	57.0	60.7		
10	20.8	26.0	31.2	36.5	41.7	46.9	52.1	57.3	62.5	67.7	72.9	78.1	83.3		
12	36.0	45.0	54.0	63.0	72.0	81.0	90.0	99.0	108.0	117.0	126.0	135.0	144.0		
14	57.2	71.5	85.7	100.0	114.3	128.6	142.9	157.2	171.5	185.8	200.1	214.4	228.7		
16	85.3	106.7	128.0	149.3	170.7	192.0	213.3	234.7	256.0	277.3	298.7	320.0	341.3		
18	121.5	151.9	182.2	212.6	243.0	273.4	303.7	334.1	364.5	394.9	425.2	455.6	486.0		
20	166.7	208.3	250.0	291.7	333.3	375.0	416.7	458.3	500.0	541.7	583.3	625.0	666.7		
22	221.8	277.3	332.7	388.2	443.7	499.1	554.6	610.0	665.5	721.0	776.4	831.9	887.3		
24	288.0	360.0	432.0	504.0	576.0	648.0	720.0	792.0	864.0	936.0	1008.0	1080.0	1152.0		
26	366.2	457.7	549.2	640.8	732.3	823.9	915.4	1007.0	1098.5	1190.0	1281.6	1373.1	1464.7		
28	457.3	571.7	686.0	800.3	914.7	1029.0	1143.3	1257.7	1372.0	1486.3	1600.7	1715.0	1829.3		
30	562.5	703.1	843.7	984.4	1125.0	1265.6	1406.2	1546.9	1687.5	1828.1	1968.7	2109.4	2250.0		
32	682.7	853.3	1024.0	1194.7	1365.3	1536.0	1706.7	1877.3	2048.0	2218.7	2389.3	2560.0	2730.6		
34	818.8	1023.5	1228.2	1432.9	1637.7	1842.4	2047.1	2251.8	2456.5	2661.2	2865.9	3070.6	3275.3		
36	972.0	1215.0	1458.0	1701.0	1944.0	2187.0	2430.0	2673.0	2916.0	3159.0	3402.0	3645.0	3888.0		
38	1143.2	1429.0	1714.7	2000.5	2286.3	2572.1	2857.9	3143.7	3429.5	3715.3	4001.1	4286.9	4572.7		
40	1333.3	1666.7	2000.0	2333.3	2666.7	3000.0	3333.3	3666.7	4000.0	4333.3	4666.7	5000.0	5333.3		
42	1543.5	1929.4	2315.2	2701.1	3087.0	3472.9	3858.7	4244.6	4630.5	5016.4	5402.2	5788.1	6174.0		
44	1774.7	2218.3	2662.0	3105.7	3549.3	3993.0	4436.7	4880.3	5324.0	5767.7	6211.3	6655.0	7098.7		
46	2027.8	2534.8	3041.7	3548.7	4055.7	4562.6	5069.6	5576.5	6083.5	6590.5	7097.4	7604.4	8111.3		
48	2304.0	2880.0	3456.0	4032.0	4608.0	5184.0	5760.0	6336.0	6912.0	7488.0	8064.0	8640.0	9216.0		
50	2604.2	3255.2	3906.2	4557.3	5208.3	5859.4	6510.4	7161.5	7812.5	8463.5	9114.6	9765.6	10417		
52	2929.3	3661.7	4394.0	5126.3	5858.7	6591.0	7323.3	8055.7	8788.0	9520.3	10253	10985	11717		
54	3280.4	4100.6	4920.7	5740.9	6561.0	7381.1	8201.2	9021.4	9841.5	10662	11482	12302	13122		
56	3658.7	4573.3	5488.0	6402.7	7317.3	8232.0	9146.7	10061	10976	11891	12805	13720	14635		
58	4064.8	5081.0	6097.2	7113.5	8129.7	9145.9	10162	11178	12194	13211	14227	15243	16259		
60	4500.0	5625.0	6750.0	7875.0	9000.0	10125	11250	12375	13500	14625	15750	16875	18000		
62	4965.2	6206.5	7447.7	8689.0	9930.3	11172	12413	13654	14895	16137	17378	18619	19861		
64	5461.3	6826.7	8192.0	9557.3	10923	12288	13653	15019	16384	17749	19115	20480	21845		
66	5989.5	7486.9	8984.2	10482	11979	13476	14974	16471	17968	19466	20963	22461	23958		
68	6550.7	8188.3	9826.0	11464	13101	14739	16377	18014	19652	21290	22927	24565	26203		
70	7145.8	8932.3	10719	12505	14291	16078	17865	19651	21437	23224	25010	26797	28583		
72	7776.0	9720.0	11664	13608	15552	17496	19440	21384	23328	25272	27216	29160	31104		
74	8442.2	10553	12663	14774	16884	18995	21105	23216	25326	27437	29548	31658	33769		
76	9145.3	11432	13718	16004	18291	20577	22863	25150	27436	29722	32009	34295	36581		
78	9886.5	12358	14830	17301	19773	22245	24716	27188	29659	32131	34603	37074	39546		
80	10667	13333	16000	18667	21333	24000	26667	29333	32000	34667	37333	40000	42667		
82	11487	14359	17230	20102	22974	25845	28717	31589	34460	37332	40204	43076	45947		
84	12348	15435	18522	21609	24696	27783	30870	33957	37044	40131	43218	46305	49392		
86	15187	18984	22781	26578	30375	34172	37969	41766	45562	49359	53156	56953	60750		
96	18432	23040	27648	32256	36864	41472	46080	50688	55296	59904	64512	69120	73728		
102	22108	27636	33163	38690	44217	49744	55271	60798	66325	71853	77380	82907	88434		
108	26244	32805	39366	45927	52488	59049	65610	72171	78732	85293	91854	98415	104976		
114	30865	38582	46298	54015	61731	69447	77164	84880	92596	100313	108029	115746	123462		
120	36000	45000	54000	63000	72000	81000	90000	99000	108000	117000	126000	135000	144000		

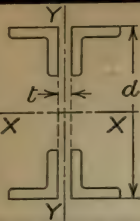


MOMENT OF INERTIA OF ONE PLATE ONE INCH DEEP ABOUT AXIS Y - Y

Various thicknesses as used for Web Plates for built up Columns and Girders.

To obtain the Moment of Inertia of any depth of Plate multiply the Tabular Value given for the correct thickness by the depth desired.

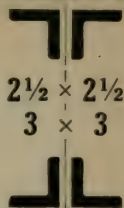
d Ins.	Thickness in Inches. t''												
	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{13}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1"
1	.00130	.00254	.00439	.00698	.01041	.01483	.02034	.02708	.03516	.04469	.05583	.06866	.08333

**MOMENTS OF INERTIA OF FOUR ANGLES****EQUAL LEG ANGLES**

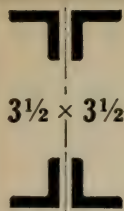
AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		2 1/2" x 2 1/2"				
Thickness		1/8	3/16	1/4	5/16	3/8
4	Area	2.44	3.60	4.76	5.88	6.92
L's	Weight	8.32	12.28	16.4	20.0	23.6
d"		I Axis X - X				
6 1/2		18	26	33	40	47
7 1/2		25	36	46	57	66
8 1/2		33	48	62	76	88
9 1/2		42	62	80	98	114
10 1/2		53	77	100	123	143
12 1/2		77	113	148	182	216
14 1/2		107	157	206	253	295
16 1/2		142	208	273	335	392
18 1/2		181	266	349	429	503
20 1/2		225	331	435	535	627
22 1/2		275	404	531	653	765
24 1/2		329	483	636	782	917
t"		I Axis Y - Y				
0"		2.6	3.9	5.3	6.6	7.9
1/4		3.1	4.6	6.2	7.8	9.3
5/16		3.2	4.8	6.5	8.1	9.7
3/8		3.3	5.0	6.7	8.5	10.1
7/16		3.4	5.2	7.0	8.8	10.5
1/2		3.6	5.4	7.3	9.2	11.0
9/16		3.7	5.6	7.6	9.5	11.4
5/8		3.9	5.8	7.9	9.9	11.9
3/4		4.2	6.3	8.5	10.7	12.8
Size		3" x 3"				
Thickness		1/4	5/16	3/8	7/16	1/2
4	Area	5.76	7.12	8.44	9.72	11.00
L's	Weight	19.6	24.4	28.8	33.2	37.6
d"		I Axis X - X				
6 1/2		38	46	54	61	68
7 1/2		54	65	76	86	96
8 1/2		72	87	102	116	130
9 1/2		93	113	134	151	169
10 1/2		117	143	167	191	214
12 1/2		174	212	250	285	320
14 1/2		242	296	348	399	448
16 1/2		321	394	464	532	598
18 1/2		412	506	597	684	770
20 1/2		515	632	746	856	964
22 1/2		629	773	913	1047	1180
24 1/2		755	928	1096	1258	1418
t"		I Axis Y - Y				
0"		9.0	11.4	13.7	16.0	18.4
1/4		10.3	13.1	15.7	18.4	21.1
5/16		10.7	13.5	16.3	19.0	21.9
3/8		11.0	14.0	16.8	19.7	22.6
7/16		11.4	14.5	17.4	20.3	23.4
1/2		11.8	15.0	18.0	21.0	24.2
9/16		12.2	15.5	18.6	21.8	25.0
5/8		12.6	16.0	19.2	22.5	25.9
3/4		13.5	17.1	20.6	24.0	27.6



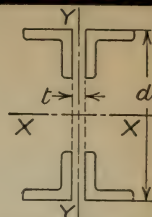
MOMENTS OF INERTIA OF FOUR ANGLES

EQUAL LEG ANGLES

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



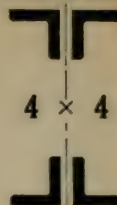
Size		3 1/2" x 3 1/2"					
Thickness		5/16	3/8	7/16	1/2	9/16	5/8
4	Area	8.36	9.92	11.48	13.00	14.48	15.92
L's	Weight	28.8	34.0	39.2	44.4	49.6	54.4
d"	I Axis X - X						
7 1/2	73	86	97	109	119	129	
8 1/2	99	116	131	147	161	175	
9 1/2	128	150	171	192	211	229	
10 1/2	162	190	217	243	267	291	
12 1/2	241	284	325	365	403	440	
14 1/2	337	398	456	513	567	619	
16 1/2	450	532	609	687	760	831	
18 1/2	580	685	787	887	982	1075	
20 1/2	727	858	987	1112	1234	1350	
22 1/2	890	1052	1210	1364	1514	1657	
24 1/2	1070	1265	1456	1642	1823	1997	
26 1/2	1266	1498	1725	1946	2161	2367	
28 1/2	1480	1750	2016	2276	2528	2770	
30 1/2	1710	2023	2331	2632	2923	3205	
32 1/2	1957	2315	2669	3014	3348	3671	
34 1/2	2220	2628	3030	3422	3802	4170	
36 1/2	2500	2960	3413	3856	4285	4700	
38 1/2	2798	3312	3820	4316	4797	5262	
40 1/2	3111	3684	4249	4802	5337	5856	
42 1/2	3441	4075	4702	5314	5907	6481	
44 1/2	3788	4487	5177	5852	6505	7139	
46 1/2	4152	4918	5776	6416	7133	7828	
48 1/2	4533	5369	6197	7006	7790	8549	
50 1/2	4930	5840	6742	7622	8475	9302	
52 1/2	5344	6331	7309	8264	9189	10087	
54 1/2	5775	6842	7899	8931	9933	10904	
56 1/2	6222	7372	8513	9625	10705	11752	
58 1/2	6686	7923	9149	10345	11507	12633	
60 1/2	7167	8494	9808	11091	12338	13546	
t"	I Axis Y - Y						
0"	18.0	21.8	25.4	29.2	32.8	36.5	
1/4	20.2	24.3	28.6	32.8	37.0	41.2	
5/16	20.8	25.0	29.5	33.7	38.1	42.5	
3/8	21.4	25.7	30.3	34.7	39.2	43.7	
7/16	22.0	26.5	31.2	35.8	40.4	45.0	
1/2	22.7	27.2	32.1	36.8	41.6	46.3	
9/16	23.3	28.0	33.1	37.9	42.8	47.7	
5/8	24.0	28.8	34.0	39.0	44.1	49.1	
3/4	25.4	30.5	36.0	41.3	46.7	52.0	

MOMENTS OF INERTIA OF FOUR ANGLES **EQUAL LEG ANGLES**

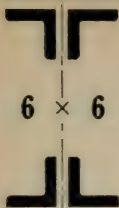
AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size	4" x 4"							
Thickness	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4 Area	9.60	11.44	13.24	15.00	16.72	18.44	20.12	21.76
L's Weight	32.8	39.2	45.2	51.2	57.2	62.8	68.4	74.0
d"	I Axis X - X							
8 1/2	109	128	146	164	179	195	210	224
9 1/2	141	166	191	213	234	255	275	294
10 1/2	179	211	241	271	297	325	351	375
12 1/2	267	316	363	408	449	491	532	570
14 1/2	376	444	511	575	634	695	753	809
16 1/2	503	596	685	772	853	935	1015	1091
18 1/2	649	770	886	999	1105	1213	1316	1416
20 1/2	815	967	1114	1256	1391	1527	1658	1785
22 1/2	1000	1187	1369	1543	1710	1879	2041	2198
24 1/2	1204	1430	1648	1860	2062	2267	2463	2656
26 1/2	1427	1695	1955	2208	2448	2692	2926	3155
28 1/2	1670	1984	2289	2585	2868	3154	3429	3697
30 1/2	1932	2295	2648	2992	3320	3652	3972	4283
32 1/2	2212	2629	3035	3429	3807	4188	4556	4914
34 1/2	2513	2986	3448	3896	4326	4760	5179	5587
36 1/2	2832	3367	3887	4393	4879	5369	5843	6304
38 1/2	3170	3769	4353	4920	5466	6016	6548	7065
40 1/2	3528	4195	4845	5477	6086	6699	7292	7869
42 1/2	3905	4644	5364	6064	6739	7478	8077	8717
44 1/2	4301	5115	5909	6681	7426	8175	8902	9609
46 1/2	4716	5610	6481	7329	8146	8969	9767	10543
48 1/2	5150	6127	7079	8006	8900	9799	10672	11522
50 1/2	5605	6667	7703	8713	9687	10667	11618	12544
52 1/2	6077	7231	8355	9450	10508	11571	12604	13609
54 1/2	6569	7816	9032	10217	11362	12512	13630	14718
56 1/2	7081	8425	9736	11014	12250	13490	14696	15870
58 1/2	7611	9057	10467	11841	13170	14505	15803	17066
60 1/2	8161	9712	11224	12698	14125	15557	16950	18306
62 1/2	8730	10389	12007	13585	15113	16646	18137	19589
64 1/2	9318	11089	12817	14502	16134	17771	19364	20915
t"	I Axis Y - Y							
0"	26.9	32.3	37.7	43.1	49.0	54.5	60.1	65.7
1/4	29.7	35.8	41.7	47.8	54.3	60.5	66.7	73.0
5/16	30.5	36.7	42.8	49.0	55.7	62.1	68.5	74.9
3/8	31.3	37.6	43.9	50.3	57.1	63.7	70.2	76.9
7/16	32.1	38.6	45.1	51.6	58.6	65.3	72.1	78.9
1/2	32.9	39.5	46.2	52.9	60.1	67.0	74.0	80.9
9/16	33.7	40.5	47.4	54.3	61.6	68.7	75.9	83.0
5/8	34.5	41.6	48.6	55.7	63.2	70.5	77.8	85.1
3/4	36.3	43.7	51.1	58.5	66.5	74.1	81.8	89.5



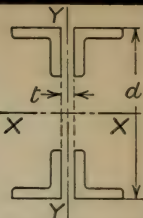
MOMENTS OF INERTIA OF FOUR ANGLES

EQUAL LEG ANGLES

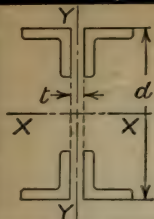
AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		6" X 6"										
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"
4	Area	17.44	20.24	23.00	25.72	28.44	31.12	33.76	36.36	38.92	41.48	44.00
L's	Weight	59.6	68.8	78.4	87.6	96.8	106.0	114.8	124.0	132.4	141.2	149.6
d"		I Axis X - X										
12	1/2	432	497	560	618	678	735	787	840	891	942	990
14	1/2	610	703	793	878	963	1046	1123	1200	1275	1349	1421
16	1/2	824	950	1072	1188	1306	1420	1526	1633	1737	1839	1938
18	1/2	1072	1237	1398	1551	1705	1855	1996	2138	2276	2412	2545
20	1/2	1354	1564	1769	1964	2161	2353	2535	2716	2894	3069	3239
22	1/2	1672	1932	2186	2429	2674	2913	3140	3367	3589	3808	4021
24	1/2	2025	2341	2649	2946	3244	3536	3813	4091	4362	4630	4892
26	1/2	2412	2790	3159	3513	3871	4220	4554	4887	5212	5535	5850
28	1/2	2835	3279	3714	4133	4555	4967	5362	5756	6141	6523	6896
30	1/2	3292	3809	4315	4804	5295	5776	6238	6698	7147	7594	8031
32	1/2	3784	4379	4962	5526	6093	6648	7181	7712	8232	8748	9253
34	1/2	4311	4990	5655	6299	6947	7581	8192	8799	9394	9985	10563
36	1/2	4873	5641	6395	7125	7858	8577	9270	9959	10634	11305	11962
38	1/2	5470	6333	7180	8001	8826	9635	10416	11192	11952	12708	13448
40	1/2	6102	7065	8011	8929	9851	10756	11629	12497	13347	14194	15022
42	1/2	6768	7838	8888	9909	10933	11938	12910	13875	14821	15762	16688
44	1/2	7470	8651	9812	10939	12072	13183	14259	15326	16372	17414	18435
46	1/2	8206	9505	10781	12022	13268	14490	15675	16850	18001	19149	20273
48	1/2	8977	10399	11796	13155	14520	15859	17158	18446	19709	20966	22200
50	1/2	9783	11334	12857	14341	15829	17291	18709	20115	21493	22867	24214
52	1/2	10624	12309	13964	15577	17196	18785	20327	21856	23356	24850	26316
54	1/2	11500	13325	15118	16865	18619	20341	22013	23671	25297	26917	28507
56	1/2	12411	14381	16317	18205	20099	21959	23767	25558	27315	29066	30785
58	1/2	13356	15478	17562	19596	21636	23639	25588	27518	29411	31299	33151
60	1/2	14337	16615	18853	21038	23230	25382	27476	29550	31585	33614	35605
62	1/2	15352	17792	20191	22532	24880	27187	29432	31655	33837	36013	38148
64	1/2	16402	19010	21574	24077	26588	29054	31456	33833	36167	38494	40778
66	1/2	17488	20269	23003	25673	28352	30984	33547	36084	38575	41058	43496
68	1/2	18608	21568	24478	27322	30173	32975	35706	38407	41060	43706	46303
70	1/2	19762	22907	25999	29022	32052	35029	37932	40803	43623	46436	49197
72	1/2	20952	24287	27567	30773	33987	37145	40225	43272	46264	49249	52179
74	1/2	22177	25708	29180	32575	35979	39324	42587	45814	48983	52145	55250
76	1/2	23436	27169	30839	34429	38027	41564	45015	48428	51780	55124	58408
78	1/2	24731	28670	32544	36334	40133	43867	47512	51115	54655	58186	61654
80	1/2	26060	30212	34295	38291	42296	46232	50075	53875	57607	61331	64989
82	1/2	27424	31794	36093	40299	44515	48660	52707	56707	60638	64559	68411
84	1/2	28823	33417	37936	42359	46792	51149	55405	59612	63746	67870	71921
90	1/2	33230	38528	43742	48847	53962	58992	63907	68764	73537	78301	82980
96	1/2	37950	44004	49961	55797	61644	67394	73016	78571	84029	89478	94831
102	1/2	42984	49844	56595	63211	69838	76357	82733	89031	95222	101401	107474
108	1/2	48332	56049	63643	71088	78544	85879	93057	100147	107116	114072	120909
114	1/2	53994	62617	71104	79427	87762	95962	103989	111916	119709	127490	135136
t"		I Axis Y - Y										
0"		108.5	126.5	144.6	163.5	181.8	200.1	219.6	238.0	256.6	275.3	294.0
3/8		119.8	139.8	159.8	180.9	201.2	221.6	243.3	263.9	284.6	305.4	326.3
7/16		121.8	142.2	162.5	184.0	204.6	225.4	247.5	268.4	289.5	310.7	332.0
1/2		123.9	144.6	165.3	187.1	208.1	229.2	251.7	273.0	294.4	316.1	337.7
5/8		128.1	149.5	171.0	193.5	215.3	237.1	260.4	282.5	304.8	327.1	349.5
3/4		132.4	154.5	176.8	200.1	222.7	245.3	269.4	292.2	315.2	338.4	361.6
7/8		136.8	159.8	182.8	206.9	230.3	253.7	278.6	302.3	326.1	350.0	374.1
1"		141.4	165.2	188.9	213.9	238.1	262.3	288.1	312.6	337.2	362.0	386.9
1 1/8		146.2	170.7	195.3	221.1	246.1	271.2	297.9	323.2	348.7	374.3	400.0
1 1/4		151.0	176.5	201.8	228.5	254.4	280.3	307.9	334.1	360.3	387.0	413.5
1 1/2		161.2	188.3	215.5	243.9	271.6	299.3	328.7	356.7	384.7	413.1	441.6



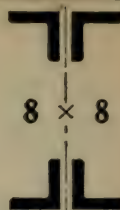
MOMENTS OF INERTIA OF FOUR ANGLES

EQUAL LEG ANGLES

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		8" x 8"										
Thickness		1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"	1 1/16	1 1/8
4	Area	31.00	34.72	38.44	42.12	45.76	49.36	52.92	56.48	60.00	63.48	66.92
L's	Weight	105.6	118.4	130.8	143.2	155.6	168.0	180.0	192.4	204.0	216.0	227.6
d"		I Axis X - X										
16	1/2	1333	1483	1631	1775	1910	2046	2179	2310	2430	2554	2674
18	1/2	1740	1937	2132	2322	2502	2683	2860	3034	3196	3361	3523
20	1/2	2208	2461	2710	2954	3186	3419	3646	3871	4082	4296	4505
22	1/2	2739	3054	3365	3670	3961	4253	4538	4821	5087	5357	5621
24	1/2	3332	3716	4097	4471	4828	5186	5536	5884	6213	6646	6871
26	1/2	3987	4448	4906	5355	5786	6217	6640	7060	7458	7861	8255
28	1/2	4703	5249	5792	6324	6835	7348	7850	8349	8824	9303	9773
30	1/2	5482	6120	6754	7377	7977	8577	9166	9751	10310	10872	11425
32	1/2	6323	7060	7794	8514	9209	9904	10587	11266	11915	12569	13210
34	1/2	7225	8070	8910	9736	10534	11331	12114	12893	13641	14392	15129
36	1/2	8190	9149	10103	11041	11950	12856	13748	14634	15486	16342	17183
38	1/2	9217	10298	11373	12431	13457	14480	15487	16488	17452	18419	19369
40	1/2	10306	11516	12720	13905	15056	16203	17331	18454	19538	20623	21690
42	1/2	11456	12803	14144	15464	16746	18024	19282	20534	21743	22954	24145
44	1/2	12669	14160	15645	17107	18528	19944	21338	22726	24069	25412	26733
46	1/2	13944	15586	17222	18833	20401	21963	23501	25032	26514	27997	29456
48	1/2	15280	17082	18877	20645	22366	24081	25769	27450	29080	30709	32312
50	1/2	16679	18647	20608	22540	24423	26291	28143	29982	31766	33548	35302
52	1/2	18140	20282	22416	24520	26571	28612	30623	32626	34571	36513	38426
54	1/2	19663	21986	24301	26584	28810	31026	33208	35384	37497	39606	41684
56	1/2	21247	23759	26263	28732	31141	33538	35900	38254	40542	42826	45075
58	1/2	22894	25602	28302	30964	33564	36149	38697	41237	43708	46172	48601
60	1/2	24603	27515	30418	33281	36078	38859	41600	44333	46994	49646	52260
62	1/2	26376	29497	32610	35681	38683	41668	44609	47543	50399	53247	56053
64	1/2	28206	31548	34880	38167	41381	44575	47724	50865	53925	56974	59980
66	1/2	30101	33669	37226	40736	44169	47581	50945	54300	57570	60829	64040
68	1/2	32058	35859	39650	43389	47049	50686	54272	57848	61336	64810	68235
70	1/2	34076	38118	42150	46127	50021	53889	57704	61509	65222	68919	72563
72	1/2	36157	40447	44727	48949	53084	57191	61242	65283	69227	73154	77025
74	1/2	38300	42846	47381	51856	56239	60592	64886	69170	73353	77516	81621
76	1/2	40505	45314	50111	54846	59485	64092	68636	73170	77598	82006	86351
78	1/2	42771	47851	52919	57921	62823	67690	72492	77283	81964	86622	91215
80	1/2	45100	50458	55804	61080	66252	71387	76453	81509	86450	91365	96213
82	1/2	47491	53134	58765	64323	69773	75183	80521	85847	91055	96235	101344
84	1/2	49943	55880	61803	67651	73385	79077	84694	90299	95781	101233	106609
90	1/2	57674	64533	71380	78139	84771	91353	97849	104332	110678	116986	123208
96	1/2	65962	73812	81648	89385	96981	104518	111956	119382	126654	133882	141011
102	1/2	74808	83715	92608	101389	110014	118570	127016	135448	143711	151920	160019
108	1/2	84212	94244	104260	114151	123871	133512	143029	152531	161848	171101	180232
114	1/2	94174	105397	116603	127672	138552	149341	159994	170630	181065	191425	201649
120	1/2	104694	117176	129639	141950	154056	166060	177912	189747	201362	212891	224270
t"		I Axis Y - Y										
0"		343.2	385.9	428.8	471.8	516.8	560.1	603.2	646.6	692.9	736.7	780.8
3/8		369.8	415.9	462.4	508.8	557.6	604.1	651.1	699.4	748.4	795.5	843.4
7/16		374.4	421.2	468.2	515.3	564.7	611.8	659.4	708.4	758.0	805.8	854.3
1/2		379.1	426.5	474.1	521.8	571.9	619.7	667.9	717.5	767.8	816.2	865.4
5/8		388.7	437.3	486.2	535.1	586.5	635.6	685.1	736.1	787.7	837.4	887.9
3/4		398.5	448.4	498.5	548.8	601.6	651.9	702.7	755.0	808.0	859.1	910.9
7/8		408.5	459.7	511.2	562.7	616.9	668.6	720.8	774.5	828.8	881.3	934.5
1"		418.9	471.3	524.2	577.0	632.6	685.7	739.2	794.3	850.1	904.0	958.5
1 1/8		429.4	483.2	537.4	591.7	648.7	703.3	758.1	813.2	871.8	927.5	983.1
1 1/4		440.2	495.4	551.0	606.6	665.1	721.2	777.3	833.9	894.1	951.2	1008.3
1 1/2		462.6	520.6	579.1	637.6	699.1	758.1	817.1	876.6	940.0	1000.0	1060.1



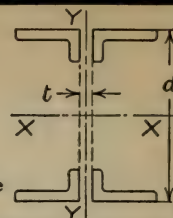
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

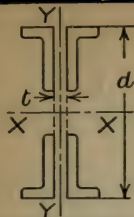
AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



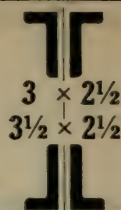
Size		$3 \times 2\frac{1}{2}$			
Thickness		$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$
4	Area	5.24	6.48	7.68	8.88
L's	Weight	18.0	22.4	26.4	30.4
d"		I Axis X - X			
6 $\frac{1}{2}$		38	47	55	62
7 $\frac{1}{2}$		53	65	75	86
8 $\frac{1}{2}$		71	86	100	115
9 $\frac{1}{2}$		91	111	129	148
10 $\frac{1}{2}$		113	139	162	186
12 $\frac{1}{2}$		167	205	240	275
14 $\frac{1}{2}$		231	283	333	382
16 $\frac{1}{2}$		305	375	441	507
18 $\frac{1}{2}$		390	480	564	649
20 $\frac{1}{2}$		485	597	703	810
22 $\frac{1}{2}$		591	728	857	987
24 $\frac{1}{2}$		707	871	1027	1183
t"		I Axis Y - Y			
0"		9.0	11.2	13.8	16.0
$\frac{1}{4}$		10.3	12.9	15.7	18.4
$\frac{5}{16}$		10.6	13.3	16.2	19.0
$\frac{3}{8}$		11.0	13.8	16.8	19.6
$\frac{7}{16}$		11.4	14.2	17.3	20.3
$\frac{1}{2}$		11.7	14.7	17.9	21.0
$\frac{9}{16}$		12.1	15.2	18.5	21.6
$\frac{5}{8}$		12.5	15.7	19.1	22.4
$\frac{3}{4}$		13.3	16.7	20.3	23.8
Size		$3\frac{1}{2} \times 2\frac{1}{2}$			
Thickness		$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$	$\frac{7}{16}$
4	Area	5.76	7.12	8.44	9.72
L's	Weight	19.6	24.4	28.8	33.2
d"		I Axis X - X			
6 $\frac{1}{2}$		44	53	62	70
7 $\frac{1}{2}$		60	73	85	97
8 $\frac{1}{2}$		79	97	113	129
9 $\frac{1}{2}$		102	124	146	166
10 $\frac{1}{2}$		127	155	182	208
12 $\frac{1}{2}$		186	228	268	306
14 $\frac{1}{2}$		257	315	371	424
16 $\frac{1}{2}$		339	416	491	562
18 $\frac{1}{2}$		433	532	627	719
20 $\frac{1}{2}$		538	661	781	895
22 $\frac{1}{2}$		655	805	951	1091
24 $\frac{1}{2}$		784	963	1138	1306
t"		I Axis Y - Y			
0"		14.3	18.1	21.4	25.1
$\frac{1}{4}$		16.0	20.2	24.2	28.2
$\frac{5}{16}$		16.4	20.7	24.9	29.0
$\frac{3}{8}$		16.9	21.3	25.6	29.8
$\frac{7}{16}$		17.4	21.9	26.3	30.7
$\frac{1}{2}$		17.9	22.5	27.0	31.5
$\frac{9}{16}$		18.3	23.1	27.8	32.4
$\frac{5}{8}$		18.9	23.8	28.5	33.3
$\frac{3}{4}$		19.9	25.1	30.1	35.1

**MOMENTS OF INERTIA OF FOUR ANGLES****UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK**

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		3 × 2½				
Thickness		¼	⅝	¾	7/16	
4	Area	5.24	6.48	7.68	8.88	
L's	Weight	18.0	22.4	26.4	30.4	
d''		I Axis X - X				
6 ½	33	41	47	53		
7 ½	47	57	66	76		
8 ½	63	77	90	102		
9 ½	82	100	117	134		
10 ½	104	127	148	169		
12 ½	154	189	222	254		
14 ½	215	266	310	357		
16 ½	287	353	415	477		
18 ½	369	454	534	615		
20 ½	462	569	669	771		
22 ½	565	696	820	944		
24 ½	679	836	986	1135		
t''		I Axis Y - Y				
0"	5.2	6.6	8.0	9.5		
¼	6.2	7.8	9.5	11.2		
⅝	6.5	8.1	9.9	11.7		
¾	6.7	8.5	10.3	12.2		
7/16	7.0	8.8	10.8	12.7		
½	7.3	9.2	11.2	13.2		
9/16	7.6	9.6	11.7	13.8		
⅝	7.9	10.0	12.2	14.4		
¾	8.6	10.8	13.2	15.6		
Size		3½ × 2½				
Thickness		¼	⅝	¾	7/16	½
4	Area	5.76	7.12	8.44	9.72	11.00
L's	Weight	19.6	24.4	28.8	33.2	37.6
d''		I Axis X - X				
7 ½	47	57	67	76	84	
8 ½	64	78	91	103	115	
9 ½	84	101	119	136	152	
10 ½	106	129	151	173	193	
12 ½	159	195	229	261	293	
14 ½	224	275	323	370	415	
16 ½	301	369	434	497	560	
18 ½	389	477	563	645	726	
20 ½	488	600	708	811	914	
22 ½	599	737	870	997	1124	
24 ½	722	888	1048	1203	1356	
t''		I Axis Y - Y				
0"	5.2	6.6	8.0	9.4	10.8	
¼	6.2	7.9	9.6	11.2	12.9	
⅝	6.5	8.3	10.0	11.7	13.5	
¾	6.8	8.6	10.4	12.2	14.1	
7/16	7.1	9.0	10.9	12.8	14.7	
½	7.4	9.4	11.3	13.3	15.4	
9/16	7.7	9.8	11.8	13.9	16.0	
⅝	8.0	10.2	12.3	14.5	16.7	
¾	8.7	11.0	13.4	15.7	18.2	

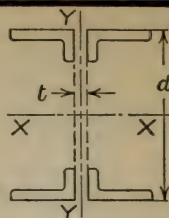
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

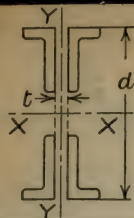
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



4 × 3

Size		4" × 3"					
Thickness		5/16	3/8	7/16	1/2	9/16	5/8
4	Area	8.36	9.92	11.48	13.00	14.48	15.92
L's	Weight	28.8	34.0	39.2	44.4	49.6	54.4
d"		I Axis X - X					
6 1/2	58	68	78	86	94	102	
7 1/2	81	95	109	121	132	144	
8 1/2	108	127	145	162	178	193	
9 1/2	140	164	188	209	231	251	
10 1/2	175	206	236	264	291	317	
12 1/2	259	305	350	392	433	472	
14 1/2	359	423	486	546	604	659	
16 1/2	476	561	646	725	804	879	
18 1/2	609	719	828	931	1032	1129	
20 1/2	760	897	1034	1163	1290	1412	
22 1/2	927	1095	1262	1421	1577	1727	
24 1/2	1110	1313	1514	1705	1892	2073	
26 1/2	1311	1550	1788	2015	2237	2451	
28 1/2	1528	1808	2085	2351	2611	2862	
30 1/2	1762	2085	2406	2713	3013	3303	
32 1/2	2012	2382	2749	3101	3445	3777	
34 1/2	2280	2699	3115	3515	3905	4283	
36 1/2	2564	3035	3504	3955	4395	4820	
38 1/2	2865	3392	3917	4421	4913	5390	
40 1/2	3182	3768	4352	4912	5460	5991	
42 1/2	3516	4164	4810	5430	6037	6624	
44 1/2	3867	4580	5291	5974	6642	7289	
46 1/2	4235	5016	5795	6544	7276	7986	
48 1/2	4619	5472	6322	7140	7939	8714	
50 1/2	5021	5948	6871	7762	8631	9475	
52 1/2	5438	6443	7444	8410	9353	10266	
54 1/2	5873	6958	8040	9084	10103	11090	
56 1/2	6324	7493	8659	9784	10882	11946	
58 1/2	6792	8048	9301	10510	11690	12834	
t"		I Axis Y - Y					
0"	26.8	32.1	37.5	43.2	48.6	54.0	
1/4	29.6	35.4	41.4	47.7	53.7	59.7	
5/16	30.3	36.3	42.4	48.9	55.1	61.2	
3/8	31.0	37.2	43.5	50.1	56.4	62.7	
7/16	31.8	38.2	44.6	51.4	57.8	64.3	
1/2	32.6	39.1	45.7	52.7	59.3	65.9	
9/16	33.4	40.1	46.8	53.9	60.7	67.5	
5/8	34.2	41.0	47.9	55.3	62.2	69.2	
3/4	35.9	43.0	50.3	58.0	65.3	72.6	



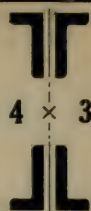
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		4" x 3"					
Thickness		5/16	3/8	7/16	1/2	9/16	5/8
4	Area	8.36	9.92	11.48	13.00	14.48	15.92
L's	Weight	28.8	34.0	39.2	44.4	49.6	54.4
d"		I Axis X - X					
8 1/2		88	103	118	131	144	156
9 1/2		115	135	155	172	190	206
10 1/2		147	172	197	220	242	264
12 1/2		222	261	299	335	370	403
14 1/2		313	369	424	476	526	575
16 1/2		422	498	573	643	712	778
18 1/2		547	646	744	836	926	1013
20 1/2		689	814	938	1055	1169	1279
22 1/2		848	1002	1155	1299	1441	1578
24 1/2		1023	1210	1395	1570	1743	1909
26 1/2		1215	1437	1657	1867	2073	2271
28 1/2		1424	1685	1943	2190	2432	2665
30 1/2		1650	1952	2252	2539	2820	3091
32 1/2		1892	2239	2584	2914	3237	3549
34 1/2		2151	2546	2939	3315	3683	4039
36 1/2		2427	2873	3316	3742	4158	4560
38 1/2		2719	3219	3717	4195	4662	5114
40 1/2		3028	3586	4141	4674	5195	5699
42 1/2		3354	3972	4587	5179	5756	6316
44 1/2		3697	4378	5057	5710	6347	6965
46 1/2		4056	4804	5549	6267	6967	7646
48 1/2		4432	5250	6065	6849	7616	8358
50 1/2		4825	5715	6603	7458	8293	9103
52 1/2		5234	6201	7164	8093	9000	9879
54 1/2		5661	6706	7749	8754	9736	10687
56 1/2		6103	7231	8356	9441	10500	11527
58 1/2		6563	7776	8986	10154	11294	12399
60 1/2		7039	8341	9639	10893	12116	13302
62 1/2		7533	8926	10316	11658	12967	14238
t"		I Axis Y - Y					
0"		11.4	13.7	16.1	18.6	21.1	23.5
1/4		13.1	15.8	18.5	21.5	24.4	27.2
5/16		13.6	16.4	19.2	22.3	25.3	28.2
3/8		14.1	17.0	19.9	23.1	26.2	29.3
7/16		14.6	17.6	20.6	24.0	27.2	30.4
1/2		15.1	18.2	21.4	24.8	28.2	31.5
9/16		15.7	18.9	22.1	25.7	29.2	32.6
5/8		16.2	19.5	22.9	26.7	30.2	33.7
3/4		17.4	20.9	24.6	28.6	32.4	36.2

MOMENTS OF INERTIA OF FOUR ANGLES

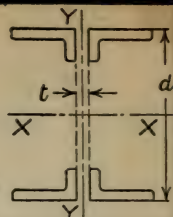
UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

 $4 \times 3\frac{1}{2}$

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		4" × 3 1/2"							
Thickness		5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4	Area	9.00	10.68	12.36	14.00	15.60	17.20	18.72	20.24
L's	Weight	30.8	36.4	42.4	47.6	53.2	58.8	64.0	69.2
d"		I Axis X - X							
7 1/2		82	95	108	121	133	144	154	164
8 1/2		109	128	146	163	179	195	209	223
9 1/2		142	165	189	212	234	255	273	292
10 1/2		178	209	239	268	296	323	347	371
12 1/2		265	311	357	401	443	485	522	560
14 1/2		370	435	500	562	622	681	734	789
16 1/2		492	580	667	751	832	912	985	1058
18 1/2		633	746	859	968	1073	1177	1272	1368
20 1/2		792	934	1076	1213	1346	1477	1597	1719
22 1/2		969	1143	1317	1486	1649	1811	1959	2110
24 1/2		1163	1373	1583	1787	1984	2179	2359	2542
26 1/2		1376	1625	1874	2116	2350	2582	2797	3014
28 1/2		1607	1898	2190	2473	2747	3019	3271	3526
30 1/2		1856	2193	2531	2858	3176	3491	3784	4079
32 1/2		2123	2509	2896	3271	3635	3997	4333	4672
34 1/2		2407	2846	3285	3712	4126	4538	4920	5306
36 1/2		2710	3205	3700	4181	4648	5112	5545	5981
38 1/2		3031	3585	4139	4678	5201	5722	6207	6696
40 1/2		3370	3986	4603	5203	5785	6365	6906	7451
42 1/2		3726	4409	5092	5756	6401	7043	7643	8247
44 1/2		4101	4853	5605	6337	7048	7756	8417	9083
46 1/2		4494	5318	6144	6946	7726	8502	9229	9960
48 1/2		4905	5805	6706	7583	8435	9284	10078	10877
50 1/2		5333	6313	7294	8248	9175	10099	10965	11835
52 1/2		5780	6843	7906	8941	9947	10949	11889	12833
54 1/2		6245	7394	8543	9662	10750	11834	12850	13872
56 1/2		6728	7966	9205	10411	11584	12753	13849	14951
58 1/2		7228	8559	9892	11188	12449	13706	14885	16071
60 1/2		7747	9174	10603	11993	13345	14693	15959	17231
t"		I Axis Y - Y							
0		26.8	32.4	37.7	43.2	48.6	54.1	60.1	65.6
1/4		29.6	35.8	41.7	47.7	53.8	59.9	66.5	72.7
5/16		30.3	36.6	42.8	49.0	55.2	61.4	68.2	74.6
3/8		31.1	37.6	43.9	50.2	56.6	63.0	70.0	76.5
7/16		31.8	38.5	45.0	51.5	58.0	64.6	71.7	78.4
1/2		32.6	39.5	46.1	52.8	59.5	66.3	73.6	80.4
9/16		33.5	40.5	47.3	54.1	61.0	67.9	75.4	82.5
5/8		34.3	41.5	48.4	55.5	62.5	69.6	77.3	84.6
3/4		36.0	43.6	50.9	58.2	65.7	73.2	81.2	88.8

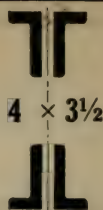
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size	4" x 3 1/2"							
Thickness	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4 Area	9.00	10.68	12.36	14.00	15.60	17.20	18.72	20.24
L's Weight	30.8	36.4	42.4	47.6	53.2	58.8	64.0	69.2
d"	I Axis X - X							
8 1/2	99	115	132	147	162	176	188	201
9 1/2	129	151	172	193	212	231	248	265
10 1/2	163	191	219	245	271	295	317	339
12 1/2	246	288	331	371	410	449	482	517
14 1/2	346	406	467	525	581	636	686	736
16 1/2	464	546	628	707	783	859	926	996
18 1/2	600	707	814	917	1017	1115	1205	1296
20 1/2	755	890	1025	1155	1281	1406	1520	1636
22 1/2	927	1093	1260	1421	1577	1732	1873	2017
24 1/2	1117	1318	1520	1715	1904	2092	2264	2438
26 1/2	1325	1565	1805	2037	2262	2486	2692	2900
28 1/2	1552	1833	2114	2387	2652	2914	3157	3403
30 1/2	1796	2122	2449	2765	3072	3377	3660	3945
32 1/2	2058	2433	2807	3171	3524	3875	4200	4529
34 1/2	2338	2764	3191	3605	4007	4407	4778	5153
36 1/2	2637	3118	3599	4067	4521	4973	5393	5817
38 1/2	2953	3492	4033	4557	5067	5574	6046	6522
40 1/2	3287	3888	4490	5075	5643	6209	6736	7267
42 1/2	3639	4306	4973	5621	6251	6878	7463	8053
44 1/2	4010	4745	5480	6195	6890	7582	8228	8879
46 1/2	4398	5205	6012	6797	7560	8320	9030	9745
48 1/2	4804	5686	6569	7427	8261	9093	9870	10653
50 1/2	5229	6189	7150	8085	8994	9900	10747	11600
52 1/2	5671	6713	7756	8771	9758	10741	11662	12588
54 1/2	6131	7259	8387	9485	10553	11617	12614	13617
56 1/2	6609	7826	9043	10227	11379	12527	13604	14686
58 1/2	7106	8414	9723	10997	12236	13472	14631	15796
60 1/2	7620	9023	10428	11795	13125	14451	15695	16946
t"	I Axis Y - Y							
0"	18.0	21.8	25.5	29.2	32.9	36.6	40.9	44.8
1/4	20.2	24.5	28.7	32.9	37.1	41.3	46.2	50.6
5/16	20.8	25.3	29.6	33.9	38.3	42.6	47.6	52.2
3/8	21.4	26.0	30.4	34.9	39.4	43.9	49.0	53.8
7/16	22.1	26.8	31.4	36.0	40.6	45.2	50.5	55.4
1/2	22.7	27.6	32.3	37.0	41.8	46.6	52.1	57.1
9/16	23.4	28.4	33.3	38.1	43.1	48.0	53.6	58.8
5/8	24.1	29.3	34.2	39.3	44.4	49.4	55.2	60.5
3/4	25.5	31.0	36.3	41.6	47.0	52.4	58.5	64.2

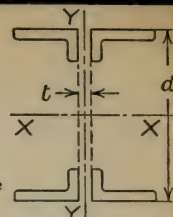
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

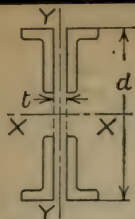
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



5 × 3

Size		5" × 3"							
Thickness		5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4	Area	9.60	11.44	13.24	15.00	16.72	18.44	20.12	21.76
L's	Weight	32.8	39.2	45.2	51.2	57.2	62.8	68.4	74.0
d"		I Axis X - X							
6 1/2		73	83	93	104	114	123	132	140
7 1/2		97	115	130	145	160	173	186	198
8 1/2		129	152	173	194	214	232	250	267
9 1/2		166	196	223	250	276	300	334	347
10 1/2		207	245	280	314	346	377	408	437
12 1/2		305	361	413	464	513	560	606	651
14 1/2		421	499	573	644	713	779	845	908
16 1/2		557	660	759	854	947	1036	1124	1209
18 1/2		712	845	970	1094	1214	1329	1443	1553
20 1/2		886	1052	1209	1364	1514	1659	1802	1941
22 1/2		1080	1282	1475	1664	1848	2026	2202	2372
24 1/2		1292	1534	1766	1994	2215	2430	2642	2847
26 1/2		1524	1810	2085	2354	2615	2871	3122	3365
28 1/2		1775	2109	2429	2744	3049	3348	3642	3927
30 1/2		2045	2430	2801	3164	3517	3863	4203	4532
32 1/2		2334	2774	3198	3614	4018	4414	4803	5181
34 1/2		2643	3142	3623	4094	4552	5002	5444	5874
36 1/2		2971	3532	4073	4604	5120	5627	6126	6610
38 1/2		3318	3945	4551	5144	5721	6289	6847	7389
40 1/2		3684	4381	5054	5714	6356	6988	7609	8212
42 1/2		4069	4839	5584	6314	7024	7724	8411	9079
44 1/2		4474	5321	6141	6944	7726	8497	9253	9989
46 1/2		4897	5825	6724	7604	8461	9306	10136	10942
48 1/2		5340	6353	7334	8294	9229	10153	11058	11939
50 1/2		5802	6903	7970	9014	10031	11036	12021	12980
52 1/2		6284	7476	8632	9764	10866	11956	13024	14064
54 1/2		6784	8072	9321	10544	11735	12913	14067	15191
56 1/2		7304	8691	10037	11354	12637	13907	15152	16363
58 1/2		7843	9333	10779	12194	13573	14938	16275	17577
t"		I Axis Y - Y							
0"		52.1	62.5	73.3	83.7	94.1	105.2	115.8	126.3
1/4		56.3	67.6	79.3	90.5	101.8	113.8	125.2	136.6
5/16		57.4	68.9	80.8	92.3	103.8	116.1	127.7	139.3
3/8		58.5	70.2	82.4	94.1	105.8	118.3	130.2	142.0
7/16		59.7	71.6	84.0	96.0	107.8	120.6	132.7	144.8
1/2		60.8	73.0	85.6	97.8	109.9	123.0	135.3	147.6
9/16		62.0	74.4	87.3	99.7	112.1	125.4	138.0	150.5
5/8		63.2	75.8	89.0	101.6	114.2	127.8	140.6	153.4
3/4		65.6	78.7	92.4	105.5	118.6	132.7	146.1	159.4



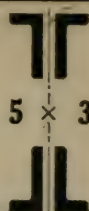
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		5" X 3"							
Thickness		5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4	Area	9.60	11.44	13.24	15.00	16.72	18.44	20.12	21.76
L's	Weight	32.8	39.2	45.2	51.2	57.2	62.8	68.4	74.0
d"		I Axis X - X							
10 1/2		147	174	198	222	244	265	286	306
12 1/2		226	266	304	342	377	411	444	476
14 1/2		323	382	437	492	544	593	642	689
16 1/2		439	520	597	672	744	813	881	947
18 1/2		575	682	782	882	977	1069	1160	1247
20 1/2		730	866	995	1122	1244	1362	1479	1592
22 1/2		904	1073	1234	1392	1544	1692	1838	1979
24 1/2		1098	1303	1499	1692	1878	2059	2238	2411
26 1/2		1310	1556	1791	2022	2245	2463	2678	2885
28 1/2		1542	1831	2109	2382	2646	2904	3158	3404
30 1/2		1793	2130	2454	2772	3080	3381	3678	3966
32 1/2		2063	2451	2825	3192	3547	3896	4239	4571
34 1/2		2352	2796	3223	3642	4048	4447	4839	5220
36 1/2		2661	3163	3647	4122	4583	5035	5480	5912
38 1/2		2989	3553	4098	4632	5151	5660	6162	6648
40 1/2		3336	3966	4575	5172	5752	6322	6883	7428
42 1/2		3702	4402	5079	5742	6386	7021	7645	8251
44 1/2		4087	4861	5609	6342	7055	7757	8447	9117
46 1/2		4492	5342	6165	6972	7756	8530	9289	10027
48 1/2		4915	5847	6748	7632	8491	9339	10172	10981
50 1/2		5358	6374	7358	8322	9260	10186	11094	11978
52 1/2		5820	6924	7994	9042	10062	11069	12057	13018
54 1/2		6302	7497	8657	9792	10897	11989	13060	14102
56 1/2		6802	8094	9346	10572	11766	12946	14104	15230
58 1/2		7322	8712	10061	11382	12668	13940	15187	16401
60 1/2		7861	9354	10803	12222	13603	14971	16311	17616
62 1/2		8419	10019	11571	13092	14573	16038	17475	18874
t"		I Axis Y - Y							
0"		11.4	1.38	16.3	18.8	21.2	24.0	26.7	29.4
1/4		13.2	16.0	19.0	21.8	24.7	28.0	31.1	34.3
5/16		13.7	16.6	19.7	22.6	25.7	29.1	32.3	35.6
3/8		14.2	17.2	20.4	23.5	26.7	30.2	33.6	37.0
7/16		14.8	17.8	21.2	24.4	27.7	31.4	34.9	38.4
1/2		15.3	18.5	22.0	25.3	28.7	32.6	36.2	39.9
9/16		15.9	19.2	22.8	26.3	29.8	33.8	37.6	41.4
5/8		16.5	19.9	23.7	27.3	30.9	35.1	39.0	42.9
3/4		17.7	21.4	25.4	29.3	33.2	37.7	41.9	46.2

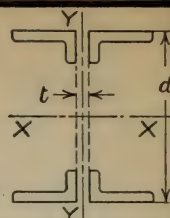
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

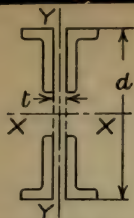
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



5 × 3½

Size		5" × 3½"							
Thickness		5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4
4	Area	10.24	12.20	14.12	16.00	17.88	19.68	21.48	23.24
L's	Weight	34.8	41.6	48.0	54.4	60.8	67.2	73.2	79.2
d"	I Axis X - X								
7 ½	98	115	131	145	160	174	187	198	
8 ½	130	153	175	195	215	233	252	268	
9 ½	167	197	226	252	279	303	328	349	
10 ½	210	248	284	318	351	382	414	442	
12 ½	311	367	422	472	524	571	620	663	
14 ½	432	511	587	659	732	800	868	930	
16 ½	573	679	781	878	976	1067	1159	1244	
18 ½	735	872	1004	1129	1256	1374	1493	1604	
20 ½	918	1088	1254	1412	1571	1721	1871	2011	
22 ½	1121	1330	1533	1727	1922	2107	2291	2464	
24 ½	1344	1595	1840	2074	2309	2532	2754	2964	
26 ½	1588	1886	2175	2453	2732	2997	3260	3510	
28 ½	1852	2200	2539	2864	3190	3501	3809	4102	
30 ½	2137	2539	2930	3306	3684	4044	4401	4741	
32 ½	2443	2902	3350	3781	4214	4626	5036	5427	
34 ½	2768	3290	3798	4288	4780	5248	5714	6159	
36 ½	3115	3702	4275	4827	5381	5909	6435	6938	
38 ½	3482	4139	4779	5398	6019	6610	7199	7763	
40 ½	3869	4600	5312	6001	6692	7350	8005	8634	
42 ½	4277	5085	5873	6636	7400	8129	8855	9552	
44 ½	4705	5595	6463	7303	8145	8948	9748	10517	
46 ½	5153	6129	7080	8001	8925	9806	10683	11527	
48 ½	5623	6687	7726	8732	9741	10703	11662	12585	
50 ½	6112	7270	8400	9495	10593	11640	12684	13688	
52 ½	6623	7878	9103	10209	11481	12616	13748	14839	
54 ½	7153	8509	9833	11117	12404	13632	14856	16035	
56 ½	7704	9165	10592	11976	13363	14687	16006	17279	
58 ½	8276	9846	11379	12867	14358	15781	17199	18569	
60 ½	8868	10551	12194	13790	15389	16914	18436	19905	
62 ½	9481	11280	13038	14744	16455	18087	19715	21288	
t"	I Axis Y - Y								
0"	52.3	62.7	73.1	84.0	94.6	105.0	115.5	126.9	
1/4	56.5	67.8	79.1	90.9	102.4	113.7	125.1	137.4	
5/16	57.6	69.2	80.7	92.7	104.4	115.9	127.6	140.1	
3/8	58.8	70.5	82.2	94.6	106.5	118.2	130.1	142.9	
7/16	59.9	71.9	83.9	96.4	108.6	120.6	132.7	145.8	
1/2	61.1	73.3	85.5	98.3	110.7	123.0	135.3	148.6	
9/16	62.3	74.7	87.2	100.2	112.9	125.4	138.0	151.6	
5/8	63.5	76.2	88.9	102.2	115.1	127.8	140.7	154.6	
3/4	65.9	79.2	92.4	106.2	119.6	132.9	146.2	160.6	



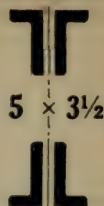
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		5" x 3 1/2"						
Thickness		5/16	3/8	7/16	1/2	9/16	5/8	11/16
Area		10.24	12.20	14.12	16.00	17.88	19.68	21.48
L's Weight		34.8	41.6	48.0	54.4	60.8	67.2	73.2
d"		I Axis X - X						
10 1/2		164	193	221	246	272	296	320
12 1/2		249	294	337	377	418	456	493
14 1/2		354	419	482	540	599	654	709
16 1/2		481	569	654	735	817	892	968
18 1/2		627	743	856	962	1070	1170	1270
20 1/2		794	942	1085	1221	1357	1487	1615
22 1/2		982	1165	1342	1511	1682	1843	2003
24 1/2		1190	1412	1628	1834	2042	2239	2434
26 1/2		1419	1684	1942	2189	2438	2674	2908
28 1/2		1668	1980	2284	2576	2869	3148	3424
30 1/2		1937	2301	2655	2995	3337	3661	3984
32 1/2		2227	2646	3054	3446	3840	4214	4587
34 1/2		2538	3015	3481	3929	4379	4807	5233
36 1/2		2869	3409	3936	4444	4953	5439	5921
38 1/2		3220	3827	4419	4990	5564	6110	6653
40 1/2		3592	4270	4931	5569	6210	6820	7427
42 1/2		3984	4737	5471	6180	6892	7570	8245
44 1/2		4397	5228	6039	6823	7610	8359	9105
46 1/2		4831	5744	6636	7498	8363	9188	10009
48 1/2		5284	6285	7260	8205	9152	10055	10955
50 1/2		5759	6849	7913	8944	9977	10963	11945
52 1/2		6254	7438	8594	9715	10838	11909	12977
54 1/2		6769	8052	9304	10518	11734	12895	14052
56 1/2		7305	8689	10041	11352	12667	13921	15170
58 1/2		7861	9352	10807	12219	13635	14985	16332
60 1/2		8437	10038	11601	13118	14639	16089	17536
62 1/2		9035	10749	12424	14049	15673	17233	18783
64 1/2		9652	11485	13274	15012	16753	18416	20073
66 1/2		10291	12245	14153	16007	17864	19638	21406
68 1/2		10949	13029	15060	17034	19011	20899	22782
70 1/2		11628	13837	15996	18093	20194	22200	24201
72 1/2		12328	14670	16959	19183	21412	23540	25663
74 1/2		13048	15528	17951	20306	22666	24920	27168
76 1/2		13789	16409	18971	21461	23956	26339	28716
t"		I Axis Y - Y						
0"		18.1	21.7	25.5	29.4	33.3	37.1	41.0
1/4		20.4	24.6	28.8	33.3	37.7	42.1	46.6
5/16		21.0	25.3	29.7	34.4	38.9	43.4	48.0
3/8		21.7	26.1	30.6	35.5	40.1	44.8	49.6
7/16		22.4	26.9	31.6	36.6	41.4	46.2	51.2
1/2		23.0	27.8	32.5	37.7	42.7	47.7	52.8
9/16		23.7	28.6	33.6	38.9	44.0	49.2	54.4
5/8		24.5	29.5	34.6	40.1	45.4	50.7	56.1
3/4		26.0	31.3	36.8	42.6	48.2	53.9	59.7

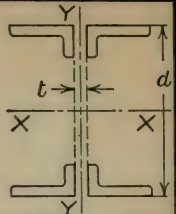
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

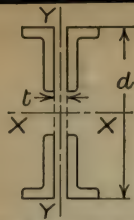
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



6 × 3½

Size		6" × 3 1/2"								
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8
4	Area	13.68	15.88	18.00	20.12	22.20	24.24	26.24	28.24	30.20
L's	Weight	46.8	54.0	61.2	68.4	75.6	82.4	89.6	96.0	102.8
d"		I Axis X - X								
7 1/2		133	153	170	187	203	219	232	246	260
8 1/2		177	203	228	250	272	294	313	332	351
9 1/2		228	262	294	323	353	381	406	433	458
10 1/2		285	328	369	406	444	481	513	547	579
12 1/2		421	485	546	603	660	716	766	818	868
14 1/2		584	674	759	840	921	999	1071	1146	1217
16 1/2		775	894	1008	1117	1226	1331	1429	1530	1627
18 1/2		992	1146	1293	1435	1576	1712	1840	1970	2097
20 1/2		1238	1430	1614	1793	1969	2141	2303	2467	2627
22 1/2		1510	1746	1971	2191	2408	2619	2818	3021	3218
24 1/2		1810	2094	2364	2629	2890	3145	3386	3631	3869
26 1/2		2137	2473	2794	3107	3417	3719	4006	4297	4580
28 1/2		2492	2884	3259	3626	3989	4342	4679	5020	5352
30 1/2		2874	3326	3760	4185	4605	5013	5404	5800	6185
32 1/2		3283	3801	4297	4784	5265	5733	6182	6636	7077
34 1/2		3720	4307	4870	5424	5969	6502	7012	7528	8030
36 1/2		4184	4845	5479	6103	6718	7319	7895	8477	9044
38 1/2		4675	5415	6124	6823	7512	8184	8830	9482	10118
40 1/2		5194	6017	6805	7583	8350	9098	9818	10544	11252
42 1/2		5740	6650	7523	8384	9232	10060	10858	11662	12447
44 1/2		6313	7315	8276	9224	10159	11071	11951	12837	13702
46 1/2		6914	8012	9065	10105	11130	12130	13096	14068	15017
48 1/2		7542	8740	9890	11026	12145	13238	14293	15356	16393
50 1/2		8198	9501	10751	11988	13205	14394	15543	16700	17830
52 1/2		8881	10293	11648	12989	14309	15599	16846	18101	19326
54 1/2		9591	11117	12581	14031	15458	16852	18201	19558	20883
56 1/2		10329	11972	13550	15113	16651	18154	19608	21072	22501
58 1/2		11094	12860	14556	16235	17888	19504	21068	22642	24179
60 1/2		11886	13779	15597	17398	19170	20903	22581	24269	25917
62 1/2		12706	14730	16674	18601	20496	22350	24146	25952	27716
64 1/2		13553	15712	17787	19844	21867	23845	25763	27691	29575
66 1/2		14427	16727	18936	21127	23282	25390	27433	29487	31495
68 1/2		15329	17773	20121	22450	24741	26982	29156	31340	33474
70 1/2		16258	18851	21342	23814	26245	28623	30930	33249	35515
72 1/2		17215	19960	22599	25218	27793	30313	32758	35214	37615
74 1/2		18199	21102	23892	26662	29386	32051	34638	37236	39777
76 1/2		19210	22275	25222	28147	31023	33837	36570	39315	41998
78 1/2		20248	23480	26587	29671	32704	35672	38555	41450	44280
80 1/2		21314	24717	27988	31236	34430	37556	40592	43641	46622
82 1/2		22408	25985	29425	32841	36200	39488	42682	45889	49025
84 1/2		23528	27286	30898	34487	38015	41468	44824	48193	51488
t"		I Axis Y - Y								
0"		108.4	126.4	144.2	163.1	181.0	199.0	218.1	236.2	254.4
3/8		119.3	139.3	158.9	179.7	199.6	219.4	240.4	260.5	280.6
7/16		121.2	141.5	161.5	182.6	202.8	223.0	244.3	264.8	285.2
1/2		123.2	143.8	164.1	185.5	206.1	226.6	248.3	269.1	289.8
5/8		127.1	148.4	169.4	191.6	212.8	233.9	256.4	277.8	299.2
3/4		131.2	153.2	174.8	197.7	219.6	241.5	264.7	286.8	308.9
7/8		135.4	158.1	180.4	204.1	226.7	249.2	273.1	296.0	318.8
1"		139.7	163.1	186.2	210.5	233.9	257.2	281.8	305.4	329.0
1 1/8		144.1	168.3	192.1	217.2	241.3	265.3	290.7	315.1	339.4



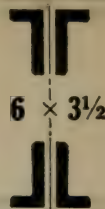
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		6" × 3 1/2"								
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8
4	Area	13.68	15.88	18.00	20.12	22.20	24.24	26.24	28.24	30.20
L's	Weight	46.8	54.0	61.2	68.4	75.6	82.4	89.6	96.0	102.8
d"		I Axis X - X								
12 1/2		294	338	379	418	457	494	528	563	596
14 1/2		423	487	547	605	662	717	768	820	870
16 1/2		579	667	752	832	912	989	1060	1133	1204
18 1/2		763	880	992	1099	1206	1309	1405	1503	1598
20 1/2		974	1124	1268	1407	1544	1677	1802	1930	2053
22 1/2		1212	1400	1580	1754	1927	2094	2252	2412	2568
24 1/2		1477	1708	1928	2142	2354	2560	2754	2952	3144
26 1/2		1771	2047	2312	2570	2825	3074	3309	3548	3780
28 1/2		2091	2419	2732	3039	3341	3636	3916	4200	4476
30 1/2		2439	2822	3188	3547	3902	4247	4576	4909	5233
32 1/2		2814	3257	3681	4096	4506	4906	5288	5674	6050
34 1/2		3216	3723	4209	4685	5156	5614	6053	6496	6928
36 1/2		3646	4221	4773	5315	5849	6370	6870	7374	7866
38 1/2		4103	4752	5373	5984	6587	7175	7739	8309	8864
40 1/2		4588	5313	6009	6694	7369	8028	8661	9300	9923
42 1/2		5100	5907	6681	7444	8196	8930	9636	10348	11042
44 1/2		5639	6532	7389	8235	9067	9880	10663	11452	12222
46 1/2		6206	7189	8133	9065	9983	10879	11742	12613	13462
48 1/2		6800	7878	8914	9936	10943	11926	12874	13830	14762
50 1/2		7421	8599	9730	10847	11947	13022	14059	15104	16123
52 1/2		8070	9351	10582	11798	12996	14166	15296	16434	17544
54 1/2		8746	10135	11470	12790	14089	15358	16585	17820	19026
56 1/2		9449	10951	12394	13821	15226	16599	17927	19263	20568
58 1/2		10180	11799	13354	14893	16408	17889	19322	20763	22170
60 1/2		10938	12678	14350	16006	17635	19227	20769	22319	23833
62 1/2		11724	13590	15382	17158	18905	20614	22268	23931	25556
64 1/2		12536	14533	16450	18351	20220	22049	23820	25600	27340
66 1/2		13377	15507	17555	19584	21580	23532	25424	27326	29184
68 1/2		14244	16514	18695	20857	22984	25064	27081	29108	31088
70 1/2		15139	17552	19871	22170	24432	26645	28790	30946	33053
72 1/2		16061	18622	21083	23524	25925	28273	30552	32841	35078
74 1/2		17011	19724	22331	24918	27462	29951	32366	34792	37164
76 1/2		17988	20857	23615	26352	29044	31677	34233	36800	39310
78 1/2		18993	22023	24935	27827	30670	33451	36152	38865	41516
80 1/2		20024	23220	26291	29341	32340	35274	38124	40986	43783
82 1/2		21083	24448	27684	30896	34055	37145	40148	43163	46110
84 1/2		22170	25709	29112	32491	35814	39065	42224	45397	48498
90 1/2		25593	29681	33612	37518	41358	45115	48769	52437	56023
96 1/2		29263	33939	38436	42907	47301	51602	55786	59985	64092
102 1/2		33179	38483	43585	48658	53644	58525	63276	68042	72705
108 1/2		37342	43313	49057	54771	60387	65884	71237	76607	81861
114 1/2		41750	48429	54853	61247	67529	73680	79672	85681	91560
t"		I Axis Y - Y								
0"		21.9	25.7	29.4	33.6	37.5	41.5	46.1	50.3	54.6
3/8		26.4	31.0	35.6	40.8	45.6	50.5	56.1	61.3	66.7
7/16		27.3	32.0	36.8	42.1	47.1	52.2	58.0	63.4	68.9
1/2		28.2	33.1	38.0	43.5	48.7	53.9	59.9	65.5	71.1
5/8		30.0	35.2	40.5	46.3	51.9	57.5	63.9	69.8	75.9
3/4		31.9	37.5	43.1	49.4	55.3	61.3	68.0	74.4	80.8
7/8		34.0	40.0	45.9	52.6	58.9	65.2	72.4	79.2	86.0
1"		36.1	42.5	48.8	55.9	62.6	69.4	77.0	84.2	91.5
1 1/8		38.4	45.2	51.9	59.4	66.5	73.7	81.7	89.4	97.1

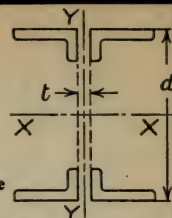
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

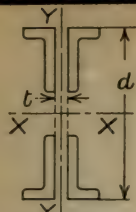
AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		6" X 4"								
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8
4	Area	14.44	16.72	19.00	21.24	23.44	25.60	27.76	29.88	31.92
L's	Weight	49.2	57.2	64.8	72.4	80.0	87.2	94.4	101.6	108.8
d"		I Axis X - X								
8 1/2		178	203	227	251	273	293	314	333	352
9 1/2		229	263	294	325	354	381	409	435	460
10 1/2		288	330	370	409	448	482	517	552	583
12 1/2		427	490	551	611	669	722	777	829	879
14 1/2		595	684	770	855	937	1013	1092	1167	1238
16 1/2		791	911	1027	1141	1252	1356	1462	1564	1662
18 1/2		1017	1171	1321	1470	1614	1750	1888	2022	2149
20 1/2		1271	1465	1654	1841	2023	2195	2369	2539	2700
22 1/2		1555	1793	2025	2255	2478	2691	2906	3115	3315
24 1/2		1867	2154	2434	2711	2981	3238	3498	3752	3993
26 1/2		2208	2548	2881	3210	3530	3837	4146	4448	4736
28 1/2		2578	2976	3366	3751	4127	4486	4850	5204	5542
30 1/2		2977	3437	3889	4335	4770	5187	5609	6020	6412
32 1/2		3404	3931	4450	4961	5460	5939	6423	6895	7346
34 1/2		3861	4459	5048	5629	6197	6743	7293	7830	8344
36 1/2		4346	5021	5685	6341	6981	7597	8219	8825	9406
38 1/2		4861	5616	6360	7094	7811	8503	9200	9880	10531
40 1/2		5404	6244	7073	7890	8689	9460	10236	10995	11720
42 1/2		5976	6906	7824	8729	9613	10468	11328	12169	12974
44 1/2		6577	7601	8613	9610	10585	11527	12476	13403	14291
46 1/2		7207	8330	9440	10533	11603	12638	13679	14697	15671
48 1/2		7866	9092	10305	11499	12668	13800	14938	16050	17116
50 1/2		8553	9887	11207	12508	13780	15012	16252	17464	18625
52 1/2		9270	10716	12148	13559	14939	16277	17622	18937	20197
54 1/2		10015	11579	13127	14652	16145	17592	19047	20470	21833
56 1/2		10789	12475	14144	15788	17397	18958	20527	22062	23533
58 1/2		11593	13404	15199	16967	18697	20376	22064	23715	25297
60 1/2		12425	14367	16292	18187	20043	21845	23655	25427	27125
62 1/2		13286	15363	17423	19451	21437	23365	25303	27199	29017
64 1/2		14175	16392	18592	20757	22877	24937	27006	29030	30972
66 1/2		15094	17455	19799	22105	24364	26559	28764	30922	32991
68 1/2		16042	18552	21043	23496	25898	28233	30578	32873	35074
70 1/2		17018	19682	22326	24929	27478	29958	32447	34885	37221
72 1/2		18023	20845	23647	26405	29106	31734	34372	36955	39432
74 1/2		19057	22042	25006	27923	30781	33561	36352	39086	41707
76 1/2		20121	23272	26403	29484	32502	35440	38388	41276	44045
78 1/2		21212	24536	27838	31087	34270	37370	40480	43526	46447
80 1/2		22333	25833	29311	32733	36086	39350	42627	45836	48914
82 1/2		23483	27164	30822	34421	37948	41383	44829	48205	51444
84 1/2		24662	28528	32370	36151	39857	43466	47087	50634	54037
90 1/2		28371	32821	37245	41598	45865	50023	54194	58281	62202
96 1/2		32340	37414	42462	47427	52295	57041	61801	66465	70941
102 1/2		36569	43309	48020	53639	59147	64520	69908	75187	80254
t"		I Axis Y - Y								
0"		108.2	126.1	144.8	162.9	180.9	200.1	218.1	236.4	254.4
3/8		119.2	138.9	156.7	179.6	199.5	220.6	240.8	261.0	280.9
7/16		121.2	141.2	162.3	182.5	202.8	224.2	244.7	265.3	285.5
1/2		123.1	143.5	164.9	185.5	206.1	227.9	248.7	269.6	290.2
5/8		127.1	148.2	170.3	191.6	212.9	235.4	256.9	278.5	299.8
3/4		131.3	153.0	175.9	197.9	219.9	243.1	265.4	287.6	309.6
7/8		135.5	157.9	181.6	204.3	227.0	251.0	274.0	297.0	319.7
1"		139.8	163.0	187.4	210.9	234.3	259.1	282.8	306.6	330.0
1 1/8		144.3	168.2	193.4	217.6	241.8	267.3	291.9	316.4	340.6
1 1/4		148.9	173.6	199.5	224.5	249.5	275.8	301.2	326.5	351.4



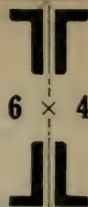
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		6" X 4"								
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8
4	Area	14.44	16.72	19.00	21.24	23.44	25.60	27.76	29.88	31.92
L's	Weight	49.2	57.2	64.8	72.4	80.0	87.2	94.4	101.6	108.8
d"		I Axis X - X								
12 1/2		322	370	414	459	502	541	581	619	655
14 1/2		461	530	595	660	723	781	840	897	951
16 1/2		629	723	814	904	991	1072	1155	1235	1311
18 1/2		825	950	1071	1190	1306	1415	1525	1632	1734
20 1/2		1051	1211	1366	1519	1668	1808	1951	2089	2221
22 1/2		1305	1505	1699	1890	2077	2253	2432	2606	2772
24 1/2		1589	1832	2070	2304	2533	2749	2969	3183	3387
26 1/2		1901	2193	2479	2760	3035	3297	3562	3819	4066
28 1/2		2242	2587	2925	3259	3585	3895	4210	4516	4808
30 1/2		2612	3015	3410	3800	4181	4545	4913	5272	5614
32 1/2		3011	3476	3933	4384	4824	5246	5672	6087	6484
34 1/2		3439	3971	4494	5010	5514	5998	6486	6963	7418
36 1/2		3895	4499	5093	5679	6251	6801	7356	7898	8416
38 1/2		4381	5060	5730	6390	7035	7656	8282	8893	9478
40 1/2		4895	5655	6405	7143	7866	8562	9263	9948	10603
42 1/2		5438	6283	7118	7940	8743	9519	10300	11062	11793
44 1/2		6010	6945	7868	8778	9668	10527	11392	12237	13046
46 1/2		6611	7640	8657	9659	10529	11586	12539	13471	14363
48 1/2		7241	8369	9484	10583	11658	12697	13742	14764	15744
50 1/2		7900	9131	10349	11549	12722	13858	15001	16118	17189
52 1/2		8588	9927	11252	12557	13834	15071	16315	17531	18697
54 1/2		9304	10756	12193	13608	14993	16335	17685	19004	20269
56 1/2		10049	11618	13172	14701	16199	17651	19110	20537	21906
58 1/2		10824	12514	14189	15837	17452	19016	20591	22130	23606
60 1/2		11627	13443	15244	17016	18751	20434	22127	23782	25370
62 1/2		12459	14406	16336	18237	20097	21903	23719	25494	27197
64 1/2		13320	15420	17467	19500	21491	23423	25366	27266	29089
66 1/2		14210	16432	18636	20806	22931	24994	27069	29098	31045
68 1/2		15128	17495	19843	22154	24418	26617	28827	30989	33064
70 1/2		16076	18591	21088	23545	25952	28291	30641	32940	35147
72 1/2		17052	19721	22371	24978	27533	30016	32510	34951	37294
74 1/2		18058	20885	23692	26454	29160	31792	34435	37022	39505
76 1/2		19092	22082	25051	27972	30835	33619	36416	39152	41780
78 1/2		20155	23312	26447	29533	32556	35498	38452	41343	44118
80 1/2		21247	24576	27882	31136	34325	37427	40543	43593	46520
82 1/2		22368	25873	29355	32782	36140	39408	42690	45902	48986
84 1/2		23517	27203	30866	34470	38002	41440	44892	48272	51516
86 1/2		24694	28567	32417	36178	39789	43269	46784	50133	53489
88 1/2		25899	29965	34008	37927	41618	45140	48716	52044	55516
90 1/2		27132	31396	35627	39709	43490	47054	50716	54044	57594
92 1/2		28393	32859	37274	41534	45406	49002	52716	56044	59674
94 1/2		29682	34354	38959	43414	47358	51002	54716	58044	61754
96 1/2		31000	35889	40729	45450	49458	53140	57002	60444	64374
98 1/2		32347	37464	42584	47644	51714	55440	59402	63044	66994
100 1/2		33724	39079	44514	49894	54054	57902	62002	65644	69674
102 1/2		35132	40683	46174	51575	56870	62034	67213	72286	77159
104 1/2		36566	42379	47961	53404	58854	64002	69282	74563	79654
106 1/2		38035	44167	49874	55484	60994	66140	71522	76844	82044
108 1/2		39539	45949	51824	57624	63204	68382	73822	79144	84544
t"		I Axis Y - Y								
0"		32.4	37.8	43.7	49.3	54.9	61.2	67.1	73.1	79.0
3/8		38.0	44.4	51.4	58.1	64.8	72.3	79.3	86.5	93.6
7/16		39.0	45.6	52.8	59.7	66.6	74.3	81.5	88.9	96.2
1/2		40.0	46.9	54.3	61.4	68.5	76.4	83.8	91.4	98.9
5/8		42.2	49.5	57.3	64.8	72.3	80.7	88.5	96.5	104.5
3/4		44.6	52.2	60.5	68.4	76.4	85.2	93.5	101.9	110.3
7/8		47.0	55.1	63.8	72.1	80.6	89.8	98.6	107.6	116.4
1"		49.5	58.0	67.3	76.1	85.0	94.7	104.0	113.4	122.8
1 1/8		52.2	61.2	70.9	80.2	89.5	99.8	109.6	119.5	129.4
1 1/4		55.0	64.4	74.6	84.4	94.3	105.1	115.4	125.8	136.2

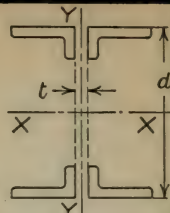
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



7 × 3½

Size

7" × 3½"

Thickness

¾

7/16

½

9/16

5/8

11/16

¾

13/16

7/8

15/16

1"

4	Area	15.20	17.60	20.00	22.36	24.68	27.00	29.24	31.48	33.68	35.88	38.00
L's	Weight	52.0	60.0	68.0	76.4	84.0	92.0	99.6	107.2	114.8	122.0	129.2

d"

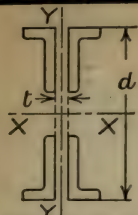
I Axis X - X

8 ½	202	231	258	286	311	335	358	381	403	422	441
9 ½	260	297	333	368	402	433	465	495	524	550	576
10 ½	324	372	417	462	505	545	585	624	662	695	729
12 ½	477	548	616	684	749	810	871	930	988	1040	1094
14 ½	660	759	855	950	1042	1129	1215	1299	1381	1457	1534
16 ½	873	1006	1134	1260	1384	1501	1617	1731	1842	1946	2050
18 ½	1117	1287	1452	1616	1775	1928	2078	2226	2370	2506	2642
20 ½	1391	1604	1811	2016	2216	2408	2597	2784	2965	3139	3310
22 ½	1696	1956	2210	2461	2706	2943	3175	3405	3628	3843	4054
24 ½	2031	2343	2649	2951	3245	3532	3811	4088	4358	4618	4874
26 ½	2396	2766	3128	3485	3834	4174	4506	4835	5157	5466	5770
28 ½	2792	3223	3646	4064	4473	4871	5259	5645	6021	6385	6742
30 ½	3219	3716	4205	4688	5160	5621	6071	6517	6953	7376	7790
32 ½	3675	4244	4804	5357	5897	6426	6941	7453	7953	8439	8914
34 ½	4162	4807	5443	6070	6683	7285	7870	8451	9020	9573	10114
36 ½	4680	5406	6122	6828	7519	8197	8857	9513	10154	10780	11390
38 ½	5227	6039	6840	7631	8404	9164	9902	10637	11356	12058	12742
40 ½	5806	6708	7599	8478	9338	10184	11006	11825	12625	13408	14170
42 ½	6414	7412	8398	9370	10322	11259	12169	13075	13961	14829	15674
44 ½	7053	8151	9237	10307	11355	12388	13390	14389	15365	16322	17254
46 ½	7723	8926	10116	11289	12438	13570	14670	15765	16836	17887	18910
48 ½	8422	9735	11034	12315	13570	14807	16008	17204	18375	19524	20642
50 ½	9153	10580	11993	13386	14751	16097	17404	18706	19981	21233	22450
52 ½	9913	11460	12992	14502	15981	17442	18859	20272	21654	23013	24334
54 ½	10704	12375	14031	15663	17261	18841	20373	21900	23394	24865	26294
56 ½	11526	13326	15110	16868	18590	20293	21945	23591	25202	26789	28330
58 ½	12377	14311	16228	18118	19969	21850	23575	25345	27078	28785	30442
60 ½	13260	15332	17387	19412	21397	23360	25264	27162	29020	30852	32630
62 ½	14172	16388	18586	20752	22874	24975	27011	29042	31030	32992	34895
64 ½	15115	17479	19825	22136	24401	26644	28817	30985	33108	35202	37235
66 ½	16089	18606	21104	23565	25977	28366	30681	32991	35252	37485	39651
68 ½	17092	19767	22422	25038	27603	30143	32604	35060	37465	39840	42143
70 ½	18127	20964	23781	26556	29277	31973	34586	37191	39744	42266	44711
72 ½	19191	22196	25180	28119	31002	33858	36625	39386	42091	44764	47355
74 ½	20286	23463	26619	29727	32775	35797	38724	41644	44505	47333	50075
76 ½	21412	24766	28098	31379	34598	37789	40880	43965	46987	49975	52871
78 ½	22567	26103	29616	33077	36470	39836	43096	46348	49535	52688	55743
80 ½	23754	27476	31175	34818	38391	41936	45369	48795	52152	55473	58691
82 ½	24970	28884	32774	36605	40363	44091	47701	51305	54835	58330	61715
84 ½	26217	30327	34413	38436	42383	46300	50092	53877	57586	61259	64815

ℓ"

I Axis Y - Y

0"	172.0	200.2	229.7	258.1	286.4	316.4	344.7	373.2	401.6	432.2	460.6
¾	186.6	217.4	249.3	280.3	311.1	343.7	374.4	405.5	436.4	469.6	500.5
7/16	189.2	220.3	252.8	284.1	315.4	348.4	379.6	411.1	442.4	476.1	507.4
½	191.8	223.3	256.2	288.0	319.7	353.2	384.8	416.7	448.5	482.7	514.4
5/8	197.0	229.5	263.2	295.9	328.5	362.9	395.4	428.2	460.9	496.0	528.6
¾	202.4	235.7	270.4	304.0	337.5	372.8	406.2	440.0	473.5	509.6	543.1
7/8	207.9	242.1	277.8	312.3	346.7	383.0	417.3	451.9	486.4	523.5	557.9
1"	213.5	248.6	285.3	320.7	356.0	393.4	428.6	464.2	499.6	537.6	573.0
1 1/8	219.2	255.3	292.9	329.3	365.6	403.9	440.1	476.7	513.0	552.1	588.4



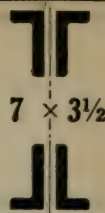
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



Size		7" × 3 1/2"										
Thickness		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"
4	Area	15.20	17.60	20.00	22.36	24.68	27.00	29.24	31.48	33.68	35.88	38.00
L's	Weight	52.0	60.0	68.0	76.4	84.0	92.0	99.6	107.2	114.8	122.0	129.2
d"		I Axis X - X										
14 1/2		424	487	547	607	664	718	771	823	873	919	965
16 1/2		585	672	756	839	920	996	1071	1145	1216	1282	1348
18 1/2		775	892	1005	1116	1225	1328	1429	1529	1626	1717	1807
20 1/2		996	1147	1294	1438	1579	1714	1846	1977	2104	2223	2342
22 1/2		1248	1438	1622	1805	1983	2154	2322	2487	2648	2802	2953
24 1/2		1529	1763	1991	2217	2436	2648	2856	3061	3261	3452	3640
26 1/2		1842	2124	2400	2673	2939	3196	3448	3698	3940	4174	4403
28 1/2		2184	2520	2849	3174	3490	3798	4099	4397	4687	4967	5242
30 1/2		2557	2951	3338	3719	4092	4454	4808	5160	5502	5833	6157
32 1/2		2961	3418	3866	4309	4742	5165	5576	5985	6384	6770	7148
34 1/2		3394	3919	4435	4944	5442	5929	6402	6873	7333	7779	8215
36 1/2		3859	4456	5044	5624	6191	6747	7287	7825	8349	8860	9358
38 1/2		4353	5028	5693	6349	6990	7619	8230	8839	9433	10012	10577
40 1/2		4878	5635	6382	7118	7838	8545	9232	9916	10584	11236	11872
42 1/2		5434	6278	7110	7932	8735	9525	10292	11056	11803	12532	13243
44 1/2		6019	6955	7879	8790	9682	10559	11411	12260	13089	13900	14690
46 1/2		6636	7668	8688	9694	10678	11647	12588	13526	14442	15339	16213
48 1/2		7282	8416	9537	10642	11724	12789	13824	14855	15862	16851	17812
50 1/2		7959	9199	10426	11635	12818	13985	15118	16247	17350	18434	19487
52 1/2		8667	10018	11354	12672	13963	15236	16471	17702	18906	20089	21238
54 1/2		9404	10871	12323	13754	15156	16540	17882	19220	20529	21815	23066
56 1/2		10173	11760	13332	14881	16399	17898	19352	20801	22219	23613	24969
58 1/2		10971	12684	14381	16053	17691	19310	20880	22445	23976	25483	26948
60 1/2		11800	13643	15470	17269	19033	20776	22466	24151	25801	27425	29003
62 1/2		12660	14638	16598	18530	20424	22296	24111	25921	27693	29439	31134
64 1/2		13550	15667	17767	19836	21864	23870	25815	27754	29652	31524	33341
66 1/2		14470	16732	18976	21187	23354	25498	27577	29650	31679	33681	35624
68 1/2		15420	17832	20225	22582	24893	27180	29397	31608	33773	35910	37983
70 1/2		16401	18967	21514	24022	26481	28916	31276	33630	35933	38211	40418
72 1/2		17413	20138	22842	25507	28119	30707	33214	35715	38164	40583	42929
74 1/2		18455	21343	24211	27036	29806	32551	35210	37862	40460	43027	45516
76 1/2		19527	22584	25620	28610	31543	34449	37264	40073	42824	45543	48179
78 1/2		20629	23860	27069	30229	33328	36401	39377	42346	45255	48131	50918
80 1/2		21762	25171	28558	31893	35164	38407	41548	44683	47753	50790	53733
82 1/2		22926	26518	30088	33601	37048	40467	43778	47082	50319	53521	56624
84 1/2		24120	27899	31656	35354	38982	42581	46066	49544	52952	56324	59591
90 1/2		27883	32255	36602	40881	45080	49247	53283	57309	61256	65164	68948
96 1/2		31921	36928	41908	46811	51622	56400	61024	65641	70165	74649	78989
102 1/2		36232	41918	47574	53144	58609	64038	69293	74539	79681	84780	89714
108 1/2		40817	47224	53601	59879	66039	72162	78088	84004	89804	95557	101124
114 1/2		45675	52847	59987	67016	73914	80773	87409	94035	100532	106980	113217
120 1/2		50807	58787	66734	74556	82233	89869	97256	104633	111867	119048	125994
t"		I Axis Y - Y										
0"		22.0	25.7	29.8	33.8	37.7	42.3	46.5	50.8	55.2	60.4	65.1
3/8		26.7	31.3	36.4	41.2	46.2	51.8	57.0	62.4	67.9	74.3	80.2
7/16		27.6	32.3	37.6	42.6	47.7	53.6	59.0	64.5	70.2	76.9	82.9
1/2		28.5	33.4	38.9	44.1	49.4	55.4	61.0	66.8	72.6	79.5	85.8
5/8		30.4	35.7	41.5	47.1	52.8	59.2	65.2	71.4	77.7	85.0	91.7
3/4		32.4	38.1	44.3	50.3	56.4	63.3	69.6	76.2	82.9	90.8	97.8
7/8		34.6	40.6	47.3	53.7	60.1	67.5	74.3	81.3	88.5	96.8	104.3
1"		36.9	43.3	50.4	57.2	64.1	72.0	79.2	86.7	94.3	103.1	111.1
1 1/8		39.3	46.1	53.7	60.9	68.3	76.6	84.3	92.3	100.3	109.7	118.2

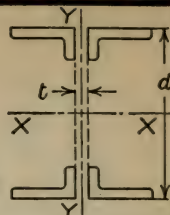
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—SHORT LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

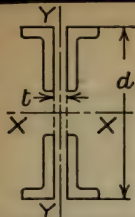
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.



8 × 6

Size		8" × 6"									
Thickness		7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"
4	Area	23.72	27.00	30.24	33.44	36.60	39.76	42.88	45.92	49.00	52.00
L's	Weight	80.8	92.0	102.8	114.0	124.8	135.2	146.0	156.4	166.8	176.8
d"		I Axis X - X									
12 1/2		624	704	778	853	926	997	1062	1128	1193	1255
14 1/2		875	989	1096	1203	1308	1410	1505	1600	1695	1786
16 1/2		1174	1328	1474	1620	1762	1902	2033	2164	2295	2420
18 1/2		1520	1721	1912	2103	2290	2474	2647	2820	2993	3159
20 1/2		1914	2168	2411	2654	2891	3125	3347	3568	3788	4001
22 1/2		2355	2669	2971	3271	3565	3856	4133	4407	4682	4947
24 1/2		2844	3224	3591	3955	4312	4667	5004	5338	5674	5998
26 1/2		3380	3833	4271	4706	5133	5556	5961	6361	6764	7152
28 1/2		3963	4497	5012	5524	6027	6526	7004	7476	7951	8411
30 1/2		4594	5214	5813	6409	6994	7575	8133	8683	9237	9773
32 1/2		5273	5985	6675	7361	8034	8703	9347	9982	10621	11239
34 1/2		5999	6810	7598	8379	9147	9911	10647	11372	12103	12810
36 1/2		6772	7689	8580	9465	10334	11198	12033	12854	13682	14484
38 1/2		7593	8622	9624	10617	11594	12565	13505	14428	15360	16263
40 1/2		8461	9609	10727	11836	12927	14012	15062	16094	17136	18145
42 1/2		9376	10650	11892	13123	14333	15538	16705	17852	19010	20131
44 1/2		10339	11746	13116	14476	15812	17143	18434	19702	20981	22222
46 1/2		11350	12895	14402	15895	17365	18828	20249	21643	23051	24416
48 1/2		12408	14098	15747	17382	18990	20593	22149	23677	25219	26715
50 1/2		13513	15355	17153	18936	20689	22437	24135	25802	27485	29117
52 1/2		14666	16666	18620	20556	22462	24360	26207	28019	29848	31623
54 1/2		15866	18031	20147	22244	24307	26364	28365	30328	32310	34234
56 1/2		17114	19450	21735	23998	26226	28446	30608	32728	34870	36948
58 1/2		18409	20923	23383	25819	28217	30608	32938	35221	37528	39767
60 1/2		19751	22450	25091	27707	30282	32850	35353	37805	40284	42689
62 1/2		21141	24032	26860	29662	32420	35171	37853	40482	43137	45715
64 1/2		22579	25667	28690	31684	34632	37572	40440	43250	46089	48846
66 1/2		24064	27356	30580	33772	36916	40052	43112	46110	49139	52080
68 1/2		25596	29099	32530	35928	39274	42612	45870	49061	52287	55419
70 1/2		27176	30896	34541	38150	41705	45251	48714	52105	55532	58861
72 1/2		28803	32747	36613	40440	44209	47970	51644	55240	58876	62407
74 1/2		30478	34652	38745	42796	46787	50768	54659	58468	62318	66058
76 1/2		32200	36611	40937	45219	49437	53646	57760	61787	65858	69812
78 1/2		33969	38625	43190	47709	52161	56603	60947	65198	69495	73671
80 1/2		35786	40692	45503	50266	54958	59640	64220	68700	73231	77633
82 1/2		37651	42813	47877	52889	57828	62757	67578	72295	77065	81699
84 1/2		39562	44988	50312	55800	60771	65953	71022	75981	80997	85870
90 1/2		45583	51837	57977	64053	70041	76017	81869	87592	93380	99005
96 1/2		52030	59173	66188	73128	79969	86798	93488	100029	106645	113076
102 1/2		58904	66994	74942	82805	90556	98294	105878	113292	120792	128083
108 1/2		66205	75301	84241	93084	101802	110506	119041	127382	135822	144027
114 1/2		73933	84095	94084	103964	113706	123434	132975	142299	151733	160906
t"		I Axis Y - Y									
0"		299.3	342.0	386.0	428.8	471.4	514.3	559.3	602.1	645.3	688.3
3/8		321.9	367.9	415.5	461.5	507.6	553.8	602.5	648.6	695.3	741.8
7/16		325.8	372.4	420.6	467.2	513.8	560.7	610.0	656.7	704.0	751.1
1/2		329.8	377.0	425.7	473.0	520.2	567.6	617.5	664.9	712.8	760.5
5/8		337.9	386.3	436.3	484.7	533.1	581.8	632.9	681.5	730.6	779.5
3/4		346.2	395.8	447.0	496.7	546.3	596.2	648.6	698.4	748.8	799.0
7/8		354.7	405.5	458.0	508.9	559.8	611.0	664.7	715.8	767.4	818.8
1"		363.3	415.4	469.2	521.4	573.5	626.0	681.1	733.4	786.4	839.1
1 1/8		372.1	425.5	480.7	534.2	587.5	641.4	697.8	751.5	805.8	859.8
1 1/4		381.2	435.9	492.4	547.2	601.9	657.1	714.9	769.9	825.5	880.9
1 1/2		399.8	457.2	516.5	574.0	631.4	689.3	750.0	807.7	866.2	924.2



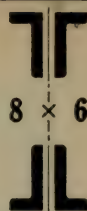
MOMENTS OF INERTIA OF FOUR ANGLES

UNEQUAL LEG ANGLES—LONG LEGS BACK TO BACK

AXIS X - X for distances measured from back to back.

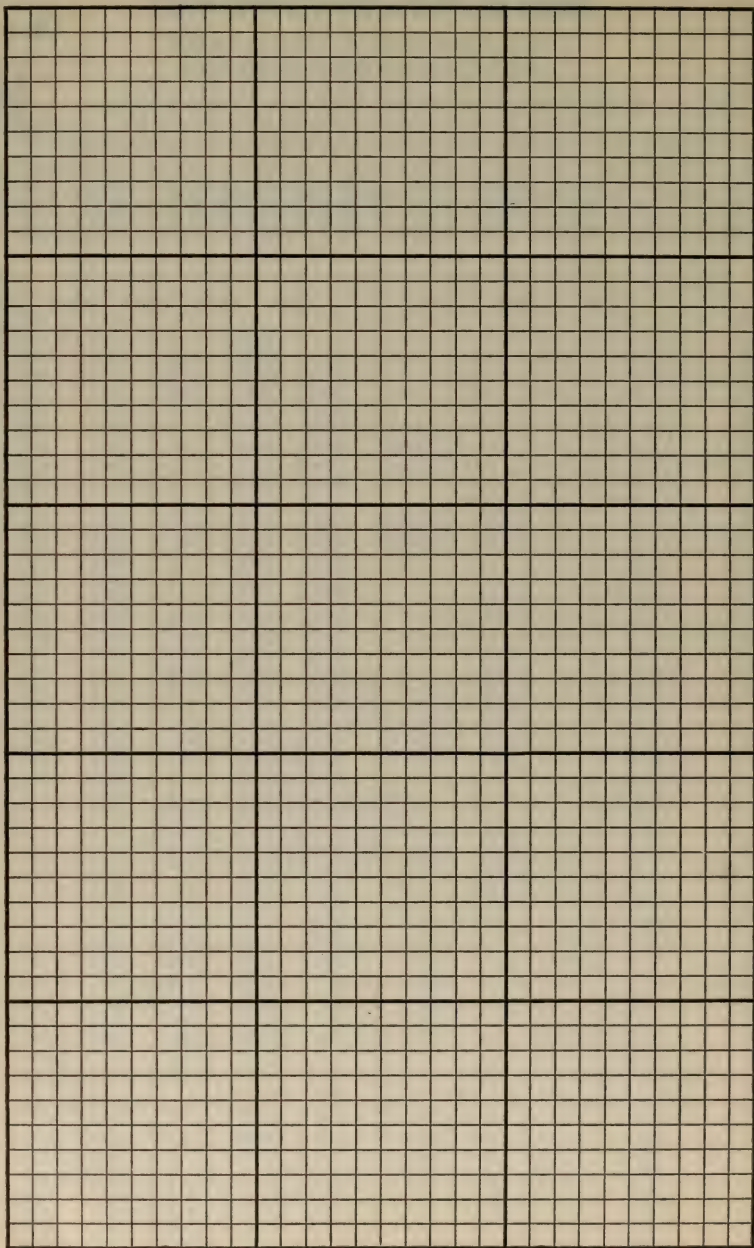
AXIS Y - Y for various thicknesses of web plates.

To find the approximate Moment of Inertia of the Net Area multiply the Tabular Value by the Net Area and divide by the Gross Area.

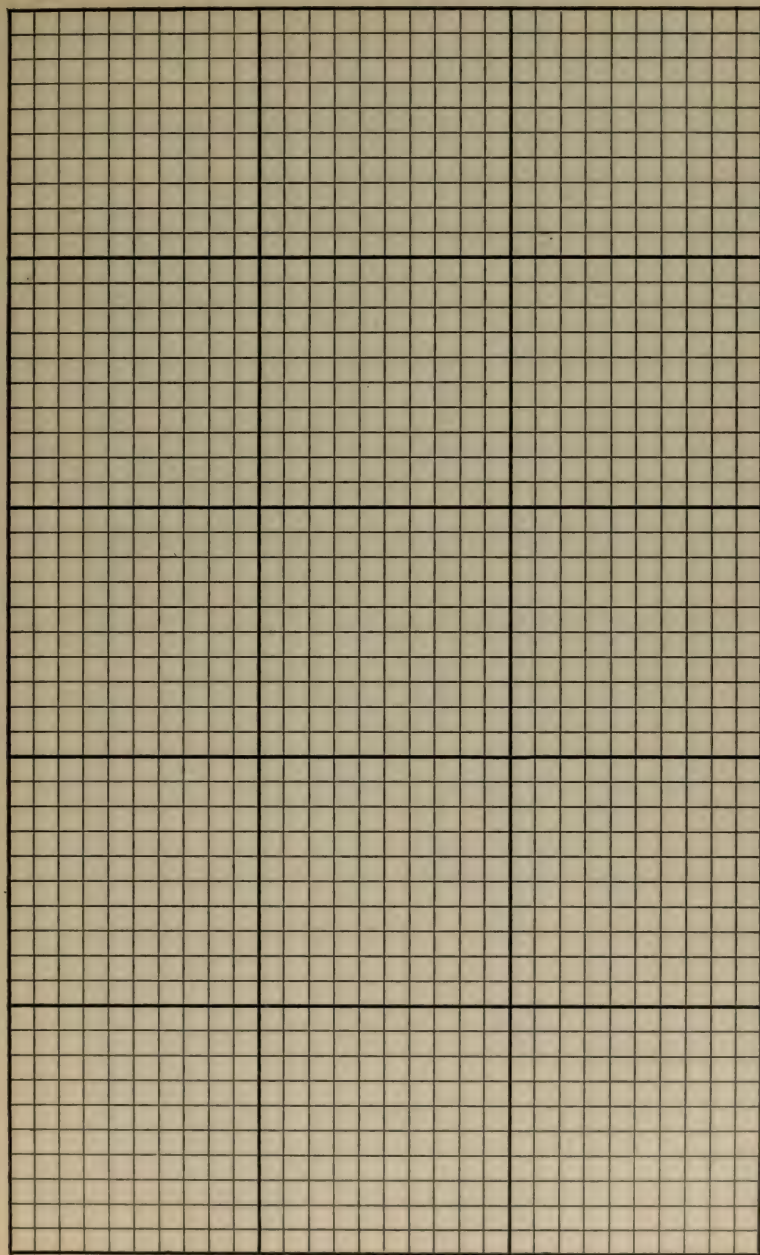


Size		8" × 6"									
Thickness		7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"
4	Area	23.72	27.00	30.24	33.44	36.60	39.76	42.88	45.92	49.00	52.00
L's	Weight	80.8	92.0	102.8	114.0	124.8	135.2	146.0	156.4	166.8	176.8
d"		I Axis X - X									
16 1/2		955	1079	1197	1314	1429	1541	1645	1750	1854	1954
18 1/2		1254	1418	1575	1731	1883	2033	2174	2314	2454	2588
20 1/2		1600	1812	2013	2215	2411	2605	2788	2970	3152	3327
22 1/2		1994	2259	2512	2765	3012	3256	3488	3717	3947	4169
24 1/2		2435	2760	3072	3382	3686	3987	4273	4557	4841	5115
26 1/2		2924	3315	3692	4066	4433	4797	5144	5488	5833	6166
28 1/2		3460	3924	4372	4818	5254	5687	6101	6511	6923	7320
30 1/2		4043	4587	5113	5635	6148	6656	7144	7626	8110	8579
32 1/2		4674	5304	5914	6520	7115	7705	8273	8833	9396	9941
34 1/2		5353	6075	6776	7472	8155	8834	9487	10131	10780	11407
36 1/2		6078	6900	7698	8491	9268	10042	10787	11522	12262	12978
38 1/2		6852	7780	8681	9576	10455	11329	12173	13004	13841	14652
40 1/2		7672	8713	9725	10728	11715	12696	13645	14578	15519	16431
42 1/2		8540	9700	10828	11948	13048	14143	15202	16244	17295	18313
44 1/2		9456	10741	11993	13234	14454	15668	16845	18002	19169	20299
46 1/2		10419	11836	13217	14587	15933	17274	18574	19852	21140	22390
48 1/2		11430	12985	14502	16007	17486	18959	20389	21793	23210	24584
50 1/2		12487	14188	15848	17493	19111	20734	22290	23827	25378	26883
52 1/2		13593	15445	17254	19047	20810	22568	24277	25952	27644	29285
54 1/2		14746	16757	18721	20667	22583	24491	26349	28169	30007	31791
56 1/2		15946	18122	20248	22355	24428	26494	28506	30478	32469	34402
58 1/2		17194	19541	21836	24109	26347	28577	30750	32878	35029	37116
60 1/2		18489	21014	23484	25930	28338	30739	33079	35371	37687	39935
62 1/2		19831	22541	25192	27818	30403	32981	35494	37955	40442	42857
64 1/2		21221	24122	26961	29773	32541	35302	37995	40631	43296	45883
66 1/2		22659	25757	28791	31795	34753	37703	40581	43400	46248	49014
68 1/2		24143	27446	30681	33884	37037	40183	43254	46259	49298	52248
70 1/2		25676	29190	32631	36039	39395	42743	46012	49211	52446	55587
72 1/2		27256	30987	34642	38261	41826	45382	48856	52255	55691	59029
74 1/2		28883	32838	36714	40551	44330	48101	51785	55390	59035	62675
76 1/2		30557	34743	38846	42907	46908	50899	54800	58617	62477	66226
78 1/2		32279	36702	41038	45330	49558	53777	57901	61937	66017	69980
80 1/2		34049	38715	43291	47820	52282	56734	61088	65347	69654	73839
82 1/2		35866	40782	45604	50377	55079	59771	64361	68850	73390	77801
84 1/2		37730	42903	47978	53000	57949	62887	67719	72445	77224	81867
90 1/2		43608	49591	55463	61273	66999	72714	78309	83780	89313	94691
96 1/2		49913	56764	63491	70147	76707	83256	89670	95941	102284	108450
102 1/2		56645	64423	72064	79623	87075	94513	101804	108929	116138	123145
108 1/2		63803	72569	81182	89702	98101	106487	114709	122744	130873	138776
114 1/2		71389	81200	90843	100382	109786	119176	128386	137385	146490	155343
120 1/2		79402	90318	101049	111664	122129	132580	142835	152853	162990	172847
t"		I Axis Y - Y									
0"		126.9	145.1	164.2	182.6	201.0	219.6	239.7	258.5	277.6	296.7
3/8		140.6	160.9	182.3	202.8	223.5	244.3	266.8	287.8	309.3	330.7
7/16		143.0	163.7	185.5	206.4	227.4	248.7	271.7	293.0	314.9	336.7
1/2		145.5	166.6	188.8	210.1	231.5	253.2	276.5	298.3	320.6	342.8
5/8		150.7	172.5	195.5	217.6	239.8	262.3	286.5	309.1	332.3	355.4
3/4		156.0	178.6	202.5	225.4	248.5	271.8	296.8	320.4	344.4	368.4
7/8		161.5	184.9	209.7	233.5	257.4	281.6	307.5	331.9	356.9	381.7
1"		167.2	191.5	217.1	241.8	266.6	291.6	318.6	343.9	369.7	395.5
1 1/8		173.0	198.3	224.8	250.4	276.0	302.1	330.0	356.1	382.9	409.6
1 1/4		179.1	205.2	232.7	259.2	285.8	312.7	341.7	368.8	396.6	424.3
1 1/2		191.8	219.8	249.3	277.6	306.2	335.0	366.1	395.2	425.0	454.6

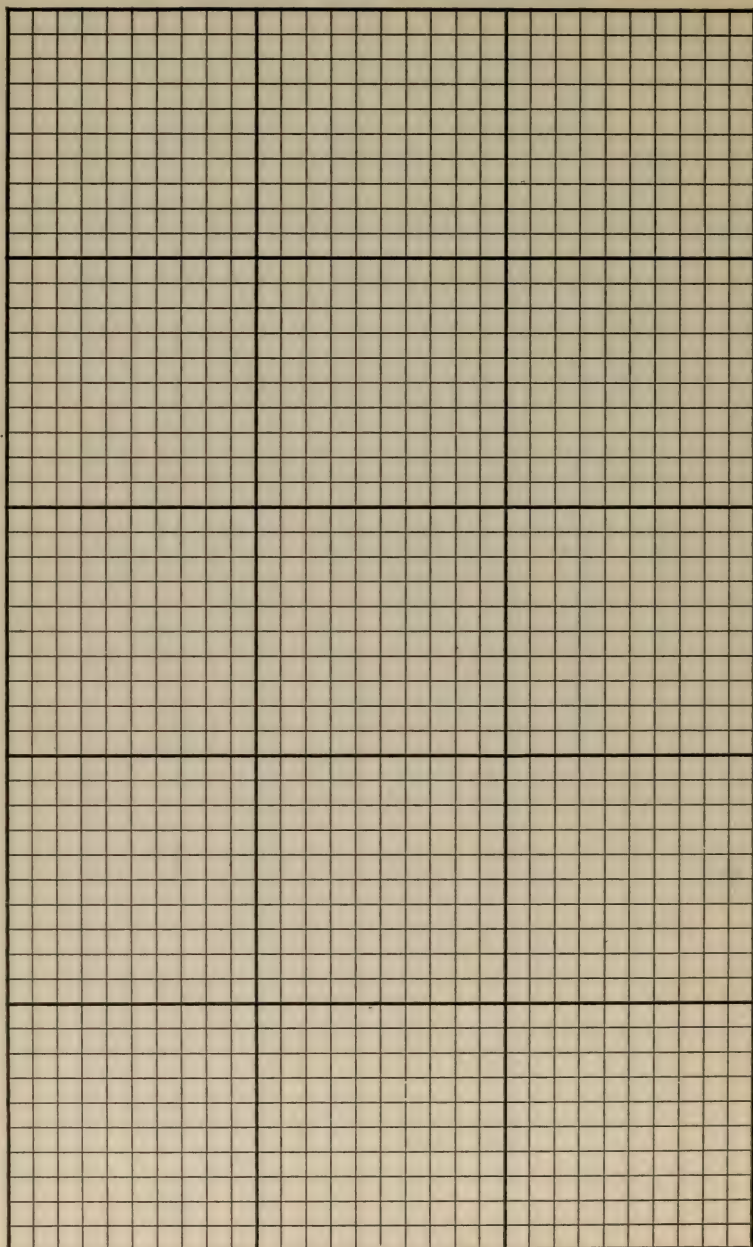
NOTES and DIAGRAMS



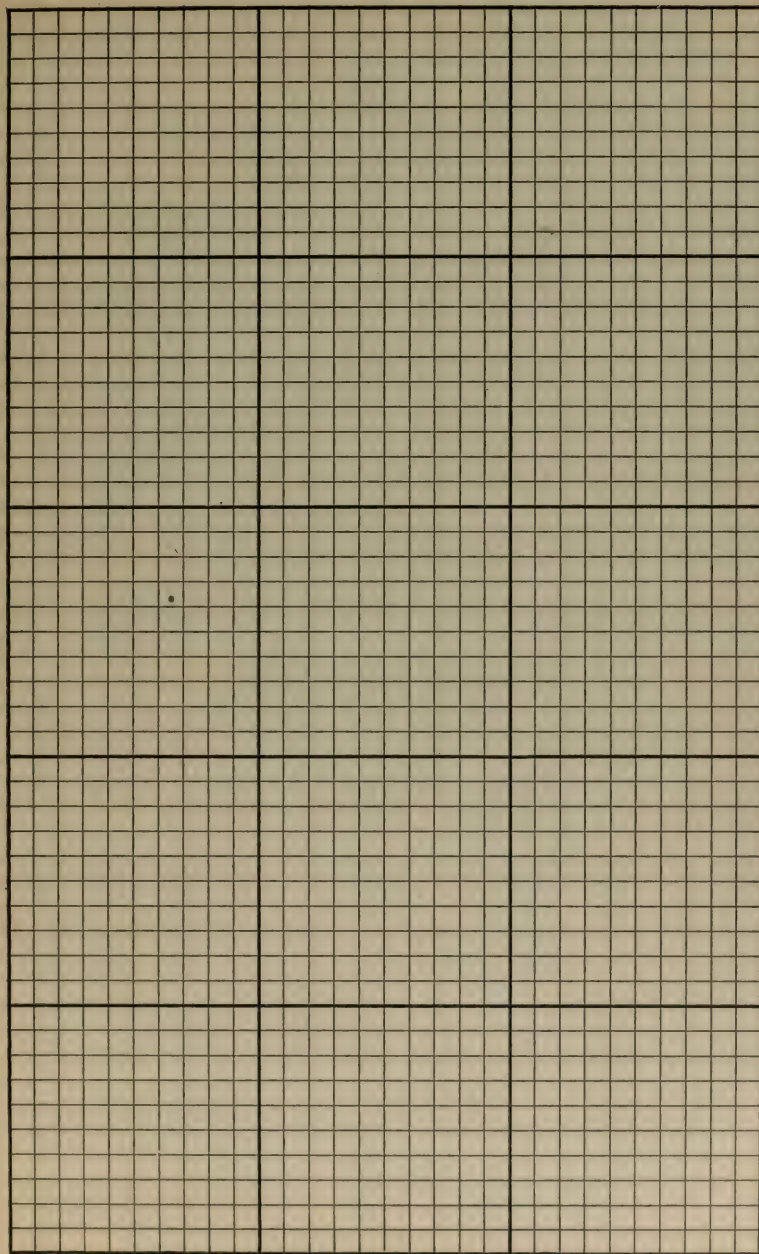
NOTES and DIAGRAMS



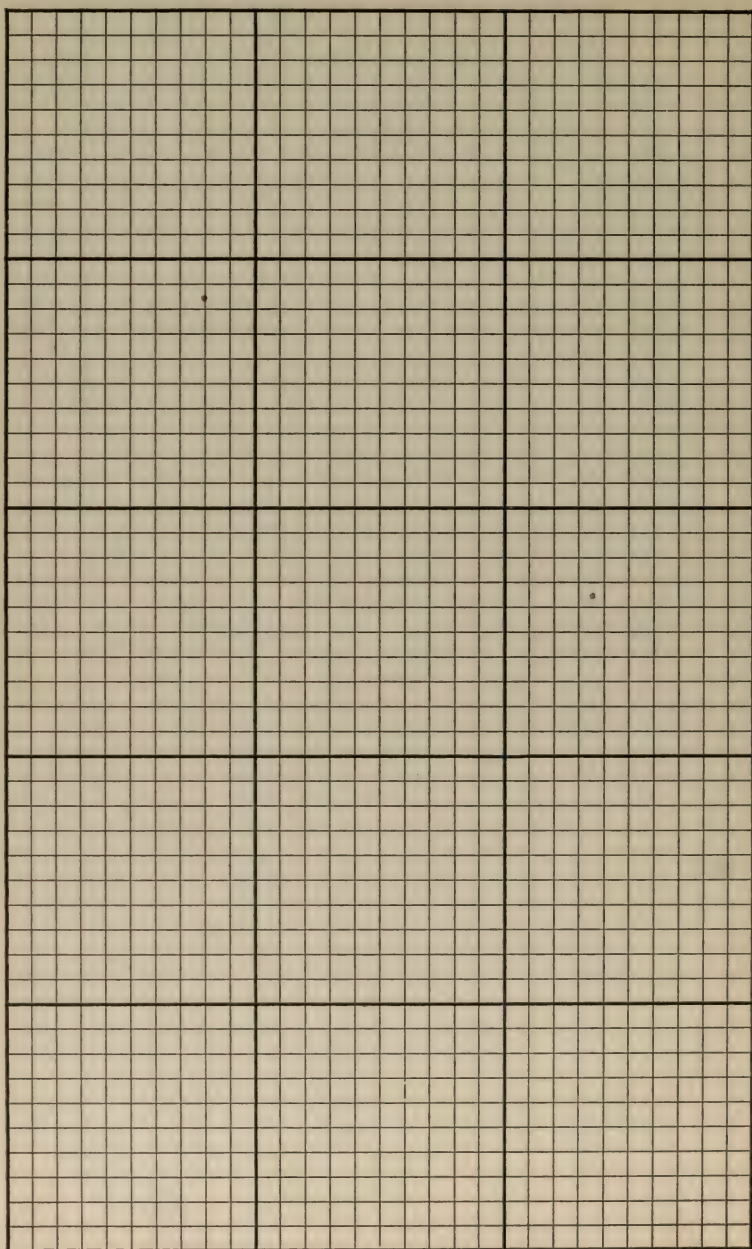
NOTES and DIAGRAMS



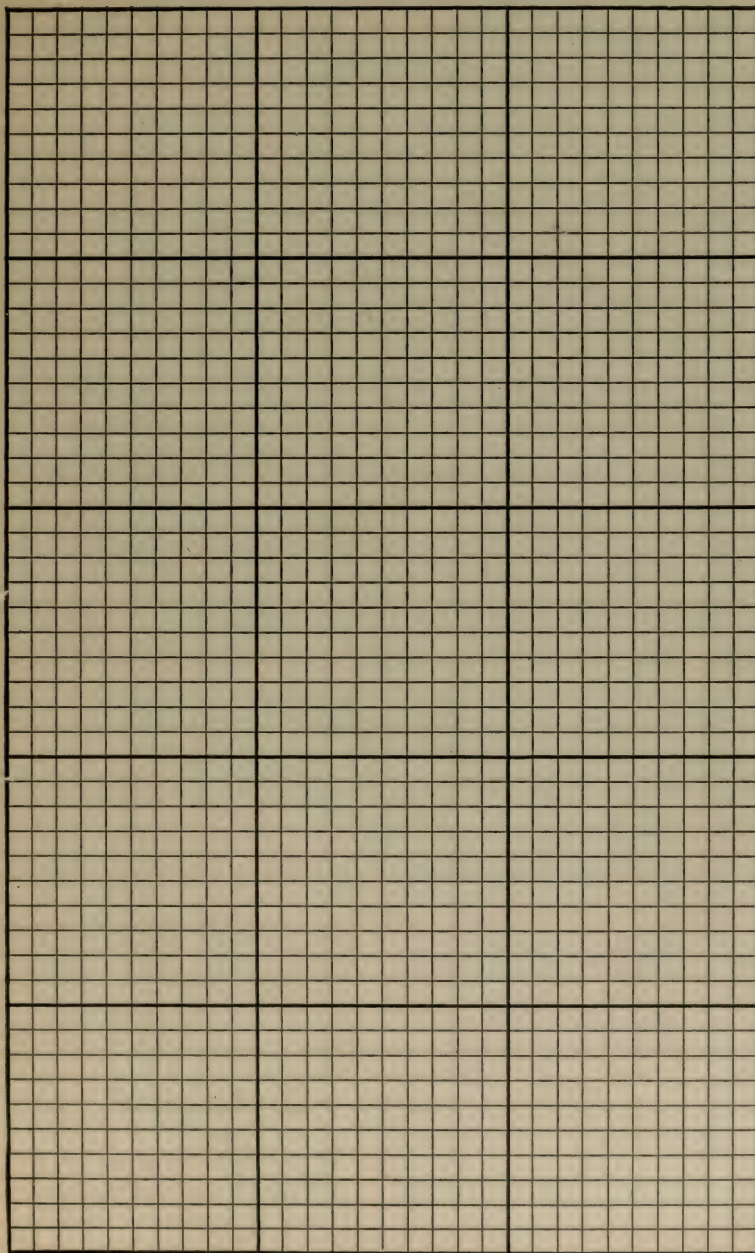
NOTES and DIAGRAMS



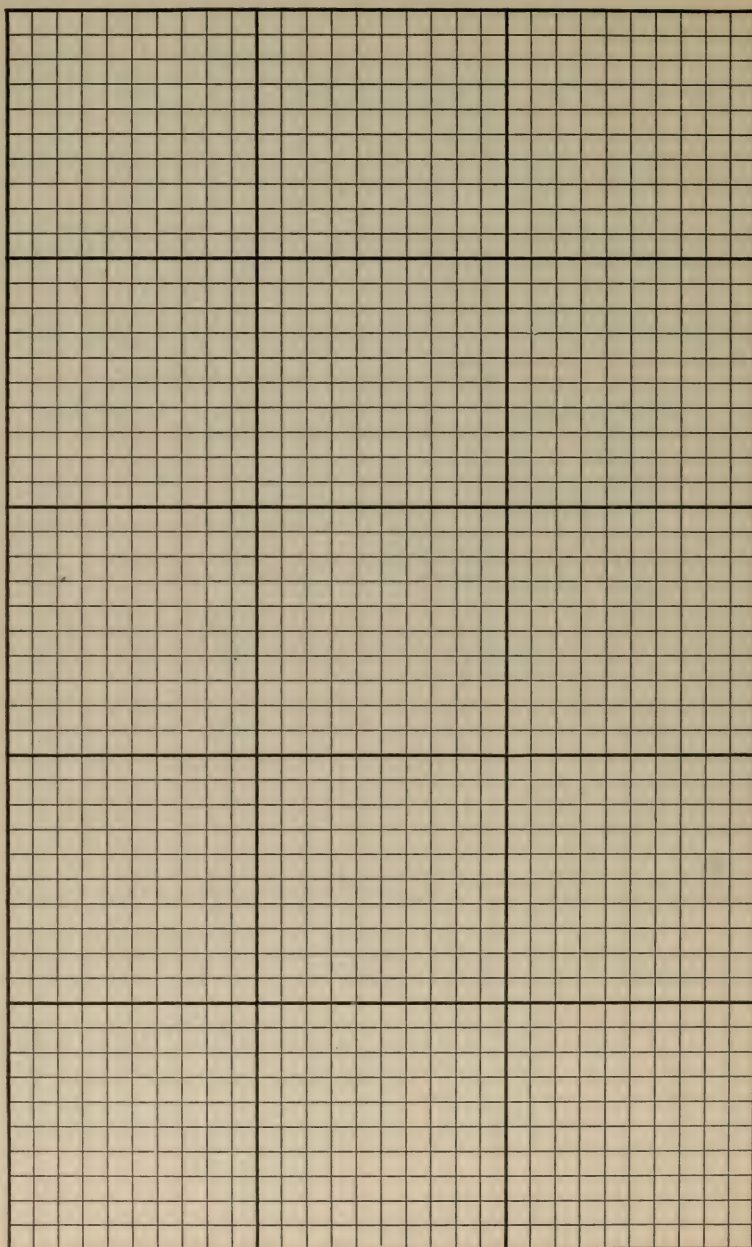
NOTES and DIAGRAMS



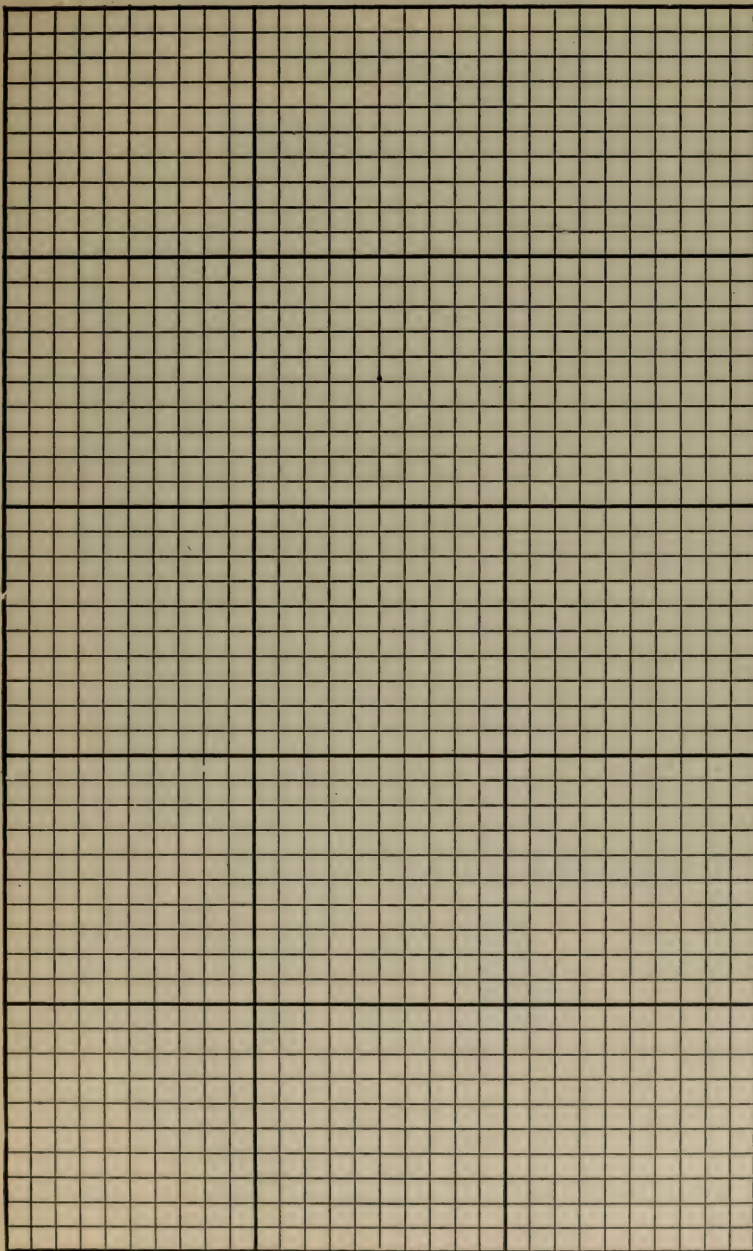
NOTES and DIAGRAMS



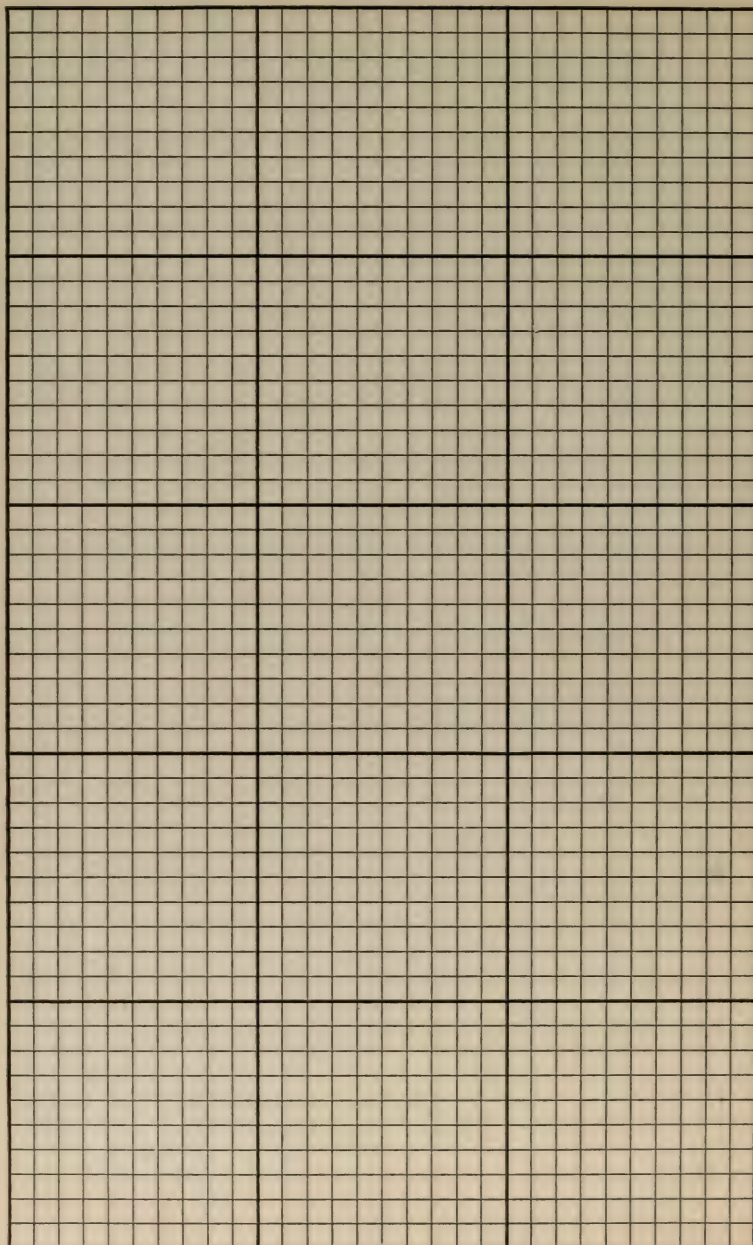
NOTES and DIAGRAMS



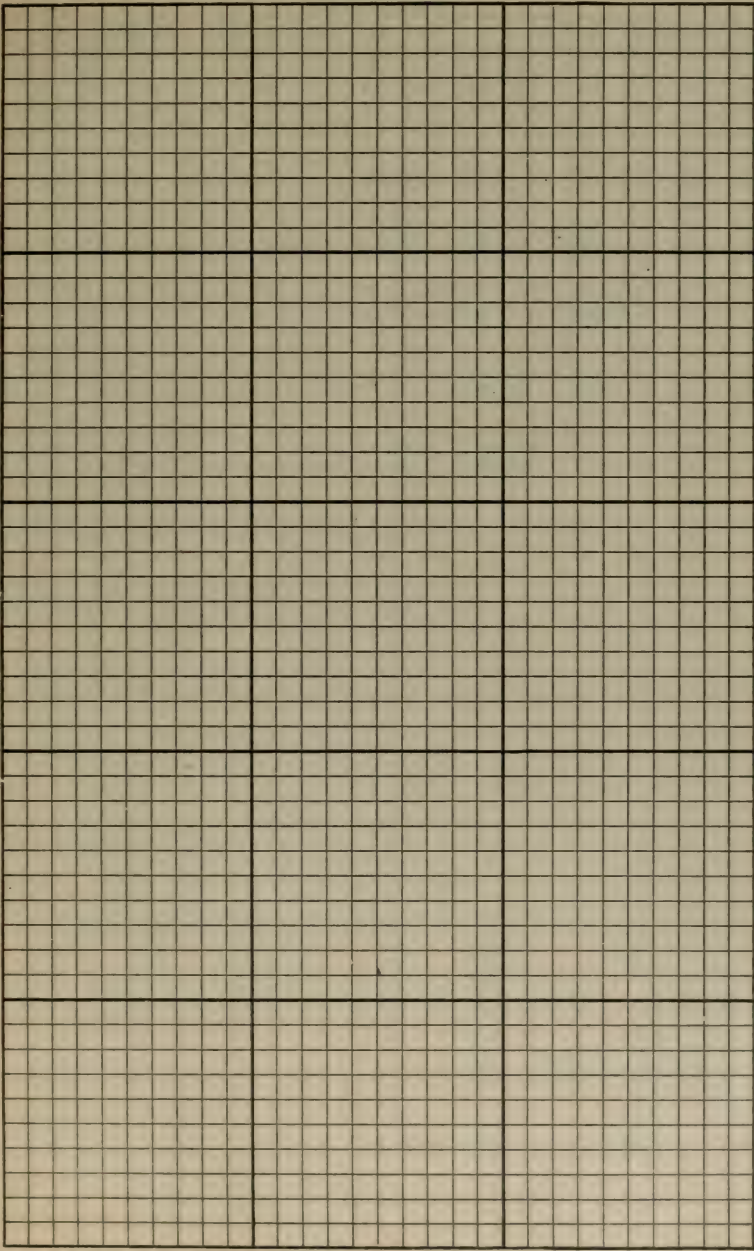
NOTES and DIAGRAMS



NOTES and DIAGRAMS



NOTES and DIAGRAMMS



AREAS OF RECTANGULAR SECTIONS

SQUARE INCHES

Width, Inches	Thickness, Inches															
	1/16	1/8	3/16	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1
1/4	.016	.031	.047	.063	.078	.094	.109	.125	.141	.156	.172	.188	.203	.22	.23	.25
1/2	.031	.063	.094	.125	.156	.188	.219	.250	.281	.313	.344	.375	.406	.44	.47	.50
3/4	.047	.094	.141	.188	.234	.281	.328	.375	.422	.469	.516	.563	.609	.66	.70	.75
1	.063	.125	.188	.250	.313	.375	.438	.500	.563	.625	.688	.750	.813	.88	.94	1.00
1 1/4	.078	.156	.234	.313	.391	.469	.547	.625	.703	.781	.859	.938	1.016	1.09	1.17	1.25
1 1/2	.094	.188	.281	.375	.469	.563	.656	.750	.844	.938	1.031	1.125	1.219	1.31	1.41	1.50
1 3/4	.109	.219	.328	.438	.547	.656	.766	.875	.984	1.094	1.203	1.313	1.422	1.53	1.64	1.75
2	.125	.250	.375	.500	.625	.750	.875	1.000	1.125	1.250	1.375	1.500	1.625	1.75	1.88	2.00
2 1/4	.141	.281	.422	.563	.703	.844	.984	1.125	1.266	1.406	1.547	1.688	1.828	1.97	2.11	2.25
2 1/2	.156	.313	.469	.625	.781	.938	1.094	1.250	1.406	1.563	1.719	1.875	2.031	2.19	2.34	2.50
2 3/4	.172	.344	.516	.688	.859	1.031	1.203	1.375	1.547	1.719	1.891	2.063	2.234	2.41	2.58	2.75
3	.188	.375	.563	.750	.938	1.125	1.313	1.500	1.688	1.875	2.063	2.250	2.438	2.63	2.81	3.00
3 1/4	.203	.406	.609	.813	1.016	1.219	1.422	1.625	1.828	2.031	2.234	2.438	2.641	2.84	3.05	3.25
3 1/2	.219	.438	.656	.875	1.094	1.313	1.531	1.750	1.969	2.188	2.406	2.625	2.844	3.06	3.28	3.50
3 3/4	.234	.469	.703	.938	1.172	1.406	1.641	1.875	2.109	2.344	2.578	2.813	3.047	3.28	3.52	3.75
4	.250	.500	.750	1.000	1.250	1.500	1.750	2.000	2.250	2.500	2.750	3.000	3.250	3.50	3.75	4.00
4 1/4	.266	.531	.797	1.063	1.328	1.594	1.859	2.125	2.391	2.656	2.922	3.188	3.453	3.72	3.98	4.25
4 1/2	.281	.563	.844	1.125	1.406	1.688	1.969	2.250	2.531	2.813	3.094	3.375	3.656	3.94	4.22	4.50
4 3/4	.297	.594	.891	1.188	1.484	1.781	2.078	2.375	2.672	2.969	3.266	3.563	3.859	4.16	4.45	4.75
5	.313	.625	.938	1.250	1.563	1.875	2.188	2.500	2.813	3.125	3.438	3.750	4.063	4.38	4.69	5.00
5 1/4	.328	.656	.984	1.313	1.641	1.969	2.297	2.625	2.953	3.281	3.609	3.938	4.266	4.59	4.92	5.25
5 1/2	.344	.688	1.031	1.375	1.719	2.063	2.406	2.750	3.094	3.438	3.781	4.125	4.469	4.81	5.16	5.50
5 3/4	.359	.719	1.078	1.438	1.797	2.156	2.516	2.875	3.234	3.594	3.953	4.313	4.672	5.03	5.39	5.75
6	.375	.750	1.125	1.500	1.875	2.250	2.625	3.000	3.375	3.750	4.125	4.500	4.875	5.25	5.63	6.00
6 1/4	.391	.781	1.172	1.563	1.953	2.344	2.734	3.125	3.516	3.906	4.297	4.688	5.078	5.47	5.86	6.25
6 1/2	.406	.813	1.219	1.625	2.031	2.438	2.844	3.250	3.656	4.063	4.469	4.875	5.281	5.69	6.09	6.50
6 3/4	.422	.844	1.266	1.688	2.109	2.531	2.953	3.375	3.797	4.219	4.641	5.063	5.484	5.91	6.33	6.75
7	.438	.875	1.313	1.750	2.188	2.625	3.063	3.500	3.938	4.375	4.813	5.250	5.688	6.13	6.56	7.00
7 1/4	.453	.906	1.359	1.813	2.266	2.719	3.172	3.625	4.078	4.531	4.984	5.438	5.891	6.34	6.80	7.25
7 1/2	.469	.938	1.406	1.875	2.344	2.813	3.281	3.750	4.219	4.688	5.156	5.625	6.094	6.56	7.03	7.50
7 3/4	.484	.969	1.453	1.938	2.422	2.906	3.391	3.875	4.359	4.844	5.328	5.813	6.297	6.78	7.27	7.75
8	.500	1.000	1.500	2.000	2.500	3.000	3.500	4.000	4.500	5.000	5.500	6.000	6.500	7.00	7.50	8.00
8 1/4	.516	1.031	1.547	2.063	2.578	3.094	3.609	4.125	4.641	5.156	5.672	6.188	6.703	7.22	7.73	8.25
8 1/2	.531	1.063	1.594	2.125	2.656	3.188	3.719	4.250	4.781	5.313	5.844	6.375	6.906	7.44	7.97	8.50
8 3/4	.547	1.094	1.641	2.188	2.734	3.281	3.828	4.375	4.922	5.469	6.016	6.563	7.109	7.66	8.20	8.75
9	.563	1.125	1.688	2.250	2.813	3.375	3.938	4.500	5.063	5.625	6.188	6.750	7.313	7.88	8.44	9.00
9 1/4	.578	1.156	1.734	2.313	2.891	3.469	4.047	4.625	5.203	5.781	6.359	6.938	7.516	8.09	8.67	9.25
9 1/2	.594	1.188	1.781	2.375	2.969	3.563	4.156	4.750	5.344	5.938	6.531	7.125	7.719	8.31	8.91	9.50
9 3/4	.609	1.219	1.828	2.438	3.047	3.656	4.266	4.875	5.484	6.094	6.703	7.313	7.922	8.53	9.14	9.75
10	.625	1.250	1.875	2.500	3.125	3.750	4.375	5.000	5.625	6.250	6.875	7.500	8.125	8.75	9.38	10.00
10 1/4	.641	1.281	1.922	2.563	3.203	3.844	4.484	5.125	5.766	6.406	7.047	7.688	8.328	8.97	9.61	10.25
10 1/2	.656	1.313	1.969	2.625	3.281	3.938	4.594	5.250	5.906	6.563	7.219	7.875	8.531	9.19	9.84	10.50
10 3/4	.672	1.344	2.016	2.688	3.359	4.031	4.703	5.375	6.047	6.719	7.391	8.063	8.734	9.41	10.08	10.75
11	.688	1.375	2.063	2.750	3.438	4.125	4.813	5.500	6.188	6.875	7.563	8.250	8.938	9.63	10.31	11.00
11 1/4	.703	1.406	2.109	2.813	3.516	4.219	4.922	5.625	6.328	7.031	7.734	8.438	9.141	9.84	10.55	11.25
11 1/2	.719	1.438	2.156	2.875	3.594	4.313	5.031	5.750	6.469	7.188	7.906	8.625	9.344	10.06	10.78	11.50
11 3/4	.734	1.469	2.203	2.938	3.672	4.406	5.141	5.875	6.609	7.344	8.078	8.813	9.547	10.28	11.02	11.75
12	.750	1.500	2.250	3.000	3.750	4.500	5.250	6.000	6.750	7.500	8.250	9.000	9.750	10.50	11.25	12.00
12 1/4	.766	1.531	2.344	3.13	3.91	4.69	5.47	6.25	7.03	7.81	8.59	9.38	10.16	10.94	11.72	12.50
12 1/2	.781	1.563	2.438	3.25	4.06	4.88	5.69	6.50	7.31	8.13	8.94	9.75	10.56	11.38	12.19	13.00
12 3/4	.797	1.594	2.479	3.313	4.125	4.969	5.781	6.594	7.406	8.219	9.031	9.844	10.656	11.469	12.281	13.09
13	.813	1.625	2.531	3.38	4.22	5.06	5.91	6.72	7.53	8.34	9.15	9.96	10.78	11.59	12.40	13.21
13 1/4	.828	1.656	2.563	3.438	4.281	5.125	5.984	6.797	7.609	8.422	9.234	10.047	10.859	11.672	12.519	13.338
13 1/2	.844	1.688	2.625	3.50	4.38	5.25	6.13	7.00	7.88	8.75	9.63	10.50	11.38	12.25	13.13	14.00
13 3/4	.859	1.719	2.656	3.563	4.438	5.313	6.188	7.063	7.938	8.813	9.688	10.563	11.438	12.313	13.188	14.063
14	.875	1.750	2.750	3.63	4.53	5.44	6.34	7.25	8.16	9.06	9.97	10.88	11.78	12.69	13.59	14.50
14 1/4	.906	1.813	2.719	3.63	4.53	5.44	6.34	7.25	8.16	9.06	9.97	10.88	11.78	12.69	13.59	14.50
14 1/2	.938	1.875	2.813	3.75	4.69	5.63	6.56	7.50	8.44	9.38	10.31	11.25	12.19	13.13	14.06	15.00
14 3/4	.969	1.938	2.906	3.88	4.84	5.81	6.78	7.75	8.72	9.69	10.66	11.63	12.59	13.56	14.53	15.50
16	1.000	2.000	3.000	4.00	5.00	6.00	7.00	8.00	9.00	10.00	11.00	12.00	13.00	14.00	15.00	16.00
16 1/4	1.031	2.063	3.094	4.13	5.16	6.19	7.22	8.25	9.28	10.31	11.34	12.38	13.41	14.44	15.47	16.50
16 1/2	1.063	2.125	3.188	4.25	5.31	6.38	7.44	8.50	9.56	10.63	11.69	12.75	13.81	14.88	15.94	17.00
16 3/4	1.094	2.188	3.281	4.38	5.47	6.56	7.66	8.75	9.84	10.94	12.03	13.13	14.22	15.31	16.41	17.50
18	1.125	2.250	3.375	4.50	5.63	6.75	7.88	9.00	10.13	11.25	12.38	13.50	14.63	15.75	16.88	18.00
18 1/4	1.156	2.313	3.469	4.63	5.78	6.94	8.09	9.25	10.41	11.56	12.72	13.88	15.03	16.19	17.34	18.50
18 1/2	1.188	2.375	3.563	4.75	5.94	7.13	8.31	9.50	10.69	11.88	13.06	14.25	15.44	16.63	17.81	19.00
19	1.219	2.438	3.656	4.88	6.09	7.31	8.53	9.75	10.97	12.19	13.41	14.63	15.84	17.06	18.28	19.50
20	1.250	2.500	3.750	5.00	6.25											

AREAS OF RECTANGULAR SECTIONS

SQUARE INCHES

Width, Inches	Thickness, Inches															
	1/16	1/8	3/16	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1
22 1/2	1.406	2.813	4.219	5.63	7.03	8.44	9.84	11.25	12.66	14.06	15.47	16.88	18.28	19.69	21.09	22.50
23	1.438	2.875	4.313	5.75	7.19	8.63	10.06	11.50	12.94	14.38	15.81	17.25	18.69	20.13	21.56	23.00
23 1/2	1.469	2.938	4.406	5.88	7.34	8.81	10.28	11.75	13.22	14.69	16.16	17.63	19.09	20.56	22.03	23.50
24	1.500	3.000	4.500	6.00	7.50	9.00	10.50	12.00	13.50	15.00	16.50	18.00	19.50	21.00	22.50	24.00
25	1.563	3.125	4.688	6.25	7.81	9.38	10.94	12.50	14.06	15.63	17.19	18.75	20.31	21.88	23.44	25.00
26	1.625	3.250	4.875	6.50	8.13	9.75	11.38	13.00	14.63	16.25	17.88	19.50	21.13	22.75	24.38	26.00
27	1.688	3.375	5.063	6.75	8.44	10.13	11.81	13.50	15.19	16.88	18.56	20.25	21.93	23.63	25.31	27.00
28	1.750	3.500	5.250	7.00	8.75	10.50	12.25	14.00	15.75	17.50	19.25	21.00	22.75	24.50	26.25	28.00
29	1.813	3.625	5.438	7.25	9.06	10.88	12.69	14.50	16.31	18.13	19.94	21.75	23.56	25.38	27.19	29.00
30	1.875	3.750	5.625	7.50	9.38	11.25	13.13	15.00	16.88	18.75	20.63	22.50	24.38	26.25	28.13	30.00
31	1.938	3.875	5.813	7.75	9.69	11.63	13.56	15.50	17.44	19.38	21.31	23.25	25.19	27.13	29.06	31.00
32	2.000	4.000	6.000	8.00	10.00	12.00	14.00	16.00	18.00	20.00	22.00	24.00	26.00	28.00	30.00	32.00
33	2.063	4.125	6.188	8.25	10.31	12.38	14.44	16.50	18.56	20.63	22.69	24.75	26.81	28.88	30.94	33.00
34	2.125	4.250	6.375	8.50	10.63	12.75	14.88	17.00	19.13	21.25	23.38	25.50	27.63	29.75	31.88	34.00
35	2.188	4.375	6.563	8.75	10.94	13.13	15.31	17.50	19.69	21.88	24.06	26.25	28.44	30.63	32.81	35.00
36	2.250	4.500	6.750	9.00	11.25	13.50	15.75	18.00	20.25	22.50	24.75	27.00	29.25	31.50	33.75	36.00
37	2.313	4.625	6.938	9.25	11.56	13.88	16.19	18.50	20.81	23.13	25.44	27.75	30.06	32.38	34.69	37.00
38	2.375	4.750	7.125	9.50	11.88	14.25	16.63	19.00	21.38	23.75	26.13	28.50	30.88	33.25	35.63	38.00
39	2.438	4.875	7.313	9.75	12.19	14.63	17.06	19.25	21.94	24.38	26.81	29.25	31.69	34.13	36.56	39.00
40	2.500	5.000	7.500	10.00	12.50	15.00	17.50	20.00	22.50	25.00	27.50	30.00	32.50	35.00	37.50	40.00
41	2.563	5.125	7.688	10.25	12.81	15.38	17.94	20.50	23.06	25.63	28.19	30.75	33.31	35.88	38.44	41.00
42	2.625	5.250	7.875	10.50	13.13	15.75	18.38	21.00	23.63	26.25	28.88	31.50	34.13	36.75	39.38	42.00
43	2.688	5.375	8.063	10.75	13.44	16.13	18.81	21.50	24.19	26.88	29.56	32.25	34.94	37.63	40.31	43.00
44	2.750	5.500	8.250	11.00	13.75	16.50	19.25	22.00	24.75	27.50	30.25	33.00	35.75	38.50	41.25	44.00
45	2.813	5.625	8.438	11.25	14.06	16.88	19.69	22.50	25.31	28.13	30.94	33.75	36.56	39.38	42.19	45.00
46	2.875	5.750	8.625	11.50	14.38	17.25	20.13	23.00	25.88	28.75	31.63	34.50	37.38	40.25	43.13	46.00
47	2.938	5.875	8.813	11.75	14.69	17.63	20.56	23.50	26.44	29.38	32.31	35.25	38.19	41.13	44.06	47.00
48	3.000	6.000	9.000	12.00	15.00	18.00	21.00	24.00	27.00	30.00	33.00	36.00	39.00	42.00	45.00	48.00
49	3.06	6.13	9.19	12.25	15.31	18.38	21.44	24.50	27.56	30.63	33.69	36.75	39.81	42.88	45.94	49.00
50	3.13	6.25	9.38	12.50	15.63	18.75	21.88	25.00	28.13	31.25	34.38	37.50	40.63	43.75	46.88	50.00
51	3.19	6.38	9.56	12.75	15.94	19.13	22.31	25.50	28.69	31.88	35.06	38.25	41.44	44.63	47.81	51.00
52	3.25	6.50	9.75	13.00	16.25	19.50	22.75	26.00	29.25	32.50	35.75	39.00	42.25	45.50	48.75	52.00
53	3.31	6.63	9.94	13.25	16.56	19.88	23.19	26.50	29.81	33.13	36.44	39.75	43.06	46.38	49.69	53.00
54	3.38	6.75	10.13	13.50	16.88	20.25	23.63	27.00	30.38	33.75	37.13	40.50	43.88	47.25	50.63	54.00
55	3.44	6.88	10.31	13.75	17.19	20.63	24.06	27.50	30.94	34.38	37.81	41.25	44.69	48.13	51.56	55.00
56	3.50	7.00	10.50	14.00	17.50	21.00	24.50	28.00	31.50	35.00	38.50	42.00	45.50	49.00	52.50	56.00
57	3.56	7.13	10.69	14.25	17.81	21.38	24.94	28.50	32.06	35.63	39.19	42.75	46.31	49.88	53.44	57.00
58	3.63	7.25	10.88	14.50	18.13	21.75	25.38	29.00	32.63	36.25	39.88	43.50	47.13	50.75	54.38	58.00
59	3.69	7.38	11.06	14.75	18.44	22.13	25.81	29.50	33.19	36.88	40.56	44.25	47.94	51.63	55.31	59.00
60	3.75	7.50	11.25	15.00	18.75	22.50	26.25	30.00	33.75	37.50	41.25	45.00	48.75	52.50	56.25	60.00
61	3.81	7.63	11.44	15.25	19.06	22.88	26.69	30.50	34.31	38.13	41.94	45.75	49.56	53.38	57.19	61.00
62	3.88	7.75	11.63	15.50	19.38	23.25	27.13	31.00	34.88	38.75	42.63	46.50	50.38	54.25	58.13	62.00
63	3.94	7.88	11.81	15.75	19.69	23.63	27.56	31.50	35.44	39.38	43.31	47.25	51.19	55.13	59.06	63.00
64	4.00	8.00	12.00	16.00	20.00	24.00	28.00	32.00	36.00	40.00	44.00	48.00	52.00	56.00	60.00	64.00
65	4.06	8.13	12.19	16.25	20.31	24.38	28.44	32.50	36.56	40.63	44.69	48.75	52.81	56.88	60.94	65.00
66	4.13	8.25	12.38	16.50	20.63	24.75	28.88	33.00	37.13	41.25	45.38	49.50	53.63	57.75	61.88	66.00
67	4.19	8.38	12.56	16.75	20.94	25.13	29.31	33.50	37.69	41.88	46.06	50.25	54.44	58.63	62.81	67.00
68	4.25	8.50	12.75	17.00	21.25	25.50	29.75	34.00	38.25	42.50	46.75	51.00	55.25	59.50	63.75	68.00
69	4.31	8.63	12.94	17.25	21.56	25.88	30.19	34.50	38.81	43.13	47.44	51.75	56.06	60.38	64.69	69.00
70	4.38	8.75	13.13	17.50	21.88	26.25	30.63	35.00	39.38	43.75	48.13	52.50	56.88	61.25	65.63	70.00
71	4.44	8.88	13.31	17.75	22.19	26.63	31.06	35.50	39.94	44.38	48.81	53.25	57.69	62.13	66.56	71.00
72	4.50	9.00	13.50	18.00	22.50	27.00	31.50	36.00	40.50	45.00	49.50	54.00	58.50	63.00	67.50	72.00
73	4.56	9.13	13.69	18.25	22.81	27.38	31.94	36.50	41.06	45.63	50.19	54.75	59.31	63.88	68.44	73.00
74	4.63	9.25	13.88	18.50	23.13	27.75	32.38	37.00	41.63	46.25	50.88	55.50	60.13	64.75	69.38	74.00
75	4.69	9.38	14.06	18.75	23.44	28.13	32.81	37.50	42.19	46.88	51.56	56.25	60.94	65.63	70.31	75.00
76	4.75	9.50	14.25	19.00	23.75	28.50	33.25	38.00	42.75	47.50	52.25	57.00	61.75	66.50	71.25	76.00
78	4.88	9.75	14.63	19.50	24.38	29.25	34.13	39.00	43.88	48.75	53.63	58.50	63.38	68.25	73.13	78.00
80	5.00	10.00	15.00	20.00	25.00	30.00	35.00	40.00	45.00	50.00	55.00	60.00	65.00	70.00	75.00	80.00
82	5.13	10.25	15.38	20.50	25.63	30.75	35.88	41.00	46.13	51.25	56.38	61.50	66.63	71.75	76.88	82.00
84	5.25	10.50	15.75	21.00	26.25	31.50	36.75	42.00	47.25	52.50	57.75	63.00	68.25	73.50	78.75	84.00
86	5.38	10.75	16.13	21.50	26.88	32.25	37.63	43.00	48.38	53.75	59.13	64.50	69.88	75.25	80.63	86.00
88	5.50	11.00	16.50	22.00	27.50	33.00	38.50	44.00	49.50	55.00	60.50	66.00	71.50	77.00	82.50	88.00
90	5.63	11.25	16.88	22.50	28.13	33.75	39.38	45.00	50.63	56.25	61.88	67.50	73.13	78.75	84.38	90.00
92	5.75	11.50	17.25	23.00	28.75	34.50	40.25	46.00	51.75	57.50	63.25	69.00	74.75	80.50	86.25	92.00
94	5.88	11.75	17.63	23.50	29.38	35.25	41.13	47.00	52.88	58.75	64.63	70.50	76.38	82.25	88.13	94.00
96	6.00	12.00	18.00	24.00	30.00	36.00	42.00	48.00	54.00	60.00	66.00	72.00	78.00	84.00	90.00	96.00
98	6.13	12.25	18.38	24.50	30.63	36.75	42.88	49.00	55.13	61.25	67.38	73.50	79.63	85.75	91.88	98

WEIGHTS OF FLAT ROLLED STEEL

POUNDS PER LINEAR FOOT

Width, Inches	Thickness, Inches															
	1/16	1/8	3/16	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1
1/4	.053	.106	.159	.213	.27	.32	.37	.43	.48	.53	.58	.64	.69	.74	.80	.85
1/2	.106	.213	.319	.425	.53	.64	.74	.85	.96	1.06	1.17	1.28	1.38	1.49	1.59	1.70
3/4	.159	.319	.478	.638	.80	.96	1.12	1.28	1.43	1.59	1.75	1.91	2.07	2.23	2.39	2.55
1	.213	.425	.638	.850	1.06	1.28	1.49	1.70	1.91	2.13	2.34	2.55	2.76	2.98	3.19	3.40
1 1/4	.266	.531	.797	1.063	1.33	1.59	1.86	2.13	2.39	2.66	2.92	3.19	3.45	3.72	3.98	4.25
1 1/2	.319	.638	.956	1.275	1.59	1.91	2.23	2.55	2.87	3.19	3.51	3.83	4.14	4.46	4.78	5.10
1 3/4	.372	.744	1.116	1.488	1.86	2.23	2.60	2.98	3.35	3.72	4.09	4.46	4.83	5.21	5.58	5.95
2	.425	.850	1.275	1.700	2.13	2.55	2.98	3.40	3.83	4.25	4.68	5.10	5.53	5.95	6.38	6.80
2 1/4	.478	.956	1.434	1.913	2.39	2.87	3.35	3.83	4.30	4.78	5.26	5.74	6.22	6.69	7.17	7.65
2 1/2	.531	1.063	1.594	2.125	2.66	3.19	3.72	4.25	4.78	5.31	5.84	6.38	6.91	7.44	7.97	8.50
2 3/4	.584	1.169	1.753	2.338	2.92	3.51	4.09	4.68	5.26	5.84	6.43	7.01	7.60	8.18	8.77	9.35
3	.638	1.275	1.913	2.550	3.19	3.83	4.46	5.10	5.74	6.38	7.01	7.65	8.29	8.93	9.56	10.20
3 1/4	.691	1.381	2.072	2.763	3.45	4.14	4.83	5.53	6.22	6.91	7.60	8.29	8.98	9.67	10.36	11.05
3 1/2	.744	1.488	2.231	2.975	3.72	4.46	5.21	5.95	6.69	7.44	8.18	8.93	9.67	10.41	11.16	11.90
3 3/4	.797	1.594	2.391	3.188	3.98	4.78	5.58	6.38	7.17	7.97	8.77	9.56	10.36	11.16	11.95	12.75
4	.850	1.700	2.550	3.400	4.25	5.10	5.95	6.80	7.65	8.50	9.35	10.20	11.05	11.90	12.75	13.60
4 1/4	.903	1.806	2.709	3.613	4.52	5.42	6.32	7.23	8.13	9.03	9.93	10.84	11.74	12.64	13.55	14.45
4 1/2	.956	1.913	2.869	3.825	4.78	5.74	6.69	7.65	8.61	9.56	10.52	11.48	12.43	13.39	14.34	15.30
4 3/4	1.009	2.019	3.028	4.038	5.05	6.06	7.07	8.08	9.08	10.09	11.10	12.11	13.12	14.13	15.14	16.15
5	1.063	2.125	3.188	4.250	5.31	6.38	7.44	8.50	9.56	10.63	11.69	12.75	13.81	14.88	15.94	17.00
5 1/4	1.116	2.231	3.347	4.463	5.58	6.69	7.81	8.93	10.04	11.16	12.27	13.39	14.50	15.62	16.73	17.85
5 1/2	1.169	2.338	3.506	4.675	5.84	7.01	8.18	9.35	10.52	11.69	12.86	14.03	15.19	16.36	17.53	18.70
5 3/4	1.222	2.444	3.666	4.888	6.11	7.33	8.55	9.78	11.00	12.22	13.44	14.66	15.88	17.11	18.33	19.55
6	1.275	2.550	3.825	5.100	6.38	7.65	8.93	10.20	11.48	12.75	14.03	15.30	16.58	17.85	19.13	20.40
6 1/4	1.328	2.656	3.984	5.313	6.64	7.97	9.30	10.63	11.95	13.28	14.61	15.94	17.27	18.59	19.92	21.25
6 1/2	1.381	2.763	4.144	5.525	6.91	8.29	9.67	11.05	12.43	13.81	15.19	16.58	17.96	19.34	20.72	22.10
6 3/4	1.434	2.869	4.303	5.738	7.17	8.61	10.04	11.48	12.91	14.34	15.78	17.21	18.65	20.08	21.52	22.95
7	1.488	2.975	4.463	5.950	7.44	8.93	10.41	11.90	13.39	14.88	16.36	17.85	19.34	20.83	22.31	23.80
7 1/4	1.541	3.081	4.622	6.163	7.70	9.24	10.78	12.33	13.87	15.41	16.95	18.49	20.03	21.57	23.11	24.65
7 1/2	1.594	3.188	4.781	6.375	7.97	9.56	11.16	12.75	14.34	15.94	17.53	19.13	20.72	22.31	23.91	25.50
7 3/4	1.647	3.294	4.941	6.588	8.23	9.88	11.53	13.18	14.82	16.47	18.12	19.76	21.41	23.06	24.70	26.35
8	1.700	3.400	5.100	6.800	8.50	10.20	11.90	13.60	15.30	17.00	18.70	20.40	22.10	23.80	25.50	27.20
8 1/4	1.753	3.506	5.259	7.013	8.77	10.52	12.27	14.03	15.78	17.53	19.28	21.04	22.79	24.54	26.30	28.05
8 1/2	1.806	3.613	5.419	7.225	9.03	10.84	12.64	14.45	16.26	18.06	19.87	21.68	23.48	25.29	27.09	28.90
8 3/4	1.859	3.719	5.578	7.438	9.30	11.16	13.02	14.88	16.73	18.59	20.45	22.31	24.17	26.03	27.89	29.75
9	1.913	3.825	5.738	7.650	9.56	11.48	13.39	15.30	17.21	19.13	21.04	22.95	24.86	26.78	28.69	30.60
9 1/4	1.966	3.931	5.897	7.863	9.83	11.79	13.76	15.73	17.69	19.66	21.62	23.59	25.55	27.52	29.48	31.45
9 1/2	2.019	4.038	6.056	8.075	10.09	12.11	14.13	16.15	18.17	20.19	22.21	24.23	26.24	28.26	30.28	32.30
9 3/4	2.072	4.144	6.216	8.288	10.36	12.43	14.50	16.58	18.65	20.72	22.79	24.86	26.93	29.01	31.08	33.15
10	2.125	4.250	6.375	8.500	10.63	12.75	14.88	17.00	19.13	21.25	23.38	25.50	27.63	29.75	31.88	34.00
10 1/4	2.178	4.356	6.534	8.713	10.89	13.07	15.25	17.43	19.60	21.78	23.96	26.14	28.32	30.49	32.67	34.85
10 1/2	2.231	4.463	6.694	8.925	11.16	13.39	15.62	17.85	20.08	22.31	24.54	26.78	29.01	31.24	33.47	35.70
10 3/4	2.284	4.569	6.853	9.138	11.42	13.71	15.99	18.28	20.56	22.84	25.13	27.41	29.70	31.98	34.27	36.55
11	2.338	4.675	7.013	9.350	11.69	14.03	16.36	18.70	21.04	23.38	25.71	28.05	30.39	32.73	35.06	37.40
11 1/4	2.391	4.781	7.172	9.563	11.95	14.34	16.73	19.13	21.52	23.91	26.30	28.69	31.08	33.47	35.86	38.25
11 1/2	2.444	4.888	7.331	9.775	12.22	14.66	17.11	19.55	21.99	24.44	26.88	29.33	31.77	34.21	36.66	39.10
11 3/4	2.497	4.994	7.491	9.988	12.48	14.98	17.48	19.98	22.47	24.97	27.47	29.96	32.46	34.96	37.45	39.95
12	2.550	5.100	7.650	10.20	12.75	15.30	17.85	20.40	22.95	25.50	28.05	30.60	33.15	35.70	38.25	40.80
12 1/2	2.66	5.31	7.97	10.63	13.28	15.94	18.59	21.25	23.91	26.56	29.2	31.9	34.5	37.2	39.8	42.5
13	2.76	5.53	8.29	11.05	13.81	16.58	19.34	22.10	24.86	27.63	30.4	33.2	35.9	38.7	41.4	44.2
13 1/2	2.87	5.74	8.61	11.48	14.37	17.21	20.08	22.95	25.82	28.69	31.6	34.4	37.3	40.2	43.0	45.9
14	2.98	5.95	8.93	11.90	14.88	17.85	20.83	23.80	26.78	29.75	32.7	35.7	38.7	41.7	44.6	47.6
14 1/2	3.08	6.16	9.24	12.33	15.41	18.49	21.57	24.65	27.73	30.81	33.9	37.0	40.1	43.1	46.2	49.3
15	3.19	6.38	9.56	12.75	15.94	19.13	22.31	25.50	28.69	31.88	35.1	38.3	41.4	44.6	47.8	51.0
15 1/2	3.29	6.59	9.88	13.18	16.47	19.76	23.06	26.35	29.64	32.94	36.2	39.5	42.8	46.1	49.4	52.7
16	3.40	6.80	10.20	13.60	17.00	20.40	23.80	27.20	30.60	34.00	37.4	40.8	44.2	47.6	51.0	54.4
16 1/2	3.51	7.01	10.52	14.03	17.53	21.04	24.54	28.05	31.56	35.06	38.6	42.1	45.6	49.1	52.6	56.1
17	3.61	7.23	10.84	14.45	18.06	21.68	25.29	28.90	32.51	36.13	39.7	43.4	47.0	50.6	54.2	57.8
17 1/2	3.72	7.44	11.16	14.88	18.59	22.31	26.03	29.75	33.47	37.19	40.9	44.6	48.3	52.1	55.8	59.5
18	3.83	7.65	11.48	15.30	19.13	22.95	26.78	30.60	34.43	38.25	42.1	45.9	49.7	53.6	57.4	61.2
18 1/2	3.93	7.86	11.79	15.73	19.66	23.59	27.52	31.45	35.38	39.31	43.2	47.2	51.1	55.0	59.0	62.9
19	4.04	8.08	12.11	16.15	20.19	24.23	28.26	32.30	36.34	40.38	44.4	48.5	52.5	56.5	60.6	64.6
19 1/2	4.14	8.29	12.43	16.58	20.72	24.86	29.01	33.15	37.29	41.44	45.6	49.7	53.9	58.0	62.2	66.3
20	4.25	8.50	12.75	17.00	21.25	25.50	29.75	34.00	38.25	42.50	46.8	51.0	55.3	59.5	63.8	68.0
20 1/2	4.36	8.71	13.07	17.43	21.78	26.14	30.49	34.85	39.21	43.56	47.9	52.3	56.6	61.0	65.3	69.7
21	4.46	8.93	13.39	17.85	22.31	26.78	31.24	35.70	40.16	44.63	49.1	53.6	58.0	62.5	66.9	71.4
21 1/2	4.57	9.14	13.71	18.28	22.84	27.41	31.98	36.55	41.12	45.69	50.3	54.8	59.4	64.0	68.5	73.1
22	4.68	9.35	14.03	18.70	23.38	28.05	32.73	37.40	42.08	46.75	51.4	56.1	60.8	65.5	70.1	74.8

WEIGHTS OF FLAT ROLLED STEEL

POUNDS PER LINEAR FOOT






Width, Inches	Thickness, Inches															
	1/16	1/8	3/16	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1
22 1/2	4.78	9.56	14.34	19.13	23.91	28.69	33.47	38.25	43.03	47.81	52.6	57.4	62.2	66.9	71.7	76.5
23	4.89	9.78	14.66	19.55	24.44	29.33	34.21	39.10	43.99	48.88	53.8	58.7	63.5	68.4	73.3	78.2
23 1/2	4.99	9.99	14.98	19.98	24.97	29.96	34.96	39.95	44.94	49.94	54.9	59.9	64.9	69.9	74.9	79.9
24	5.10	10.20	15.30	20.40	25.50	30.60	35.70	40.80	45.90	51.00	56.1	61.2	66.3	71.4	76.5	81.6
25	5.31	10.63	15.94	21.25	26.56	31.88	37.19	42.50	47.81	53.13	58.4	63.8	69.1	74.4	79.7	85.0
26	5.53	11.05	16.58	22.10	27.63	33.15	38.68	44.20	49.73	55.25	60.8	66.3	71.8	77.4	82.9	88.4
27	5.74	11.48	17.21	22.95	28.69	34.43	40.16	45.90	51.64	57.38	63.1	68.9	74.6	80.3	86.1	91.8
28	5.95	11.90	17.85	23.80	29.75	35.70	41.65	47.60	53.55	59.50	65.5	71.4	77.4	83.3	89.3	95.2
29	6.16	12.33	18.49	24.65	30.81	36.98	43.14	49.30	55.46	61.63	67.8	74.0	80.1	86.3	92.4	98.6
30	6.38	12.75	19.13	25.50	31.88	38.25	44.63	51.00	57.38	63.75	70.1	76.5	82.9	89.3	95.6	102.0
31	6.59	13.18	19.76	26.35	32.94	39.53	46.11	52.70	59.29	65.88	72.5	79.1	85.6	92.2	98.8	105.4
32	6.80	13.60	20.40	27.20	34.00	40.80	47.60	54.40	61.20	68.00	74.8	81.6	88.4	95.2	102.0	108.8
33	7.01	14.03	21.04	28.05	35.06	42.08	49.09	56.10	63.11	70.13	77.1	84.2	91.2	98.2	105.2	112.2
34	7.23	14.45	21.68	28.90	36.13	43.35	50.58	57.80	65.03	72.25	79.5	86.7	93.9	101.2	108.4	115.6
35	7.44	14.88	22.31	29.75	37.19	44.63	52.06	59.50	66.94	74.38	81.8	89.3	96.7	104.1	111.6	119.0
36	7.65	15.30	22.95	30.60	38.25	45.90	53.55	61.20	68.85	76.50	84.2	91.8	99.5	107.1	114.8	122.4
37	7.86	15.73	23.59	31.45	39.31	47.18	55.04	62.90	70.76	78.63	86.5	94.4	102.2	110.1	117.9	125.8
38	8.08	16.15	24.23	32.30	40.38	48.45	56.53	64.60	72.68	80.75	88.8	96.9	105.0	113.1	121.1	129.2
39	8.29	16.58	24.86	33.15	41.44	49.73	58.01	66.30	74.59	82.88	91.2	99.5	107.7	116.0	124.3	132.6
40	8.50	17.00	25.50	34.00	42.50	51.00	59.50	68.00	76.50	85.00	93.5	102.0	110.5	119.0	127.5	136.0
41	8.71	17.43	26.14	34.85	43.56	52.28	60.99	69.70	78.41	87.13	95.8	104.6	113.3	122.0	130.7	139.4
42	8.93	17.85	26.78	35.70	44.63	53.55	62.48	71.40	80.33	89.25	98.2	107.1	116.0	125.0	133.9	142.8
43	9.14	18.28	27.41	36.55	45.69	54.83	63.96	73.10	82.24	91.38	100.5	109.7	118.8	127.9	137.1	146.2
44	9.35	18.70	28.05	37.40	46.75	56.10	65.45	74.80	84.15	93.50	102.9	112.2	121.6	130.9	140.3	149.6
45	9.56	19.13	28.69	38.25	47.81	57.38	66.94	76.50	86.06	95.63	105.2	114.8	124.3	133.9	143.4	153.0
46	9.78	19.55	29.33	39.10	48.88	58.65	68.43	78.20	87.98	97.75	107.5	117.3	127.1	136.9	146.6	156.4
47	9.99	19.98	29.96	39.95	49.94	59.93	69.91	79.90	89.89	99.88	109.9	119.9	129.8	139.8	149.8	159.8
48	10.20	20.40	30.60	40.80	51.00	61.20	71.40	81.60	91.80	102.0	112.2	122.4	132.6	142.8	153.0	163.2
49	10.4	20.8	31.2	41.7	52.1	62.5	72.9	83.3	93.7	104.1	114.5	125.0	135.4	145.8	156.2	166.6
50	10.6	21.3	31.9	42.5	53.1	63.8	74.4	85.0	95.6	106.3	116.9	127.5	138.1	148.8	159.4	170.0
51	10.8	21.7	32.5	43.4	54.2	65.0	75.9	86.7	97.5	108.4	119.2	130.1	140.9	151.7	162.6	173.4
52	11.1	22.1	33.2	44.2	55.3	66.3	77.4	88.4	99.5	110.5	121.6	132.6	143.7	154.7	165.8	176.8
53	11.3	22.5	33.8	45.1	56.3	67.6	78.8	90.1	101.4	112.6	123.9	135.2	146.4	157.7	168.9	180.2
54	11.5	23.0	34.4	45.9	57.4	68.9	80.3	91.8	103.3	114.8	126.2	137.7	149.2	160.7	172.1	183.6
55	11.7	23.4	35.1	46.8	58.4	70.1	81.8	93.5	105.2	116.9	128.6	140.3	151.9	163.6	175.3	187.0
56	11.9	23.8	35.7	47.6	59.5	71.4	83.3	95.2	107.1	119.0	130.9	142.8	154.7	166.6	178.5	190.4
57	12.1	24.2	36.3	48.5	60.6	72.7	84.8	96.9	109.0	121.1	133.2	145.4	157.5	169.6	181.7	193.8
58	12.3	24.7	37.0	49.3	61.6	74.0	86.3	98.6	110.9	123.1	135.6	147.9	160.2	172.6	184.9	197.2
59	12.5	25.1	37.6	50.2	62.7	75.2	87.8	100.3	112.8	125.4	137.9	150.5	163.0	175.5	188.1	200.6
60	12.8	25.5	38.3	51.0	63.8	76.5	89.3	102.0	114.8	127.5	140.3	153.0	165.8	178.5	191.3	204.0
61	13.0	25.9	38.9	51.9	64.8	77.8	90.7	103.7	116.7	129.6	142.6	155.6	168.5	181.5	194.4	207.4
62	13.2	26.4	39.5	52.7	65.9	79.1	92.2	105.4	118.6	131.8	144.9	158.1	171.3	184.5	197.6	210.8
63	13.4	26.8	40.2	53.6	66.9	80.3	93.7	107.1	120.5	133.9	147.3	160.7	174.0	187.4	200.8	214.2
64	13.6	27.2	40.8	54.4	68.0	81.6	95.2	108.8	122.4	136.0	149.6	163.2	176.8	190.4	204.0	217.6
65	13.8	27.6	41.4	55.3	69.1	82.9	96.7	110.5	124.3	138.1	151.9	165.8	179.6	193.4	207.2	221.0
66	14.0	28.1	42.1	56.1	70.1	84.2	98.2	112.2	126.2	140.4	154.3	168.3	182.3	196.4	210.4	224.0
67	14.2	28.5	42.7	57.0	71.2	85.4	99.7	113.9	128.1	142.4	156.6	170.9	185.1	199.3	213.6	227.8
68	14.5	28.9	43.4	57.8	72.3	86.7	101.2	115.6	130.1	144.5	159.0	173.4	187.9	202.3	216.8	231.2
69	14.7	29.3	44.0	58.7	73.3	88.0	102.6	117.3	132.0	146.6	161.3	176.0	190.6	205.3	219.9	234.6
70	14.9	29.8	44.6	59.5	74.4	89.3	104.1	119.0	133.9	148.8	163.6	178.5	193.4	208.3	223.1	238.0
71	15.1	30.2	45.3	60.4	75.4	90.5	105.6	120.7	135.8	150.9	166.0	181.1	196.1	211.2	226.3	241.4
72	15.3	30.6	45.9	61.2	76.5	91.8	107.1	122.4	137.7	153.0	168.3	183.6	198.9	214.2	229.5	244.8
73	15.5	31.0	46.5	62.1	77.6	93.1	108.6	124.1	139.6	155.1	170.6	186.2	201.7	217.2	232.7	248.2
74	15.7	31.5	47.2	62.9	78.6	94.4	110.1	125.8	141.5	157.3	173.0	188.7	204.4	220.2	235.9	251.6
75	15.9	31.9	47.8	63.8	79.7	95.6	111.6	127.5	143.4	159.4	175.3	191.3	207.2	223.1	239.1	255.0
76	16.2	32.3	48.5	64.6	80.8	96.9	113.1	129.2	145.4	161.5	177.7	193.8	210.0	226.1	242.3	258.4
78	16.6	33.2	49.7	66.3	82.9	99.5	116.0	132.6	149.2	165.8	182.3	198.9	215.5	232.1	248.6	265.2
80	17.0	34.0	51.0	68.0	85.0	102.0	119.0	136.0	153.0	170.0	187.0	204.0	221.0	238.0	255.0	272.0
82	17.4	34.9	52.3	69.7	87.1	104.6	122.0	139.4	156.8	174.3	191.7	209.1	226.5	244.0	261.4	278.8
84	17.9	35.7	53.6	71.4	89.3	107.1	125.0	142.8	160.7	178.5	196.4	214.2	232.1	249.9	267.8	285.6
86	18.3	36.6	54.8	73.1	91.4	109.7	127.9	146.2	164.5	182.8	201.0	219.3	237.6	255.9	274.1	292.4
88	18.7	37.4	56.1	74.8	93.5	112.2	130.9	149.6	168.3	187.0	205.7	224.4	243.1	261.8	280.5	299.2
90	19.1	38.3	57.4	76.5	95.6	114.8	133.9	153.0	172.1	191.3	210.4	229.5	248.6	267.8	286.9	306.0
92	19.6	39.1	58.7	78.2	97.8	117.3	136.9	156.4	176.0	195.5	215.1	234.6	254.2	273.7	293.3	312.8
94	20.0	40.0	59.9	79.9	99.9	119.9	139.8	159.8	179.8	199.8	219.7	239.7	259.7	279.7	299.6	319.6
96	20.4	40.8	61.2	81.6	102.0	122.4	142.8	163.2	183.6	204.0	224.4	244.8	265.2	285.6	306.0	326.4
98	20.8	41.7	62.5	83.3	104.1	125.0	145.8	166.6	187.4	208.3	229.1	249.9	270.7	291.6	312.4	333.2
100	21.3	42.5	63.8	85.0	106.3	127.5	148.8	170.0	191.3	212.5	233.8	255.0	276.3	297.5	318.8	340.0






WIRE AND SHEET METAL GAUGES

IN DECIMALS OF AN INCH





Number of Gauge	Birmingham or Stubs Iron Wire Gauge (B. W. G.)	American or Brown & Sharpe Wire Gauge.	United States Standard Gauge for Sheet and Plate Iron and Steel.	American Steel & Wire Co. formerly Washburn & Moen John A. Roebling's Sons Co.	Trenton Iron Co. Wire Gauge.	British Imperial or English Legal Standard Wire Gauge.	New Birmingham Standard Sheet and Hoop Gauge (B. G.)
00000005500	.6666
00000046875	.4600464	.625
000004375	.4300	.450	.432	.5883
0000	.454	.460000	.40625	.3938	.400	.400	.5416
000	.425	.409642	.375	.3625	.360	.372	.500
00	.380	.364796	.34375	.3310	.330	.348	.4452
0	.340	.324861	.3125	.3065	.305	.324	.3964
1	.300	.289297	.28125	.2830	.285	.300	.3532
2	.284	.257627	.265625	.2625	.265	.276	.3147
3	.259	.229423	.25	.2437	.245	.252	.2804
4	.238	.204307	.234375	.2253	.225	.232	.250
5	.220	.181940	.21875	.2070	.205	.212	.2225
6	.203	.162023	.203125	.1920	.190	.192	.1981
7	.180	.144285	.1875	.1770	.175	.176	.1764
8	.165	.128490	.171875	.1620	.160	.160	.1570
9	.148	.114423	.15625	.1483	.145	.144	.1398
10	.134	.101897	.140625	.1350	.130	.128	.1250
11	.120	.090742	.125	.1205	.1175	.116	.1113
12	.109	.080808	.109375	.1055	.105	.104	.0991
13	.095	.071962	.09375	.0915	.0925	.092	.0882
14	.083	.064084	.078125	.0800	.0806	.080	.0785
15	.072	.057068	.0703125	.0720	.070	.072	.0699
16	.065	.050821	.0625	.0625	.061	.064	.0625
17	.058	.045257	.05625	.0540	.0525	.056	.0556
18	.049	.040303	.05	.0475	.045	.048	.0495
19	.042	.035890	.04375	.0410	.040	.040	.0440
20	.035	.031961	.0375	.0348	.035	.036	.0392
21	.032	.028462	.034375	.03175	.031	.032	.0349
22	.028	.025346	.03125	.0286	.028	.028	.03125
23	.025	.022572	.028125	.0258	.025	.024	.02782
24	.022	.020101	.025	.0230	.0225	.022	.02476
25	.020	.017900	.021875	.0204	.020	.020	.02204
26	.018	.015941	.01875	.0181	.018	.018	.01961
27	.016	.014195	.0171875	.0173	.017	.0164	.01745
28	.014	.012641	.015625	.0162	.016	.0148	.015625
29	.013	.011257	.0140625	.0150	.015	.0136	.0139
30	.012	.010025	.0125	.0140	.014	.0124	.0123
31	.010	.008928	.0109375	.0132	.013	.0116	.0110
32	.009	.007950	.01015625	.0128	.012	.0108	.0098
33	.008	.007080	.009375	.0118	.011	.0100	.0087
34	.007	.006305	.00859375	.0104	.010	.0092	.0077
35	.005	.005615	.0078125	.0095	.0095	.0084	.0069
36	.004	.005000	.00703125	.0090	.009	.0076	.0061
37004453	.006640625	.0085	.0085	.0068	.0054
38003965	.00625	.0080	.008	.0060	.0048
390035310075	.0075	.0052	.0043
400031440070	.007	.0048	.00386






SQUARE AND ROUND BARS**1/16 TO 15/16****WEIGHTS, AREAS AND CIRCUMFERENCE**

Thickness or Diameter in Inches	Weight in Pounds				Area in Sq. Inches		 Circum- ference
	Square 		Round 				
	One Inch Long	One Foot Long	One Inch Long	One Foot Long			
1/16	.001	.013	.001	.010	.0039	.0031	.1964
5/64	.002	.021	.001	.016	.0061	.0048	.2454
3/32	.002	.030	.002	.023	.0088	.0069	.2945
7/64	.003	.041	.003	.032	.0120	.0094	.3436
1/8	.004	.053	.004	.042	.0156	.0123	.3927
9/64	.006	.067	.004	.053	.0198	.0155	.4418
5/32	.007	.083	.005	.065	.0244	.0192	.4909
11/64	.008	.100	.007	.079	.0295	.0232	.5400
3/16	.010	.120	.008	.094	.0352	.0276	.5891
13/64	.012	.140	.009	.110	.0413	.0324	.6381
7/32	.014	.163	.011	.128	.0479	.0376	.6872
15/64	.016	.187	.012	.147	.0549	.0431	.7363
1/4	.018	.212	.014	.167	.0625	.0491	.7854
17/64	.020	.240	.016	.188	.0706	.0554	.8345
9/32	.022	.269	.018	.211	.0791	.0621	.8836
19/64	.025	.300	.020	.235	.0881	.0692	.9327
5/16	.028	.332	.022	.261	.0977	.0767	.9818
21/64	.031	.366	.024	.288	.1077	.0846	1.0308
11/32	.033	.402	.026	.316	.1182	.0928	1.0799
23/64	.037	.439	.029	.345	.1292	.1014	1.1290
3/8	.040	.478	.031	.376	.1406	.1104	1.1781
25/64	.043	.519	.034	.407	.1526	.1198	1.2272
13/32	.047	.561	.037	.441	.1650	.1296	1.2763
27/64	.050	.605	.040	.475	.1780	.1398	1.3254
7/16	.054	.651	.043	.511	.1914	.1503	1.3745
29/64	.058	.698	.046	.548	.2053	.1613	1.4235
15/32	.062	.747	.049	.587	.2197	.1726	1.4726
31/64	.066	.798	.052	.627	.2346	.1843	1.5217
1/2	.071	.850	.056	.668	.2500	.1963	1.5708
33/64	.075	.904	.060	.710	.2659	.2088	1.6199
17/32	.080	.960	.063	.754	.2822	.2217	1.6690
35/64	.085	1.017	.067	.799	.2991	.2349	1.7181
9/16	.090	1.076	.070	.845	.3164	.2485	1.7672
37/64	.095	1.136	.074	.893	.3342	.2625	1.8162
19/32	.100	1.199	.078	.941	.3525	.2769	1.8653
39/64	.105	1.263	.083	.992	.3713	.2916	1.9144
5/8	.111	1.328	.087	1.043	.3906	.3068	1.9635
41/64	.116	1.395	.091	1.096	.4104	.3223	2.0126
21/32	.122	1.464	.096	1.150	.4307	.3382	2.0617
43/64	.128	1.535	.100	1.205	.4514	.3545	2.1108
11/16	.134	1.607	.105	1.262	.4727	.3712	2.1599
45/64	.140	1.681	.110	1.320	.4944	.3883	2.2089
23/32	.146	1.756	.115	1.380	.5166	.4057	2.2580
47/64	.153	1.834	.120	1.440	.5393	.4236	2.3071
3/4	.159	1.913	.125	1.502	.5625	.4418	2.3562
13/16	.187	2.245	.147	1.763	.6602	.5185	2.5526
7/8	.217	2.603	.170	2.044	.7656	.6013	2.7489
15/16	.249	2.988	.196	2.347	.8789	.6903	2.9453






1" to 3 15/16		SQUARE AND ROUND BARS						
		WEIGHTS, AREAS AND CIRCUMFERENCE						
Thickness or Diameter in Inches	Weight in Pounds				Area in Sq. Inches		 Circum- ference	
	Square 		Round 		 Square	 Round		
	One Inch Long	One Foot Long	One Inch Long	One Foot Long				
1"	.28	3.400	.22	2.670	1.0000	.7854	3.1416	
1 1/16	.32	3.838	.25	3.015	1.1289	.8866	3.3380	
1 1/8	.36	4.303	.28	3.380	1.2656	.9940	3.5343	
1 3/16	.40	4.795	.31	3.766	1.4102	1.1075	3.7306	
1 1/4	.44	5.313	.35	4.172	1.5625	1.2272	3.9270	
1 5/16	.49	5.857	.38	4.600	1.7227	1.3530	4.1234	
1 3/8	.54	6.428	.42	5.049	1.8906	1.4849	4.3197	
1 7/16	.58	7.026	.46	5.518	2.0664	1.6230	4.5161	
1 1/2	.64	7.650	.50	6.008	2.2500	1.7671	4.7124	
1 9/16	.69	8.301	.54	6.519	2.4414	1.9175	4.9088	
1 5/8	.75	8.978	.59	7.051	2.6406	2.0739	5.1051	
1 11/16	.81	9.682	.63	7.604	2.8477	2.2365	5.3015	
1 3/4	.87	10.41	.68	8.178	3.0625	2.4053	5.4978	
1 13/16	.94	11.17	.73	8.773	3.2852	2.5802	5.6942	
1 7/8	1.00	11.95	.78	9.388	3.5156	2.7612	5.8905	
1 15/16	1.06	12.76	.84	10.02	3.7539	2.9483	6.0869	
2"	1.13	13.60	.89	10.68	4.0000	3.1416	6.2832	
1 1/16	1.21	14.46	.95	11.36	4.2539	3.3410	6.4796	
1 1/8	1.28	15.35	1.01	12.06	4.5156	3.5466	6.6759	
1 3/16	1.36	16.27	1.07	12.78	4.7852	3.7583	6.8723	
1 1/4	1.43	17.21	1.13	13.52	5.0625	3.9761	7.0686	
1 5/16	1.52	18.18	1.19	14.28	5.3477	4.2000	7.2650	
1 3/8	1.60	19.18	1.26	15.06	5.6406	4.4301	7.4613	
1 7/16	1.68	20.20	1.32	15.87	5.9414	4.6664	7.6577	
1 1/2	1.77	21.25	1.39	16.69	6.2500	4.9087	7.8540	
1 9/16	1.86	22.33	1.46	17.53	6.5664	5.1573	8.0504	
1 5/8	1.95	23.43	1.54	18.40	6.8906	5.4119	8.2467	
1 11/16	2.05	24.56	1.61	19.29	7.2227	5.6727	8.4431	
1 3/4	2.14	25.71	1.69	20.19	7.5625	5.9396	8.6394	
1 13/16	2.24	26.90	1.76	21.12	7.9102	6.2126	8.8358	
1 7/8	2.34	28.10	1.84	22.07	8.2656	6.4918	9.0321	
1 15/16	2.44	29.34	1.92	23.04	8.6289	6.7771	9.2285	
3"	2.55	30.60	2.01	24.03	9.0000	7.0686	9.4248	
1 1/16	2.66	31.89	2.09	25.05	9.3789	7.3662	9.6212	
1 1/8	2.77	33.20	2.18	26.08	9.7656	7.6699	9.8175	
1 3/16	2.88	34.55	2.26	27.13	10.160	7.9798	10.014	
1 1/4	2.99	35.92	2.35	28.21	10.563	8.2958	10.210	
1 5/16	3.11	37.31	2.44	29.30	10.973	8.6179	10.407	
1 3/8	3.23	38.73	2.53	30.42	11.391	8.9462	10.603	
1 7/16	3.35	40.18	2.63	31.55	11.816	9.2806	10.799	
1 1/2	3.47	41.65	2.73	32.71	12.250	9.6211	10.996	
1 9/16	3.60	43.15	2.82	33.89	12.691	9.9678	11.192	
1 5/8	3.72	44.68	2.92	35.09	13.141	10.321	11.388	
1 11/16	3.85	46.23	3.03	36.31	13.598	10.680	11.585	
1 3/4	3.98	47.82	3.13	37.55	14.063	11.045	11.781	
1 13/16	4.12	49.42	3.23	38.81	14.535	11.416	11.977	
1 7/8	4.25	51.05	3.34	40.10	15.016	11.793	12.174	
1 15/16	4.39	52.71	3.45	41.40	15.504	12.177	12.370	

SQUARE AND ROUND BARS**4" to 6 15/16****WEIGHTS, AREAS AND CIRCUMFERENCE**

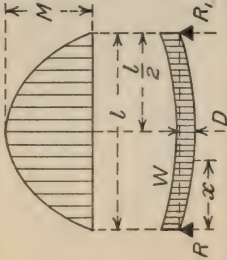
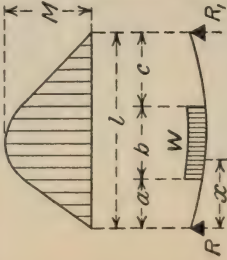
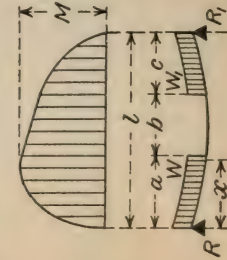
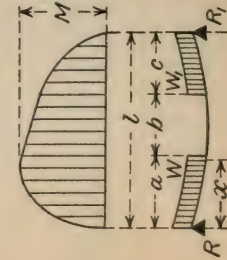
Thickness or Diameter in Inches	Weight in Pounds				Area in Sq. Inches		Circum- ference
	Square 		Round 				
	One Inch Long	One Foot Long	One Inch Long	One Foot Long	Square	Round	
4"	4.53	54.40	3.57	42.73	16.000	12.566	12.566
1 1/16	4.68	56.11	3.67	44.07	16.504	12.962	12.763
1 1/8	4.82	57.85	3.79	45.44	17.016	13.364	12.959
3/16	4.97	59.62	3.90	46.83	17.535	13.772	13.155
1/4	5.12	61.41	4.02	48.24	18.063	14.186	13.352
5/16	5.27	63.23	4.14	49.66	18.598	14.607	13.548
3/8	5.42	65.08	4.26	51.11	19.141	15.033	13.745
7/16	5.58	66.95	4.38	52.58	19.691	15.466	13.941
1/2	5.74	68.85	4.51	54.07	20.250	15.904	14.137
9/16	5.90	70.78	4.63	55.59	20.816	16.349	14.334
5/8	6.06	72.73	4.76	57.12	21.391	16.800	14.530
11/16	6.23	74.71	4.89	58.67	21.973	17.257	14.726
3/4	6.39	76.71	5.02	60.25	22.563	17.721	14.923
13/16	6.56	78.74	5.15	61.85	23.160	18.190	15.119
7/8	6.73	80.80	5.29	63.46	23.766	18.665	15.315
15/16	6.91	82.89	5.42	65.10	24.379	19.147	15.512
5"	7.08	85.00	5.56	66.76	25.000	19.635	15.708
1 1/2	7.26	87.14	5.70	68.44	25.629	20.129	15.904
1 1/8	7.44	89.30	5.84	70.14	26.266	20.629	16.101
3/16	7.62	91.49	5.99	71.86	26.910	21.135	16.297
1/4	7.81	93.71	6.13	73.60	27.563	21.648	16.493
5/16	8.00	95.96	6.28	75.37	28.223	22.166	16.690
3/8	8.19	98.23	6.43	77.15	28.891	22.691	16.886
7/16	8.38	100.5	6.58	78.95	29.566	23.221	17.082
1/2	8.57	102.9	6.73	80.78	30.250	23.758	17.279
9/16	8.77	105.2	6.88	82.62	30.941	24.301	17.475
5/8	8.96	107.6	7.04	84.49	31.641	24.851	17.672
11/16	9.16	110.0	7.20	86.38	32.348	25.406	17.868
3/4	9.37	112.4	7.36	88.29	33.063	25.967	18.064
13/16	9.57	114.9	7.52	90.22	33.785	26.535	18.261
7/8	9.78	117.4	7.68	92.17	34.516	27.109	18.457
15/16	9.99	119.9	7.84	94.14	35.254	27.688	18.653
6"	10.20	122.4	8.01	96.13	36.000	28.274	18.850
1 1/16	10.41	125.0	8.18	98.15	36.754	28.867	19.046
1 1/8	10.63	127.6	8.35	100.2	37.516	29.465	19.242
3/16	10.85	130.2	8.52	102.2	38.285	30.069	19.439
1/4	11.07	132.8	8.69	104.3	39.063	30.680	19.635
5/16	11.29	135.5	8.87	106.4	39.848	31.296	19.831
3/8	11.51	138.2	9.04	108.5	40.641	31.919	20.028
7/16	11.74	140.9	9.22	110.7	41.441	32.548	20.224
1/2	11.97	143.7	9.40	112.8	42.250	33.183	20.420
9/16	12.20	146.5	9.58	115.0	43.066	33.824	20.617
5/8	12.43	149.2	9.77	117.2	43.891	34.472	20.813
11/16	12.67	152.1	9.95	119.4	44.723	35.125	21.009
3/4	12.91	154.9	10.14	121.7	45.563	35.785	21.206
13/16	13.15	157.8	10.33	123.9	46.410	36.451	21.402
7/8	13.39	160.7	10.52	126.2	47.266	37.122	21.599
15/16	13.64	163.6	10.71	128.5	48.129	37.800	21.795

7" TO 9 15/16		SQUARE AND ROUND BARS						
		WEIGHTS, AREAS AND CIRCUMFERENCE						
Thickness or Diameter in Inches	Weight in Pounds				Area in Sq. Inches			Circum- ference
	Square 		Round 					
	One Inch Long	One Foot Long	One Inch Long	One Foot Long				
7"	13.88	166.6	10.90	130.8	49.000	38.485		21.991
1 1/16	14.13	169.6	11.10	133.2	49.879	39.175		22.188
1 1/8	14.38	172.6	11.30	135.6	50.766	39.871		22.384
3 1/16	14.64	175.6	11.50	138.0	51.660	40.574		22.580
1 1/4	14.89	178.7	11.70	140.4	52.563	41.283		22.777
5 1/16	15.15	181.8	11.90	142.8	53.473	41.997		22.973
3 3/8	15.41	184.9	12.10	145.2	54.391	42.718		23.169
7 1/16	15.67	188.1	12.31	147.7	55.316	43.446		23.366
1 1/2	15.94	191.3	12.52	150.2	56.250	44.179		23.562
9 1/16	16.20	194.5	12.73	152.7	57.191	44.918		23.758
5 5/8	16.47	197.7	12.94	155.3	58.141	45.664		23.955
11 1/16	16.74	200.9	13.15	157.8	59.098	46.415		24.151
3 3/4	17.02	204.2	13.36	160.4	60.063	47.173		24.347
13 1/16	17.29	207.5	13.58	163.0	61.035	47.937		24.544
7 7/8	17.57	210.9	13.80	165.6	62.016	48.707		24.740
15 1/16	17.85	214.2	14.02	168.2	63.004	49.483		24.936
8"	18.11	217.6	14.24	170.9	64.000	50.266		25.133
1 1/16	18.42	221.0	14.46	173.6	65.004	51.054		25.329
1 1/8	18.70	224.5	14.69	176.3	66.016	51.849		25.526
3 1/16	18.99	227.9	14.92	179.0	67.035	52.649		25.722
1 1/4	19.28	231.4	15.14	181.8	68.063	53.456		25.918
5 1/16	19.58	234.9	15.38	184.5	69.098	54.269		26.115
3 3/8	19.87	238.5	15.61	187.3	70.141	55.088		26.311
7 1/16	20.17	242.1	15.84	190.1	71.191	55.914		26.507
1 1/2	20.47	245.7	16.08	192.9	72.250	56.745		26.704
9 1/16	20.77	249.3	16.31	195.8	73.316	57.583		26.900
5 5/8	21.08	252.9	16.55	198.6	74.391	58.426		27.096
11 1/16	21.38	256.6	16.79	201.5	75.473	59.276		27.293
3 3/4	21.69	260.3	17.04	204.4	76.563	60.132		27.489
13 1/16	22.00	264.0	17.28	207.4	77.660	60.994		27.685
7 7/8	22.31	267.8	17.53	210.3	78.766	61.863		27.882
15 1/16	22.63	271.6	17.77	213.3	79.879	62.737		28.078
9"	22.95	275.4	18.02	216.3	81.000	63.617		28.274
1 1/16	23.27	279.2	18.27	219.3	82.129	64.504		28.471
1 1/8	23.59	283.1	18.53	222.3	83.266	65.397		28.667
3 1/16	23.91	287.0	18.78	225.4	84.410	66.296		28.863
1 1/4	24.24	290.9	19.04	228.5	85.563	67.201		29.060
5 1/16	24.57	294.9	19.30	231.6	86.723	68.112		29.256
3 3/8	24.90	298.8	19.56	234.7	87.891	69.029		29.453
7 1/16	25.23	302.8	19.82	237.8	89.066	69.953		29.649
1 1/2	25.57	306.9	20.08	241.0	90.250	70.882		29.845
9 1/16	25.91	310.9	20.35	244.2	91.441	71.818		30.042
5 5/8	26.25	315.0	20.61	247.4	92.641	72.760		30.238
11 1/16	26.59	319.1	20.88	250.6	93.848	73.708		30.434
3 3/4	26.93	323.2	21.15	253.8	95.063	74.662		30.631
13 1/16	27.28	327.4	21.42	257.1	96.285	75.622		30.827
7 7/8	27.63	331.6	21.70	260.4	97.516	76.589		31.023
15 1/16	27.98	335.8	21.97	263.7	98.754	77.561		31.220

SQUARE AND ROUND BARS**10" TO 15³/₄"****WEIGHTS, AREAS AND CIRCUMFERENCE**

Thickness or Diameter in Inches	Weight in Pounds				Area in Sq. Inches		 Circum- ference
	 Square		 Round		 Square	 Round	
	One Inch Long	One Foot Long	One Inch Long	One Foot Long			
10"	28.33	340.0	22.25	267.0	100.00	78.540	31.416
1 ¹ / ₁₆	28.69	344.3	22.53	270.4	101.25	79.525	31.612
1 ¹ / ₈	29.04	348.6	22.81	273.8	102.52	80.516	31.809
3 ¹ / ₁₆	29.41	352.9	23.09	277.1	103.79	81.513	32.005
1 ¹ / ₄	29.77	357.2	23.38	280.6	105.06	82.516	32.201
5 ¹ / ₁₆	30.13	361.6	23.66	284.0	106.35	83.525	32.398
3 ¹ / ₈	30.50	366.0	23.95	287.4	107.64	84.541	32.594
7 ¹ / ₁₆	30.87	370.4	24.24	290.9	108.94	85.563	32.790
1 ¹ / ₂	31.24	374.9	24.53	294.4	110.25	86.590	32.987
9 ¹ / ₁₆	31.61	379.3	24.82	297.9	111.57	87.624	33.183
5 ¹ / ₈	31.98	383.8	25.12	301.5	112.89	88.664	33.380
11 ¹ / ₁₆	32.36	388.4	25.42	305.0	114.22	89.710	33.576
3 ¹ / ₄	32.74	392.9	25.71	308.6	115.56	90.763	33.772
13 ¹ / ₁₆	33.12	397.5	26.01	312.2	116.91	91.821	33.969
7 ¹ / ₈	33.51	402.1	26.32	315.8	118.27	92.886	34.165
15 ¹ / ₁₆	33.89	406.7	26.62	319.5	119.63	93.957	34.361
11"	34.28	411.4	26.92	323.1	121.00	95.033	34.558
1 ¹ / ₁₆	34.67	416.1	27.23	326.8	122.38	96.116	34.754
1 ¹ / ₈	35.06	420.8	27.54	330.5	123.77	97.206	34.950
3 ¹ / ₁₆	35.46	425.5	27.85	334.3	125.16	98.301	35.147
1 ¹ / ₄	35.86	430.3	28.16	338.0	126.56	99.402	35.343
5 ¹ / ₁₆	36.26	435.1	28.48	341.7	127.97	100.51	35.539
3 ¹ / ₈	36.66	439.9	28.79	345.5	129.39	101.62	35.736
7 ¹ / ₁₆	37.06	444.8	29.11	349.3	130.82	102.74	35.932
1 ¹ / ₂	37.47	449.7	29.43	353.2	132.25	103.87	36.128
9 ¹ / ₁₆	37.88	454.6	29.75	357.0	133.69	105.00	36.325
5 ¹ / ₈	38.29	459.5	30.07	360.9	135.14	106.14	36.521
11 ¹ / ₁₆	38.70	464.4	30.39	364.8	136.60	107.28	36.717
3 ¹ / ₄	39.12	469.4	30.72	368.7	138.06	108.43	36.914
13 ¹ / ₁₆	39.53	474.4	31.04	372.6	139.54	109.59	37.110
7 ¹ / ₈	39.95	479.5	31.38	376.6	141.02	110.75	37.307
15 ¹ / ₁₆	40.37	484.5	31.71	380.5	142.50	111.92	37.503
12"	40.80	489.5	32.04	384.5	144.00	113.10	37.699
1 ¹ / ₄	42.52	510.1	33.39	400.7	150.06	117.86	38.485
1 ¹ / ₂	44.27	531.2	34.77	417.2	156.25	122.72	39.270
3 ¹ / ₄	46.05	552.6	36.17	434.1	162.56	127.68	40.055
13"	47.88	574.5	37.60	451.2	169.00	132.73	40.841
1 ¹ / ₄	49.74	596.8	39.06	468.8	175.56	137.89	41.626
1 ¹ / ₂	51.63	619.6	40.55	486.6	182.25	143.14	42.412
3 ¹ / ₄	53.56	642.7	42.07	504.8	189.06	148.49	43.197
14"	55.53	666.3	43.62	523.3	196.00	153.94	43.982
1 ¹ / ₄	57.53	690.3	45.18	542.2	203.06	159.48	44.768
1 ¹ / ₂	59.57	714.8	46.78	561.4	210.25	165.13	45.553
3 ¹ / ₄	61.64	739.6	48.41	580.9	217.56	170.87	46.339
15"	63.75	764.9	50.06	600.7	225.00	176.71	47.124
1 ¹ / ₄	65.89	790.6	51.75	620.9	232.56	182.65	47.909
1 ¹ / ₂	68.07	816.8	53.46	641.5	240.25	188.69	48.695
3 ¹ / ₄	70.28	843.3	55.20	662.3	248.06	194.83	49.480

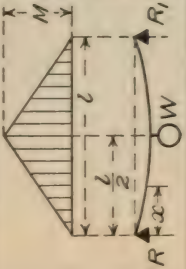
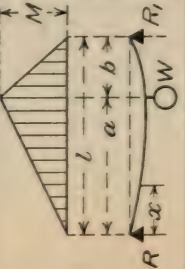
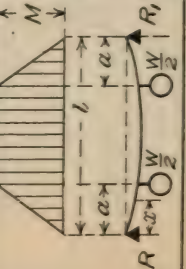
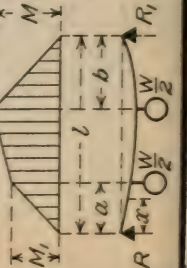
GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS R AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = R_1 = V(\max) = \frac{W}{2}$	<p>At center</p> $M(\max) = \frac{Wl}{8}$	<p>At center</p> $D(\max) = \frac{5}{384} \frac{Wl^3}{EI}$
	<p>At x</p> $V = \frac{W}{2} - \frac{Wx}{l}$	<p>At x</p> $M = \frac{Wx}{2l} (l - x)$	<p>At x</p> $D = \frac{Wx}{24 EI} (l^3 - 2lx^2 + x^3)$
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, PARTIALLY DISTRIBUTED			
	$R = \frac{W(2c + b)}{2l}$ $R_1 = \frac{W(2a + b)}{2l}$ $V(\max) = R \text{ when } a < c,$ $= R_1 \text{ when } a > c$ <p>At x, when $x > a$, or $< (a + b)$</p> $V = \frac{W(2c + b)}{2l} - \frac{W(x - a)}{b}$	<p>At x: when $x = a + \frac{Rb}{W}$</p> $M(\max) = \frac{W(2c + b)}{8l^2} [4al + b(2c + b)]$ <p>when $x < a$ or $= a$; $M = Rx$ when $x < (a + b)$ or $> a$ $M = Rx - \frac{2b}{W(x - a)^2}$ when $x > (a + b)$ $M = Rx - \frac{W(2a - 2a - b)}{2}$</p>	
BEAM SUPPORTED BOTH ENDS. TWO CONTINUOUS LOADS, DISTRIBUTED ONE AT EACH END			
	$R = \frac{W(2l - a) + W_1c}{2l}$ $R_1 = \frac{W_1(2l - c) + Wa}{2l}$ $V(\max) = R \text{ when } W > W_1$ $= R_1 \text{ when } W < W_1$ <p>At x, when $x < a$</p> $V = R - \frac{Wx}{a}$	<p>At x: when $Wa > W_1c$</p> $\text{when } x = \frac{2W_1a l - W_1c^2 + W_1ca}{2Wl}$ $M(\max) = \frac{R^2a}{2W}$ <p>when $x < a$ $M = Rx - \frac{Wx^2}{2a}$ when $x > a$ $M = Rx - \frac{W(2x - a)}{2}$</p>	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, INCREASING UNIFORMLY TO CENTER			
	$R = R_1 = V(max) = \frac{W}{2}$	At center $M(max) = \frac{Wl}{6}$	At center $D(max) = \frac{Wl^3}{60EI}$
	At x $V = \frac{W}{2} - \frac{2Wx^2}{l^2}$	At x $M = Wx \left(\frac{1}{2} - \frac{2x^2}{3l^2} \right)$	At x $D = \frac{Wx}{6EI l^2} \left(\frac{l^2 x^2}{2} - \frac{x^4}{5} - \frac{5l^4}{16} \right)$
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, DECREASING UNIFORMLY TO CENTER			
	$R = R_1 = V(max) = \frac{W}{2}$	At center $M(max) = \frac{Wl}{12}$	At center $D(max) = \frac{3Wl^3}{320EI}$
	At x $V = \frac{W}{2l^2} (l - 2x)^2$	At x $M = Wx \left(\frac{1}{2} - \frac{x}{l} + \frac{2x^2}{3l^2} \right)$	
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, INCREASING UNIFORMLY TO ONE END			
	$R = \frac{W}{3}$	At x : when $x = \frac{l\sqrt{3}}{3}$	At x : when $x = l \sqrt{1 - \sqrt{\frac{8}{15}}} = .519 l$
	$R_1 = V(max) = \frac{2W}{3}$	At x $M(max) = \frac{2Wl}{9\sqrt{3}} = .128 Wl$	At x $D(max) = \frac{.013044 Wl^3}{EI}$
BEAM SUPPORTED BOTH ENDS. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED, PLUS LOAD INCREASING UNIFORMLY TO ONE END			
	$R = \frac{W}{2} + \frac{W_1}{3}$	At x : when $x = 0.5 l$ to $0.577 l$	At x : when $x = .5 l$ approx.
	$R_1 = V(max) = \frac{W}{2} + \frac{2W_1}{3}$	At x $M(max) = \left(W + W_1 \right) \frac{l}{8} \text{ approx.}$	At x $D(max) = \frac{5Wl^3}{384EI} + \frac{.013044 W_1 l^3}{EI}$

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM SUPPORTED BOTH ENDS. CONCENTRATED LOAD AT CENTER			
	$R = R_1 = V(\max) = \frac{W}{2}$ <p>At x</p> $V = \frac{W}{2}$	<p>At center</p> $M(\max) = \frac{Wl}{4}$ <p>At x</p> $M = \frac{Wx}{2}$	<p>At center</p> $D(\max) = \frac{Wl^3}{48EI}$ <p>When $x < \frac{l}{2}$</p> <p>At x</p> $D = \frac{W}{48EI} (3l^2x - 4x^3)$
BEAM SUPPORTED BOTH ENDS. CONCENTRATED LOAD NEAR ONE END			
	$R = \frac{Wb}{l}$ $R_1 = \frac{W}{l}$ <p>$V(\max) = R$ when $a < b$ and R_1 when $a > b$</p> <p>At x</p> $V = \frac{Wb}{l}$	<p>At point of load</p> $M(\max) = \frac{Wab}{l}$ <p>At x: when $x < a$</p> $M = \frac{Wbx}{l}$	<p>At x: when $x = \sqrt{a(a+2b) + 3}$ and $a > b$</p> $D(\max) = \frac{Wab(a+2b)\sqrt{3a(a+2b)} + 27EI}{27EI}$ <p>At x: when $x < a$</p> $D = \frac{Wbx}{6EI} \left[\frac{2l(l-x) - b^2 - (l-x)^2}{2} \right]$ <p>At x: when $x > a$</p> $D = \frac{W}{6EI} \left[\frac{2lb - b^2 - (l-x)^2}{2} \right]$
BEAM SUPPORTED BOTH ENDS. TWO EQUAL CONCENTRATED LOADS, SYMMETRICALLY DISTRIBUTED			
	$R = R_1 = V(\max) = \frac{W}{2}$ <p>At x: when $x < a$</p> $V = \frac{W}{2}$ <p>At x: when $x > a$ and $< (l-a)$</p> $V = 0$	<p>At and between loads</p> $M(\max) = \frac{Wa}{2}$ <p>At x</p> $M = \frac{Wx}{2}$	<p>At center</p> $D(\max) = \frac{Wa}{12EI} \left(\frac{3l^2}{4} - a^2 \right)$ <p>At x: when $x < a$</p> $D = \frac{Wx}{12EI} \left(3la - 3a^2 - x^2 \right)$ <p>At x: when $x > a$ and $< (l-a)$</p> $D = \frac{W}{12EI} \left(3lx - 3x^2 - a^2 \right)$
BEAM SUPPORTED BOTH ENDS. TWO EQUAL CONCENTRATED LOADS, UNEQUALLY DISTRIBUTED			
	<p>When $a < b$</p> $R = V(\max) = \frac{W}{2l} (l - a + b)$ $R_1 = \frac{W}{2l} (l - b + a)$ <p>$V(\max) = R$ when $a < b$</p> <p>$V(\max) = R_1$ when $a > b$</p>	<p>At x: when $x = l - b$ when $b > a$</p> $M(\max) = \frac{Wb}{2l} (l + a - b)$ <p>At x: when $x = a$</p> $M = \frac{Wa}{2l} (l - a + b)$ <p>At x: when $x > a$ or $< (l-b)$</p> $M = Rx - \frac{W}{2} (x - a)$	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM SUPPORTED BOTH ENDS. TWO UNEQUAL CONCENTRATED LOADS, UNEQUALLY DISTRIBUTED			
	$R = \frac{1}{l} [W(l-a) + W_1 b]$	At point of load W $M = \frac{a}{l} [W(l-a) + W_1 b]$	
	$R_1 = \frac{1}{l} [W a + W_1 (l-b)]$	At point of load W1 $M_1 = \frac{b}{l} [W a + W_1 (l-b)]$	
	$V(\max) = \text{Maximum Reaction}$		
	At x: when $x > a$ and $< (l-b)$ $V = R - W$	At x: when $x > a$ or $< (l-b)$ $M = W \frac{a}{l} (l-x) + W_1 \frac{bx}{l}$	
BEAM SUPPORTED BOTH ENDS. THREE EQUAL CONCENTRATED LOADS, SYMMETRICALLY DISTRIBUTED			
	$R = R_1 = V(\max) = \frac{W}{2}$	At center $M(\max) = \frac{WL}{6}$	At center $D(\max) = \frac{19}{384} \frac{W l^3}{EI}$
	At x: when $x < \frac{l}{4}$ $V = \frac{W}{2}$		
	At x: when $x > \frac{l}{4}$ and $< \frac{l}{2}$ $V = \frac{W}{6}$	At x: when $x = \frac{l}{4}$ $M_1 = \frac{WL}{8}$	
BEAM SUPPORTED BOTH ENDS. THREE UNEQUAL CONCENTRATED LOADS, UNEQUALLY DISTRIBUTED			
	$R = \frac{Wb + W_1 b_1 + W_2 b_2}{l}$	At x: when $x = a$ $M = Ra$	
	$R_1 = \frac{W a + W_1 a_1 + W_2 a_2}{l}$	At x: when $x = a_1$ $M_1 = Ra_1 - W(a_1 - a)$	
	$V(\max) = \text{Maximum Reaction}$	At x: when $x = a_2$ $M_2 = Ra_2 - W(a_2 - a) - W_1(a_2 - a_1)$	
	At x: when $x > a$ and $< a_1$ $V = R - W$	$M(\max) = M \text{ when } W = R \text{ or } > R$	
	At x: when $x > a_1$ and $< a_2$ $V = R - W - W_1$	$M(\max) = M_1 \text{ when } \begin{cases} W_1 + W = R \text{ or } > R \\ W_1 + W_2 = R_1 \text{ or } > R_1 \end{cases}$	

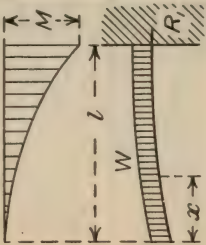
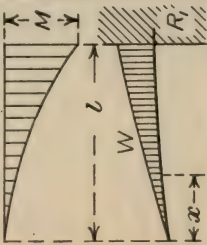
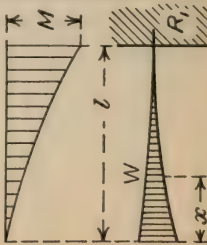
GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT BOTH ENDS. CONTINUOUS LOAD, INCREASING UNIFORMLY TO CENTER			
	$R = R_1 = V(\max) = \frac{W}{2}$	At center $M(\max) = \frac{Wl}{16}$	
	At $\frac{x}{2}$ $V = \frac{W}{2} - \frac{2Wx^2}{l^2}$	At support $M^1(\max) = \frac{5Wl}{48}$	
		At x $M = M^1 + \frac{Wx}{2} - \frac{2Wx^3}{3l^2}$	
BEAM FIXED AT BOTH ENDS. CONTINUOUS LOAD, DECREASING UNIFORMLY TO CENTER			
	$R = R_1 = V(\max) = \frac{W}{2}$	At center $M(\max) = \frac{Wl}{48}$	
	At x $V = \frac{W}{2l^2} (l - 2x)^2$	At support $M^1(\max) = \frac{Wl}{16}$	
BEAM FIXED AT BOTH ENDS. CONTINUOUS LOAD, INCREASING UNIFORMLY TO ONE END			
	$R = \frac{3W}{10}$	At x : when $x = .548 l$ $M(\max) = .043 Wl$	
	$R_1 = V(\max) = \frac{7W}{10}$	At support $M^1 = \frac{Wl}{10}$	
	At x $V = \frac{3W}{10} - \frac{Wx^2}{l^2}$	At x $M = \frac{3Wx}{10} - \frac{Wl}{15} - \frac{Wx^3}{3l^2}$	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

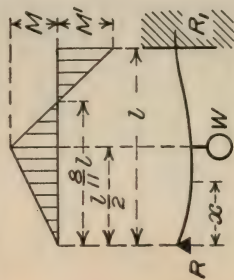
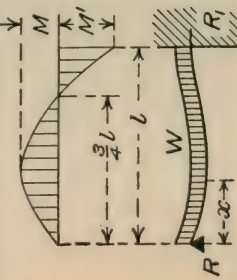
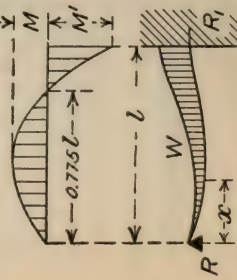
LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT BOTH ENDS. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = R_1 = V(\max) = \frac{Wl}{2}$	At center $M(\max) = \frac{Wl^2}{24}$	At center $D(\max) = \frac{1}{384} \frac{Wl^4}{EI}$
	$V = \frac{W}{2} - \frac{Wx}{l}$	At supports $M^1(\max) = \frac{Wl^2}{12}$	At x $D = \frac{Wx^2}{24EI} \left(l^2 - 2lx + x^2 \right)$
		At x $M = \frac{W}{2l} \left(-\frac{l^2}{6} + lx - x^2 \right)$	
BEAM FIXED AT BOTH ENDS. CONCENTRATED LOAD, AT CENTER			
	$R = R_1 = V(\max) = \frac{W}{2}$	At center $M(\max) = \frac{Wl^2}{8}$	At center $D(\max) = \frac{1}{192} \frac{Wl^3}{EI}$
	$V = \frac{W}{2}$	At supports $M^1(\max) = \frac{Wl^2}{8}$	At x $D = \frac{Wx^2}{6EI} \left(-\frac{1}{2}x + \frac{3}{8}l \right)$
		At x : when $x < \frac{l}{2}$ $M = \frac{W}{2} \left(x - \frac{l}{4} \right)$	
BEAM FIXED AT BOTH ENDS. CONCENTRATED LOAD, NEAR ONE END			
	$R = W \left(\frac{b^2(3a+b)}{l^3} \right)$	At support R $M^1(\max, \text{neg. mom.}) = -\frac{Wab^2}{l^2}$	At x : when $x = \frac{2a}{3a+b}$ and $a > b$ $D(\max) = \frac{2Wab^2}{3EI(3a+b)^2}$
	$R_1 = W \left(\frac{a^2(3b+a)}{l^3} \right)$	At support R1 $M^2(\max, \text{neg. mom.}) = -\frac{Wab^2}{l^2}$	when $x < a$ $D = \frac{Wb^2x^2}{6EI^3} \left(3al - 3ax - bx \right)$
	$V(\max) = R$ when $a < b$ $= R_1$ when $a > b$ At x : when $x < a$ $V = R$	At point of load $M(\max) = Ra + M^1 = Ra - W \frac{ab^2}{l^2}$	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT ONE END (CANTILEVER). CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R_1 = V(\max) = W$ At x $V = \frac{Wx}{l}$	At fixed end $M(\max) = \frac{Wl}{2}$ At x $M = \frac{Wx^2}{2l}$	At free end $D(\max) = \frac{Wl^3}{8EI}$ At x $D = \frac{W}{24EI} (x^4 - 4l^3x + 3l^4)$
BEAM FIXED AT ONE END (CANTILEVER). CONTINUOUS LOAD, INCREASING UNIFORMLY TO FIXED END			
	$R_1 = V(\max) = W$ At x $V = \frac{Wx^2}{l^2}$	At fixed end $M(\max) = \frac{Wl}{3}$ At x $M = \frac{Wx^3}{3l^2}$	At free end $D(\max) = \frac{Wl^3}{15EI}$ At x $D = \frac{W}{60EI^2} (x^5 - 5l^4x + 4l^5)$
BEAM FIXED AT ONE END (CANTILEVER). CONTINUOUS LOAD, INCREASING UNIFORMLY TO FREE END			
	$R_1 = V(\max) = W$ At x $V = \frac{Wx}{l^2} (2l - x)$	At fixed end $M(\max) = \frac{2Wl}{3}$ At x $M = \frac{Wx^2}{3l^2} (3l - x)$	At free end $D(\max) = \frac{11Wl^3}{60EI}$

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS			
LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT ONE END (CANTILEVER). CONCENTRATED LOAD AT FREE END			
	$R_1 = V (\max) = W$ At x $V = W$	At fixed end $M (\max) = Wl$ At x $M = Wx$	At free end $D (\max) = \frac{Wl^3}{3EI}$ At x $D = \frac{W}{6EI} (2l^3 - 3lx^2 + x^3)$
BEAM FIXED AT ONE END (CANTILEVER). CONCENTRATED LOAD AT ANY POINT			
	$R_1 = V (\max) = W$ At x : when $x > a$ $V = W$ At x : when $x < a$ $V = 0$	At fixed end $M (\max) = Wb$ At x : when $x > a$ $M = W(x - a)$	At free end $D (\max) = \frac{Wl^3}{6EI} \left[2 - \frac{3a}{l} + \left(\frac{a}{l} \right)^3 \right]$ At point of load $D = \frac{W}{3EI} (l - a)^3$ At x : when $x > a$ $D = \frac{W}{6EI} \left(-3al^2 + 2l^3 + x^3 - 3ax^2 - 3l^2x + 6alx \right)$
BEAM FIXED AT ONE END, SUPPORTED AT OTHER. CONCENTRATED LOAD AT ANY POINT			
	$R = W \left(\frac{3b^2l - b^3}{2l^3} \right)$ $R_1 = W \left(\frac{3al^2 - a^3}{2l^3} \right)$ At x when $x < a$ $V = R$ At x when $x > a$ $V = R - W$	At point of load $M (\max) = Wa \left(\frac{3b^2l - b^3}{2l^3} \right)$ At fixed end $M^1 (\max) = Wl \left(\frac{3b^2l - b^3}{2l^3} \right) - W(l - a)$ At x : when $x < a$ $M = Wx \left(\frac{3b^2l - b^3}{2l^3} \right)$ At x : when $x > a$ $M = Wx \left(\frac{3b^2l - b^3}{2l^3} \right) - W(x - a)$	At x : when $x = a = .414l$ $D (\max) = .0098 \frac{Wl^3}{EI}$ At x : when $x < a$ $D = \frac{1}{6EI} \left[\frac{3Rlx - Rx^3}{3W(l - a)^2 x} \right]$ At x : when $x > a$ $D = \frac{1}{6EI} \left[\frac{R_1 (2l^3 - 3l^2x + x^3) - R_2 (l - x)^2}{3W(l - a)^2} \right]$

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT ONE END, SUPPORTED AT OTHER. CONCENTRATED LOAD, AT CENTER			
	$R = \frac{5}{16} W$ $R_1 = V (max) = \frac{11}{16} W$	<p>At center</p> $M (max) = \frac{5}{32} Wl$ <p>At fixed end</p> $M^1 (max) = \frac{3}{16} Wl$ <p>At x: when $x < l/2$</p> $M = \frac{5}{16} Wx$ <p>At x: when $x > l/2$</p> $M = \frac{1}{2} Wl - \frac{11}{16} Wx$	<p>At x: when $x = .4472 l$</p> $D (max) = .00932 \frac{Wl^3}{EI}$ <p>At x: when $x < l/2$</p> $D = \frac{Wx}{96 EI} (5x^2 - 3l^2)$ <p>At x: when $x > l/2$</p> $D = \frac{W}{96 EI} \left[-2l^3 + 15l^2x - 24lx^2 + 11x^3 \right]$
BEAM FIXED AT ONE END, SUPPORTED AT OTHER. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = \frac{3}{8} W$ $R_1 = V (max) = \frac{5}{8} W$ <p>At x</p> $V = \frac{3}{8} W - \frac{Wx}{l}$	<p>At x: when $x = \frac{3}{8} l$</p> $M (max) = \frac{9}{128} Wl$ <p>At fixed end</p> $M^1 (max) = \frac{1}{8} Wl$ <p>At x</p> $M = \frac{Wx}{l} \left(\frac{3}{8} l - \frac{1}{2} x \right)$	<p>At x: when $x = .4215 l$</p> $D (max) = .0054 \frac{Wl^4}{EI}$ <p>At x</p> $D = \frac{Wx}{48 EI} \left[-3lx^2 + 2x^3 + l^3 \right]$
BEAM FIXED AT ONE END, SUPPORTED AT OTHER. CONTINUOUS LOAD, INCREASING UNIFORMLY TO FIXED END			
	$R = \frac{1}{5} W$ $R_1 = V (max) = \frac{4}{5} W$ <p>At x</p> $V = \frac{W}{5} - \frac{Wx^2}{l^2}$	<p>At x: when $x = .4474 l$</p> $M (max) = .06 Wl$ <p>At fixed end</p> $M^1 (max) = \frac{2}{15} Wl = .1333 Wl$ <p>At x</p> $M = \frac{Wx}{5} - \frac{Wx^3}{3l^2}$	<p>At x: when $x = .4474 l$</p> $D (max) = .1333 \frac{Wl^4}{EI}$

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM FIXED AT ONE END, FREE BUT GUIDED AT OTHER. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = V(\max) = W$ $V = \frac{W(l-x)}{l}$ At x	At <i>fixed end</i> $M(\max) = \frac{Wl^2}{3}$ At <i>free end</i> $Ml = \frac{Wl}{6}$	At <i>free end</i> $D(\max) = \frac{Wl^3}{24EI}$ At x $D = \frac{Wx^2}{24EI} (2l-x)^2$
	$R = V(\max) = W$ $V = W$ At x	At <i>fixed end</i> $M(\max) = \frac{Wl}{2}$ At <i>free end</i> $Ml = \frac{Wl}{2}$	At <i>free end</i> $D(\max) = \frac{Wl^3}{12EI}$ At x $D = \frac{Wx^2}{12EI} (3l-2x)$
BEAM OVERHANGING BOTH SUPPORTS, UNSYMMETRICALLY PLACED. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$\frac{W}{a+l+b} = w = \text{load per unit of length}$ $R = w[(a+D)^2 - b^2] \div 2l$ $R_1 = w[(b+D)^2 - a^2] \div 2l$ $V(\max) = wa \text{ or } R - wa$ At x : when $x < a$ $V = w(a-x)$ At x_1 : when $x_1 < l$ $V = R - w(a+x_1)$ At x_2 : when $x_2 < b$ $V = w(b-x_2)$	At x_1 : when $x_1 = \frac{R}{w} - a$ $M(\max) = R \left(\frac{R}{2w} - a \right)$ At R $Ml = \frac{1}{2} wa^2$ At R_1 $Ml = \frac{1}{2} wb^2$ At x : when $x < a$ $M = \frac{1}{2} w(a-x)^2$ At x_1 : when $x_1 < l$ $M = \frac{1}{2} w(a+x_1)^2 - Rx_1$ At x_2 : when $x_2 < b$ $M = \frac{1}{2} w(b-x_2)^2$	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM OVERHANGING BOTH SUPPORTS, UNSYMMETRICALLY PLACED. TWO CONCENTRATED LOADS AT ENDS			
	$R = \frac{W_1 a - W_2 b}{l} + W_1$ $R_1 = \frac{W_2 b - W_1 a}{l} + W_2$ <p>At x: when $x < a$ $V = W_1$</p> <p>At x_1: when $x_1 < l$ $V = W_1 - R$</p> <p>At x_2: when $x_2 < b$ $V = W_2$</p>	<p>At R $M = W_1 a$</p> <p>At R_1 $M = W_2 b$</p> <p>At x: when $x < a$ $M = W_1 (a - x)$</p> <p>At x_1: when $x_1 < l$ $M = W_1 a + (W_1 - R) x_1$</p> <p>At x_2: when $x_2 < b$ $M = W_2 (b - x_2)$</p>	
BEAM OVERHANGING BOTH SUPPORTS, UNSYMMETRICALLY PLACED. CONCENTRATED LOAD AT ANY POINT			
	$R = \frac{W b}{l}$ $R_1 = \frac{W a}{l}$ <p>$V(max) = R$ when $a < b$</p> <p>At x: when $x < a$ $V = R$</p> <p>At x_1: when $x_1 < b$ $V = R_1$</p>	<p>At point of load $M(max) = \frac{Wab}{l}$</p> <p>At x: when $x < a$ $M = \frac{Wbx}{l}$</p> <p>At x_1: when $x_1 < b$ $M = \frac{W}{l} (l - x_1) - W(b - x_1)$</p>	<p>At x_1: when $x_1 = b \sqrt{\frac{1}{3} + \frac{2a}{3b}}$ $D(max) = \frac{Wax_1^3}{3EI}$</p> <p>At x_2: when $x_2 = c$ $D = \frac{Wabc}{6EI} (l + b)$</p> <p>At x_1: when $x_1 = d$ $D = \frac{Wabd}{6EI} (l + a)$</p>
BEAM OVERHANGING BOTH SUPPORTS, SYMMETRICALLY PLACED. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = R_1 = \frac{W}{2}$ $V(max) = \frac{Wa}{l + 2a} \text{ or } \frac{Wl}{2(l + 2a)}$	<p>At center $M = \frac{W(l - 2a)}{8}$</p> <p>At supports $M_1 = \frac{Wa^2}{2(l + 2a)}$</p> <p>At x: when $x < a$ $M = \frac{W}{2(l + 2a)} (a - x)^2$</p> <p>At x_1: when $x_1 < l$ $M = \frac{W}{2(l + 2a)} (a + x_1)^2 - Rx_1$</p>	

GENERAL FORMULAE FOR BEAMS UNDER VARIOUS LOADING CONDITIONS

LOADING DIAGRAM	REACTIONS AND SHEAR V	BENDING MOMENT M	DEFLECTION D
BEAM OVERHANGING BOTH SUPPORTS, SYMMETRICALLY PLACED. TWO EQUAL CONCENTRATED LOADS AT ENDS			
	$R = R_1 = V(\max) = \frac{W}{2}$ <p>At x: when $x < a$</p> $V = \frac{W}{2}$	<p>At x_1: when $x_1 < l$</p> $M(\max) = \frac{W a}{2}$ <p>At x: when $x < a$</p> $M = \frac{W}{2} (a - x)$	<p>At free ends</p> $D = \frac{W a^2 (3 l + 2 a)}{12 E I}$ <p>At center</p> $D = \frac{W a l^2}{16 E I}$
BEAM OVERHANGING ONE SUPPORT. CONTINUOUS LOAD, UNIFORMLY DISTRIBUTED			
	$R = \frac{W l}{2(l+a)} - \frac{W a^2}{2 l(l+a)}$ $R_1 = \frac{W l}{2(l+a)} + \frac{W a}{l+a} + \frac{W a^2}{2 l(l+a)}$ <p>At x: when $x < l$</p> $V = R - \frac{W x}{l+a}$ <p>At x_1: when $x_1 < a$</p> $V = \frac{W}{l+a} (a - x_1)$	<p>At x: when $x = \frac{1}{2} \left(l - \frac{a^2}{l} \right)$</p> $M(\max) = \frac{R^2 (l+a)}{2 W}$ <p>At x: when $x = l$</p> $M_1(\max) = \frac{W a^2}{2(l+a)}$ <p>At x</p> $M = R x - \frac{W x^2}{2(l+a)}$ <p>At x_1</p> $M = \frac{W (a - x_1)^2}{2(l+a)}$	<p>At x</p> $D = \frac{1}{24 E I} \left[4 R (x^3 - l^2 x) - \frac{W}{l+a} (x^4 - l^2 x) \right]$ <p>At x_1</p> $D = \frac{1}{24 E I} \left[\frac{W}{l+a} (6 a^2 x_1^2 - 4 a x_1^3 + 3 l^2 x_1 + x_1^4) - 8 R l^2 x_1 \right]$
BEAM OVERHANGING ONE SUPPORT. CONCENTRATED LOADS AT FREE END AND BETWEEN SUPPORTS			
	$R = \frac{W b - W_1 a}{l}$ $R_1 = \frac{W (l-b) + W_1 (a+l)}{l}$ <p>At x: when $x < (l-b)$</p> $V = R$ <p>At x_1: when $x_1 > (l-b)$ and $< l$</p> $V = R - W$ <p>At x_2: when $x_2 < a$</p> $V = W_1$	<p>At x: when $x < (l-b)$</p> $M = R x$ <p>At x_1: when $x_1 > (l-b)$ and $< l$</p> $M = R x_1 - W (b + x_1 - l)$ <p>At x_2</p> $M = W_1 (a - x_2)$	

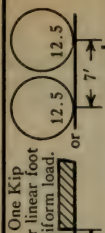
MOMENTS IN FOOT-KIPS FOR CLASS E-10 ENGINE LOADING ONE TRACK OF TWO RAILS

Wheel Numbers	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	One Kip per linear foot uniform load.
Axle Loads	5.0	10.0	10.0	10.0	10.0	10.0	6.5	6.5	6.5	5.0	10.0	10.0	10.0	10.0	6.5	6.5	6.5	6.5	6.5
Spacing in feet	8	8	5	5	5	9	5	6	5	8	8	5	5	5	9	5	6	5	5
Totals from end of train	Kips	142.0	137.0	127.0	117.0	107.0	97.0	90.5	84.0	77.5	71.0	66.0	56.0	46.0	36.0	26.0	19.5	13.0	6.5
Feet	109	101	96	91	86	77	72	66	61	53	45	40	35	30	21	16	10	5	0
End of Train	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
Wheel Number	18	17	16	15	14	13	12	11	10	9	8	7	6	5	4	3	2	1	0
Moments of wheel Loads about	8182.0	7637.0	6627.0	5667.0	4757.0	3897.0	3396.5	2928.5	2499.5	2103.0	1838.0	1588.0	1388.0	1188.0	988.0	838.0	701.5	587.5	32.5
	7472.0	6952.0	5992.0	5082.1	4222.0	3412.0	2944.0	2508.5	2112.0	1748.0	1508.0	1308.0	1108.0	958.0	808.0	688.0	588.0	508.0	32.5
	6794.5	6299.5	5389.2	4529.5	3719.5	2959.5	2524.0	2121.0	1757.0	1425.5	1210.5	1060.5	910.5	760.5	630.5	510.5	410.5	330.5	32.5
	6020.5	5555.6	4705.5	3905.5	3155.6	2455.5	2059.0	1695.0	1370.0	1077.5	892.5	762.5	662.5	582.5	512.5	452.5	392.5	332.5	110.5
	5408.0	4968.0	4168.0	3418.0	2718.0	2068.0	1704.0	1372.5	1080.0	820.0	660.0	540.0	420.0	330.0	250.0	180.0	120.0	80.0	208.0
	4364.0	3969.0	3259.0	2599.0	1989.0	1429.0	1123.5	850.5	616.5	415.0	300.0	210.0	150.0	100.0	50.0	20.0	10.0	5.0	442.0
	3834.0	3464.0	2804.0	2194.0	1634.0	1124.0	851.0	610.5	409.0	240.0	150.0	50.0	50.0	50.0	50.0	141.0	264.5	427.0	622.0
	3354.0	3009.0	2399.0	1839.0	1329.0	869.0	628.5	420.5	251.5	115.0	50.0	50.0	50.0	50.0	50.0	273.5	429.5	624.5	852.0
	2924.0	2604.0	2044.0	1534.0	1074.0	664.0	456.0	280.5	144.0	40.0	50.0	50.0	50.0	50.0	50.0	456.0	644.5	872.0	1132.0
	2316.0	2036.0	1556.0	1126.0	746.0	416.0	260.0	136.5	52.0	80.0	210.0	390.0	620.0	828.0	1068.5	1348.0	1660.0		
	1748.0	1508.0	1108.0	758.0	458.0	208.0	104.0	32.5	40.0	200.0	410.0	670.0	980.0	1240.0	1532.5	1864.0	2228.0		
	1425.5	1210.5	860.5	560.5	310.5	110.5	39.0	32.5	307.5	567.5	877.5	1237.5	1530.0	1855.0	2199.0	2615.5			
	1077.2	892.5	602.5	362.5	172.5	32.5	39.0	110.5	205.5	475.5	795.5	1165.5	1585.5	1917.0	2281.0	2684.0	3119.5		
	890.0	660.0	420.0	230.0	90.0	32.5	104.0	208.0	328.0	648.0	1018.0	1438.0	1908.0	2272.0	2668.5	3104.0	3572.0		
	415.0	300.0	150.0	50.0	58.5	149.5	279.5	442.0	607.0	1017.0	1477.0	1987.0	2547.0	2969.5	3424.5	3918.5	4445.0		
	240.0	150.0	50.0	50.0	141.0	264.5	427.0	622.0	812.0	1272.0	1782.0	2342.0	2952.0	3407.0	3894.5	4421.0	4980.0		
	115.0	50.0	50.0	50.0	273.5	429.5	624.5	852.0	1067.0	1577.0	2137.0	2747.0	3407.0	3894.5	4414.4	4973.5	5565.0		
	40.0	50.0	150.0	300.0	456.0	644.5	872.0	1132.0	1372.0	1932.0	2542.0	3202.0	3912.0	4432.0	4984.5	5576.0	6200.0		
	80.0	210.0	390.0	620.0	828.0	1068.5	1348.0	1660.0	1940.0	2580.0	3270.0	4010.0	4800.0	5372.0	5976.5	6620.0	7296.0		
Totals from wheel No. 1	Kips	5.0	15.0	25.0	35.0	45.0	51.5	58.0	64.5	71.0	76.0	86.0	96.0	106.0	116.0	122.5	129.0	135.5	142.0
Feet	0	8	13	18	23	32	37	43	48	56	64	69	74	79	88	93	99	104	109

For E 40 loading multiply Moments tabulated above by 4; for E 50 loading multiply by 5; for E 60 loading multiply by 6.

MAXIMUM MOMENTS, SHEARS, AND REACTIONS FOR CLASS E-10 ENGINE LOADING ONE TRACK OF TWO RAILS

One Kip per linear foot uniform load.														
Span in Feet	Maximum Moment in Foot-Kips	Maximum Shear in Kips	Maximum Floor-beam Reaction Kips	Equivalent Uniform Load			Span in Feet	Maximum Moment in Foot-Kips	Maximum Shear in Kips	Maximum Floor-beam Reaction Kips	Equivalent Uniform Load			Reaction
				Moment	Shear	Reaction					Moment	Shear	Reaction	
7	21.9	12.5	15.1	3.57	3.57	2.15	42	356.7	39.2	56.0	1.62	1.87	1.34	
7 1/2	23.5	13.4	16.0	3.33	3.56	2.12	44	385.8	40.3	58.2	1.60	1.83	1.32	
8	25.0	14.0	16.8	3.12	3.51	2.11	46	414.9	41.4	60.3	1.57	1.80	1.31	
9	28.1	15.3	18.2	2.78	3.39	2.02	48	443.8	42.4	62.4	1.54	1.77	1.30	
10	31.2	16.2	19.2	2.50	3.25	1.92	50	475.5	43.5	64.3	1.52	1.74	1.29	
11	34.4	17.0	21.0	2.28	3.09	1.90	52	507.6	44.6	66.7	1.50	1.72	1.28	
12	40.0	17.7	23.3	2.22	2.95	1.94	54	540.5	45.6	69.0	1.48	1.69	1.28	
13	47.5	18.3	24.6	2.25	2.81	1.90	56	576.1	46.5	71.4	1.47	1.66	1.27	
14	55.0	18.8	26.1	2.25	2.68	1.86	58	611.6	47.7	74.0	1.46	1.65	1.28	
15	62.5	20.0	27.3	2.22	2.67	1.82	60	649.5	48.8	76.6	1.44	1.63	1.28	
16	70.0	21.3	28.5	2.19	2.66	1.78	62	688.2	50.0	79.1	1.43	1.61	1.27	
17	77.5	22.4	29.4	2.15	2.63	1.73	64	727.7	51.3	81.5	1.42	1.60	1.27	
18	85.0	23.3	30.3	2.10	2.59	1.69	66	769.7	52.5	83.9	1.41	1.59	1.27	
19	93.3	24.2	31.5	2.07	2.55	1.66	68	811.7	53.9	86.2	1.40	1.59	1.27	
20	103.1	25.0	32.8	2.06	2.50	1.64	70	853.7	55.3	88.5	1.39	1.58	1.26	
21	112.9	25.7	34.0	2.05	2.45	1.62	72	896.7	56.7	90.7	1.38	1.58	1.26	
22	122.8	26.3	35.1	2.03	2.40	1.60	74	939.0	58.1	93.0	1.37	1.57	1.26	
23	132.7	27.0	36.1	2.01	2.34	1.57	76	986.0	59.5	95.2	1.36	1.57	1.25	
24	142.6	27.7	37.0	1.98	2.31	1.54	78	1032.7	60.9	97.3	1.36	1.56	1.25	
25	152.5	28.4	37.8	1.95	2.27	1.51	80	1080.0	62.1	99.4	1.35	1.55	1.24	
26	162.4	29.1	38.8	1.92	2.24	1.49	82	1128.3	63.5	101.5	1.34	1.55	1.24	
27	172.3	29.6	40.0	1.89	2.20	1.48	84	1177.7	64.8	103.5	1.34	1.54	1.23	
28	182.7	30.2	41.2	1.86	2.16	1.47	86	1229.7	66.1	105.4	1.33	1.54	1.23	
29	194.0	30.8	42.2	1.84	2.12	1.46	88	1282.0	67.4	107.3	1.32	1.53	1.22	
30	205.2	31.5	43.1	1.82	2.10	1.44	90	1334.7	68.6	109.3	1.32	1.53	1.22	
31	216.5	32.2	44.3	1.80	2.08	1.43	92	1388.3	69.9	111.2	1.31	1.52	1.21	
32	227.7	32.9	45.5	1.78	2.05	1.42	94	1442.7	71.2	113.1	1.31	1.52	1.20	
33	239.0	33.5	46.7	1.75	2.03	1.41	96	1497.3	72.4	115.0	1.30	1.51	1.20	
34	250.3	34.1	47.8	1.73	2.00	1.40	98	1552.7	73.7	116.8	1.29	1.51	1.19	
35	261.5	34.6	48.8	1.71	1.98	1.39	100	1609.7	75.0	118.6	1.29	1.50	1.19	
36	274.3	35.3	49.8	1.69	1.96	1.38	125	2497.7	89.7	140.5	1.28	1.44	1.12	
37	287.2	35.9	50.7	1.68	1.94	1.37	150	3531.0	103.7	162.7	1.25	1.38	1.08	
38	300.0	36.5	51.8	1.66	1.92	1.36	175	4676.3	117.3	185.8	1.22	1.34	1.06	
39	313.3	37.2	52.9	1.65	1.90	1.36	200	5939.0	130.5	209.5	1.19	1.31	1.05	
40	327.8	37.7	54.0	1.64	1.88	1.35	250	8796.3	156.6	257.6	1.13	1.25	1.03	



DEFLECTION

Based on Modulus of Elasticity of 29 000 000.

$$D = \frac{0.01862 L^2}{d}$$

Def. Coef. = 0.01862 L²

D = Deflection in inches for Symmetrical Beams and Girders, simple span, uniformly loaded to cause an 18000 # per sq. in. stress in the extreme fibre of the flange. (See notes below).

L = Span in feet

d = depth in inches

For deflection of beams of depths not listed below divide the Deflection Coefficient by the depth in inches.

Span in Feet	Deflection Coefficient	d = depth in inches										
		3	4	5	6	7	8	9	10	12	14	15
3	.1676	.056	.042	.033	.028	.024	.021	.019	.017	.014	.012	.011
4	.2979	.099	.074	.059	.050	.043	.037	.033	.030	.025	.021	.020
5	.4655	.155	.116	.093	.078	.067	.058	.052	.047	.039	.033	.031
6	.6703	.223	.168	.134	.112	.096	.084	.074	.067	.056	.048	.045
7	.9123	.304	.228	.182	.152	.130	.114	.101	.091	.076	.065	.061
8	1.192	.396	.298	.238	.198	.170	.149	.132	.119	.099	.085	.079
9	1.508	.503	.378	.302	.252	.216	.189	.168	.151	.126	.108	.101
10	1.862	.620	.465	.372	.310	.266	.233	.207	.186	.155	.133	.124
11	2.253	.750	.562	.450	.375	.321	.281	.250	.225	.188	.161	.150
12	2.681	.896	.670	.537	.447	.383	.335	.298	.268	.223	.192	.179
13	3.147	1.05	.787	.630	.525	.450	.394	.350	.315	.263	.225	.210
14	3.650	1.22	.912	.730	.608	.521	.456	.406	.365	.304	.261	.243
15	4.190	1.39	1.05	.838	.698	.599	.524	.466	.419	.349	.299	.279
16	4.767	1.19	.955	.795	.681	.596	.530	.477	.398	.341	.318
17	5.381	1.35	1.08	.897	.769	.673	.598	.538	.448	.384	.359
18	6.033	1.51	1.20	1.01	.861	.754	.670	.603	.503	.431	.402
19	6.722	1.68	1.34	1.12	.960	.840	.747	.672	.560	.480	.448
20	7.448	1.86	1.49	1.24	1.06	.931	.828	.745	.621	.530	.497
21	8.211	1.64	1.37	1.17	1.03	.912	.821	.684	.587	.547
22	9.012	1.80	1.51	1.29	1.13	1.00	.901	.751	.644	.601
23	9.850	1.97	1.64	1.41	1.23	1.10	.985	.820	.704	.657
24	10.725	2.14	1.79	1.53	1.34	1.19	1.07	.894	.766	.715
25	11.638	2.33	1.94	1.66	1.46	1.29	1.16	.970	.831	.776
26	12.587	2.10	1.80	1.57	1.40	1.26	1.05	.899	.839
27	13.574	2.26	1.94	1.70	1.51	1.36	1.13	.970	.905
28	14.598	2.43	2.09	1.83	1.62	1.46	1.22	1.04	.973
29	15.659	2.61	2.24	1.96	1.74	1.57	1.31	1.12	1.04
30	16.758	2.79	2.39	2.10	1.86	1.68	1.40	1.20	1.12
31	17.894	2.56	2.24	1.99	1.79	1.49	1.28	1.19
32	19.067	2.72	2.38	2.12	1.91	1.59	1.36	1.27
33	20.277	2.90	2.54	2.25	2.03	1.69	1.45	1.35
34	21.525	3.08	2.69	2.39	2.15	1.79	1.54	1.44
35	22.810	3.26	2.85	2.53	2.28	1.90	1.63	1.52
36	24.132	3.02	2.68	2.41	2.01	1.72	1.61
37	25.491	3.19	2.83	2.55	2.13	1.82	1.70
38	26.887	3.36	2.99	2.69	2.24	1.92	1.79
39	28.321	3.54	3.15	2.83	2.36	2.02	1.89
40	29.792	3.72	3.31	2.98	2.48	2.13	1.99
42	32.846	3.65	3.29	2.74	2.35	2.19
44	36.048	4.01	3.61	3.00	2.57	2.40
46	39.400	3.94	3.28	2.81	2.63
48	42.901	4.29	3.58	3.06	2.86
50	46.550	4.66	3.88	3.33	3.10
52	50.348	4.20	3.60	3.36
54	54.296	4.53	3.88	3.62
56	58.392	4.87	4.17	3.89
58	62.638	5.22	4.47	4.18
60	67.032	5.59	4.79	4.47
65	78.670	5.62	5.24
70	91.238	6.52	6.08
75	104.738	6.98
80	119.168	7.94
85	134.530	8.97

For Simple Spans a Concentrated Center Load causing an 18000 # per sq. inch fibre stress is 50% of the Uniformly Distributed Load. Deflection caused by a Concentrated Center Load is 0.01490 L² or 80% of that of a Uniformly Distributed Load shown in the above tables.

For fibre stresses other than 18000 # per sq. inch on which the above table is based, the deflection is directly proportional to the flange stress developed. Thus a fibre stress of 12000 # per sq. inch gives a deflection equal to $\frac{2}{3}$ of that shown in the above tables.

DEFLECTION

Based on Modulus of Elasticity of 29 000 000.

$$D = \frac{0.01862 L^2}{d}$$

Def. Coef. = 0.01862 L²

D = Deflection in inches for Symmetrical Beams and Girders, simple span, uniformly loaded to cause an 18000 # per sq. in. stress in the extreme fibre of the flange. (See notes below).

L = Span in feet

d = depth in inches

For deflection of beams of depths not listed below divide the Deflection Coefficient by the depth in inches.

Span in Feet	Deflection Coefficient	d = depth in inches										
		16	18	20	21	22	24	26	27	28	30	33
6	.6703	.042	.037	.034	.032	.030	.028	.026	.025	.024	.022	.020
7	.9123	.057	.051	.046	.043	.041	.038	.035	.034	.033	.030	.028
8	1.192	.075	.066	.060	.057	.054	.050	.046	.044	.043	.040	.036
9	1.508	.094	.084	.076	.072	.069	.063	.058	.056	.054	.050	.046
10	1.862	.116	.103	.093	.089	.085	.078	.072	.069	.066	.062	.056
11	2.253	.141	.125	.113	.107	.102	.094	.087	.083	.080	.075	.068
12	2.681	.168	.149	.134	.123	.122	.112	.103	.099	.096	.089	.081
13	3.147	.197	.175	.158	.150	.143	.131	.121	.117	.113	.105	.095
14	3.650	.228	.203	.183	.174	.166	.152	.140	.135	.132	.122	.111
15	4.190	.262	.233	.210	.200	.191	.175	.161	.155	.150	.140	.127
16	4.767	.298	.265	.239	.227	.217	.199	.183	.177	.170	.159	.144
17	5.381	.336	.299	.269	.256	.245	.224	.207	.199	.192	.179	.163
18	6.033	.377	.335	.302	.287	.274	.251	.232	.223	.215	.201	.183
19	6.722	.420	.373	.336	.320	.305	.280	.258	.249	.240	.224	.204
20	7.448	.466	.414	.373	.355	.339	.310	.287	.276	.266	.248	.226
21	8.211	.513	.456	.411	.391	.373	.342	.316	.304	.293	.274	.249
22	9.012	.563	.501	.451	.429	.410	.375	.347	.334	.322	.300	.273
23	9.850	.616	.547	.493	.469	.448	.410	.379	.365	.352	.328	.298
24	10.725	.670	.596	.537	.511	.488	.447	.413	.397	.383	.358	.325
25	11.638	.727	.647	.582	.554	.529	.485	.448	.431	.416	.388	.353
26	12.587	.787	.699	.630	.600	.572	.525	.484	.466	.450	.420	.381
27	13.574	.848	.754	.679	.646	.617	.566	.522	.503	.485	.452	.411
28	14.598	.912	.811	.736	.695	.664	.608	.562	.540	.521	.487	.442
29	15.659	.979	.870	.783	.746	.712	.653	.602	.580	.559	.522	.475
30	16.758	1.05	.931	.838	.798	.762	.698	.645	.621	.599	.559	.508
31	17.894	1.12	.994	.895	.852	.813	.746	.688	.662	.639	.596	.542
32	19.067	1.19	1.06	.954	.908	.867	.795	.733	.706	.681	.636	.578
33	20.277	1.27	1.13	1.01	.966	.927	.845	.780	.751	.724	.676	.614
34	21.525	1.35	1.20	1.08	1.03	.979	.897	.832	.797	.769	.718	.652
35	22.810	1.43	1.27	1.14	1.09	1.04	.950	.877	.844	.815	.760	.691
36	24.132	1.51	1.34	1.21	1.15	1.10	1.01	.928	.894	.862	.804	.731
37	25.491	1.59	1.42	1.28	1.21	1.16	1.06	.981	.944	.911	.850	.772
38	26.887	1.68	1.49	1.34	1.28	1.22	1.12	1.03	.996	.960	.896	.815
39	28.321	1.77	1.57	1.42	1.35	1.29	1.18	1.09	1.05	1.01	.944	.858
40	29.792	1.86	1.66	1.49	1.42	1.35	1.24	1.15	1.10	1.06	.993	.903
42	32.846	2.05	1.83	1.64	1.56	1.49	1.37	1.26	1.22	1.17	1.10	.995
44	36.048	2.25	2.00	1.80	1.72	1.64	1.50	1.39	1.34	1.29	1.20	1.09
46	39.400	2.46	2.19	1.97	1.88	1.79	1.64	1.52	1.46	1.40	1.31	1.19
48	42.901	2.68	2.38	2.15	2.04	1.95	1.79	1.65	1.59	1.53	1.43	1.30
50	46.550	2.91	2.59	2.33	2.21	2.12	1.94	1.79	1.72	1.66	1.55	1.41
52	50.348	3.15	2.80	2.52	2.40	2.29	2.10	1.94	1.86	1.80	1.68	1.53
54	54.296	3.39	3.02	2.72	2.59	2.47	2.26	2.09	2.01	1.94	1.81	1.65
56	58.392	3.65	3.24	2.92	2.78	2.65	2.43	2.25	2.16	2.09	1.95	1.77
58	62.638	3.91	3.48	3.13	2.98	2.85	2.61	2.41	2.32	2.24	2.09	1.90
60	67.032	4.19	3.72	3.35	3.19	3.05	2.79	2.58	2.48	2.39	2.23	2.03
65	78.670	4.92	4.37	3.93	3.75	3.58	3.28	3.03	2.91	2.81	2.62	2.38
70	91.238	5.70	5.07	4.56	4.34	4.15	3.80	3.51	3.38	3.26	3.04	2.76
75	104.738	6.55	5.82	5.24	4.99	4.76	4.36	4.03	3.88	3.74	3.49	3.17
80	119.168	7.45	6.62	5.96	5.68	5.42	4.97	4.58	4.41	4.26	3.97	3.61
85	134.530	7.47	6.73	6.41	6.12	5.61	5.17	4.98	4.80	4.48	4.08
90	150.822	8.38	7.54	7.18	6.89	6.28	5.81	5.59	5.39	5.03	4.57
95	168.046	8.40	8.00	7.64	7.00	6.46	6.22	6.00	5.60	5.09
100	186.200	8.87	8.46	7.76	7.16	6.90	6.65	6.21	5.64

For Simple Spans a Concentrated Center Load causing an 18000 # per sq. inch fibre stress is 50% of the Uniformly Distributed Load. Deflection caused by a Concentrated Center Load is 0.01490 L² or 80% of that of a Uniformly Distributed Load shown in the above tables.

For fibre stresses other than 18000 # per sq. inch on which the above table is based, the deflection is directly proportional to the flange stress developed. Thus a fibre stress of 12000 # per sq. inch gives a deflection equal to $\frac{2}{3}$ of that shown in the above tables.

DEFLECTION

Based on Modulus of Elasticity of 29 000 000.

$$D = \frac{0.01862 L^2}{d}$$

Def. Coef. = 0.01862 L²

D = Deflection in inches for Symmetrical Beams and Girders, simple span, uniformly loaded to cause an 18000 # per sq. in. stress in the extreme fibre of the flange. (See notes below).

L = Span in feet

d = depth in inches

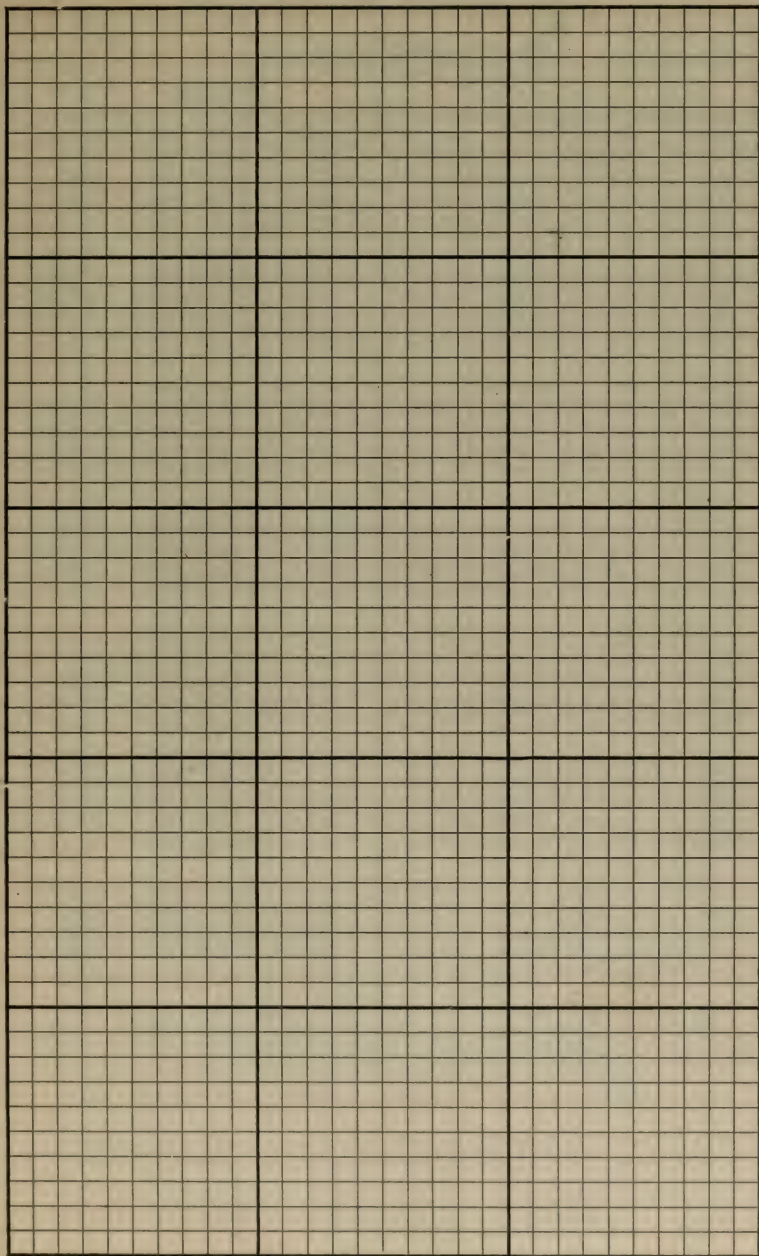
For deflection of beams of depths not listed below divide the Deflection Coefficient by the depth in inches.

Span in Feet	Deflection Coefficient	d = depth in inches.										
		36	39	42	48	54	60	66	72	84	96	108
6	.6703	.019
7	.9123	.025
8	1.192	.033
9	1.508	.042
10	1.862	.052	.048	.044	.039
11	2.253	.063	.058	.054	.047
12	2.681	.074	.069	.064	.056
13	3.147	.087	.081	.075	.066
14	3.650	.101	.094	.087	.076
15	4.190	.116	.107	.100	.087	.078	.070
16	4.767	.132	.122	.114	.099	.088	.080
17	5.381	.149	.138	.128	.112	.100	.090
18	6.033	.168	.155	.144	.126	.112	.101
19	6.722	.187	.172	.160	.140	.124	.112
20	7.448	.207	.191	.177	.155	.138	.124	.113	.103	.088	.078	.069
21	8.211	.228	.211	.195	.171	.152	.137	.124	.114	.098	.086	.076
22	9.012	.250	.231	.215	.188	.167	.150	.137	.125	.107	.094	.083
23	9.850	.274	.253	.235	.205	.183	.164	.149	.137	.117	.103	.091
24	10.725	.298	.275	.255	.224	.199	.179	.163	.149	.128	.112	.099
25	11.638	.323	.298	.277	.243	.216	.194	.176	.162	.139	.121	.108
26	12.587	.350	.323	.300	.262	.233	.210	.191	.175	.150	.131	.117
27	13.574	.377	.348	.323	.283	.251	.226	.206	.188	.162	.141	.126
28	14.598	.406	.374	.348	.304	.270	.243	.221	.203	.174	.152	.135
29	15.659	.435	.402	.373	.326	.290	.261	.237	.218	.186	.163	.145
30	16.758	.466	.430	.399	.349	.310	.279	.254	.233	.200	.175	.155
31	17.894	.497	.459	.426	.373	.331	.298	.271	.249	.213	.186	.166
32	19.067	.530	.489	.454	.398	.353	.318	.289	.265	.227	.199	.177
33	20.277	.563	.520	.483	.423	.376	.338	.307	.282	.241	.211	.188
34	21.525	.598	.552	.513	.449	.399	.359	.326	.299	.256	.224	.199
35	22.810	.634	.585	.543	.475	.422	.380	.346	.317	.272	.238	.211
36	24.132	.670	.619	.575	.503	.447	.402	.366	.335	.287	.251	.223
37	25.491	.708	.654	.607	.531	.472	.425	.386	.354	.304	.266	.236
38	26.887	.747	.689	.640	.560	.498	.448	.407	.373	.320	.280	.249
39	28.321	.787	.726	.674	.590	.525	.472	.429	.393	.337	.295	.262
40	29.792	.828	.764	.709	.621	.552	.497	.451	.414	.355	.310	.276
42	32.846	.912	.842	.782	.684	.608	.548	.498	.456	.390	.342	.304
44	36.048	1.00	.924	.858	.751	.668	.601	.546	.501	.429	.376	.334
46	39.400	1.09	1.01	.938	.821	.730	.657	.597	.547	.469	.410	.365
48	42.901	1.19	1.10	1.02	.894	.794	.745	.650	.596	.511	.447	.397
50	46.550	1.29	1.19	1.11	.970	.862	.776	.705	.647	.554	.485	.431
52	50.348	1.40	1.29	1.20	1.05	.932	.839	.763	.699	.599	.524	.466
54	54.296	1.51	1.39	1.29	1.11	1.01	.905	.823	.754	.646	.566	.503
56	58.392	1.62	1.50	1.39	1.22	1.08	.973	.885	.811	.695	.608	.541
58	62.638	1.74	1.61	1.49	1.31	1.16	1.04	.949	.870	.746	.653	.580
60	67.032	1.86	1.72	1.60	1.40	1.24	1.12	1.02	.931	.798	.698	.621
65	78.670	2.19	2.02	1.87	1.64	1.46	1.31	1.19	1.09	.937	.819	.728
70	91.238	2.53	2.34	2.17	1.90	1.69	1.52	1.38	1.27	1.09	.950	.845
75	104.738	2.91	2.69	2.49	2.18	1.94	1.75	1.59	1.45	1.25	1.09	.970
80	119.168	3.31	3.06	2.84	2.48	2.21	1.99	1.81	1.66	1.42	1.24	1.10
85	134.530	3.74	3.45	3.20	2.81	2.49	2.24	2.04	1.87	1.60	1.40	1.25
90	150.822	4.19	3.87	3.59	3.14	2.79	2.51	2.29	2.10	1.80	1.57	1.40
95	168.046	4.67	4.31	4.00	3.50	3.11	2.80	2.55	2.33	2.00	1.75	1.56
100	186.200	5.17	4.77	4.43	3.88	3.45	3.10	2.82	2.59	2.22	1.94	1.72

For Simple Spans a Concentrated Center Load causing an 18000 # per sq. inch fibre stress is 50% of the Uniformly Distributed Load. Deflection caused by a Concentrated Center Load is 0.01490 L² or 80% of that of a Uniformly Distributed Load shown in the above tables.

For fibre stresses other than 18000 # per sq. inch on which the above table is based, the deflection is directly proportional to the flange stress developed. Thus a fibre stress of 12000 # per sq. inch gives a deflection equal to $\frac{2}{3}$ of that shown in the above tables.

NOTES and DIAGRAMS



.01 TO .49 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
.01	.0001	.000001	0.1000	0.2154	$\bar{2}.00000$	100000.000	.03142	.000079
.02	.0004	.000008	0.1414	0.2714	$\bar{2}.30103$	50000.000	.06283	.000314
.03	.0009	.000027	0.1732	0.3107	$\bar{2}.47712$	33333.333	.09425	.000707
.04	.0016	.000064	0.2000	0.3420	$\bar{2}.60206$	25000.000	.12566	.001257
.05	.0025	.000125	0.2236	0.3684	$\bar{2}.69897$	20000.000	.15708	.001964
.06	.0036	.000216	0.2449	0.3915	$\bar{2}.77815$	16666.667	.18850	.002827
.07	.0049	.000343	0.2646	0.4121	$\bar{2}.84510$	14285.714	.21991	.003849
.08	.0064	.000512	0.2828	0.4309	$\bar{2}.90309$	12500.000	.25133	.005027
.09	.0081	.000729	0.3000	0.4481	$\bar{2}.95424$	11111.111	.28274	.006362
.10	.0100	.001000	0.3162	0.4642	$\bar{1}.00000$	10000.000	.31416	.007854
.11	.0121	.001331	0.3317	0.4791	$\bar{1}.04139$	9090.909	.34558	.009503
.12	.0144	.001728	0.3464	0.4932	$\bar{1}.07918$	8333.333	.37699	.011310
.13	.0169	.002197	0.3606	0.5066	$\bar{1}.11394$	7692.308	.40841	.013273
.14	.0196	.002744	0.3742	0.5192	$\bar{1}.14613$	7142.857	.43982	.015394
.15	.0225	.003375	0.3873	0.5313	$\bar{1}.17609$	6666.667	.47124	.017672
.16	.0256	.004096	0.4000	0.5429	$\bar{1}.20412$	6250.000	.50265	.020106
.17	.0289	.004913	0.4123	0.5540	$\bar{1}.23045$	5882.353	.53407	.022698
.18	.0324	.005832	0.4243	0.5646	$\bar{1}.25527$	5555.556	.56549	.025447
.19	.0361	.006859	0.4359	0.5749	$\bar{1}.27875$	5263.158	.59690	.028353
.20	.0400	.008000	0.4472	0.5848	$\bar{1}.30103$	5000.000	.62832	.031416
.21	.0441	.009261	0.4583	0.5944	$\bar{1}.32222$	4761.905	.65973	.034636
.22	.0484	.010648	0.4690	0.6037	$\bar{1}.34242$	4545.455	.69115	.038013
.23	.0529	.012167	0.4796	0.6127	$\bar{1}.36173$	4347.826	.72257	.041548
.24	.0576	.013824	0.4899	0.6214	$\bar{1}.38021$	4166.667	.75398	.045239
.25	.0625	.015625	0.5000	0.6300	$\bar{1}.39794$	4000.000	.78540	.049087
.26	.0676	.017576	0.5099	0.6383	$\bar{1}.41497$	3846.154	.81681	.053093
.27	.0729	.019683	0.5196	0.6463	$\bar{1}.43136$	3703.704	.84823	.057256
.28	.0784	.021952	0.5292	0.6542	$\bar{1}.44716$	3571.429	.87965	.061575
.29	.0841	.024389	0.5385	0.6619	$\bar{1}.46240$	3448.276	.91106	.066052
.30	.0900	.027000	0.5477	0.6694	$\bar{1}.47712$	3333.333	.94248	.070686
.31	.0961	.029791	0.5568	0.6768	$\bar{1}.49136$	3225.807	.97389	.075477
.32	.1024	.032768	0.5657	0.6840	$\bar{1}.50515$	3125.000	1.00531	.080425
.33	.1089	.035937	0.5745	0.6910	$\bar{1}.51851$	3030.303	1.03673	.085530
.34	.1156	.039304	0.5831	0.6980	$\bar{1}.53148$	2941.177	1.06814	.090792
.35	.1225	.042875	0.5916	0.7047	$\bar{1}.54407$	2857.143	1.09956	.096211
.36	.1296	.046656	0.6000	0.7114	$\bar{1}.55630$	2777.778	1.13097	.101788
.37	.1369	.050653	0.6083	0.7179	$\bar{1}.56820$	2702.703	1.16239	.107521
.38	.1444	.054872	0.6164	0.7243	$\bar{1}.57978$	2631.579	1.19381	.113411
.39	.1521	.059319	0.6245	0.7306	$\bar{1}.59106$	2564.103	1.22522	.119459
.40	.1600	.064000	0.6325	0.7368	$\bar{1}.60206$	2500.000	1.2566	.125664
.41	.1681	.068921	0.6403	0.7429	$\bar{1}.61278$	2439.024	1.2881	.132025
.42	.1764	.074088	0.6481	0.7489	$\bar{1}.62325$	2380.952	1.3195	.138544
.43	.1849	.079507	0.6557	0.7548	$\bar{1}.63347$	2325.581	1.3509	.145220
.44	.1936	.085184	0.6633	0.7606	$\bar{1}.64345$	2272.727	1.3823	.152053
.45	.2025	.091125	0.6708	0.7663	$\bar{1}.65321$	2222.222	1.4137	.159043
.46	.2116	.097336	0.6782	0.7719	$\bar{1}.66276$	2173.913	1.4451	.166190
.47	.2209	.103823	0.6856	0.7775	$\bar{1}.67210$	2127.660	1.4765	.173494
.48	.2304	.110592	0.6928	0.7830	$\bar{1}.68124$	2083.333	1.5080	.180956
.49	.2401	.117649	0.7000	0.7884	$\bar{1}.69020$	2040.816	1.5394	.188574

FUNCTIONS OF NUMBERS

.50 TO .99

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
.50	.2500	.125000	0.7071	0.7937	$\bar{1}.69897$	2000.000	1.5708	.19635
.51	.2601	.132651	0.7141	0.7990	$\bar{1}.70757$	1960.784	1.6022	.20428
.52	.2704	.140608	0.7211	0.8041	$\bar{1}.71600$	1923.077	1.6336	.21237
.53	.2809	.148877	0.7280	0.8093	$\bar{1}.72428$	1886.793	1.6650	.22062
.54	.2916	.157464	0.7348	0.8143	$\bar{1}.73239$	1851.852	1.6965	.22902
.55	.3025	.166375	0.7416	0.8193	$\bar{1}.74036$	1818.182	1.7279	.23758
.56	.3136	.175616	0.7483	0.8243	$\bar{1}.74819$	1785.714	1.7593	.24630
.57	.3249	.185193	0.7550	0.8291	$\bar{1}.75587$	1754.386	1.7907	.25518
.58	.3364	.195112	0.7616	0.8340	$\bar{1}.76343$	1724.138	1.8221	.26401
.59	.3481	.205379	0.7681	0.8387	$\bar{1}.77085$	1694.915	1.8535	.27340
.60	.3600	.216000	0.7746	0.8434	$\bar{1}.77815$	1666.667	1.8850	.28274
.61	.3721	.226981	0.7810	0.8481	$\bar{1}.78533$	1639.344	1.9164	.29225
.62	.3844	.238328	0.7874	0.8527	$\bar{1}.79239$	1612.903	1.9478	.30191
.63	.3969	.250047	0.7937	0.8573	$\bar{1}.79934$	1587.302	1.9792	.31173
.64	.4096	.262144	0.8000	0.8618	$\bar{1}.80618$	1562.500	2.0106	.32170
.65	.4225	.274625	0.8062	0.8662	$\bar{1}.81291$	1538.462	2.0420	.33183
.66	.4356	.287496	0.8124	0.8707	$\bar{1}.81954$	1515.152	2.0735	.34212
.67	.4489	.300763	0.8185	0.8750	$\bar{1}.82607$	1492.537	2.1049	.35257
.68	.4624	.314432	0.8246	0.8794	$\bar{1}.83251$	1470.588	2.1363	.36317
.69	.4761	.328509	0.8307	0.8837	$\bar{1}.83885$	1449.275	2.1677	.37393
.70	.4900	.343000	0.8367	0.8879	$\bar{1}.84510$	1428.571	2.1991	.38485
.71	.5041	.357911	0.8426	0.8921	$\bar{1}.85126$	1408.451	2.2305	.39592
.72	.5184	.373248	0.8485	0.8963	$\bar{1}.85733$	1388.889	2.2620	.40715
.73	.5329	.389017	0.8544	0.9004	$\bar{1}.86332$	1369.863	2.2934	.41854
.74	.5476	.405224	0.8602	0.9045	$\bar{1}.86923$	1351.351	2.3248	.43008
.75	.5625	.421875	0.8660	0.9086	$\bar{1}.87506$	1333.333	2.3562	.44179
.76	.5776	.438976	0.8718	0.9126	$\bar{1}.88081$	1315.790	2.3876	.45365
.77	.5929	.456533	0.8775	0.9166	$\bar{1}.88649$	1298.701	2.4190	.46566
.78	.6084	.474552	0.8832	0.9205	$\bar{1}.89209$	1282.051	2.4504	.47784
.79	.6241	.493039	0.8888	0.9244	$\bar{1}.89763$	1265.823	2.4819	.49017
.80	.6400	.512000	0.8944	0.9283	$\bar{1}.90309$	1250.000	2.5133	.50266
.81	.6561	.531441	0.9000	0.9322	$\bar{1}.90849$	1234.568	2.5447	.51530
.82	.6724	.551368	0.9055	0.9360	$\bar{1}.91381$	1219.512	2.5761	.52810
.83	.6889	.571787	0.9110	0.9398	$\bar{1}.91908$	1204.819	2.6075	.54106
.84	.7056	.592704	0.9165	0.9435	$\bar{1}.92428$	1190.476	2.6389	.55418
.85	.7225	.614125	0.9220	0.9473	$\bar{1}.92942$	1176.471	2.6704	.56745
.86	.7396	.636056	0.9274	0.9510	$\bar{1}.93450$	1162.791	2.7018	.58088
.87	.7569	.658503	0.9327	0.9546	$\bar{1}.93952$	1149.425	2.7332	.59447
.88	.7744	.681472	0.9381	0.9583	$\bar{1}.94448$	1136.364	2.7646	.60821
.89	.7921	.704969	0.9434	0.9619	$\bar{1}.94939$	1123.596	2.7960	.62211
.90	.8100	.729000	0.9487	0.9655	$\bar{1}.95424$	1111.111	2.8274	.63617
.91	.8281	.753571	0.9539	0.9691	$\bar{1}.95904$	1098.901	2.8589	.65039
.92	.8464	.778688	0.9592	0.9726	$\bar{1}.96379$	1086.957	2.8903	.66476
.93	.8649	.804357	0.9644	0.9761	$\bar{1}.96848$	1075.269	2.9217	.67929
.94	.8836	.830584	0.9695	0.9796	$\bar{1}.97313$	1063.830	2.9531	.69398
.95	.9025	.857375	0.9747	0.9830	$\bar{1}.97772$	1052.632	2.9845	.70882
.96	.9216	.884736	0.9798	0.9865	$\bar{1}.98227$	1041.667	3.0159	.72382
.97	.9409	.912673	0.9849	0.9899	$\bar{1}.98677$	1030.928	3.0473	.73898
.98	.9604	.941192	0.9899	0.9933	$\bar{1}.99123$	1020.408	3.0788	.75430
.99	.9801	.970299	0.9950	0.9967	$\bar{1}.99564$	1010.101	3.1102	.76977

1 TO 49 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
1	1	1	1.0000	1.0000	0.00000	1000.000	3.142	0.7854
2	4	8	1.4142	1.2599	0.30103	500.000	6.283	3.1416
3	9	27	1.7321	1.4422	0.47712	333.333	9.425	7.0686
4	16	64	2.0000	1.5874	0.60206	250.000	12.566	12.5664
5	25	125	2.2361	1.7100	0.69897	200.000	15.708	19.6350
6	36	216	2.4495	1.8171	0.77815	166.667	18.850	28.2743
7	49	343	2.6458	1.9129	0.84510	142.857	21.991	38.4845
8	64	512	2.8284	2.0000	0.90309	125.000	25.133	50.2655
9	81	729	3.0000	2.0801	0.95424	111.111	28.274	63.6173
10	100	1000	3.1623	2.1544	1.00000	100.000	31.416	78.5398
11	121	1331	3.3166	2.2240	1.04139	90.9091	34.558	95.0332
12	144	1728	3.4641	2.2894	1.07918	83.3333	37.699	113.097
13	169	2197	3.6056	2.3513	1.11394	76.9231	40.841	132.732
14	196	2744	3.7417	2.4101	1.14613	71.4286	43.982	153.938
15	225	3375	3.8730	2.4662	1.17609	66.6667	47.124	176.715
16	256	4096	4.0000	2.5198	1.20412	62.5000	50.265	201.062
17	289	4913	4.1231	2.5713	1.23045	58.8235	53.407	226.980
18	324	5832	4.2426	2.6207	1.25527	55.5556	56.549	254.469
19	361	6859	4.3589	2.6684	1.27875	52.6316	59.690	283.529
20	400	8000	4.4721	2.7144	1.30103	50.0000	62.832	314.159
21	441	9261	4.5826	2.7589	1.32222	47.6190	65.973	346.361
22	484	10648	4.6904	2.8020	1.34242	45.4545	69.115	380.133
23	529	12167	4.7958	2.8439	1.36173	43.4783	72.257	415.476
24	576	13824	4.8990	2.8845	1.38021	41.6667	75.398	452.389
25	625	15625	5.0000	2.9240	1.39794	40.0000	78.540	490.874
26	676	17576	5.0990	2.9625	1.41497	38.4615	81.681	530.929
27	729	19683	5.1962	3.0000	1.43136	37.0370	84.823	572.555
28	784	21952	5.2915	3.0366	1.44716	35.7143	87.965	615.752
29	841	24389	5.3852	3.0723	1.46240	34.4828	91.106	660.520
30	900	27000	5.4772	3.1072	1.47712	33.3333	94.248	706.858
31	961	29791	5.5678	3.1414	1.49136	32.2581	97.389	754.768
32	1024	32768	5.6569	3.1748	1.50515	31.2500	100.531	804.248
33	1089	35937	5.7446	3.2075	1.51851	30.3030	103.673	855.299
34	1156	39304	5.8310	3.2396	1.53148	29.4118	106.814	907.920
35	1225	42875	5.9161	3.2711	1.54407	28.5714	109.956	962.113
36	1296	46656	6.0000	3.3019	1.55630	27.7778	113.097	1017.88
37	1369	50653	6.0828	3.3322	1.56820	27.0270	116.239	1075.21
38	1444	54872	6.1644	3.3620	1.57978	26.3158	119.381	1134.11
39	1521	59319	6.2450	3.3912	1.59106	25.6410	122.522	1194.59
40	1600	64000	6.3246	3.4200	1.60206	25.0000	125.66	1256.64
41	1681	68921	6.4031	3.4482	1.61278	24.3902	128.81	1320.25
42	1764	74088	6.4807	3.4760	1.62325	23.8095	131.95	1385.44
43	1849	79507	6.5574	3.5034	1.63347	23.2558	135.09	1452.20
44	1936	85184	6.6332	3.5303	1.64345	22.7273	138.23	1520.53
45	2025	91125	6.7082	3.5569	1.65321	22.2222	141.37	1590.43
46	2116	97336	6.7823	3.5830	1.66276	21.7391	144.51	1661.90
47	2209	103823	6.8557	3.6088	1.67210	21.2766	147.65	1734.94
48	2304	110592	6.9282	3.6342	1.68124	20.8333	150.80	1809.56
49	2401	117649	7.0000	3.6593	1.69020	20.4082	153.94	1885.74

FUNCTIONS OF NUMBERS

50 TO 99

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000	No. = Diameter	
						× Reciprocal	Circum.	Area
50	2500	125000	7.0711	3.6840	1.69897	20.0000	157.08	1963.50
51	2601	132651	7.1414	3.7084	1.70757	19.6078	160.22	2042.82
52	2704	140608	7.2111	3.7325	1.71600	19.2308	163.36	2123.72
53	2809	148877	7.2801	3.7563	1.72428	18.8679	166.50	2206.18
54	2916	157464	7.3485	3.7798	1.73239	18.5185	169.65	2290.22
55	3025	166375	7.4162	3.8030	1.74036	18.1818	172.79	2375.83
56	3136	175616	7.4833	3.8259	1.74819	17.8571	175.93	2463.01
57	3249	185193	7.5498	3.8485	1.75587	17.5439	179.07	2551.76
58	3364	195112	7.6158	3.8709	1.76343	17.2414	182.21	2642.08
59	3481	205379	7.6811	3.8930	1.77085	16.9492	185.35	2733.97
60	3600	216000	7.7460	3.9149	1.77815	16.6667	188.50	2827.43
61	3721	226981	7.8102	3.9365	1.78533	16.3934	191.64	2922.47
62	3844	238328	7.8740	3.9579	1.79239	16.1290	194.78	3019.07
63	3969	250047	7.9373	3.9791	1.79934	15.8730	197.92	3117.25
64	4096	262144	8.0000	4.0000	1.80618	15.6250	201.06	3216.99
65	4225	274625	8.0623	4.0207	1.81291	15.3846	204.20	3318.31
66	4356	287496	8.1240	4.0412	1.81954	15.1515	207.35	3421.19
67	4489	300763	8.1854	4.0615	1.82607	14.9254	210.49	3525.65
68	4624	314432	8.2462	4.0817	1.83251	14.7059	213.63	3631.68
69	4761	328509	8.3066	4.1016	1.83885	14.4928	216.77	3739.28
70	4900	343000	8.3666	4.1213	1.84510	14.2857	219.91	3848.45
71	5041	357911	8.4261	4.1408	1.85126	14.0845	223.05	3959.19
72	5184	373248	8.4853	4.1602	1.85733	13.8889	226.19	4071.50
73	5329	389017	8.5440	4.1793	1.86332	13.6986	229.34	4185.39
74	5476	405224	8.6023	4.1983	1.86923	13.5135	232.48	4300.84
75	5625	421875	8.6603	4.2172	1.87506	13.3333	235.62	4417.86
76	5776	438976	8.7178	4.2358	1.88081	13.1579	238.76	4536.46
77	5929	456533	8.7750	4.2543	1.88649	12.9870	241.90	4656.63
78	6084	474552	8.8318	4.2727	1.89209	12.8205	245.04	4778.36
79	6241	493039	8.8882	4.2908	1.89763	12.6582	248.19	4901.67
80	6400	512000	8.9443	4.3089	1.90309	12.5000	251.33	5026.55
81	6561	531441	9.0000	4.3267	1.90849	12.3457	254.47	5153.00
82	6724	551368	9.0554	4.3445	1.91381	12.1951	257.61	5281.02
83	6889	571787	9.1104	4.3621	1.91908	12.0482	260.75	5410.61
84	7056	592704	9.1652	4.3795	1.92428	11.9048	263.89	5541.77
85	7225	614125	9.2195	4.3968	1.92942	11.7647	267.04	5674.50
86	7396	636056	9.2736	4.4140	1.93450	11.6279	270.18	5808.80
87	7569	658503	9.3274	4.4310	1.93952	11.4943	273.32	5944.68
88	7744	681472	9.3808	4.4480	1.94448	11.3636	276.46	6082.12
89	7921	704969	9.4340	4.4647	1.94939	11.2360	279.60	6221.14
90	8100	729000	9.4868	4.4814	1.95424	11.1111	282.74	6361.73
91	8281	753571	9.5394	4.4979	1.95904	10.9890	285.88	6503.88
92	8464	778688	9.5917	4.5144	1.96379	10.8696	289.03	6647.61
93	8649	804357	9.6437	4.5307	1.96848	10.7527	292.17	6792.91
94	8836	830584	9.6954	4.5468	1.97313	10.6383	295.31	6939.78
95	9025	857375	9.7468	4.5629	1.97772	10.5263	298.45	7088.22
96	9216	884736	9.7980	4.5789	1.98227	10.4167	301.59	7238.23
97	9409	912673	9.8489	4.5947	1.98677	10.3093	304.73	7389.81
98	9604	941192	9.8995	4.6104	1.99123	10.2041	307.88	7542.96
99	9801	970299	9.9499	4.6261	1.99564	10.1010	311.02	7697.69

100 TO 149

FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000	No. = Diameter	
						×	Circum.	Area
						Reciprocal		
100	10000	1000000	10.0000	4.6416	2.00000	10.0000	314.16	7853.98
101	10201	1030301	10.0499	4.6570	2.00432	9.90099	317.30	8011.85
102	10404	1061208	10.0995	4.6723	2.00860	9.80392	320.44	8171.28
103	10609	1092727	10.1489	4.6875	2.01284	9.70874	323.58	8332.29
104	10816	1124864	10.1980	4.7027	2.01703	9.61538	326.73	8494.87
105	11025	1157625	10.2470	4.7177	2.02119	9.52381	329.87	8659.01
106	11236	1191016	10.2956	4.7326	2.02531	9.43396	333.01	8824.73
107	11449	1225043	10.3441	4.7475	2.02938	9.34579	336.15	8992.02
108	11664	1259712	10.3923	4.7622	2.03342	9.25926	339.29	9160.88
109	11881	1295029	10.4403	4.7769	2.03743	9.17431	342.43	9331.32
110	12100	1331000	10.4881	4.7914	2.04139	9.09091	345.58	9503.32
111	12321	1367631	10.5357	4.8059	2.04532	9.00901	348.72	9676.89
112	12544	1404928	10.5830	4.8203	2.04922	8.92857	351.86	9852.03
113	12769	1442897	10.6301	4.8346	2.05308	8.84956	355.00	10028.7
114	12996	1481544	10.6771	4.8488	2.05690	8.77193	358.14	10207.0
115	13225	1520875	10.7238	4.8629	2.06070	8.69565	361.28	10386.9
116	13456	1560896	10.7703	4.8770	2.06446	8.62069	364.42	10568.3
117	13689	1601613	10.8167	4.8910	2.06819	8.54701	367.57	10751.3
118	13924	1643032	10.8628	4.9049	2.07188	8.47458	370.71	10935.9
119	14161	1685159	10.9087	4.9187	2.07555	8.40336	373.85	11122.0
120	14400	1728000	10.9545	4.9324	2.07918	8.33333	376.99	11309.7
121	14641	1771561	11.0000	4.9461	2.08279	8.26446	380.13	11499.0
122	14884	1815848	11.0454	4.9597	2.08636	8.19672	383.27	11689.9
123	15129	1860867	11.0905	4.9732	2.08991	8.13008	386.42	11882.3
124	15376	1906624	11.1355	4.9866	2.09342	8.06452	389.56	12076.3
125	15625	1953125	11.1803	5.0000	2.09691	8.00000	392.70	12271.8
126	15876	2000376	11.2250	5.0133	2.10037	7.93651	395.84	12469.0
127	16129	2048383	11.2694	5.0265	2.10380	7.87402	398.98	12667.7
128	16384	2097152	11.3137	5.0397	2.10721	7.81250	402.12	12868.0
129	16641	2146689	11.3578	5.0528	2.11059	7.75194	405.27	13069.8
130	16900	2197000	11.4018	5.0658	2.11394	7.69231	408.41	13273.2
131	17161	2248091	11.4455	5.0788	2.11727	7.63359	411.55	13478.2
132	17424	2299968	11.4891	5.0916	2.12057	7.57576	414.69	13684.8
133	17689	2352637	11.5326	5.1045	2.12385	7.51880	417.83	13892.9
134	17956	2406104	11.5758	5.1172	2.12710	7.46269	420.97	14102.6
135	18225	2460375	11.6190	5.1299	2.13033	7.40741	424.12	14313.9
136	18496	2515456	11.6619	5.1426	2.13354	7.35294	427.26	14526.7
137	18769	2571353	11.7047	5.1551	2.13672	7.29927	430.40	14741.1
138	19044	2628072	11.7473	5.1676	2.13988	7.24638	433.54	14957.1
139	19321	2685619	11.7898	5.1801	2.14301	7.19424	436.68	15174.7
140	19600	2744000	11.8322	5.1925	2.14613	7.14286	439.82	15393.8
141	19881	2803221	11.8743	5.2048	2.14922	7.09220	442.96	15614.5
142	20164	2863288	11.9164	5.2171	2.15229	7.04225	446.11	15836.8
143	20449	2924207	11.9583	5.2293	2.15534	6.99301	449.25	16060.6
144	20736	2985984	12.0000	5.2415	2.15836	6.94444	452.39	16286.0
145	21025	3048625	12.0416	5.2536	2.16137	6.89655	455.53	16513.0
146	21316	3112136	12.0830	5.2656	2.16435	6.84932	458.67	16741.5
147	21609	3176523	12.1244	5.2776	2.16732	6.80272	461.81	16971.7
148	21904	3241792	12.1655	5.2896	2.17026	6.75676	464.96	17203.4
149	22201	3307949	12.2066	5.3015	2.17319	6.71141	468.10	17436.6

FUNCTIONS OF NUMBERS

150 TO 199

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
150	22500	3375000	12.2474	5.3133	2.17609	6.66667	471.24	17671.5
151	22801	3442951	12.2882	5.3251	2.17898	6.62252	474.38	17907.9
152	23104	3511808	12.3288	5.3368	2.18184	6.57895	477.52	18145.8
153	23409	3581577	12.3693	5.3485	2.18469	6.53595	480.66	18385.4
154	23716	3652264	12.4097	5.3601	2.18752	6.49351	483.81	18626.5
155	24025	3723875	12.4499	5.3717	2.19033	6.45161	486.95	18869.2
156	24336	3796416	12.4900	5.3832	2.19312	6.41026	490.09	19113.4
157	24649	3869893	12.5300	5.3947	2.19590	6.36943	493.23	19359.3
158	24964	3944312	12.5698	5.4061	2.19866	6.32911	496.37	19606.7
159	25281	4019679	12.6095	5.4175	2.20140	6.28931	499.51	19855.7
160	25600	4096000	12.6491	5.4288	2.20412	6.25000	502.65	20106.2
161	25921	4173281	12.6886	5.4401	2.20683	6.21118	505.80	20358.3
162	26244	4251528	12.7279	5.4514	2.20952	6.17284	508.94	20612.0
163	26569	4330747	12.7671	5.4626	2.21219	6.13497	512.08	20867.2
164	26896	4410944	12.8062	5.4737	2.21484	6.09756	515.22	21124.1
165	27225	4492125	12.8452	5.4848	2.21748	6.06061	518.36	21382.5
166	27556	4574296	12.8841	5.4959	2.22011	6.02410	521.50	21642.4
167	27889	4657463	12.9228	5.5069	2.22272	5.98802	524.65	21904.0
168	28224	4741632	12.9615	5.5178	2.22531	5.95238	527.79	22167.1
169	28561	4826809	13.0000	5.5288	2.22789	5.91716	530.93	22431.8
170	28900	4913000	13.0384	5.5397	2.23045	5.88235	534.07	22698.0
171	29241	5000211	13.0767	5.5505	2.23300	5.84795	537.21	22965.8
172	29584	5088448	13.1149	5.5613	2.23553	5.81395	540.35	23235.2
173	29929	5177717	13.1529	5.5721	2.23805	5.78035	543.50	23506.2
174	30276	5268024	13.1909	5.5828	2.24055	5.74713	546.64	23778.7
175	30625	5359375	13.2288	5.5934	2.24304	5.71429	549.78	24052.8
176	30976	5451776	13.2665	5.6041	2.24551	5.68182	552.92	24328.5
177	31329	5545233	13.3041	5.6147	2.24797	5.64972	556.06	24605.7
178	31684	5639752	13.3417	5.6252	2.25042	5.61798	559.20	24884.6
179	32041	5735339	13.3791	5.6357	2.25285	5.58659	562.35	25164.9
180	32400	5832000	13.4164	5.6462	2.25527	5.55556	565.49	25446.9
181	32761	5929741	13.4536	5.6567	2.25768	5.52486	568.63	25730.4
182	33124	6028568	13.4907	5.6671	2.26007	5.49451	571.77	26015.5
183	33489	6128487	13.5277	5.6774	2.26245	5.46448	574.91	26302.2
184	33856	6229504	13.5647	5.6877	2.26482	5.43478	578.05	26590.4
185	34225	6331625	13.6015	5.6980	2.26717	5.40541	581.19	26880.3
186	34596	6434856	13.6382	5.7083	2.26951	5.37634	584.34	27171.6
187	34969	6539203	13.6748	5.7185	2.27184	5.34759	587.48	27464.6
188	35344	6644672	13.7113	5.7287	2.27416	5.31915	590.62	27759.1
189	35721	6751269	13.7477	5.7388	2.27646	5.29101	593.76	28055.2
190	36100	6859000	13.7840	5.7489	2.27875	5.26316	596.90	28352.9
191	36481	6967871	13.8203	5.7590	2.28103	5.23560	600.04	28652.1
192	36864	7077888	13.8564	5.7690	2.28330	5.20833	603.19	28952.9
193	37249	7189057	13.8924	5.7790	2.28556	5.18135	606.33	29255.3
194	37636	7301384	13.9284	5.7890	2.28780	5.15464	609.47	29559.2
195	38025	7414875	13.9642	5.7989	2.29003	5.12821	612.61	29864.8
196	38416	7529536	14.0000	5.8088	2.29226	5.10204	615.75	30171.9
197	38809	7645373	14.0357	5.8186	2.29447	5.07614	618.89	30480.5
198	39204	7762392	14.0712	5.8285	2.29667	5.05051	622.04	30790.7
199	39601	7880599	14.1067	5.8383	2.29885	5.02513	625.18	31102.6

200 TO 249

FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×		No. = Diameter	
						Reciprocal		Circum.	Area
200	40000	8000000	14.1421	5.8480	2.30103	5.00000		628.32	31415.9
201	40401	8120601	14.1774	5.8578	2.30320	4.97512		631.46	31730.9
202	40804	8242408	14.2127	5.8675	2.30535	4.95050		634.60	32047.4
203	41209	8365427	14.2478	5.8771	2.30750	4.92611		637.74	32365.5
204	41616	8489664	14.2829	5.8868	2.30963	4.90196		640.88	32685.1
205	42025	8615125	14.3178	5.8964	2.31175	4.87805		644.03	33006.4
206	42436	8741816	14.3527	5.9059	2.31387	4.85437		647.17	33329.2
207	42849	8869743	14.3875	5.9155	2.31597	4.83092		650.31	33653.5
208	43264	8998912	14.4222	5.9250	2.31806	4.80769		653.45	33979.5
209	43681	9129329	14.4568	5.9345	2.32015	4.78469		656.59	34307.0
210	44100	9261000	14.4914	5.9439	2.32222	4.76190		659.73	34636.1
211	44521	9393931	14.5258	5.9533	2.32428	4.73934		662.88	34966.7
212	44944	9528128	14.5602	5.9627	2.32634	4.71698		666.02	35298.9
213	45369	9663597	14.5945	5.9721	2.32838	4.69484		669.16	35632.7
214	45796	9800344	14.6287	5.9814	2.33041	4.67290		672.30	35968.1
215	46225	9938375	14.6629	5.9907	2.33244	4.65116		675.44	36305.0
216	46656	10077696	14.6969	6.0000	2.33445	4.62963		678.58	36643.5
217	47089	10218313	14.7309	6.0092	2.33646	4.60829		681.73	36983.6
218	47524	10360232	14.7648	6.0185	2.33846	4.58716		684.87	37325.3
219	47961	10503459	14.7986	6.0277	2.34044	4.56621		688.01	37668.5
220	48400	10648000	14.8324	6.0368	2.34242	4.54545		691.15	38013.3
221	48841	10793861	14.8661	6.0459	2.34439	4.52489		694.29	38359.6
222	49284	10941048	14.8997	6.0550	2.34635	4.50450		697.43	38707.6
223	49729	11089567	14.9332	6.0641	2.34830	4.48430		700.58	39057.1
224	50176	11239424	14.9666	6.0732	2.35025	4.46429		703.72	39408.1
225	50625	11390625	15.0000	6.0822	2.35218	4.44444		706.86	39760.8
226	51076	11543176	15.0333	6.0912	2.35411	4.42478		710.00	40115.0
227	51529	11697083	15.0665	6.1002	2.35603	4.40529		713.14	40470.8
228	51984	11852352	15.0997	6.1091	2.35793	4.38596		716.28	40828.1
229	52441	12008989	15.1327	6.1180	2.35984	4.36681		719.42	41187.1
230	52900	12167000	15.1658	6.1269	2.36173	4.34783		722.57	41547.6
231	53361	12326391	15.1987	6.1358	2.36361	4.32900		725.71	41909.6
232	53824	12487168	15.2315	6.1446	2.36549	4.31034		728.85	42273.3
233	54289	12649337	15.2643	6.1534	2.36736	4.29185		731.99	42638.5
234	54756	12812904	15.2971	6.1622	2.36922	4.27350		735.13	43005.3
235	55225	12977875	15.3297	6.1710	2.37107	4.25532		738.27	43373.6
236	55696	13144256	15.3623	6.1797	2.37291	4.23729		741.42	43743.5
237	56169	13312053	15.3948	6.1885	2.37475	4.21941		744.56	44115.0
238	56644	13481272	15.4272	6.1972	2.37658	4.20168		747.70	44488.1
239	57121	13651919	15.4596	6.2058	2.37840	4.18410		750.84	44862.7
240	57600	13824000	15.4919	6.2145	2.38021	4.16667		753.98	45238.9
241	58081	13997521	15.5242	6.2231	2.38202	4.14938		757.12	45616.7
242	58564	14172488	15.5563	6.2317	2.38382	4.13223		760.27	45996.1
243	59049	14348907	15.5885	6.2403	2.38561	4.11523		763.41	46377.0
244	59536	14526784	15.6205	6.2488	2.38739	4.09836		766.55	46759.5
245	60025	14706125	15.6525	6.2573	2.38917	4.08163		769.69	47143.5
246	60516	14886936	15.6844	6.2658	2.39094	4.06504		772.83	47529.2
247	61009	15069223	15.7162	6.2743	2.39270	4.04858		775.97	47916.4
248	61504	15252992	15.7480	6.2828	2.39445	4.03226		779.12	48305.1
249	62001	15438249	15.7797	6.2912	2.39620	4.01606		782.26	48695.5

FUNCTIONS OF NUMBERS

250 TO 299

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 × Reciprocal	No. = Diameter	
							Circum.	Area
250	62500	15625000	15.8114	6.2996	2.39794	4.00000	785.40	49087.4
251	63001	15813251	15.8430	6.3080	2.39967	3.98406	788.54	49480.9
252	63504	16003008	15.8745	6.3164	2.40140	3.96825	791.68	49875.9
253	64009	16194277	15.9060	6.3247	2.40312	3.95257	794.82	50272.6
254	64516	16387064	15.9374	6.3330	2.40483	3.93701	797.96	50670.7
255	65025	16581375	15.9687	6.3413	2.40654	3.92157	801.11	51070.5
256	65536	16777216	16.0000	6.3496	2.40824	3.90625	804.25	51471.9
257	66049	16974593	16.0312	6.3579	2.40993	3.89105	807.39	51874.8
258	66564	17173512	16.0624	6.3661	2.41162	3.87597	810.53	52279.2
259	67081	17373979	16.0935	6.3743	2.41330	3.86100	813.67	52685.3
260	67600	17576000	16.1245	6.3825	2.41497	3.84615	816.81	53092.9
261	68121	17779581	16.1555	6.3907	2.41664	3.83142	819.96	53502.1
262	68644	17984728	16.1864	6.3988	2.41830	3.81679	823.10	53912.9
263	69169	18191447	16.2173	6.4070	2.41996	3.80228	826.24	54325.2
264	69696	18399744	16.2481	6.4151	2.42160	3.78788	829.38	54739.1
265	70225	18609625	16.2788	6.4232	2.42325	3.77358	832.52	55154.6
266	70756	18821096	16.3095	6.4312	2.42488	3.75940	835.66	55571.6
267	71289	19034163	16.3401	6.4393	2.42651	3.74532	838.81	55990.2
268	71824	19248832	16.3707	6.4473	2.42813	3.73134	841.95	56410.4
269	72361	19465109	16.4012	6.4553	2.42975	3.71747	845.09	56832.2
270	72900	19683000	16.4317	6.4633	2.43136	3.70370	848.23	57255.5
271	73441	19902511	16.4621	6.4713	2.43297	3.69004	851.37	57680.4
272	73984	20123648	16.4924	6.4792	2.43457	3.67647	854.51	58106.9
273	74529	20346417	16.5227	6.4872	2.43616	3.66300	857.65	58534.9
274	75076	20570824	16.5529	6.4951	2.43775	3.64964	860.80	58964.6
275	75625	20796875	16.5831	6.5030	2.43933	3.63636	863.94	59395.7
276	76176	21024576	16.6132	6.5108	2.44091	3.62319	867.08	59828.5
277	76729	21253933	16.6433	6.5187	2.44248	3.61011	870.22	60262.8
278	77284	21484952	16.6733	6.5265	2.44404	3.59712	873.36	60698.7
279	77841	21717639	16.7033	6.5343	2.44560	3.58423	876.50	61136.2
280	78400	21952000	16.7332	6.5421	2.44716	3.57143	879.65	61575.2
281	78961	22188041	16.7631	6.5499	2.44871	3.55872	882.79	62015.8
282	79524	22425768	16.7929	6.5577	2.45025	3.54610	885.93	62458.0
283	80089	22665187	16.8226	6.5654	2.45179	3.53357	889.07	62901.8
284	80656	22906304	16.8523	6.5731	2.45332	3.52113	892.21	63347.1
285	81225	23149125	16.8819	6.5808	2.45484	3.50877	895.35	63794.0
286	81796	23393656	16.9115	6.5885	2.45637	3.49650	898.50	64242.4
287	82369	23639903	16.9411	6.5962	2.45788	3.48432	901.64	64692.5
288	82944	23887872	16.9706	6.6039	2.45939	3.47222	904.78	65144.1
289	83521	24137569	17.0000	6.6115	2.46090	3.46021	907.92	65597.2
290	84100	24389000	17.0294	6.6191	2.46240	3.44828	911.06	66052.0
291	84681	24642171	17.0587	6.6267	2.46389	3.43643	914.20	66508.3
292	85264	24897088	17.0880	6.6343	2.46538	3.42466	917.35	66966.2
293	85849	25153757	17.1172	6.6419	2.46687	3.41297	920.49	67425.6
294	86436	25412184	17.1464	6.6494	2.46835	3.40136	923.63	67886.7
295	87025	25672375	17.1756	6.6569	2.46982	3.38983	926.77	68349.3
296	87616	25934336	17.2047	6.6644	2.47129	3.37838	929.91	68813.4
297	88209	26198073	17.2337	6.6719	2.47276	3.36700	933.05	69279.2
298	88804	26463592	17.2627	6.6794	2.47422	3.35570	936.19	69746.5
299	89401	26730899	17.2916	6.6869	2.47567	3.34448	939.34	70215.4

300 TO 349 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
300	90000	27000000	17.3205	6.6943	2.47712	3.33333	942.48	70685.8
301	90601	27270901	17.3494	6.7018	2.47857	3.32226	945.62	71157.9
302	91204	27543608	17.3781	6.7092	2.48001	3.31126	948.76	71631.5
303	91809	27818127	17.4069	6.7166	2.48144	3.30033	951.90	72106.6
304	92416	28094464	17.4356	6.7240	2.48287	3.28947	955.04	72583.4
305	93025	28372625	17.4642	6.7313	2.48430	3.27869	958.19	73061.7
306	93636	28652616	17.4929	6.7387	2.48572	3.26797	961.33	73541.5
307	94249	28934443	17.5214	6.7460	2.48714	3.25733	964.47	74023.0
308	94864	29218112	17.5499	6.7533	2.48855	3.24675	967.61	74506.0
309	95481	29503629	17.5784	6.7606	2.48996	3.23625	970.75	74990.6
310	96100	29791000	17.6068	6.7679	2.49136	3.22581	973.89	75476.8
311	96721	30080231	17.6352	6.7752	2.49276	3.21543	977.04	75964.5
312	97344	30371328	17.6635	6.7824	2.49415	3.20513	980.18	76453.8
313	97969	30664297	17.6918	6.7897	2.49554	3.19489	983.32	76944.7
314	98596	30959144	17.7200	6.7969	2.49693	3.18471	986.46	77437.1
315	99225	31255875	17.7482	6.8041	2.49831	3.17460	989.60	77931.1
316	99856	31554496	17.7764	6.8113	2.49969	3.16456	992.74	78426.7
317	100489	31855013	17.8045	6.8185	2.50106	3.15457	995.88	78923.9
318	101124	32157432	17.8326	6.8256	2.50243	3.14465	999.03	79422.6
319	101761	32461759	17.8606	6.8328	2.50379	3.13480	1002.2	79922.9
320	102400	32768000	17.8885	6.8399	2.50515	3.12500	1005.3	80424.8
321	103041	33076161	17.9165	6.8470	2.50651	3.11526	1008.5	80928.2
322	103684	33386248	17.9444	6.8541	2.50786	3.10559	1011.6	81433.2
323	104329	33698267	17.9722	6.8612	2.50920	3.09598	1014.7	81939.8
324	104976	34012224	18.0000	6.8683	2.51055	3.08642	1017.9	82448.0
325	105625	34328125	18.0278	6.8753	2.51188	3.07692	1021.0	82957.7
326	106276	34645976	18.0555	6.8824	2.51322	3.06749	1024.2	83469.0
327	106929	34965783	18.0831	6.8894	2.51455	3.05810	1027.3	83981.8
328	107584	35287552	18.1108	6.8964	2.51587	3.04878	1030.4	84496.3
329	108241	35611289	18.1384	6.9034	2.51720	3.03951	1033.6	85012.3
330	108900	35937000	18.1659	6.9104	2.51851	3.03030	1036.7	85529.9
331	109561	36264691	18.1934	6.9174	2.51983	3.02115	1039.9	86049.0
332	110224	36594368	18.2209	6.9244	2.52114	3.01205	1043.0	86569.7
333	110889	36926037	18.2483	6.9313	2.52244	3.00300	1046.2	87092.0
334	111556	37259704	18.2757	6.9382	2.52375	2.99401	1049.3	87615.9
335	112225	37595375	18.3030	6.9451	2.52504	2.98507	1052.4	88141.3
336	112896	37933056	18.3303	6.9521	2.52634	2.97619	1055.6	88668.3
337	113569	38272753	18.3576	6.9589	2.52763	2.96736	1058.7	89196.9
338	114244	38614472	18.3848	6.9658	2.52892	2.95858	1061.9	89727.0
339	114921	38958219	18.4120	6.9727	2.53020	2.94985	1065.0	90258.7
340	115600	39304000	18.4391	6.9795	2.53148	2.94118	1068.1	90792.0
341	116281	39651821	18.4662	6.9864	2.53275	2.93255	1071.3	91326.9
342	116964	40001688	18.4932	6.9932	2.53403	2.92398	1074.4	91863.3
343	117649	40353607	18.5203	7.0000	2.53529	2.91545	1077.6	92401.3
344	118336	40707584	18.5472	7.0068	2.53656	2.90698	1080.7	92940.9
345	119025	41063625	18.5742	7.0136	2.53782	2.89855	1083.8	93482.0
346	119716	41421736	18.6011	7.0203	2.53908	2.89017	1087.0	94024.7
347	120409	41781923	18.6279	7.0271	2.54033	2.88184	1090.1	94569.0
348	121104	42144192	18.6548	7.0338	2.54158	2.87356	1093.3	95114.9
349	121801	42508549	18.6815	7.0406	2.54283	2.86533	1096.4	95662.3

FUNCTIONS OF NUMBERS

350 TO 399

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000	No. = Diameter	
						×	Circum.	Area
						Reciprocal		
350	122500	42875000	18.7083	7.0473	2.54407	2.85714	1099.6	96211.3
351	123201	43243551	18.7350	7.0540	2.54531	2.84900	1102.7	96761.8
352	123904	43614208	18.7617	7.0607	2.54654	2.84091	1105.8	97314.0
353	124609	43986977	18.7883	7.0674	2.54777	2.83286	1109.0	97867.7
354	125316	44361864	18.8149	7.0740	2.54900	2.82486	1112.1	98423.0
355	126025	44738875	18.8414	7.0807	2.55023	2.81690	1115.3	98979.8
356	126736	45118016	18.8680	7.0873	2.55145	2.80899	1118.4	99538.2
357	127449	45499293	18.8944	7.0940	2.55267	2.80112	1121.5	100098
358	128164	45882712	18.9209	7.1006	2.55388	2.79330	1124.7	100660
359	128881	46268279	18.9473	7.1072	2.55509	2.78552	1127.8	101223
360	129600	46656000	18.9737	7.1138	2.55630	2.77778	1131.0	101788
361	130321	47045881	19.0000	7.1204	2.55751	2.77008	1134.1	102354
362	131044	47437928	19.0263	7.1269	2.55871	2.76243	1137.3	102922
363	131769	47832147	19.0526	7.1335	2.55991	2.75482	1140.4	103491
364	132496	48228544	19.0788	7.1400	2.56110	2.74725	1143.5	104062
365	133225	48627125	19.1050	7.1466	2.56229	2.73973	1146.7	104635
366	133956	49027896	19.1311	7.1531	2.56348	2.73224	1149.8	105209
367	134689	49430863	19.1572	7.1596	2.56467	2.72480	1153.0	105785
368	135424	49836032	19.1833	7.1661	2.56585	2.71739	1156.1	106362
369	136161	50243409	19.2094	7.1726	2.56703	2.71003	1159.2	106941
370	136900	50653000	19.2354	7.1791	2.56820	2.70270	1162.4	107521
371	137641	51064811	19.2614	7.1855	2.56937	2.69542	1165.5	108103
372	138384	51478848	19.2873	7.1920	2.57054	2.68817	1168.7	108687
373	139129	51895117	19.3132	7.1984	2.57171	2.68097	1171.8	109272
374	139876	52313624	19.3391	7.2048	2.57287	2.67380	1175.0	109858
375	140625	52734375	19.3649	7.2112	2.57403	2.66667	1178.1	110447
376	141376	53157376	19.3907	7.2177	2.57519	2.65957	1181.2	111036
377	142129	53582633	19.4165	7.2240	2.57634	2.65252	1184.4	111628
378	142884	54010152	19.4422	7.2304	2.57749	2.64550	1187.5	112221
379	143641	54439939	19.4679	7.2368	2.57864	2.63852	1190.7	112815
380	144400	54872000	19.4936	7.2432	2.57978	2.63158	1193.8	113411
381	145161	55306341	19.5192	7.2495	2.58093	2.62467	1196.9	114009
382	145924	55742968	19.5448	7.2558	2.58206	2.61780	1200.1	114608
383	146689	56181887	19.5704	7.2622	2.58320	2.61097	1203.2	115209
384	147456	56623104	19.5959	7.2685	2.58433	2.60417	1206.4	115812
385	148225	57066625	19.6214	7.2748	2.58546	2.59740	1209.5	116416
386	148996	57512456	19.6469	7.2811	2.58659	2.59067	1212.7	117021
387	149769	57960603	19.6723	7.2874	2.58771	2.58398	1215.8	117628
388	150544	58411072	19.6977	7.2936	2.58883	2.57732	1218.9	118237
389	151321	58863869	19.7231	7.2999	2.58995	2.57069	1222.1	118847
390	152100	59319000	19.7484	7.3061	2.59106	2.56410	1225.2	119459
391	152881	59776471	19.7737	7.3124	2.59218	2.55754	1228.4	120072
392	153664	60236288	19.7990	7.3186	2.59329	2.55102	1231.5	120687
393	154449	60698457	19.8242	7.3248	2.59439	2.54453	1234.6	121304
394	155236	61162984	19.8494	7.3310	2.59550	2.53807	1237.8	121922
395	156025	61629875	19.8746	7.3372	2.59660	2.53165	1240.9	122542
396	156816	62099136	19.8997	7.3434	2.59770	2.52525	1244.1	123163
397	157609	62570773	19.9249	7.3496	2.59879	2.51889	1247.2	123786
398	158404	63044792	19.9499	7.3558	2.59988	2.51256	1250.4	124410
399	159201	63521199	19.9750	7.3619	2.60097	2.50627	1253.5	125036

400 TO 449 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm /	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
400	160000	64000000	20.0000	7.3681	2.60206	2.50000	1256.6	125664
401	160801	64481201	20.0250	7.3742	2.60314	2.49377	1259.8	126293
402	161604	64964808	20.0499	7.3803	2.60423	2.48756	1262.9	126923
403	162409	65450827	20.0749	7.3864	2.60531	2.48139	1266.1	127556
404	163216	65939264	20.0998	7.3925	2.60638	2.47525	1269.2	128190
405	164025	66430125	20.1246	7.3986	2.60746	2.46914	1272.3	128825
406	164836	66923416	20.1494	7.4047	2.60853	2.46305	1275.5	129462
407	165649	67419143	20.1742	7.4108	2.60959	2.45700	1278.6	130100
408	166464	67917312	20.1990	7.4169	2.61066	2.45098	1281.8	130741
409	167281	68417929	20.2237	7.4229	2.61172	2.44499	1284.9	131382
410	168100	68921000	20.2485	7.4290	2.61278	2.43902	1288.1	132025
411	168921	69426531	20.2731	7.4350	2.61384	2.43309	1291.2	132670
412	169744	69934528	20.2978	7.4410	2.61490	2.42718	1294.3	133317
413	170569	70444997	20.3224	7.4470	2.61595	2.42131	1297.5	133965
414	171396	70957944	20.3470	7.4530	2.61700	2.41546	1300.6	134614
415	172225	71473375	20.3715	7.4590	2.61805	2.40964	1303.8	135265
416	173056	71991296	20.3961	7.4650	2.61909	2.40385	1306.9	135918
417	173889	72511713	20.4206	7.4710	2.62014	2.39808	1310.0	136572
418	174724	73034632	20.4450	7.4770	2.62118	2.39234	1313.2	137228
419	175561	73560059	20.4695	7.4829	2.62221	2.38663	1316.3	137885
420	176400	74088000	20.4939	7.4889	2.62325	2.38095	1319.5	138544
421	177241	74618461	20.5183	7.4948	2.62428	2.37530	1322.6	139205
422	178084	75151448	20.5426	7.5007	2.62531	2.36967	1325.8	139867
423	178929	75686967	20.5670	7.5067	2.62634	2.36407	1328.9	140531
424	179776	76225024	20.5913	7.5126	2.62737	2.35849	1332.0	141196
425	180625	76765625	20.6155	7.5185	2.62839	2.35294	1335.2	141863
426	181476	77308776	20.6398	7.5244	2.62941	2.34742	1338.3	142531
427	182329	77854483	20.6640	7.5302	2.63043	2.34192	1341.5	143201
428	183184	78402752	20.6882	7.5361	2.63144	2.33645	1344.6	143872
429	184041	78953589	20.7123	7.5420	2.63246	2.33100	1347.7	144545
430	184900	79507000	20.7364	7.5478	2.63347	2.32558	1350.9	145220
431	185761	80062991	20.7605	7.5537	2.63448	2.32019	1354.0	145896
432	186624	80621568	20.7846	7.5595	2.63548	2.31481	1357.2	146574
433	187489	81182737	20.8087	7.5654	2.63649	2.30947	1360.3	147254
434	188356	81746504	20.8327	7.5712	2.63749	2.30415	1363.5	147934
435	189225	82312875	20.8567	7.5770	2.63849	2.29885	1366.6	148617
436	190096	82881856	20.8806	7.5828	2.63949	2.29358	1369.7	149301
437	190969	83453453	20.9045	7.5886	2.64048	2.28833	1372.9	149987
438	191844	84027672	20.9284	7.5944	2.64147	2.28311	1376.0	150674
439	192721	84604519	20.9523	7.6001	2.64246	2.27790	1379.2	151363
440	193600	85184000	20.9762	7.6059	2.64345	2.27273	1382.3	152053
441	194481	85766121	21.0000	7.6117	2.64444	2.26757	1385.4	152745
442	195364	86350888	21.0238	7.6174	2.64542	2.26244	1388.6	153439
443	196249	86938307	21.0476	7.6232	2.64640	2.25734	1391.7	154134
444	197136	87528384	21.0713	7.6289	2.64738	2.25225	1394.9	154830
445	198025	88121125	21.0950	7.6346	2.64836	2.24719	1398.0	155528
446	198916	88716536	21.1187	7.6403	2.64933	2.24215	1401.2	156228
447	199809	89314623	21.1424	7.6460	2.65031	2.23714	1404.3	156930
448	200704	89915392	21.1660	7.6517	2.65128	2.23214	1407.4	157633
449	201601	90518849	21.1896	7.6574	2.65225	2.22717	1410.6	158337

FUNCTIONS OF NUMBERS

450 TO 499

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
450	202500	91125000	21.2132	7.6631	2.65321	2.22222	1413.7	159043
451	203401	91733851	21.2368	7.6688	2.65418	2.21729	1416.9	159751
452	204304	92345408	21.2603	7.6744	2.65514	2.21239	1420.0	160460
453	205209	92959677	21.2838	7.6801	2.65610	2.20751	1423.1	161171
454	206116	93576664	21.3073	7.6857	2.65706	2.20264	1426.3	161883
455	207025	94196375	21.3307	7.6914	2.65801	2.19780	1429.4	162597
456	207936	94818816	21.3542	7.6970	2.65896	2.19298	1432.6	163313
457	208849	95443993	21.3776	7.7026	2.65992	2.18818	1435.7	164030
458	209764	96071912	21.4009	7.7082	2.66087	2.18341	1438.8	164748
459	210681	96702579	21.4243	7.7138	2.66181	2.17865	1442.0	165468
460	211600	97336000	21.4476	7.7194	2.66276	2.17391	1445.1	166190
461	212521	97972181	21.4709	7.7250	2.66370	2.16920	1448.3	166914
462	213444	98611128	21.4942	7.7306	2.66464	2.16450	1451.4	167639
463	214369	99252847	21.5174	7.7362	2.66558	2.15983	1454.6	168365
464	215296	99897344	21.5407	7.7418	2.66652	2.15517	1457.7	169093
465	216225	100544625	21.5639	7.7473	2.66745	2.15054	1460.8	169823
466	217156	101194966	21.5870	7.7529	2.66839	2.14592	1464.0	170554
467	218089	101847563	21.6102	7.7584	2.66932	2.14133	1467.1	171287
468	219024	102503232	21.6333	7.7639	2.67025	2.13675	1470.3	172021
469	219961	103161709	21.6564	7.7695	2.67117	2.13220	1473.4	172757
470	220900	103823000	21.6795	7.7750	2.67210	2.12766	1476.5	173494
471	221841	104487111	21.7025	7.7805	2.67302	2.12314	1479.7	174234
472	222784	105154048	21.7256	7.7860	2.67394	2.11864	1482.8	174974
473	223729	105823817	21.7486	7.7915	2.67486	2.11416	1486.0	175716
474	224676	106496424	21.7715	7.7970	2.67578	2.10970	1489.1	176460
475	225625	107171875	21.7945	7.8025	2.67669	2.10526	1492.3	177205
476	226576	107850176	21.8174	7.8079	2.67761	2.10084	1495.4	177952
477	227529	108531333	21.8403	7.8134	2.67852	2.09644	1498.5	178701
478	228484	109215352	21.8632	7.8188	2.67943	2.09205	1501.7	179451
479	229441	109902239	21.8861	7.8243	2.68034	2.08768	1504.8	180203
480	230400	110592000	21.9089	7.8297	2.68124	2.08333	1508.0	180956
481	231361	111284641	21.9317	7.8352	2.68215	2.07900	1511.1	181711
482	232324	111980168	21.9545	7.8406	2.68305	2.07469	1514.2	182467
483	233289	112678587	21.9773	7.8460	2.68395	2.07039	1517.4	183225
484	234256	113379904	22.0000	7.8514	2.68485	2.06612	1520.5	183984
485	235225	114084125	22.0227	7.8568	2.68574	2.06186	1523.7	184745
486	236196	114791256	22.0454	7.8622	2.68664	2.05761	1526.8	185508
487	237169	115501303	22.0681	7.8676	2.68753	2.05339	1530.0	186272
488	238144	116214272	22.0907	7.8730	2.68842	2.04918	1533.1	187038
489	239121	116930169	22.1133	7.8784	2.68931	2.04499	1536.2	187805
490	240100	117649000	22.1359	7.8837	2.69020	2.04082	1539.4	188574
491	241081	118370771	22.1585	7.8891	2.69108	2.03666	1542.5	189345
492	242064	119095488	22.1811	7.8944	2.69197	2.03252	1545.7	190117
493	243049	119823157	22.2036	7.8998	2.69285	2.02840	1548.8	190890
494	244036	120553784	22.2261	7.9051	2.69373	2.02429	1551.9	191665
495	245025	121287375	22.2486	7.9105	2.69461	2.02020	1555.1	192442
496	246016	122023936	22.2711	7.9158	2.69548	2.01613	1558.2	193221
497	247009	122763473	22.2935	7.9211	2.69636	2.01207	1561.4	194000
498	248004	123505992	22.3159	7.9264	2.69723	2.00803	1564.5	194782
499	249001	124251499	22.3383	7.9317	2.69810	2.00401	1567.7	195565

500 TO 549

FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000		No. = Diameter	
						×	Reciprocal	Circum.	Area
500	250000	125000000	22.3607	7.9370	2.69897	2.00000		1570.8	196350
501	251001	125751501	22.3830	7.9423	2.69984	1.99601		1573.9	197136
502	252004	126506008	22.4054	7.9476	2.70070	1.99203		1577.1	197923
503	253009	127263527	22.4277	7.9528	2.70157	1.98807		1580.2	198713
504	254016	128024064	22.4499	7.9581	2.70243	1.98413		1583.4	199504
505	255025	128787625	22.4722	7.9634	2.70329	1.98020		1586.5	200296
506	256036	129554216	22.4944	7.9686	2.70415	1.97628		1589.6	201090
507	257049	130323843	22.5167	7.9739	2.70501	1.97239		1592.8	201886
508	258064	131096512	22.5389	7.9791	2.70586	1.96850		1595.9	202683
509	259081	131872229	22.5610	7.9843	2.70672	1.96464		1599.1	203482
510	260100	132651000	22.5832	7.9896	2.70757	1.96078		1602.2	204282
511	261121	133432831	22.6053	7.9948	2.70842	1.95695		1605.4	205084
512	262144	134217728	22.6274	8.0000	2.70927	1.95312		1608.5	205887
513	263169	135005697	22.6495	8.0052	2.71012	1.94932		1611.6	206692
514	264196	135796744	22.6716	8.0104	2.71096	1.94553		1614.8	207499
515	265225	136590875	22.6936	8.0156	2.71181	1.94175		1617.9	208307
516	266256	137388096	22.7156	8.0208	2.71265	1.93798		1621.1	209117
517	267289	138188413	22.7376	8.0260	2.71349	1.93424		1624.2	209928
518	268324	138991832	22.7596	8.0311	2.71433	1.93050		1627.3	210741
519	269361	139798359	22.7816	8.0363	2.71517	1.92678		1630.5	211556
520	270400	140608000	22.8035	8.0415	2.71600	1.92308		1633.6	212372
521	271441	141420761	22.8254	8.0466	2.71684	1.91939		1636.8	213189
522	272484	142236648	22.8473	8.0517	2.71767	1.91571		1639.9	214008
523	273529	143055667	22.8692	8.0569	2.71850	1.91205		1643.1	214829
524	274576	143877824	22.8910	8.0620	2.71933	1.90840		1646.2	215651
525	275625	144703125	22.9129	8.0671	2.72016	1.90476		1649.3	216475
526	276676	145531576	22.9347	8.0723	2.72099	1.90114		1652.5	217301
527	277729	146363183	22.9565	8.0774	2.72181	1.89753		1655.6	218128
528	278784	147197952	22.9783	8.0825	2.72263	1.89394		1658.8	218956
529	279841	148035889	23.0000	8.0876	2.72346	1.89036		1661.9	219787
530	280900	148877000	23.0217	8.0927	2.72428	1.88679		1665.0	220618
531	281961	149721291	23.0434	8.0978	2.72509	1.88324		1668.2	221452
532	283024	150568768	23.0651	8.1028	2.72591	1.87970		1671.3	222287
533	284089	151419437	23.0868	8.1079	2.72673	1.87617		1674.5	223123
534	285156	152273304	23.1084	8.1130	2.72754	1.87266		1677.6	223961
535	286225	153130375	23.1301	8.1180	2.72835	1.86916		1680.8	224801
536	287296	153990656	23.1517	8.1231	2.72916	1.86567		1683.9	225642
537	288369	154854153	23.1733	8.1281	2.72997	1.86220		1687.0	226484
538	289444	155720872	23.1948	8.1332	2.73078	1.85874		1690.2	227329
539	290521	156590819	23.2164	8.1382	2.73159	1.85529		1693.3	228175
540	291600	157464000	23.2379	8.1433	2.73239	1.85185		1696.5	229022
541	292681	158340421	23.2594	8.1483	2.73320	1.84843		1699.6	229871
542	293764	159220088	23.2809	8.1533	2.73400	1.84502		1702.7	230722
543	294849	160103007	23.3024	8.1583	2.73480	1.84162		1705.9	231574
544	295936	160989184	23.3238	8.1633	2.73560	1.83824		1709.0	232428
545	297025	161878625	23.3452	8.1683	2.73640	1.83486		1712.2	233283
546	298116	162771336	23.3666	8.1733	2.73719	1.83150		1715.3	234140
547	299209	163667323	23.3880	8.1783	2.73799	1.82815		1718.5	234998
548	300304	164566592	23.4094	8.1833	2.73878	1.82482		1721.6	235858
549	301401	165469149	23.4307	8.1882	2.73957	1.82149		1724.7	236720

FUNCTIONS OF NUMBERS 550 TO 599

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
550	302500	166375000	23.4521	8.1932	2.74036	1.81818	1727.9	237583
551	303601	167284151	23.4734	8.1982	2.74115	1.81488	1731.0	238448
552	304704	168196608	23.4947	8.2031	2.74194	1.81159	1734.2	239314
553	305809	169112377	23.5160	8.2081	2.74273	1.80832	1737.3	240182
554	306916	170031464	23.5372	8.2130	2.74351	1.80505	1740.4	241051
555	308025	170953875	23.5584	8.2180	2.74429	1.80180	1743.6	241922
556	309136	171879616	23.5797	8.2229	2.74507	1.79856	1746.7	242795
557	310249	172808693	23.6008	8.2278	2.74586	1.79533	1749.9	243669
558	311364	173741112	23.6220	8.2327	2.74663	1.79211	1753.0	244545
559	312481	174676879	23.6432	8.2377	2.74741	1.78891	1756.2	245422
560	313600	175616000	23.6643	8.2426	2.74819	1.78571	1759.3	246301
561	314721	176558481	23.6854	8.2475	2.74896	1.78253	1762.4	247181
562	315844	177504328	23.7065	8.2524	2.74974	1.77936	1765.6	248063
563	316969	178453547	23.7276	8.2573	2.75051	1.77620	1768.7	248947
564	318096	179406144	23.7487	8.2621	2.75128	1.77305	1771.9	249832
565	319225	180362125	23.7697	8.2670	2.75205	1.76991	1775.0	250719
566	320356	181321496	23.7908	8.2719	2.75282	1.76678	1778.1	251607
567	321489	182284263	23.8118	8.2768	2.75358	1.76367	1781.3	252497
568	322624	183250432	23.8328	8.2816	2.75435	1.76056	1784.4	253388
569	323761	184220009	23.8537	8.2865	2.75511	1.75747	1787.6	254281
570	324900	185193000	23.8747	8.2913	2.75587	1.75439	1790.7	255176
571	326041	186169411	23.8956	8.2962	2.75664	1.75131	1793.8	256072
572	327184	187149248	23.9165	8.3010	2.75740	1.74825	1797.0	256970
573	328329	188132517	23.9374	8.3059	2.75815	1.74520	1800.1	257869
574	329476	189119224	23.9583	8.3107	2.75891	1.74216	1803.3	258770
575	330625	190109375	23.9792	8.3155	2.75967	1.73913	1806.4	259672
576	331776	191102976	24.0000	8.3203	2.76042	1.73611	1809.6	260576
577	332929	192100033	24.0208	8.3251	2.76118	1.73310	1812.7	261482
578	334084	193100552	24.0416	8.3300	2.76193	1.73010	1815.8	262389
579	335241	194104539	24.0624	8.3348	2.76268	1.72712	1819.0	263298
580	336400	195112000	24.0832	8.3396	2.76343	1.72414	1822.1	264208
581	337561	196122941	24.1039	8.3443	2.76418	1.72117	1825.3	265120
582	338724	197137368	24.1247	8.3491	2.76492	1.71821	1828.4	266033
583	339889	198155287	24.1454	8.3539	2.76567	1.71527	1831.6	266948
584	341056	199176704	24.1661	8.3587	2.76641	1.71233	1834.7	267865
585	342225	200201625	24.1868	8.3634	2.76716	1.70940	1837.8	268783
586	343396	201230056	24.2074	8.3682	2.76790	1.70648	1841.0	269703
587	344569	202262003	24.2281	8.3730	2.76864	1.70358	1844.1	270624
588	345744	203297472	24.2487	8.3777	2.76938	1.70068	1847.3	271547
589	346921	204336469	24.2693	8.3825	2.77012	1.69779	1850.4	272471
590	348100	205379000	24.2899	8.3872	2.77085	1.69492	1853.5	273397
591	349281	206425071	24.3105	8.3919	2.77159	1.69205	1856.7	274325
592	350464	207474688	24.3311	8.3967	2.77232	1.68919	1859.8	275254
593	351649	208527857	24.3516	8.4014	2.77305	1.68634	1863.0	276184
594	352836	209584584	24.3721	8.4061	2.77379	1.68350	1866.1	277117
595	354025	210644875	24.3926	8.4108	2.77452	1.68067	1869.2	278051
596	355216	211708736	24.4131	8.4155	2.77525	1.67785	1872.4	278986
597	356409	212776173	24.4336	8.4202	2.77597	1.67504	1875.5	279923
598	357604	213847192	24.4540	8.4249	2.77670	1.67224	1878.7	280862
599	358801	214921799	24.4745	8.4296	2.77743	1.66945	1881.8	281802

600 TO 649 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
600	360000	216000000	24.4949	8.4343	2.77815	1.66667	1885.0	282743
601	361201	217081801	24.5153	8.4390	2.77887	1.66389	1888.1	283687
602	362404	218167208	24.5357	8.4437	2.77960	1.66113	1891.2	284631
603	363609	219256227	24.5561	8.4484	2.78032	1.65837	1894.4	285578
604	364816	220348864	24.5764	8.4530	2.78104	1.65563	1897.5	286526
605	366025	221445125	24.5967	8.4577	2.78176	1.65289	1900.7	287475
606	367236	222545016	24.6171	8.4623	2.78247	1.65017	1903.8	288426
607	368449	223648543	24.6374	8.4670	2.78319	1.64745	1906.9	289379
608	369664	224755712	24.6577	8.4716	2.78390	1.64474	1910.1	290333
609	370881	225866529	24.6779	8.4763	2.78462	1.64204	1913.2	291289
610	372100	226981000	24.6982	8.4809	2.78533	1.63934	1916.4	292247
611	373321	228099131	24.7184	8.4856	2.78604	1.63666	1919.5	293206
612	374544	229220928	24.7386	8.4902	2.78675	1.63399	1922.7	294166
613	375769	230346397	24.7588	8.4948	2.78746	1.63132	1925.8	295128
614	376996	231475544	24.7790	8.4994	2.78817	1.62866	1928.9	296092
615	378225	232608375	24.7992	8.5040	2.78888	1.62602	1932.1	297057
616	379456	233744896	24.8193	8.5086	2.78958	1.62338	1935.2	298024
617	380689	234885113	24.8395	8.5132	2.79029	1.62075	1938.4	298992
618	381924	236029032	24.8596	8.5178	2.79099	1.61812	1941.5	299962
619	383161	237176659	24.8797	8.5224	2.79169	1.61551	1944.6	300934
620	384400	238328000	24.8998	8.5270	2.79239	1.61290	1947.8	301907
621	385641	239483061	24.9199	8.5316	2.79309	1.61031	1950.9	302882
622	386884	240641848	24.9399	8.5362	2.79379	1.60772	1954.1	303858
623	388129	241804367	24.9600	8.5408	2.79449	1.60514	1957.2	304836
624	389376	242970624	24.9800	8.5453	2.79518	1.60256	1960.4	305815
625	390625	244140625	25.0000	8.5499	2.79588	1.60000	1963.5	306796
626	391876	245314376	25.0200	8.5544	2.79657	1.59744	1966.6	307779
627	393129	246491883	25.0400	8.5590	2.79727	1.59490	1969.8	308763
628	394384	247673152	25.0599	8.5635	2.79796	1.59236	1972.9	309748
629	395641	248858189	25.0799	8.5681	2.79865	1.58983	1976.1	310736
630	396900	250047000	25.0998	8.5726	2.79934	1.58730	1979.2	311725
631	398161	251239591	25.1197	8.5772	2.80003	1.58479	1982.3	312715
632	399424	252435968	25.1396	8.5817	2.80072	1.58228	1985.5	313707
633	400689	253636137	25.1595	8.5862	2.80140	1.57978	1988.6	314700
634	401956	254840104	25.1794	8.5907	2.80209	1.57729	1991.8	315696
635	403225	256047875	25.1992	8.5952	2.80277	1.57480	1994.9	316692
636	404496	257259456	25.2190	8.5997	2.80346	1.57233	1998.1	317690
637	405769	258474853	25.2389	8.6043	2.80414	1.56986	2001.2	318690
638	407044	259694072	25.2587	8.6088	2.80482	1.56740	2004.3	319692
639	408321	260917119	25.2784	8.6132	2.80550	1.56495	2007.5	320695
640	409600	262144000	25.2982	8.6177	2.80618	1.56250	2010.6	321699
641	410881	263374721	25.3180	8.6222	2.80686	1.56006	2013.8	322705
642	412164	264609288	25.3377	8.6267	2.80754	1.55763	2016.9	323713
643	413449	265847707	25.3574	8.6312	2.80821	1.55521	2020.0	324722
644	414736	267089984	25.3772	8.6357	2.80889	1.55280	2023.2	325733
645	416025	268336125	25.3969	8.6401	2.80956	1.55039	2026.3	326745
646	417316	269586136	25.4165	8.6446	2.81023	1.54799	2029.5	327759
647	418609	270840023	25.4362	8.6490	2.81090	1.54560	2032.6	328775
648	419904	272097792	25.4558	8.6535	2.81158	1.54321	2035.8	329792
649	421201	273359449	25.4755	8.6579	2.81224	1.54083	2038.9	330810

FUNCTIONS OF NUMBERS

650 TO 699

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
650	422500	274625000	25.4951	8.6624	2.81291	1.53846	2042.0	331831
651	423801	275894451	25.5147	8.6668	2.81358	1.53616	2045.2	332853
652	425104	277167808	25.5343	8.6713	2.81425	1.53374	2048.3	333876
653	426409	278445077	25.5539	8.6757	2.81491	1.53139	2051.5	334901
654	427716	279726264	25.5734	8.6801	2.81558	1.52905	2054.6	335927
655	429025	281011375	25.5930	8.6845	2.81624	1.52672	2057.7	336955
656	430336	282300416	25.6125	8.6890	2.81690	1.52439	2060.9	337985
657	431649	283593393	25.6320	8.6934	2.81757	1.52207	2064.0	339016
658	432964	284890312	25.6515	8.6978	2.81823	1.51976	2067.2	340049
659	434281	286191179	25.6710	8.7022	2.81889	1.51745	2070.3	341084
660	435600	287496000	25.6905	8.7066	2.81954	1.51515	2073.5	342119
661	436921	288804781	25.7099	8.7110	2.82020	1.51286	2076.6	343157
662	438244	290117528	25.7294	8.7154	2.82086	1.51057	2079.7	344196
663	439569	291434247	25.7488	8.7198	2.82151	1.50830	2082.9	345237
664	440896	292754944	25.7682	8.7241	2.82217	1.50602	2086.0	346279
665	442225	294079625	25.7876	8.7285	2.82282	1.50376	2089.2	347323
666	443556	295408296	25.8070	8.7329	2.82347	1.50150	2092.3	348368
667	444889	296740963	25.8263	8.7373	2.82413	1.49925	2095.4	349415
668	446224	298077632	25.8457	8.7416	2.82478	1.49701	2098.6	350464
669	447561	299418309	25.8650	8.7460	2.82543	1.49477	2101.7	351514
670	448900	300763000	25.8844	8.7503	2.82607	1.49254	2104.9	352565
671	450241	302111711	25.9037	8.7547	2.82672	1.49031	2108.0	353618
672	451584	303464448	25.9230	8.7590	2.82737	1.48810	2111.2	354673
673	452929	304821217	25.9422	8.7634	2.82802	1.48588	2114.3	355730
674	454276	306182024	25.9615	8.7677	2.82866	1.48368	2117.4	356788
675	455625	307546875	25.9808	8.7721	2.82930	1.48148	2120.6	357847
676	456976	308915776	26.0000	8.7764	2.82995	1.47929	2123.7	358908
677	458329	310288733	26.0192	8.7807	2.83059	1.47710	2126.9	359971
678	459684	311665752	26.0384	8.7850	2.83123	1.47493	2130.0	361035
679	461041	313046839	26.0576	8.7893	2.83187	1.47275	2133.1	362101
680	462400	314432000	26.0768	8.7937	2.83251	1.47059	2136.3	363168
681	463761	315821241	26.0960	8.7980	2.83315	1.46843	2139.4	364237
682	465124	317214568	26.1151	8.8023	2.83378	1.46628	2142.6	365308
683	466489	318611987	26.1343	8.8066	2.83442	1.46413	2145.7	366380
684	467856	320013504	26.1534	8.8109	2.83506	1.46199	2148.8	367453
685	469225	321419125	26.1725	8.8152	2.83569	1.45985	2152.0	368528
686	470596	322828856	26.1916	8.8194	2.83632	1.45773	2155.1	369605
687	471969	324242703	26.2107	8.8237	2.83696	1.45560	2158.3	370684
688	473344	325660672	26.2298	8.8280	2.83759	1.45349	2161.4	371764
689	474721	327082769	26.2488	8.8323	2.83822	1.45138	2164.6	372845
690	476100	328509000	26.2679	8.8366	2.83885	1.44928	2167.7	373928
691	477481	329939371	26.2869	8.8408	2.83948	1.44718	2170.8	375013
692	478864	331373888	26.3059	8.8451	2.84011	1.44509	2174.0	376099
693	480249	332812557	26.3249	8.8493	2.84073	1.44300	2177.1	377187
694	481636	334255384	26.3439	8.8536	2.84136	1.44092	2180.3	378276
695	483025	335702375	26.3629	8.8578	2.84198	1.43885	2183.4	379367
696	484416	337155356	26.3818	8.8621	2.84261	1.43678	2186.5	380459
697	485809	338608873	26.4008	8.8663	2.84323	1.43472	2189.7	381553
698	487204	340068392	26.4197	8.8706	2.84386	1.43266	2192.8	382649
699	488601	341532099	26.4386	8.8748	2.84448	1.43062	2196.0	383746

700 TO 749 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
700	490000	343000000	26.4575	8.8790	2.84510	1.42857	2199.1	384845
701	491401	344472101	26.4764	8.8833	2.84572	1.42653	2202.3	385945
702	492804	345948408	26.4953	8.8875	2.84634	1.42450	2205.4	387047
703	494209	347428927	26.5141	8.8917	2.84696	1.42248	2208.5	388151
704	495616	348913664	26.5330	8.8959	2.84757	1.42045	2211.7	389256
705	497025	350402625	26.5518	8.9001	2.84819	1.41844	2214.8	390363
706	498436	351895816	26.5707	8.9043	2.84880	1.41643	2218.0	391471
707	499849	353393243	26.5895	8.9085	2.84942	1.41443	2221.1	392580
708	501264	354894912	26.6083	8.9127	2.85003	1.41243	2224.2	393692
709	502681	356400829	26.6271	8.9169	2.85065	1.41044	2227.4	394805
710	504100	357911000	26.6458	8.9211	2.85126	1.40845	2230.5	395919
711	505521	359425431	26.6646	8.9253	2.85187	1.40647	2233.7	397035
712	506944	360944128	26.6833	8.9295	2.85248	1.40449	2236.8	398153
713	508369	362467097	26.7021	8.9337	2.85309	1.40252	2240.0	399272
714	509796	363994344	26.7208	8.9378	2.85370	1.40056	2243.1	400393
715	511225	365525875	26.7395	8.9420	2.85431	1.39860	2246.2	401515
716	512656	367061696	26.7582	8.9462	2.85491	1.39665	2249.4	402639
717	514089	368601813	26.7769	8.9503	2.85552	1.39470	2252.5	403765
718	515524	370146232	26.7955	8.9545	2.85612	1.39276	2255.7	404892
719	516961	371694959	26.8142	8.9587	2.85673	1.39082	2258.8	406020
720	518400	373248000	26.8328	8.9628	2.85733	1.38889	2261.9	407150
721	519841	374805361	26.8514	8.9670	2.85794	1.38696	2265.1	408282
722	521284	376367048	26.8701	8.9711	2.85854	1.38504	2268.2	409415
723	522729	377933067	26.8887	8.9752	2.85914	1.38313	2271.4	410550
724	524176	379503424	26.9072	8.9794	2.85974	1.38122	2274.5	411687
725	525625	381078125	26.9258	8.9835	2.86034	1.37931	2277.7	412825
726	527076	382657176	26.9444	8.9876	2.86094	1.37741	2280.8	413965
727	528529	384240583	26.9629	8.9918	2.86153	1.37552	2283.9	415106
728	529984	385828352	26.9815	8.9959	2.86213	1.37363	2287.1	416248
729	531441	387420489	27.0000	9.0000	2.86273	1.37174	2290.2	417393
730	532900	389017000	27.0185	9.0041	2.86332	1.36986	2293.4	418539
731	534361	390617891	27.0370	9.0082	2.86392	1.36799	2296.5	419686
732	535824	392223168	27.0555	9.0123	2.86451	1.36612	2299.6	420835
733	537289	393832837	27.0740	9.0164	2.86510	1.36426	2302.8	421986
734	538756	395446904	27.0924	9.0205	2.86570	1.36240	2305.9	423138
735	540225	397065375	27.1109	9.0246	2.86629	1.36054	2309.1	424293
736	541696	398688256	27.1293	9.0287	2.86688	1.35870	2312.2	425447
737	543169	400315553	27.1477	9.0328	2.86747	1.35685	2315.4	426604
738	544644	401947272	27.1662	9.0369	2.86806	1.35501	2318.5	427762
739	546121	403583419	27.1846	9.0410	2.86864	1.35318	2321.6	428922
740	547600	405224000	27.2029	9.0450	2.86923	1.35135	2324.8	430084
741	549081	406869021	27.2213	9.0491	2.86982	1.34953	2327.9	431247
742	550564	408518488	27.2397	9.0532	2.87040	1.34771	2331.1	432412
743	552049	410172407	27.2580	9.0572	2.87099	1.34590	2334.2	433578
744	553536	411830784	27.2764	9.0613	2.87157	1.34409	2337.3	434746
745	555025	413493625	27.2947	9.0654	2.87216	1.34228	2340.5	435916
746	556516	415160936	27.3130	9.0694	2.87274	1.34048	2343.6	437087
747	558009	416832723	27.3313	9.0735	2.87332	1.33869	2346.8	438259
748	559504	418508992	27.3496	9.0775	2.87390	1.33690	2349.9	439433
749	561001	420189749	27.3679	9.0816	2.87448	1.33511	2353.1	440609

FUNCTIONS OF NUMBERS

750 TO 799

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
750	562500	421875000	27.3861	9.0856	2.87506	1.33333	2356.2	441786
751	564001	423564751	27.4044	9.0896	2.87564	1.33156	2359.3	442965
752	565504	425259008	27.4226	9.0937	2.87622	1.32979	2362.5	444146
753	567009	426957777	27.4408	9.0977	2.87680	1.32802	2365.6	445328
754	568516	428661064	27.4591	9.1017	2.87737	1.32626	2368.8	446511
755	570025	430368875	27.4773	9.1057	2.87795	1.32450	2371.9	447697
756	571536	432081216	27.4955	9.1098	2.87852	1.32275	2375.0	448883
757	573049	433798093	27.5136	9.1138	2.87910	1.32100	2378.2	450072
758	574564	435519512	27.5318	9.1178	2.87967	1.31926	2381.3	451265
759	576081	437245479	27.5500	9.1218	2.88024	1.31752	2384.5	452453
760	577600	438976000	27.5681	9.1258	2.88081	1.31579	2387.6	453646
761	579121	440711081	27.5862	9.1298	2.88138	1.31406	2390.8	454841
762	580644	442450728	27.6043	9.1338	2.88196	1.31234	2393.9	456037
763	582169	444194947	27.6225	9.1378	2.88252	1.31062	2397.0	457234
764	583696	445943744	27.6405	9.1418	2.88309	1.30890	2400.2	458434
765	585225	447697125	27.6586	9.1458	2.88366	1.30719	2403.3	459635
766	586756	449455096	27.6767	9.1498	2.88423	1.30548	2406.5	460837
767	588289	451217663	27.6948	9.1537	2.88480	1.30378	2409.6	462041
768	589824	452984832	27.7128	9.1577	2.88536	1.30208	2412.7	463247
769	591361	454756609	27.7308	9.1617	2.88593	1.30039	2415.9	464454
770	592900	456533000	27.7489	9.1657	2.88649	1.29870	2419.0	465663
771	594441	458314011	27.7669	9.1696	2.88705	1.29702	2422.2	466873
772	595984	460099648	27.7849	9.1736	2.88762	1.29534	2425.3	468085
773	597529	461889917	27.8029	9.1775	2.88818	1.29366	2428.5	469298
774	599076	463684824	27.8209	9.1815	2.88874	1.29199	2431.6	470513
775	600625	465484375	27.8388	9.1855	2.88930	1.29032	2434.7	471730
776	602176	467288576	27.8568	9.1894	2.88986	1.28866	2437.9	472948
777	603729	469097433	27.8747	9.1933	2.89042	1.28700	2441.0	474168
778	605284	470910952	27.8927	9.1973	2.89098	1.28535	2444.2	475389
779	606841	472729139	27.9106	9.2012	2.89154	1.28370	2447.3	476612
780	608400	474552000	27.9285	9.2052	2.89209	1.28205	2450.4	477836
781	609961	476379541	27.9464	9.2091	2.89265	1.28041	2453.6	479062
782	611524	478211768	27.9643	9.2130	2.89321	1.27877	2456.7	480290
783	613089	480048687	27.9821	9.2170	2.89376	1.27714	2459.9	481519
784	614656	481890304	28.0000	9.2209	2.89432	1.27551	2463.0	482750
785	616225	483736625	28.0179	9.2248	2.89487	1.27389	2466.2	483982
786	617796	485587656	28.0357	9.2287	2.89542	1.27226	2469.3	485216
787	619369	487443403	28.0535	9.2326	2.89597	1.27065	2472.4	486451
788	620944	489303872	28.0713	9.2365	2.89653	1.26904	2475.6	487688
789	622521	491169069	28.0891	9.2404	2.89708	1.26743	2478.7	488927
790	624100	493039000	28.1069	9.2443	2.89763	1.26582	2481.9	490167
791	625681	494913671	28.1247	9.2482	2.89818	1.26422	2485.0	491409
792	627264	496793088	28.1425	9.2521	2.89873	1.26263	2488.1	492652
793	628849	498677257	28.1603	9.2560	2.89927	1.26103	2491.3	493897
794	630436	500566184	28.1780	9.2599	2.89982	1.25945	2494.4	495143
795	632025	502459875	28.1957	9.2638	2.90037	1.25786	2497.6	496391
796	633616	504358336	28.2135	9.2677	2.90091	1.25628	2500.7	497641
797	635209	506261573	28.2312	9.2716	2.90146	1.25471	2503.8	498892
798	636804	508169592	28.2489	9.2754	2.90200	1.25313	2507.0	500145
799	638401	510082399	28.2666	9.2793	2.90255	1.25156	2510.1	501399

800 TO 849 FUNCTIONS OF NUMBERS

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
800	640000	512000000	28.2843	9.2832	2.90309	1.25000	2513.3	502655
801	641601	513922401	28.3019	9.2870	2.90363	1.24844	2516.4	503912
802	643204	515849608	28.3196	9.2909	2.90417	1.24688	2519.6	505171
803	644809	517781627	28.3373	9.2948	2.90472	1.24533	2522.7	506432
804	646416	519718464	28.3549	9.2986	2.90526	1.24378	2525.8	507694
805	648025	521660125	28.3725	9.3025	2.90580	1.24224	2529.0	508958
806	649636	523606616	28.3901	9.3063	2.90634	1.24069	2532.1	510223
807	651249	525557943	28.4077	9.3102	2.90687	1.23916	2535.3	511490
808	652864	527514112	28.4253	9.3140	2.90741	1.23762	2538.4	512758
809	654481	529475129	28.4429	9.3179	2.90795	1.23609	2541.5	514028
810	656100	531441000	28.4605	9.3217	2.90849	1.23457	2544.7	515300
811	657721	533411731	28.4781	9.3255	2.90902	1.23305	2547.8	516573
812	659344	535387328	28.4956	9.3294	2.90956	1.23153	2551.0	517848
813	660969	537367797	28.5132	9.3332	2.91009	1.23001	2554.1	519124
814	662596	539353144	28.5307	9.3370	2.91062	1.22850	2557.3	520402
815	664225	541343375	28.5482	9.3408	2.91116	1.22699	2560.4	521681
816	665856	543338496	28.5657	9.3447	2.91169	1.22549	2563.5	522962
817	667489	545338513	28.5832	9.3485	2.91222	1.22399	2566.7	524245
818	669124	547343432	28.6007	9.3523	2.91275	1.22249	2569.8	525529
819	670761	549353259	28.6182	9.3561	2.91328	1.22100	2573.0	526814
820	672400	551368000	28.6356	9.3599	2.91381	1.21951	2576.1	528102
821	674041	553387661	28.6531	9.3637	2.91434	1.21803	2579.2	529391
822	675684	555412248	28.6705	9.3675	2.91487	1.21655	2582.4	530681
823	677329	557441767	28.6880	9.3713	2.91540	1.21507	2585.5	531973
824	678976	559476224	28.7054	9.3751	2.91593	1.21359	2588.7	533267
825	680625	561515625	28.7228	9.3789	2.91645	1.21212	2591.8	534562
826	682276	563559976	28.7402	9.3827	2.91698	1.21065	2595.0	535858
827	683929	565609283	28.7576	9.3865	2.91751	1.20919	2598.1	537157
828	685584	567663552	28.7750	9.3902	2.91803	1.20773	2601.2	538456
829	687241	569722789	28.7924	9.3940	2.91855	1.20627	2604.4	539758
830	688900	571787000	28.8097	9.3978	2.91908	1.20482	2607.5	541061
831	690561	573856191	28.8271	9.4016	2.91960	1.20337	2610.7	542365
832	692224	575930368	28.8444	9.4053	2.92012	1.20192	2613.8	543671
833	693889	578009537	28.8617	9.4091	2.92065	1.20048	2616.9	544979
834	695556	580093704	28.8791	9.4129	2.92117	1.19904	2620.1	546288
835	697225	582182875	28.8964	9.4166	2.92169	1.19760	2623.2	547599
836	698896	584277056	28.9137	9.4204	2.92221	1.19617	2626.4	548912
837	700569	586376253	28.9310	9.4241	2.92273	1.19474	2629.5	550226
838	702244	588480472	28.9482	9.4279	2.92324	1.19332	2632.7	551541
839	703921	590589719	28.9655	9.4316	2.92376	1.19190	2635.8	552858
840	705600	592704000	28.9828	9.4354	2.92428	1.19048	2638.9	554177
841	707281	594823321	29.0000	9.4391	2.92480	1.18906	2642.1	555497
842	708964	596947688	29.0172	9.4429	2.92531	1.18765	2645.2	556819
843	710649	599077107	29.0345	9.4466	2.92583	1.18624	2648.4	558142
844	712336	601211584	29.0517	9.4503	2.92634	1.18483	2651.5	559467
845	714025	603351125	29.0689	9.4541	2.92686	1.18343	2654.6	560794
846	715716	605495736	29.0861	9.4578	2.92737	1.18203	2657.8	562122
847	717409	607645423	29.1033	9.4615	2.92788	1.18064	2660.9	563452
848	719104	609800192	29.1204	9.4652	2.92840	1.17925	2664.1	564783
849	720801	611960049	29.1376	9.4690	2.92891	1.17786	2667.2	566116

FUNCTIONS OF NUMBERS

850 TO 899

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 × Reciprocal	No. = Diameter	
							Circum.	Area
850	722500	614125000	29.1548	9.4727	2.92942	1.17647	2670.4	567450
851	724201	616295051	29.1719	9.4764	2.92993	1.17509	2673.5	568786
852	725904	618470208	29.1890	9.4801	2.93044	1.17371	2676.6	570124
853	727609	620650477	29.2062	9.4838	2.93095	1.17233	2679.8	571463
854	729316	622835864	29.2233	9.4875	2.93146	1.17096	2682.9	572803
855	731025	625026375	29.2404	9.4912	2.93197	1.16959	2686.1	574146
856	732736	627222016	29.2575	9.4949	2.93247	1.16822	2689.2	575490
857	734449	629422793	29.2746	9.4986	2.93298	1.16686	2692.3	576835
858	736164	631628712	29.2916	9.5023	2.93349	1.16550	2695.5	578182
859	737881	633839779	29.3087	9.5060	2.93399	1.16414	2698.6	579530
860	739600	636056000	29.3258	9.5097	2.93450	1.16279	2701.8	580880
861	741321	638277381	29.3428	9.5134	2.93500	1.16144	2704.9	582232
862	743044	640503928	29.3598	9.5171	2.93551	1.16009	2708.1	583585
863	744769	642735647	29.3769	9.5207	2.93601	1.15875	2711.2	584940
864	746496	644972544	29.3939	9.5244	2.93651	1.15741	2714.3	586297
865	748225	647214625	29.4109	9.5281	2.93702	1.15607	2717.5	587655
866	749956	649461896	29.4279	9.5317	2.93752	1.15473	2720.6	589014
867	751689	651714363	29.4449	9.5354	2.93802	1.15340	2723.8	590375
868	753424	653972032	29.4618	9.5391	2.93852	1.15207	2726.9	591738
869	755161	656234909	29.4788	9.5427	2.93902	1.15075	2730.0	593102
870	756900	658503000	29.4958	9.5464	2.93952	1.14943	2733.2	594468
871	758641	660776311	29.5127	9.5501	2.94002	1.14811	2736.3	595835
872	760384	663054884	29.5296	9.5537	2.94052	1.14679	2739.5	597204
873	762129	665338617	29.5466	9.5574	2.94101	1.14548	2742.6	598575
874	763876	667627624	29.5635	9.5610	2.94151	1.14416	2745.8	599947
875	765625	669921875	29.5804	9.5647	2.94201	1.14286	2748.9	601320
876	767376	672221376	29.5973	9.5683	2.94250	1.14155	2752.0	602696
877	769129	674526133	29.6142	9.5719	2.94300	1.14025	2755.2	604073
878	770884	676836152	29.6311	9.5756	2.94349	1.13895	2758.3	605451
879	772641	679151439	29.6479	9.5792	2.94399	1.13766	2761.5	606831
880	774400	681472000	29.6648	9.5828	2.94448	1.13636	2764.6	608212
881	776161	683797841	29.6816	9.5865	2.94498	1.13507	2767.7	609595
882	777924	686128968	29.6985	9.5901	2.94547	1.13379	2770.9	610980
883	779689	688465387	29.7153	9.5937	2.94596	1.13250	2774.0	612366
884	781456	690807104	29.7321	9.5973	2.94645	1.13122	2777.2	613754
885	783225	693154125	29.7489	9.6010	2.94694	1.12994	2780.3	615143
886	784996	695506456	29.7658	9.6046	2.94743	1.12867	2783.5	616534
887	786769	697864103	29.7825	9.6082	2.94792	1.12740	2786.6	617927
888	788544	700227072	29.7993	9.6118	2.94841	1.12613	2789.7	619321
889	790321	702595369	29.8161	9.6154	2.94890	1.12486	2792.9	620717
890	792100	704969000	29.8329	9.6190	2.94939	1.12360	2796.0	622114
891	793881	707347971	29.8496	9.6226	2.94988	1.12233	2799.2	623513
892	795664	709732288	29.8664	9.6262	2.95036	1.12108	2802.3	624913
893	797449	712121957	29.8831	9.6298	2.95085	1.11982	2805.4	626315
894	799236	714516984	29.8998	9.6334	2.95134	1.11857	2808.6	627718
895	801025	716917375	29.9166	9.6370	2.95182	1.11732	2811.7	629124
896	802816	719323136	29.9333	9.6406	2.95231	1.11607	2814.9	630530
897	804609	721734273	29.9500	9.6442	2.95279	1.11483	2818.0	631938
898	806404	724150792	29.9666	9.6477	2.95328	1.11359	2821.2	633348
899	808201	726572699	29.9833	9.6513	2.95376	1.11235	2824.3	634760

900 TO 949

FUNCTIONS OF NUMBERS

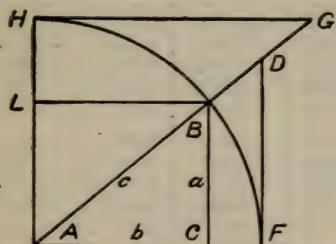
No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
900	810000	729000000	30.0000	9.6549	2.95424	1.11111	2827.4	636173
901	811801	731432701	30.0167	9.6585	2.95472	1.10988	2830.6	637587
902	813604	733870808	30.0333	9.6620	2.95521	1.10865	2833.7	639003
903	815409	736314327	30.0500	9.6656	2.95569	1.10742	2836.9	640421
904	817216	738763264	30.0666	9.6692	2.95617	1.10619	2840.0	641840
905	819025	741217625	30.0832	9.6727	2.95665	1.10497	2843.1	643261
906	820836	743677416	30.0998	9.6763	2.95713	1.10375	2846.3	644683
907	822649	746142643	30.1164	9.6799	2.95761	1.10254	2849.4	646107
908	824464	7486143312	30.1330	9.6834	2.95809	1.10132	2852.6	647533
909	826281	751089429	30.1496	9.6870	2.95856	1.10011	2855.7	648960
910	828100	753571000	30.1662	9.6905	2.95904	1.09890	2858.8	650388
911	829921	756058031	30.1828	9.6941	2.95952	1.09769	2862.0	651818
912	831744	758550528	30.1993	9.6976	2.95999	1.09649	2865.1	653250
913	833569	761048497	30.2159	9.7012	2.96047	1.09529	2868.3	654684
914	835396	763551944	30.2324	9.7047	2.96095	1.09409	2871.4	656118
915	837225	766060875	30.2490	9.7082	2.96142	1.09290	2874.6	657555
916	839056	768575296	30.2655	9.7118	2.96190	1.09170	2877.7	658993
917	840889	771095213	30.2820	9.7153	2.96237	1.09051	2880.8	660433
918	842724	773620632	30.2985	9.7188	2.96284	1.08932	2884.0	661874
919	844561	776151559	30.3150	9.7224	2.96332	1.08814	2887.1	663317
920	846400	778688000	30.3315	9.7259	2.96379	1.08696	2890.3	664761
921	848241	781229961	30.3480	9.7294	2.96426	1.08578	2893.4	666207
922	850084	783777448	30.3645	9.7329	2.96473	1.08460	2896.5	667654
923	851929	786330467	30.3809	9.7364	2.96520	1.08342	2899.7	669103
924	853776	788889024	30.3974	9.7400	2.96567	1.08225	2902.8	670554
925	855625	791453125	30.4138	9.7435	2.96614	1.08108	2906.0	672006
926	857476	794022776	30.4302	9.7470	2.96661	1.07991	2909.1	673460
927	859329	796597983	30.4467	9.7505	2.96708	1.07875	2912.3	674915
928	861184	799178752	30.4631	9.7540	2.96755	1.07759	2915.4	676372
929	863041	801765089	30.4795	9.7575	2.96802	1.07643	2918.5	677831
930	864900	804357000	30.4959	9.7610	2.96848	1.07527	2921.7	679291
931	866761	806954491	30.5123	9.7645	2.96895	1.07411	2924.8	680752
932	868624	809557568	30.5287	9.7680	2.96942	1.07296	2928.0	682216
933	870489	812166237	30.5450	9.7715	2.96988	1.07181	2931.1	683680
934	872356	814780504	30.5614	9.7750	2.97035	1.07066	2934.2	685147
935	874225	817400375	30.5778	9.7785	2.97081	1.06952	2937.4	686615
936	876096	820025856	30.5941	9.7819	2.97128	1.06838	2940.5	688084
937	877969	822656953	30.6105	9.7854	2.97174	1.06724	2943.7	689555
938	879844	825293672	30.6268	9.7889	2.97220	1.06610	2946.8	691028
939	881721	827936019	30.6431	9.7924	2.97267	1.06496	2950.0	692502
940	883600	830584000	30.6594	9.7959	2.97313	1.06383	2953.1	693978
941	885481	833237621	30.6757	9.7993	2.97359	1.06270	2956.2	695455
942	887364	835896888	30.6920	9.8028	2.97405	1.06157	2959.4	696934
943	889249	838561807	30.7083	9.8063	2.97451	1.06045	2962.5	698415
944	891136	841232384	30.7246	9.8097	2.97497	1.05932	2965.7	699897
945	893025	843908625	30.7409	9.8132	2.97543	1.05820	2968.8	701380
946	894916	846590536	30.7571	9.8167	2.97589	1.05708	2971.9	702865
947	896809	849278123	30.7734	9.8201	2.97635	1.05597	2975.1	704352
948	898704	851971392	30.7896	9.8236	2.97681	1.05485	2978.2	705840
949	900601	854670349	30.8058	9.8270	2.97727	1.05374	2981.4	707330

FUNCTIONS OF NUMBERS 950 TO 999

No.	Square	Cube	Square Root	Cubic Root	Logarithm	1000 ×	No. = Diameter	
						Reciprocal	Circum.	Area
950	902500	857375000	30.8221	9.8305	2.97772	1.05263	2984.5	708822
951	904401	860085351	30.8383	9.8339	2.97818	1.05152	2987.7	710315
952	906304	862801408	30.8545	9.8374	2.97864	1.05042	2990.8	711809
953	908209	865523177	30.8707	9.8408	2.97909	1.04932	2993.9	713306
954	910116	868250664	30.8869	9.8443	2.97955	1.04822	2997.1	714803
955	912025	870983875	30.9031	9.8477	2.98000	1.04712	3000.2	716303
956	913936	873722816	30.9192	9.8511	2.98046	1.04603	3003.4	717804
957	915849	876467493	30.9354	9.8546	2.98091	1.04493	3006.5	719306
958	917764	879217912	30.9516	9.8580	2.98137	1.04384	3009.6	720810
959	919681	881974079	30.9677	9.8614	2.98182	1.04275	3012.8	722316
960	921600	884736000	30.9839	9.8648	2.98227	1.04167	3015.9	723823
961	923521	887503681	31.0000	9.8683	2.98272	1.04058	3019.1	725332
962	925444	890277128	31.0161	9.8717	2.98318	1.03950	3022.2	726842
963	927369	893056347	31.0322	9.8751	2.98363	1.03842	3025.4	728354
964	929296	895841344	31.0483	9.8785	2.98408	1.03734	3028.5	729867
965	931225	898632125	31.0644	9.8819	2.98453	1.03627	3031.6	731382
966	933156	901428696	31.0805	9.8854	2.98498	1.03520	3034.8	732899
967	935089	904231063	31.0966	9.8888	2.98543	1.03413	3037.9	734417
968	937024	907039232	31.1127	9.8922	2.98588	1.03306	3041.1	735937
969	938961	909853209	31.1288	9.8956	2.98632	1.03199	3044.2	737458
970	940900	912673000	31.1448	9.8990	2.98677	1.03093	3047.3	738981
971	942841	915498611	31.1609	9.9024	2.98722	1.02987	3050.5	740506
972	944784	918330048	31.1769	9.9058	2.98767	1.02881	3053.6	742032
973	946729	921167317	31.1929	9.9092	2.98811	1.02775	3056.8	743559
974	948676	924010424	31.2090	9.9126	2.98856	1.02669	3059.9	745088
975	950625	926859375	31.2250	9.9160	2.98900	1.02564	3063.1	746619
976	952576	929714176	31.2410	9.9194	2.98945	1.02459	3066.2	748151
977	954529	932574833	31.2570	9.9227	2.98989	1.02354	3069.3	749685
978	956484	935441352	31.2730	9.9261	2.99034	1.02249	3072.5	751221
979	958441	938313739	31.2890	9.9295	2.99078	1.02145	3075.6	752758
980	960400	941192000	31.3050	9.9329	2.99123	1.02041	3078.8	754296
981	962361	944076141	31.3209	9.9363	2.99167	1.01937	3081.9	755837
982	964324	946966168	31.3369	9.9396	2.99211	1.01833	3085.0	757378
983	966289	949862087	31.3528	9.9430	2.99255	1.01729	3088.2	758922
984	968256	952763904	31.3688	9.9464	2.99300	1.01626	3091.3	760466
985	970225	955671625	31.3847	9.9497	2.99344	1.01523	3094.5	762013
986	972196	958585256	31.4006	9.9531	2.99388	1.01420	3097.6	763561
987	974169	961504803	31.4166	9.9565	2.99432	1.01317	3100.8	765111
988	976144	964430272	31.4325	9.9598	2.99476	1.01215	3103.9	766662
989	978121	967361669	31.4484	9.9632	2.99520	1.01112	3107.0	768214
990	980100	970299000	31.4643	9.9666	2.99564	1.01010	3110.2	769769
991	982081	973242271	31.4802	9.9699	2.99607	1.00908	3113.3	771325
992	984064	976191488	31.4960	9.9733	2.99651	1.00806	3116.5	772882
993	986049	979146657	31.5119	9.9766	2.99695	1.00705	3119.6	774441
994	988036	982107784	31.5278	9.9800	2.99739	1.00604	3122.7	776002
995	990025	985074875	31.5436	9.9833	2.99782	1.00503	3125.9	777564
996	992016	988047936	31.5595	9.9866	2.99826	1.00402	3129.0	779128
997	994009	991026973	31.5753	9.9900	2.99870	1.00301	3132.2	780693
998	996004	994011992	31.5911	9.9933	2.99913	1.00200	3135.3	782260
999	998001	997002999	31.6070	9.9967	2.99957	1.00100	3138.5	783828

TRIGONOMETRIC FORMULAE

TRIGONOMETRIC FUNCTIONS



$$\text{Radius } AF = 1$$

$$= \sin^2 A + \cos^2 A = \sin A \operatorname{cosec} A$$

$$= \cos A \sec A = \tan A \cot A$$

$$\text{Sine } A = \frac{\cos A}{\cot A} = \frac{1}{\operatorname{cosec} A} = \cos A \tan A = \sqrt{1 - \cos^2 A} = BC$$

$$\text{Cosine } A = \frac{\sin A}{\tan A} = \frac{1}{\sec A} = \sin A \cot A = \sqrt{1 - \sin^2 A} = AC$$

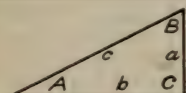
$$\text{Tangent } A = \frac{\sin A}{\cos A} = \frac{1}{\cot A} = \sin A \sec A = FD$$

$$\text{Cotangent } A = \frac{\cos A}{\sin A} = \frac{1}{\tan A} = \cos A \operatorname{cosec} A = HG$$

$$\text{Secant } A = \frac{\tan A}{\sin A} = \frac{1}{\cos A} = AD$$

$$\text{Cosecant } A = \frac{\cot A}{\cos A} = \frac{1}{\sin A} = AG$$

TRIGONOMETRIC SOLUTION OF TRIANGLES

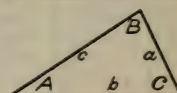


$$a^2 = b^2 + c^2 - 2bc \cos A$$

$$b^2 = a^2 + c^2 - 2ac \cos B$$

$$c^2 = a^2 + b^2 - 2ab \cos C$$

$$s = \frac{a + b + c}{2}$$



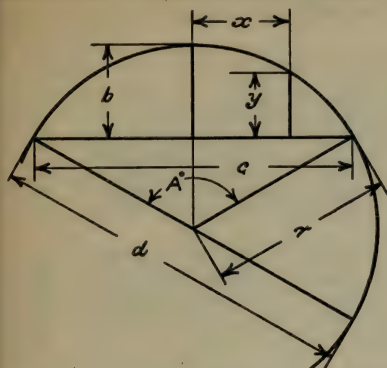
RIGHT ANGLED TRIANGLES

Known,	Required						
	A	B	C	a	b	c	Area
a, b	$\tan A = \frac{a}{b}$	$\tan B = \frac{b}{a}$	90°			$\sqrt{a^2 + b^2}$	$\frac{ab}{2}$
a, c	$\sin A = \frac{a}{c}$	$\cos B = \frac{a}{c}$	90°		$\sqrt{c^2 - a^2}$		$\frac{a \sqrt{c^2 - a^2}}{2}$
A, a		$90^\circ - A$	90°		$a \cot A$	$\frac{a}{\sin A}$	$\frac{a^2 \cot A}{2}$
A, b		$90^\circ - A$	90°	$b \tan A$		$\frac{b}{\cos A}$	$\frac{b^2 \tan A}{2}$
A, c		$90^\circ - A$	90°	$c \sin A$	$c \cos A$		$\frac{c^2 \sin 2A}{4}$

OBLIQUE ANGLED TRIANGLES

Known	Required					
	A	B	C	b	c	Area
a, b, c	$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$	$\cos \frac{1}{2} B = \sqrt{\frac{s(s-b)}{ac}}$	$\cos \frac{1}{2} C = \sqrt{\frac{s(s-c)}{ab}}$			$\sqrt{s(s-a)(s-b)(s-c)}$
a, A, B			$180^\circ - (A+B)$	$\frac{a \sin B}{\sin A}$	$\frac{a \sin C}{\sin A}$	
a, b, A		$\sin B = \frac{b \sin A}{a}$			$\frac{b \sin C}{\sin B}$	
a, b, C	$\tan A = \frac{a \sin C}{b - a \cos C}$				$\sqrt{a^2 + b^2 - 2ab \cos C}$	$\frac{ab \sin C}{2}$

PROPERTIES OF THE CIRCLE



$$\pi = 3.14159265359$$

$$\text{Circumference} = 2 \pi r = \pi d$$

$$\text{Diameter} = \text{Circumference} \times 0.31831$$

$$\text{Area} = \pi r^2$$

$$\begin{aligned} \text{Diameter of Circle of equal periphery as square} \\ = \text{side of square} \times 1.27324 \end{aligned}$$

$$\begin{aligned} \text{Side of Square of equal periphery as circle} \\ = \text{diameter of circle} \times 0.78540 \end{aligned}$$

$$\begin{aligned} \text{Diameter of Circle circumscribed about square} \\ = \text{side of square} \times 1.41421 \end{aligned}$$

$$\begin{aligned} \text{Side of Square inscribed in a circle} \\ = \text{diameter of circle} \times 0.70711 \end{aligned}$$

$$\text{Arc } a = \frac{\pi r A^\circ}{180} = 0.017453 r A^\circ$$

$$\text{Angle } A = \frac{180^\circ a}{\pi r} = 57.29578 \frac{a}{r}$$

$$\text{Radius } r = \frac{4b^2 + c^2}{8b}$$

$$\text{Chord } c = 2 \sqrt{2br - b^2} = 2r \sin \frac{A^\circ}{2}$$

$$\begin{aligned} \text{Rise } b &= r - \frac{1}{2} \sqrt{4r^2 - c^2} = \frac{c}{2} \tan \frac{A^\circ}{4} \\ &= 2r \sin^2 \frac{A}{4} = r + y - \sqrt{r^2 - x^2} \\ y &= b - r + \sqrt{r^2 - x^2} \\ x &= \sqrt{r^2 - (r + y - b)^2} \end{aligned}$$

$$\pi^2 = 9.8696044, \log = 0.9942997$$

$$\frac{1}{\pi} = 0.3183099, \log = \bar{1}.5028501$$

$$\sqrt{\frac{1}{\pi}} = 0.5641896, \log = \bar{1}.7514251$$

$$\pi^3 = 31.0062767, \log = 1.4914496$$

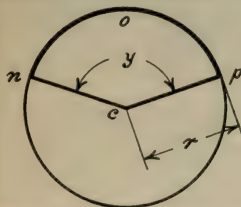
$$\frac{1}{\pi^2} = 0.1013212, \log = \bar{1}.0057003$$

$$\frac{\pi}{180} = 0.0174533, \log = \bar{2}.2418774$$

$$\sqrt{\pi} = 1.7724539, \log = 0.2485749$$

$$\frac{1}{\pi^3} = 0.0322515, \log = \bar{2}.5085500$$

$$\frac{180}{\pi} = 57.2957795, \log = 1.7581226$$



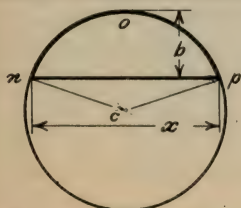
CIRCULAR SECTOR

$$r = \text{radius of circle} \quad y = \text{angle } ncp \text{ in degrees}$$

$$\text{Area of Sector } ncp = \frac{1}{2} (\text{length of arc } nop \times r)$$

$$= \text{Area of Circle} \times \frac{y}{360}$$

$$= 0.0087266 \times r^2 \times y$$



CIRCULAR SEGMENT

$$r = \text{radius of circle} \quad x = \text{chord} \quad b = \text{rise}$$

$$\text{Area of Segment } nop = \text{Area of Sector } ncp - \text{Area of triangle } ncp$$

$$= \frac{(\text{Length of arc } nop \times r) - x(r - b)}{2}$$

$$\text{Area of Segment } nsp = \text{Area of Circle} - \text{Area of Segment } nop$$

NATURAL SINES AND COSINES

De- grees	Sines							Co- sines
	0'	10'	20'	30'	40'	50'	60'	
0	0.00000	0.00291	0.00582	0.00873	0.01164	0.01454	0.01745	89
1	0.01745	0.02036	0.02327	0.02618	0.02908	0.03199	0.03490	88
2	0.03490	0.03781	0.04071	0.04362	0.04653	0.04943	0.05234	87
3	0.05234	0.05524	0.05814	0.06105	0.06395	0.06685	0.06976	86
4	0.06976	0.07266	0.07556	0.07846	0.08136	0.08426	0.08716	85
5	0.08716	0.09005	0.09295	0.09585	0.09874	0.10164	0.10453	84
6	0.10453	0.10742	0.11031	0.11320	0.11609	0.11898	0.12187	83
7	0.12187	0.12476	0.12764	0.13053	0.13341	0.13629	0.13917	82
8	0.13917	0.14205	0.14493	0.14781	0.15069	0.15356	0.15643	81
9	0.15643	0.15931	0.16218	0.16505	0.16792	0.17078	0.17365	80
10	0.17365	0.17651	0.17937	0.18224	0.18509	0.18795	0.19081	79
11	0.19081	0.19366	0.19652	0.19937	0.20222	0.20507	0.20791	78
12	0.20791	0.21076	0.21360	0.21644	0.21928	0.22212	0.22495	77
13	0.22495	0.22778	0.23062	0.23345	0.23627	0.23910	0.24192	76
14	0.24192	0.24474	0.24756	0.25038	0.25320	0.25601	0.25882	75
15	0.25882	0.26163	0.26443	0.26724	0.27004	0.27284	0.27564	74
16	0.27564	0.27843	0.28123	0.28402	0.28680	0.28959	0.29237	73
17	0.29237	0.29515	0.29793	0.30071	0.30348	0.30625	0.30902	72
18	0.30902	0.31178	0.31454	0.31730	0.32006	0.32282	0.32557	71
19	0.32557	0.32832	0.33106	0.33381	0.33655	0.33929	0.34202	70
20	0.34202	0.34475	0.34748	0.35021	0.35293	0.35565	0.35837	69
21	0.35837	0.36108	0.36379	0.36650	0.36921	0.37191	0.37461	68
22	0.37461	0.37730	0.37999	0.38268	0.38537	0.38805	0.39073	67
23	0.39073	0.39341	0.39608	0.39875	0.40142	0.40408	0.40674	66
24	0.40674	0.40939	0.41204	0.41469	0.41734	0.41998	0.42262	65
25	0.42262	0.42525	0.42788	0.43051	0.43313	0.43575	0.43837	64
26	0.43837	0.44098	0.44359	0.44620	0.44880	0.45140	0.45399	63
27	0.45399	0.45658	0.45917	0.46175	0.46433	0.46690	0.46947	62
28	0.46947	0.47204	0.47460	0.47716	0.47971	0.48226	0.48481	61
29	0.48481	0.48735	0.48989	0.49242	0.49495	0.49748	0.50000	60
30	0.50000	0.50252	0.50503	0.50754	0.51004	0.51254	0.51504	59
31	0.51504	0.51753	0.52002	0.52250	0.52498	0.52745	0.52992	58
32	0.52992	0.53238	0.53484	0.53730	0.53975	0.54220	0.54464	57
33	0.54464	0.54708	0.54951	0.55194	0.55436	0.55678	0.55919	56
34	0.55919	0.56160	0.56401	0.56641	0.56880	0.57119	0.57358	55
35	0.57358	0.57596	0.57833	0.58070	0.58307	0.58543	0.58779	54
36	0.58779	0.59014	0.59248	0.59482	0.59716	0.59949	0.60182	53
37	0.60182	0.60414	0.60645	0.60876	0.61107	0.61337	0.61566	52
38	0.61566	0.61795	0.62024	0.62251	0.62479	0.62706	0.62932	51
39	0.62932	0.63158	0.63383	0.63608	0.63832	0.64056	0.64279	50
40	0.64279	0.64501	0.64723	0.64945	0.65166	0.65386	0.65606	49
41	0.65606	0.65825	0.66044	0.66262	0.66480	0.66697	0.66913	48
42	0.66913	0.67129	0.67344	0.67559	0.67773	0.67987	0.68200	47
43	0.68200	0.68412	0.68624	0.68835	0.69046	0.69256	0.69466	46
44	0.69466	0.69675	0.69883	0.70091	0.70298	0.70505	0.70711	45
Sines	60'	50'	40'	30'	20'	10'	0'	De- grees
	Cosines							

NATURAL SINES AND COSINES

De- grees	Cosines							Sines
	0'	10'	20'	30'	40'	50'	60'	
0	1.00000	1.00000	0.99998	0.99996	0.99993	0.99989	0.99985	89
1	0.99985	0.99979	0.99973	0.99966	0.99958	0.99949	0.99939	88
2	0.99939	0.99929	0.99917	0.99905	0.99892	0.99878	0.99863	87
3	0.99863	0.99847	0.99831	0.99813	0.99795	0.99776	0.99756	86
4	0.99756	0.99736	0.99714	0.99692	0.99668	0.99644	0.99619	85
5	0.99619	0.99594	0.99567	0.99540	0.99511	0.99482	0.99452	84
6	0.99452	0.99421	0.99390	0.99357	0.99324	0.99290	0.99255	83
7	0.99255	0.99219	0.99182	0.99144	0.99106	0.99067	0.99027	82
8	0.99027	0.98986	0.98944	0.98902	0.98858	0.98814	0.98769	81
9	0.98769	0.98723	0.98676	0.98629	0.98580	0.98531	0.98481	80
10	0.98481	0.98430	0.98378	0.98325	0.98272	0.98218	0.98163	79
11	0.98163	0.98107	0.98050	0.97992	0.97934	0.97875	0.97815	78
12	0.97815	0.97754	0.97692	0.97630	0.97566	0.97502	0.97437	77
13	0.97437	0.97371	0.97304	0.97237	0.97169	0.97100	0.97030	76
14	0.97030	0.96959	0.96887	0.96815	0.96742	0.96667	0.96593	75
15	0.96593	0.96517	0.96440	0.96363	0.96285	0.96206	0.96126	74
16	0.96126	0.96046	0.95964	0.95882	0.95799	0.95715	0.95630	73
17	0.95630	0.95545	0.95459	0.95372	0.95284	0.95195	0.95106	72
18	0.95106	0.95015	0.94924	0.94832	0.94740	0.94646	0.94552	71
19	0.94552	0.94457	0.94361	0.94264	0.94167	0.94068	0.93969	70
20	0.93969	0.93869	0.93769	0.93667	0.93565	0.93462	0.93358	69
21	0.93358	0.93253	0.93148	0.93042	0.92935	0.92827	0.92718	68
22	0.92718	0.92609	0.92499	0.92388	0.92276	0.92164	0.92050	67
23	0.92050	0.91936	0.91822	0.91706	0.91590	0.91472	0.91355	66
24	0.91355	0.91236	0.91116	0.90996	0.90875	0.90753	0.90631	65
25	0.90631	0.90507	0.90383	0.90259	0.90133	0.90007	0.89879	64
26	0.89879	0.89752	0.89623	0.89493	0.89363	0.89232	0.89101	63
27	0.89101	0.88968	0.88835	0.88701	0.88566	0.88431	0.88295	62
28	0.88295	0.88158	0.88020	0.87882	0.87743	0.87603	0.87462	61
29	0.87462	0.87321	0.87178	0.87036	0.86892	0.86748	0.86603	60
30	0.86603	0.86457	0.86310	0.86163	0.86015	0.85866	0.85717	59
31	0.85717	0.85567	0.85416	0.85264	0.85112	0.84959	0.84805	58
32	0.84805	0.84650	0.84495	0.84339	0.84182	0.84025	0.83867	57
33	0.83867	0.83708	0.83549	0.83389	0.83228	0.83066	0.82904	56
34	0.82904	0.82741	0.82577	0.82413	0.82248	0.82082	0.81915	55
35	0.81915	0.81748	0.81580	0.81412	0.81242	0.81072	0.80902	54
36	0.80902	0.80730	0.80558	0.80386	0.80212	0.80038	0.79864	53
37	0.79864	0.79688	0.79512	0.79335	0.79158	0.78980	0.78801	52
38	0.78801	0.78622	0.78442	0.78261	0.78079	0.77897	0.77715	51
39	0.77715	0.77531	0.77347	0.77162	0.76977	0.76791	0.76604	50
40	0.76604	0.76417	0.76229	0.76041	0.75851	0.75661	0.75471	49
41	0.75471	0.75280	0.75088	0.74896	0.74703	0.74509	0.74314	48
42	0.74314	0.74120	0.73924	0.73728	0.73531	0.73333	0.73135	47
43	0.73135	0.72937	0.72737	0.72537	0.72337	0.72136	0.71934	46
44	0.71934	0.71732	0.71529	0.71325	0.71121	0.70916	0.70711	45
Co- sines	60'	50'	40'	30'	20'	10'	0'	De- grees
	Sines							

NATURAL TANGENTS AND COTANGENTS

De- grees	Tangents							Cotan- gents
	0'	10'	20'	30'	40'	50'	60'	
0	0.00000	0.00291	0.00582	0.00873	0.01164	0.01455	0.01746	89
1	0.01746	0.02036	0.02328	0.02619	0.02910	0.03201	0.03492	88
2	0.03492	0.03783	0.04075	0.04366	0.04658	0.04949	0.05241	87
3	0.05241	0.05533	0.05824	0.06116	0.06408	0.06700	0.06993	86
4	0.06993	0.07285	0.07578	0.07870	0.08163	0.08456	0.08749	85
5	0.08749	0.09042	0.09335	0.09629	0.09923	0.10216	0.10510	84
6	0.10510	0.10805	0.11099	0.11394	0.11688	0.11983	0.12278	83
7	0.12278	0.12574	0.12869	0.13165	0.13461	0.13758	0.14054	82
8	0.14054	0.14351	0.14648	0.14945	0.15243	0.15540	0.15838	81
9	0.15838	0.16137	0.16435	0.16734	0.17033	0.17333	0.17633	80
10	0.17633	0.17933	0.18233	0.18534	0.18835	0.19136	0.19438	79
11	0.19438	0.19740	0.20042	0.20345	0.20648	0.20952	0.21256	78
12	0.21256	0.21560	0.21864	0.22169	0.22475	0.22781	0.23087	77
13	0.23087	0.23393	0.23700	0.24008	0.24316	0.24624	0.24933	76
14	0.24933	0.25242	0.25552	0.25862	0.26172	0.26483	0.26795	75
15	0.26795	0.27107	0.27419	0.27732	0.28046	0.28360	0.28675	74
16	0.28675	0.28990	0.29305	0.29621	0.29938	0.30255	0.30573	73
17	0.30573	0.30891	0.31210	0.31530	0.31850	0.32171	0.32492	72
18	0.32492	0.32814	0.33136	0.33460	0.33783	0.34108	0.34433	71
19	0.34433	0.34758	0.35085	0.35412	0.35740	0.36068	0.36397	70
20	0.36397	0.36727	0.37057	0.37388	0.37720	0.38053	0.38386	69
21	0.38386	0.38721	0.39055	0.39391	0.39727	0.40065	0.40403	68
22	0.40403	0.40741	0.41081	0.41421	0.41763	0.42105	0.42447	67
23	0.42447	0.42791	0.43136	0.43481	0.43828	0.44175	0.44523	66
24	0.44523	0.44872	0.45222	0.45573	0.45924	0.46277	0.46631	65
25	0.46631	0.46985	0.47341	0.47698	0.48055	0.48414	0.48773	64
26	0.48773	0.49134	0.49495	0.49858	0.50222	0.50587	0.50953	63
27	0.50953	0.51320	0.51688	0.52057	0.52427	0.52798	0.53171	62
28	0.53171	0.53545	0.53920	0.54296	0.54674	0.55051	0.55431	61
29	0.55431	0.55812	0.56194	0.56577	0.56962	0.57348	0.57735	60
30	0.57735	0.58124	0.58513	0.58905	0.59297	0.59691	0.60086	59
31	0.60086	0.60483	0.60881	0.61280	0.61681	0.62083	0.62487	58
32	0.62487	0.62892	0.63299	0.63707	0.64117	0.64528	0.64941	57
33	0.64941	0.65355	0.65771	0.66189	0.66608	0.67028	0.67451	56
34	0.67451	0.67875	0.68301	0.68728	0.69157	0.69588	0.70021	55
35	0.70021	0.70455	0.70891	0.71329	0.71769	0.72211	0.72654	54
36	0.72654	0.73100	0.73547	0.73996	0.74447	0.74900	0.75355	53
37	0.75355	0.75812	0.76272	0.76733	0.77196	0.77661	0.78129	52
38	0.78129	0.78598	0.79070	0.79544	0.80020	0.80498	0.80978	51
39	0.80978	0.81461	0.81946	0.82434	0.82923	0.83415	0.83910	50
40	0.83910	0.84407	0.84906	0.85408	0.85912	0.86419	0.86929	49
41	0.86929	0.87441	0.87955	0.88473	0.88992	0.89515	0.90040	48
42	0.90040	0.90569	0.91099	0.91633	0.92170	0.92709	0.93252	47
43	0.93252	0.93797	0.94345	0.94896	0.95451	0.96008	0.96569	46
44	0.96569	0.97133	0.97700	0.98270	0.98843	0.99420	1.00000	45
Tan- gents	60'	50'	40'	30'	20'	10'	0'	De- grees

NATURAL TANGENTS AND COTANGENTS

De- grees	Cotangents							Tan- gents
	0'	10'	20'	30'	40'	50'	60'	
0	∞	343.77371	171.88540	114.58865	85.93979	68.75009	57.28996	89
1	57.28996	49.10388	42.96408	38.18846	34.36777	31.24158	28.63625	88
2	28.63625	26.43160	24.54176	22.90377	21.47040	20.20555	19.08114	87
3	19.08114	18.07498	17.16934	16.34986	15.60478	14.92442	14.30067	86
4	14.30067	13.72674	13.19688	12.70621	12.25051	11.82617	11.43005	85
5	11.43005	11.05943	10.71191	10.38540	10.07803	9.78817	9.51436	84
6	9.51436	9.25530	9.00983	8.77689	8.55555	8.34496	8.14435	83
7	8.14435	7.95302	7.77035	7.59575	7.42871	7.26873	7.11537	82
8	7.11537	6.96823	6.82694	6.69116	6.56055	6.43484	6.31375	81
9	6.31375	6.19703	6.08444	5.97576	5.87080	5.76937	5.67128	80
10	5.67128	5.57638	5.48451	5.39552	5.30928	5.22566	5.14455	79
11	5.14455	5.06584	4.98940	4.91516	4.84300	4.77286	4.70463	78
12	4.70463	4.63825	4.57363	4.51071	4.44942	4.38969	4.33148	77
13	4.33148	4.27471	4.21933	4.16530	4.11256	4.06107	4.01078	76
14	4.01078	3.96165	3.91364	3.86671	3.82083	3.77595	3.73205	75
15	3.73205	3.68909	3.64705	3.60588	3.56557	3.52609	3.48741	74
16	3.48741	3.44951	3.41236	3.37594	3.34023	3.30521	3.27085	73
17	3.27085	3.23714	3.20406	3.17159	3.13972	3.10842	3.07768	72
18	3.07768	3.04749	3.01783	2.98869	2.96004	2.93189	2.90421	71
19	2.90421	2.87700	2.85023	2.82391	2.79802	2.77254	2.74748	70
20	2.74748	2.72281	2.69853	2.67462	2.65109	2.62791	2.60509	69
21	2.60509	2.58261	2.56046	2.53865	2.51715	2.49597	2.47509	68
22	2.47509	2.45451	2.43422	2.41421	2.39449	2.37504	2.35585	67
23	2.35585	2.33693	2.31826	2.29984	2.28167	2.26374	2.24604	66
24	2.24604	2.22857	2.21132	2.19430	2.17749	2.16090	2.14451	65
25	2.14451	2.12832	2.11233	2.09654	2.08094	2.06553	2.05030	64
26	2.05030	2.03526	2.02039	2.00569	1.99116	1.97680	1.96261	63
27	1.96261	1.94858	1.93470	1.92098	1.90741	1.89400	1.88073	62
28	1.88073	1.86760	1.85462	1.84177	1.82907	1.81649	1.80405	61
29	1.80405	1.79174	1.77955	1.76749	1.75556	1.74375	1.73205	60
30	1.73205	1.72047	1.70901	1.69766	1.68643	1.67530	1.66428	59
31	1.66428	1.65337	1.64256	1.63185	1.62125	1.61074	1.60033	58
32	1.60033	1.59002	1.57981	1.56969	1.55966	1.54972	1.53987	57
33	1.53987	1.53010	1.52043	1.51084	1.50133	1.49190	1.48256	56
34	1.48256	1.47330	1.46411	1.45501	1.44598	1.43703	1.42815	55
35	1.42815	1.41934	1.41061	1.40195	1.39336	1.38484	1.37638	54
36	1.37638	1.36800	1.35968	1.35142	1.34323	1.33511	1.32704	53
37	1.32704	1.31904	1.31110	1.30323	1.29541	1.28764	1.27994	52
38	1.27994	1.27230	1.26471	1.25717	1.24969	1.24227	1.23490	51
39	1.23490	1.22758	1.22031	1.21310	1.20593	1.19882	1.19175	50
40	1.19175	1.18474	1.17777	1.17085	1.16398	1.15715	1.15037	49
41	1.15037	1.14363	1.13694	1.13029	1.12369	1.11713	1.11061	48
42	1.11061	1.10414	1.09770	1.09131	1.08496	1.07864	1.07237	47
43	1.07237	1.06613	1.05994	1.05378	1.04766	1.04158	1.03553	46
44	1.03553	1.02952	1.02355	1.01761	1.01170	1.00583	1.00000	45
Co- tan- gents	60'	50'	40'	30'	20'	10'	0'	De- grees
	Tangents							

NATURAL SECANTS AND COSECANTS

De- grees	Secants							Cose- cants
	0'	10'	20'	30'	40'	50'	60'	
0	1.00000	1.00000	1.00002	1.00004	1.00007	1.00011	1.00015	89
1	1.00015	1.00021	1.00027	1.00034	1.00042	1.00051	1.00061	88
2	1.00061	1.00072	1.00083	1.00095	1.00108	1.00122	1.00137	87
3	1.00137	1.00153	1.00169	1.00187	1.00205	1.00224	1.00244	86
4	1.00244	1.00265	1.00287	1.00309	1.00333	1.00357	1.00382	85
5	1.00382	1.00408	1.00435	1.00463	1.00491	1.00521	1.00551	84
6	1.00551	1.00582	1.00614	1.00647	1.00681	1.00715	1.00751	83
7	1.00751	1.00787	1.00825	1.00863	1.00902	1.00942	1.00983	82
8	1.00983	1.01024	1.01067	1.01111	1.01155	1.01200	1.01247	81
9	1.01247	1.01294	1.01342	1.01391	1.01440	1.01491	1.01543	80
10	1.01543	1.01595	1.01649	1.01703	1.01758	1.01815	1.01872	79
11	1.01872	1.01930	1.01989	1.02049	1.02110	1.02171	1.02234	78
12	1.02234	1.02298	1.02362	1.02428	1.02494	1.02562	1.02630	77
13	1.02630	1.02700	1.02770	1.02842	1.02914	1.02987	1.03061	76
14	1.03061	1.03137	1.03213	1.03290	1.03368	1.03447	1.03528	75
15	1.03528	1.03609	1.03691	1.03774	1.03858	1.03944	1.04030	74
16	1.04030	1.04117	1.04206	1.04295	1.04385	1.04477	1.04569	73
17	1.04569	1.04663	1.04757	1.04853	1.04950	1.05047	1.05146	72
18	1.05146	1.05246	1.05347	1.05449	1.05552	1.05657	1.05762	71
19	1.05762	1.05869	1.05976	1.06085	1.06195	1.06306	1.06418	70
20	1.06418	1.06531	1.06645	1.06761	1.06878	1.06995	1.07115	69
21	1.07115	1.07235	1.07356	1.07479	1.07602	1.07727	1.07853	68
22	1.07853	1.07981	1.08109	1.08239	1.08370	1.08503	1.08636	67
23	1.08636	1.08771	1.08907	1.09044	1.09183	1.09323	1.09464	66
24	1.09464	1.09606	1.09750	1.09895	1.10041	1.10189	1.10338	65
25	1.10338	1.10488	1.10640	1.10793	1.10947	1.11103	1.11260	64
26	1.11260	1.11419	1.11579	1.11740	1.11903	1.12067	1.12233	63
27	1.12233	1.12400	1.12568	1.12738	1.12910	1.13083	1.13257	62
28	1.13257	1.13433	1.13610	1.13789	1.13970	1.14152	1.14335	61
29	1.14335	1.14521	1.14707	1.14896	1.15085	1.15277	1.15470	60
30	1.15470	1.15665	1.15861	1.16059	1.16259	1.16460	1.16663	59
31	1.16663	1.16868	1.17075	1.17283	1.17493	1.17704	1.17918	58
32	1.17918	1.18133	1.18350	1.18569	1.18790	1.19012	1.19236	57
33	1.19236	1.19463	1.19691	1.19920	1.20152	1.20386	1.20622	56
34	1.20622	1.20859	1.21099	1.21341	1.21584	1.21830	1.22077	55
35	1.22077	1.22327	1.22579	1.22833	1.23089	1.23347	1.23607	54
36	1.23607	1.23869	1.24134	1.24400	1.24669	1.24940	1.25214	53
37	1.25214	1.25489	1.25767	1.26047	1.26330	1.26615	1.26902	52
38	1.26902	1.27191	1.27483	1.27778	1.28075	1.28374	1.28676	51
39	1.28676	1.28980	1.29287	1.29597	1.29909	1.30223	1.30541	50
40	1.30541	1.30861	1.31183	1.31509	1.31837	1.32168	1.32501	49
41	1.32501	1.32838	1.33177	1.33519	1.33864	1.34212	1.34563	48
42	1.34563	1.34917	1.35274	1.35634	1.35997	1.36363	1.36733	47
43	1.36733	1.37105	1.37481	1.37860	1.38242	1.38628	1.39016	46
44	1.39016	1.39409	1.39804	1.40203	1.40606	1.41012	1.41421	45
Se- cants	60'	50'	40'	30'	20'	10'	0'	De- grees
	Cosecants							

NATURAL SECANTS AND COSECANTS

De- grees	Cosecants							Se- cants
	0'	10'	20'	30'	40'	50'	60'	
0	∞	343.77516	171.88831	114.59301	85.94561	68.75736	57.29869	89
1	57.29869	49.11406	42.97571	38.20155	34.38232	31.25758	28.65371	88
2	28.65371	26.45051	24.56212	22.92559	21.49368	20.23028	19.10732	87
3	19.10732	18.10262	17.19843	16.38041	15.63679	14.95788	14.33559	86
4	14.33559	13.76312	13.23472	12.74550	12.29125	11.86837	11.47371	85
5	11.47371	11.10455	10.75849	10.43343	10.12752	9.83912	9.56677	84
6	9.56677	9.30917	9.06515	8.83367	8.61379	8.40466	8.20551	83
7	8.20551	8.01565	7.83443	7.66130	7.49571	7.33719	7.18530	82
8	7.18530	7.03962	6.89979	6.76547	6.63633	6.51208	6.39245	81
9	6.39245	6.27719	6.16607	6.05886	5.95536	5.85539	5.75877	80
10	5.75877	5.66533	5.57493	5.48740	5.40263	5.32049	5.24084	79
11	5.24084	5.16359	5.08863	5.01585	4.94517	4.87649	4.80973	78
12	4.80973	4.74482	4.68167	4.62023	4.56041	4.50216	4.44541	77
13	4.44541	4.39012	4.33622	4.28366	4.23239	4.18238	4.13357	76
14	4.13357	4.08591	4.03938	3.99393	3.94952	3.90613	3.86370	75
15	3.86370	3.82223	3.78166	3.74198	3.70315	3.66515	3.62796	74
16	3.62796	3.59154	3.55587	3.52094	3.48671	3.45317	3.42030	73
17	3.42030	3.38808	3.35649	3.32551	3.29512	3.26531	3.23607	72
18	3.23607	3.20737	3.17920	3.15155	3.12440	3.09774	3.07155	71
19	3.07155	3.04584	3.02057	2.99574	2.97135	2.94737	2.92380	70
20	2.92380	2.90063	2.87785	2.85545	2.83342	2.81175	2.79043	69
21	2.79043	2.76945	2.74881	2.72850	2.70851	2.68884	2.66947	68
22	2.66947	2.65040	2.63162	2.61313	2.59491	2.57698	2.55930	67
23	2.55930	2.54190	2.52474	2.50784	2.49119	2.47477	2.45859	66
24	2.45859	2.44264	2.42692	2.41142	2.39614	2.38107	2.36620	65
25	2.36620	2.35154	2.33708	2.32282	2.30875	2.29487	2.28117	64
26	2.28117	2.26766	2.25432	2.24116	2.22817	2.21535	2.20269	63
27	2.20269	2.19019	2.17786	2.16568	2.15366	2.14178	2.13005	62
28	2.13005	2.11847	2.10704	2.09574	2.08458	2.07356	2.06267	61
29	2.06267	2.05191	2.04128	2.03077	2.02039	2.01014	2.00000	60
30	2.00000	1.98998	1.98008	1.97029	1.96062	1.95106	1.94160	59
31	1.94160	1.93226	1.92302	1.91388	1.90485	1.89591	1.88709	58
32	1.88708	1.87834	1.86970	1.86116	1.85271	1.84435	1.83608	57
33	1.83608	1.82790	1.81981	1.81180	1.80388	1.79604	1.78829	56
34	1.78829	1.78062	1.77303	1.76552	1.75808	1.75073	1.74345	55
35	1.74345	1.73624	1.72911	1.72205	1.71506	1.70815	1.70130	54
36	1.70130	1.69452	1.68782	1.68117	1.67460	1.66809	1.66164	53
37	1.66164	1.65526	1.64894	1.64268	1.63648	1.63035	1.62427	52
38	1.62427	1.61825	1.61229	1.60639	1.60054	1.59475	1.58902	51
39	1.58902	1.58333	1.57771	1.57213	1.56661	1.56114	1.55572	50
40	1.55572	1.55036	1.54504	1.53977	1.53455	1.52938	1.52425	49
41	1.52425	1.51918	1.51415	1.50916	1.50422	1.49933	1.49448	48
42	1.49448	1.48967	1.48491	1.48019	1.47551	1.47087	1.46628	47
43	1.46628	1.46173	1.45721	1.45274	1.44831	1.44391	1.43956	46
44	1.43956	1.43524	1.43096	1.42672	1.42251	1.41835	1.41421	45
Cose- cants	60'	50'	40'	30'	20'	10'	0'	De- grees
	Secants							

LENGTH OF CIRCULAR ARCS FOR THE RADIUS 1

DEGREES					MINUTES		SECONDS		
0°	0.000 0000	60°	1.047 1976	120°	2.094 3951	0'	0.000 0000	0"	0.000 0000
1	0.017 4533	61	1.064 6508	121	2.111 8484	1	0.000 2909	1	0.000 0048
2	0.034 9066	62	1.082 1041	122	2.129 3017	2	0.000 5813	2	0.000 0097
3	0.052 3599	63	1.099 5574	123	2.146 7550	3	0.000 8727	3	0.000 0145
4	0.069 8132	64	1.117 0107	124	2.164 2083	4	0.001 1636	4	0.000 0194
5	0.087 2665	65	1.134 4640	125	2.181 6616	5	0.001 4544	5	0.000 0242
6	0.104 7198	66	1.151 9173	126	2.199 1149	6	0.001 7453	6	0.000 0291
7	0.122 1730	67	1.169 3706	127	2.216 5682	7	0.002 0362	7	0.000 0339
8	0.139 6263	68	1.186 8239	128	2.234 0214	8	0.002 3271	8	0.000 0388
9	0.157 0796	69	1.204 2772	129	2.251 4747	9	0.002 6180	9	0.000 0436
10	0.174 5329	70	1.221 7305	130	2.268 9280	10	0.002 9089	10	0.000 0485
11	0.191 9862	71	1.239 1838	131	2.286 3813	11	0.003 1998	11	0.000 0533
12	0.209 4395	72	1.256 6371	132	2.303 8346	12	0.003 4907	12	0.000 0582
13	0.226 8928	73	1.274 0904	133	2.321 2879	13	0.003 7815	13	0.000 0630
14	0.244 3461	74	1.291 5436	134	2.338 7412	14	0.004 0724	14	0.000 0679
15	0.261 7994	75	1.308 9969	135	2.356 1945	15	0.004 3633	15	0.000 0727
16	0.279 2527	76	1.326 4502	136	2.373 6478	16	0.004 6542	16	0.000 0776
17	0.296 7060	77	1.343 9035	137	2.391 1011	17	0.004 9451	17	0.000 0824
18	0.314 1593	78	1.361 3568	138	2.408 5544	18	0.005 2360	18	0.000 0873
19	0.331 6126	79	1.378 8101	139	2.426 0077	19	0.005 5269	19	0.000 0921
20	0.349 0659	80	1.396 2634	140	2.443 4610	20	0.005 8178	20	0.000 0970
21	0.366 5191	81	1.413 7167	141	2.460 9142	21	0.006 1087	21	0.000 1018
22	0.383 9724	82	1.431 1700	142	2.478 3675	22	0.006 3995	22	0.000 1067
23	0.401 4257	83	1.448 6233	143	2.495 8208	23	0.006 6904	23	0.000 1115
24	0.418 8790	84	1.466 0766	144	2.513 2741	24	0.006 9813	24	0.000 1164
25	0.436 3323	85	1.483 5299	145	2.530 7274	25	0.007 2722	25	0.000 1212
26	0.453 7856	86	1.500 9832	146	2.548 1807	26	0.007 5631	26	0.000 1261
27	0.471 2389	87	1.518 4364	147	2.565 6340	27	0.007 8540	27	0.000 1309
28	0.488 6922	88	1.535 8897	148	2.583 0873	28	0.008 1449	28	0.000 1357
29	0.506 1455	89	1.553 3430	149	2.600 5406	29	0.008 4358	29	0.000 1406
30	0.523 5988	90	1.570 7963	150	2.617 9939	30	0.008 7266	30	0.000 1454
31	0.541 0521	91	1.588 2496	151	2.635 4472	31	0.009 0175	31	0.000 1503
32	0.558 5054	92	1.605 7029	152	2.652 9005	32	0.009 3084	32	0.000 1551
33	0.575 9587	93	1.623 1562	153	2.670 3538	33	0.009 5993	33	0.000 1600
34	0.593 4119	94	1.640 6095	154	2.687 8070	34	0.009 8902	34	0.000 1648
35	0.610 8652	95	1.658 0628	155	2.705 2603	35	0.010 1811	35	0.000 1697
36	0.628 3185	96	1.675 5161	156	2.722 7136	36	0.010 4720	36	0.000 1745
37	0.645 7718	97	1.692 9694	157	2.740 1669	37	0.010 7629	37	0.000 1794
38	0.663 2251	98	1.710 4227	158	2.757 6202	38	0.011 0538	38	0.000 1842
39	0.680 6784	99	1.727 8760	159	2.775 0735	39	0.011 3446	39	0.000 1891
40	0.698 1317	100	1.745 3293	160	2.792 5268	40	0.011 6355	40	0.000 1939
41	0.715 5850	101	1.762 7825	161	2.809 9801	41	0.011 9264	41	0.000 1988
42	0.733 0383	102	1.780 2358	162	2.827 4334	42	0.012 2173	42	0.000 2036
43	0.750 4916	103	1.797 6891	163	2.844 8867	43	0.012 5082	43	0.000 2085
44	0.767 9449	104	1.815 1424	164	2.862 3400	44	0.012 7991	44	0.000 2133
45	0.785 3982	105	1.832 5957	165	2.879 7933	45	0.013 0900	45	0.000 2182
46	0.802 8515	106	1.850 0490	166	2.897 2466	46	0.013 3809	46	0.000 2230
47	0.820 3047	107	1.867 5023	167	2.914 6999	47	0.013 6717	47	0.000 2279
48	0.837 7580	108	1.884 9556	168	2.932 1531	48	0.013 9626	48	0.000 2327
49	0.855 2113	109	1.902 4089	169	2.949 6064	49	0.014 2535	49	0.000 2376
50	0.872 6646	110	1.919 8622	170	2.967 0597	50	0.014 5444	50	0.000 2424
51	0.890 1179	111	1.937 3155	171	2.984 5130	51	0.014 8353	51	0.000 2473
52	0.907 5712	112	1.954 7688	172	3.001 9663	52	0.015 1262	52	0.000 2521
53	0.925 0245	113	1.972 2221	173	3.019 4196	53	0.015 4171	53	0.000 2570
54	0.942 4778	114	1.989 6753	174	3.036 8729	54	0.015 7080	54	0.000 2618
55	0.959 9311	115	2.007 1286	175	3.054 3262	55	0.015 9989	55	0.000 2666
56	0.977 3844	116	2.024 5819	176	3.071 7795	56	0.016 2897	56	0.000 2715
57	0.994 8377	117	2.042 0352	177	3.089 2328	57	0.016 5806	57	0.000 2763
58	1.012 2910	118	2.059 4885	178	3.106 6861	58	0.016 8715	58	0.000 2812
59	1.029 7443	119	2.076 9418	179	3.124 1394	59	0.017 1624	59	0.000 2860
60	1.047 1976	120	2.094 3951	180	3.141 5927	60	0.017 4533	60	0.000 2909

By the use of the above table, the length of any arc may be found if the length of the radius and the angle of the segment be known.

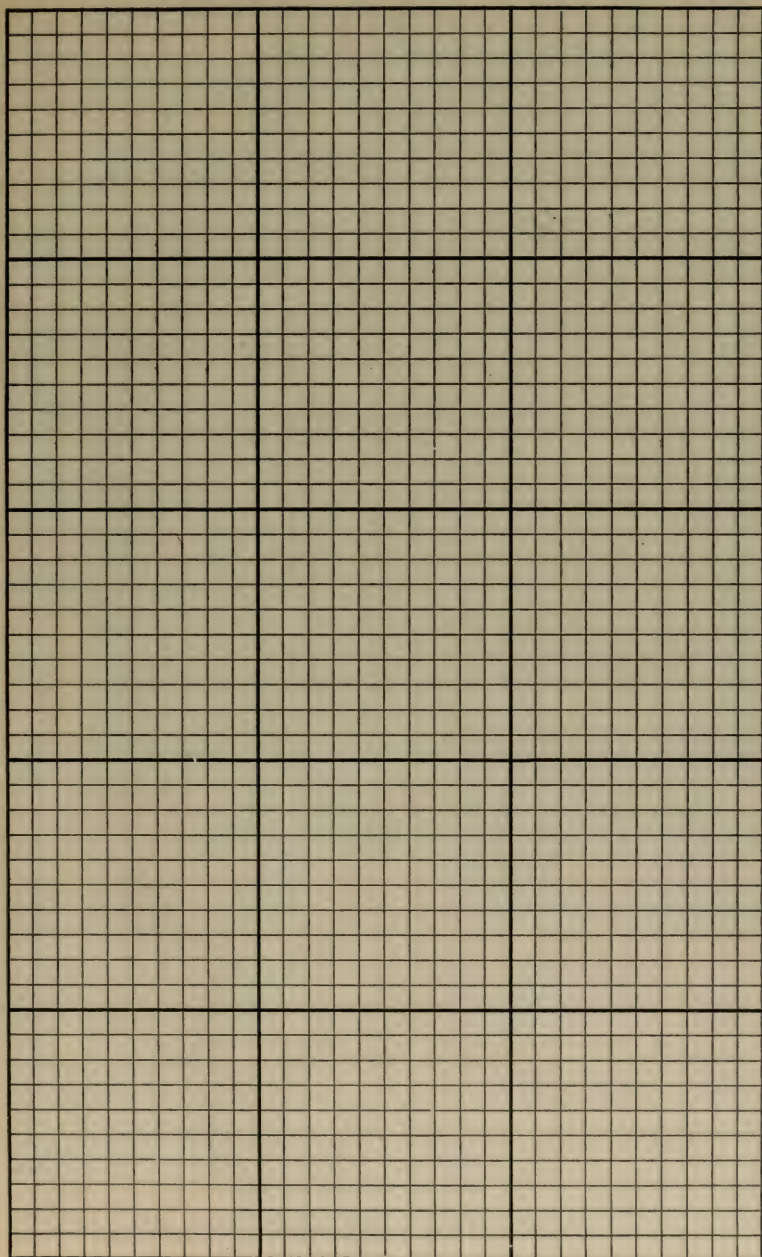
Example:— Required the length of arc of segment of $32^{\circ} 15' 27''$ with radius of 24 feet 3 inches.

From table, Length of arc (Radius 1) for $32^{\circ} = .5585054$
 $15' = .0043633$
 $27'' = .0001309$

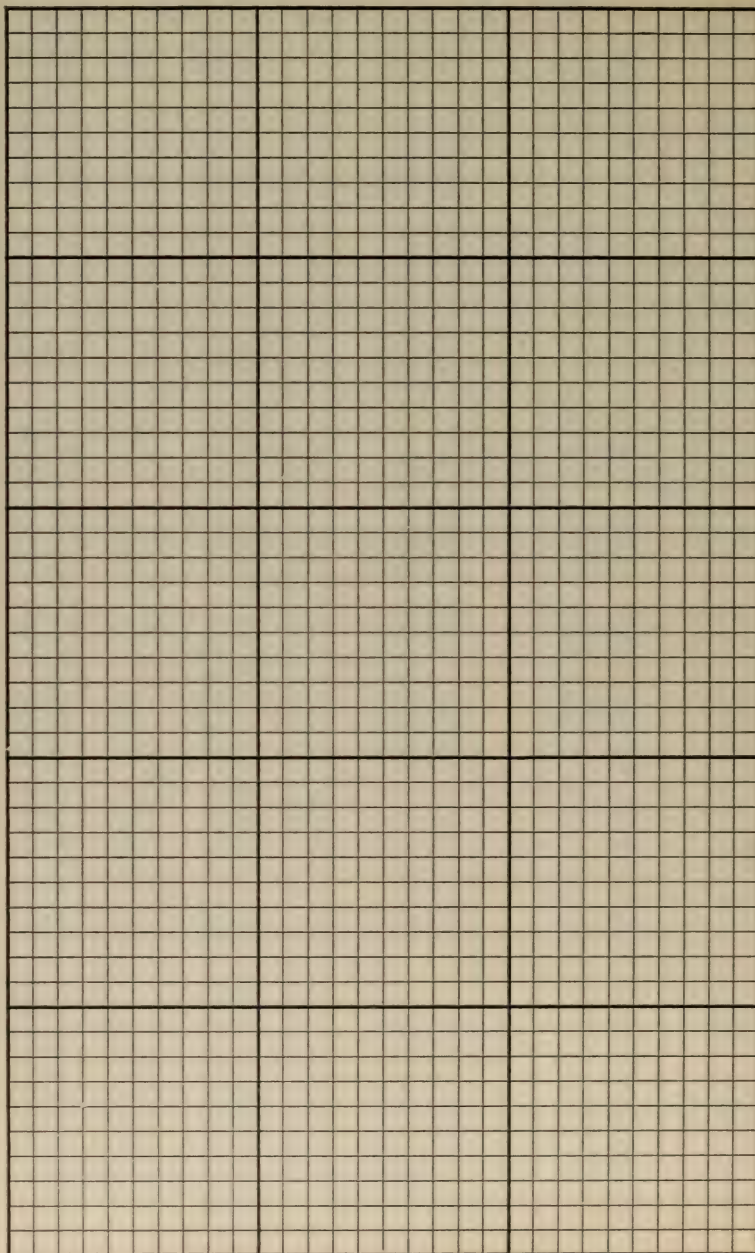
5629996

$.5629996 \times 24.25$ (length of radius) = $13.65' = \text{Ans.}$

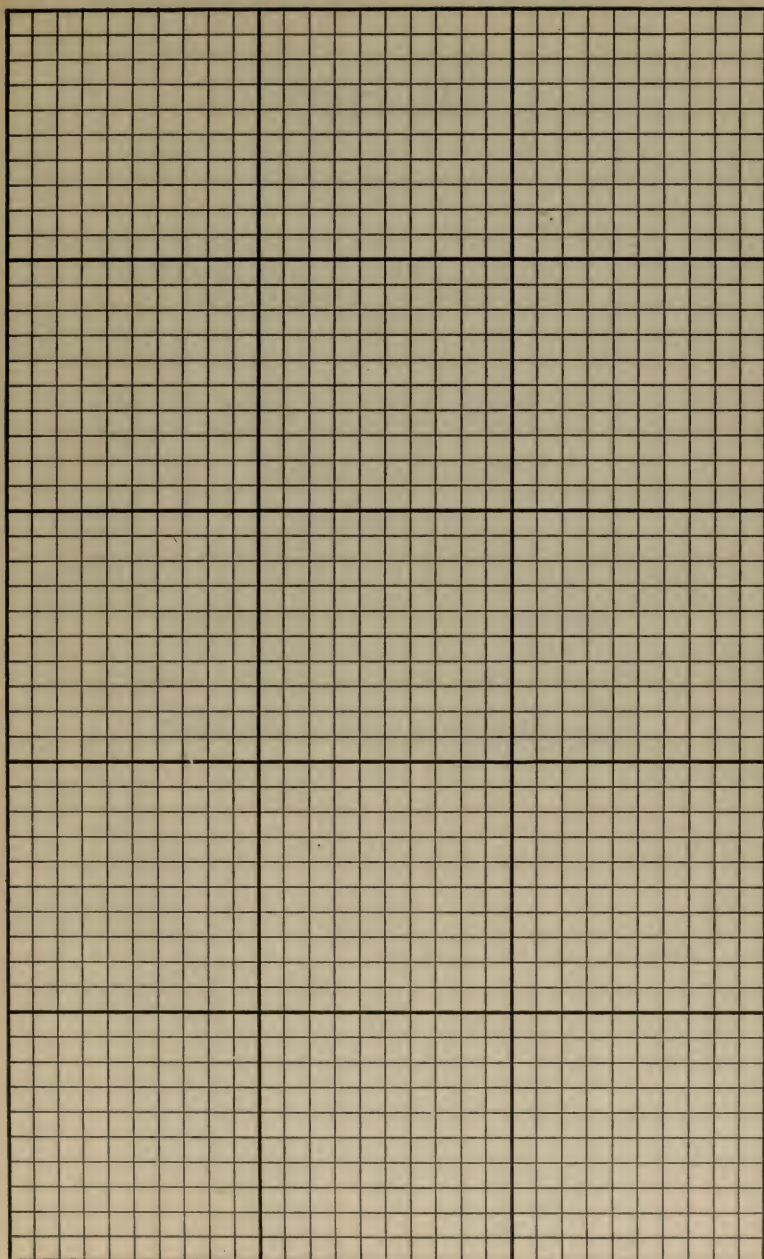
NOTES and DIAGRAMS



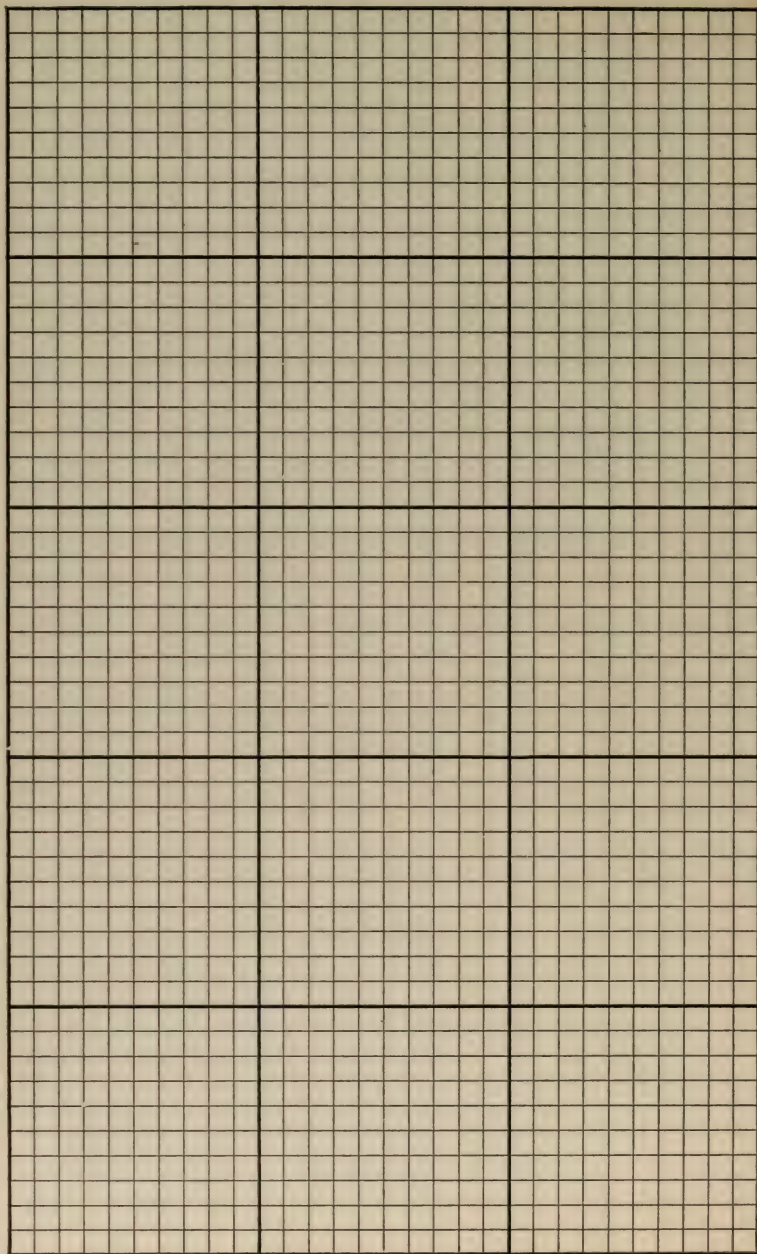
NOTES and DIAGRAMS



NOTES and DIAGRAMS



NOTES and DIAGRAMS



Part III

Building Materials

Strength of Materials

Specific Gravities

**Properties of
American Standard Yard Lumber and Timber**

Safe Loads for Timber Columns

Unit Stresses for Structural Lumber

Contents of Storage Warehouses

STRENGTH OF MATERIALS

STRESS IN KIPS PER SQUARE INCH

Metals and Alloys	Tension, Ultimate	Elastic Limit	Compression, Ultimate	Bending, Ultimate	Shearing, Ultimate	Modulus of Elasticity, Pounds	Elongation, %
Aluminum, cast.....	15	6.5	12	12	11000000
“ bars, sheets.....	24-28	12-14
“ wire, hard.....	30-65	16-30
“ “ annealed.....	20-35	14
“ 2-7% Ni, Cu, Fe, etc.....	40-50	25
Aluminum Bronze, 5% to 7½% Al.....	75	40	120
“ “ 10% Al.....	85-100	60
Brass, 17% Zn.....	32.6	8.2	23.2	26.7
“ 23% “.....	7.6	42	22.3	35.8
“ 30% “.....	28.1	8.6	26.9	20.7
“ 39% “.....	41.1	17.4	75	39	20.7
“ 50% “.....	31	17.9	117	33.5	5.0
“ cast, common.....	18-24	6	30	20	36	9000000
“ wire, hard.....	80
“ “ annealed.....	50	16	14000000
Bronze 8% Sn.....	28.5	19	42	43.7	10000000	5.5
“ 13% “.....	29.4	20	53	34.5	3.3
“ 20% “.....	33	78	56.7	0.04
“ 24% “.....	22	22	114	32	0
“ 30% “.....	5.6	5.6	147	12.1	0
gun metal, 9 Cu, 1 Sn.....	25-55	10	52	10000000
“ Manganese, cast } 10% Sn.....	60	30	125
“ “ rolled } 2% Mn.....	100	80
“ Phosphorus, cast } 9% Sn.....	50	24
“ “ wire } 1% P.....	100
“ Silicon, cast, 3% Si.....	55
“ “ 5% Si.....	75
“ “ wire.....	108
“ Tobin, cast } 38% Zn.....	66
“ “ rolled } 1½% Sn.....	80	40	4500000
“ “ cold rolled } ½% Pb.....	100
Copper, cast.....	25	6	40	22	30	10000000
“ plates, rods, bolts.....	32-35	10	32
“ wire, hard.....	55-65	18000000
“ wire, annealed.....	36	10	15000000
Delta Metal, cast } 55-60% Cu.....	45
“ “ plates } 38-40% Zn.....	68
“ “ bars } 2-4% Fe.....	85
“ “ wire } 1-2% Sn.....	100
German Silver, 25% Zn, 20% Ni.....
Gold, cast.....	20	4	8000000
“ wire.....	30
“ copper, 5 Au, 1 Cu.....	50
Iron, cast, common.....	15-18	6	80	30	18-20	12000000
“ “ gray.....	18-24	25-33
“ “ malleable.....	27-35	15-20	46	30	40
Iron, wrought, shapes.....	48	26	tensile	tensile	% tens.	28000000
“ “ bars.....	50	27	tensile	tensile	% tens.	28000000
“ “ wire, unannealed.....	80	15000000
“ “ annealed.....	60	27	25000000
Lead, cast.....	1.8	1000000
“ pipe, wire.....	2.2-2.5	1000000
“ rolled, sheets.....	3.3	720000
Platinum, wire, unannealed.....	53
“ “ annealed.....	32
Silver, cast.....	40
Steel, boiler plates*, fire box.....	55-65	½ tens.	tensile	tensile	¾ tens.	29000000	27.3-23.0
“ “ flange plates.....	52-62	½ tens.	tensile	tensile	¾ tens.	29000000	28.8-24.2
“ castings*, soft.....	60	27	tensile	tensile	¾ tens.	29000000	22.0
“ “ medium.....	70	31.5	tensile	tensile	¾ tens.	29000000	18.0
“ “ hard.....	80	36	tensile	tensile	¾ tens.	29000000	15.0
“ reinforcing bars*, plain, structural grade.....	55-70	33	tensile	tensile	¾ tens.	29000000	25.4-20.0
“ “ “ intermediate.....	70-85	40	tensile	tensile	¾ tens.	29000000	18.6-15.3
“ “ “ hard.....	80	50	tensile	tensile	¾ tens.	29000000	15.0
“ “ deformed, struct'l grade.....	55-70	33	tensile	tensile	¾ tens.	29000000	22.7-17.9
“ “ “ intermediate.....	70-85	40	tensile	tensile	¾ tens.	29000000	16.1-13.2
“ “ “ hard.....	80	50	tensile	tensile	¾ tens.	29000000	12.5
“ “ cold twisted.....	55	tensile	tensile	¾ tens.	29000000	5.0
“ rivets*, boilers.....	45-55	½ tens.	tensile	tensile	¾ tens.	29000000	33.3-27.3
“ “ bridges.....	46-56	½ tens.	tensile	tensile	¾ tens.	29000000	32.6-26.8
“ “ buildings.....	46-56	½ tens.	tensile	tensile	¾ tens.	29000000	30.4-25.0
“ “ cars.....	48-58	½ tens.	tensile	tensile	¾ tens.	29000000	31.3-25.9
“ “ ships.....	55-65	½ tens.	tensile	tensile	¾ tens.	29000000	27.3-23.0

STRENGTH OF MATERIALS**STRESS IN KIPS PER SQUARE INCH**

Metals and Alloys	Tension, Ultimate	Elastic Limit	Compression, Ultimate	Bending, Ultimate	Shearing, Ultimate	Modulus of Elasticity, Pounds	Elongation, %
Steel Shapes, bridges.....	55-65	1/2 tens.	tensile	tensile	3/4 tens.	290000000	27.3-23.0
" " buildings.....	55-65	1/2 tens.	tensile	tensile	3/4 tens.	290000000	25.4-21.5
" " cars.....	50-65	1/2 tens.	tensile	tensile	3/4 tens.	290000000	30.0-23.0
" " locomotives.....	55-65	1/2 tens.	tensile	tensile	3/4 tens.	290000000	27.3-23.0
" " ships.....	58-68	1/2 tens.	tensile	tensile	3/4 tens.	290000000	25.9-22.1
Steel Alloys, Nickel Steel,* 3.25% N.							
" " " shapes, plates, bars.....	85-100	50	tensile	tensile	3/4 tens.	290000000	17.6-15.0
" " " rivets.....	70-80	45	tensile	tensile	3/4 tens.	290000000	21.4-18.8
" " " eye bars, unannealed.....	95-110	55	tensile	tensile	3/4 tens.	290000000	15.8-13.6
" " " " annealed.....	90-105	52	tensile	tensile	3/4 tens.	290000000	20.0
" " Copper Steel, 0.50% Cu.....	60-68	37-38	tensile	tensile	3/4 tens.	290000000	29.0-23.0
Steel Springs, untempered.....	65-110	40-70
Steel Wire, unannealed.....	120	60
" " annealed.....	80	40
" " bridge cable.....	200	95
Tin, cast.....	3.5-4.6	1.5-1.8	6	4	4000000
" antimony, 10 Sn, 1 Sb.....	11
Zinc, cast.....	4-6	4	18	7	13000000
" rolled sheets.....	7-16

STRESS IN POUNDS PER SQUARE INCH

Building Materials	Ultimate Average Stress			Modulus of Elasticity	Safe Working Stress		
	Compress	Tension	Bending		Compress.	Bearing	Shearing
Brick, Common, good.....	10000	200	600
" " medium burned.....	11000
" " hard burned.....	15000
" Pressed and paving.....	6000
Concrete. **
Masonry, Granite.....	420	600
" Limestone, bluestone.....	350	500
" Sandstone.....	280	400
" Rubble.....	140	250
" " coursed.....	168	250
" Brick, common.....	168	300
" " hard burned.....	210	300
Stone, Bluestone.....	12000	1200	2500	7000000	1200	1200	200
" Granite, gneiss.....	12000	1200	1600	7000000	1200	1200	200
" Limestone, marble.....	8000	800	1500	7000000	800	800	150
" Sandstone.....	5000	150	1200	3000000	500	500	150
" Slate.....	10000	3000	5000	14000000	1000	1000	175
Miscellaneous, Glass, common.....	30000	3000	3000	8000000
" " flooring.....	10000	3000	3000
" Plaster.....	700	70
" Terra cotta.....	5000
" Ropes, cast steel hoisting.....	80000
" " standing, derrick.....	70000
" " manila.....	8000
" Belts, solid woven, cotton.....	7300
" " " " flax.....	9900

*See Specifications of the American Society for Testing Materials.

**Extensive laboratory tests recently conducted, indicate that the water cement ratio in concrete mixtures has a very important influence on the ultimate strength of the finished product. Data on this subject can be obtained from the Portland Cement Association, Chicago.

SPECIFIC GRAVITIES AND WEIGHTS

Substance	Specific Gravity	Weight, Pounds per Cu. Ft.	Substance	Specific Gravity	Weight, Pounds per Cu. Ft.
Metals, Alloys, Ores			Timber, U. S. Seasoned		
Aluminum, cast-hammered.....	2.55-2.75	165	Ash, white-red.....	0.62-0.65	40
Aluminum, bronze.....	7.7	481	Cedar, white-red.....	0.32-0.38	22
Brass, cast-rolled.....	8.4-8.7	534	Chestnut.....	0.66	41
Bronze, 7.9 to 14% Sn.....	7.4-8.9	509	Cypress.....	0.48	30
Copper, cast-rolled.....	8.8-9.0	556	Fir, Douglas spruce.....	0.51	32
Copper ore, pyrites.....	4.1-4.3	262	Fir, eastern.....	0.40	25
Gold, cast-hammered.....	19.25-19.3	1205	Elm, white.....	0.72	45
Iron, cast, pig.....	7.2	450	Hemlock.....	0.42-0.52	29
Iron, wrought.....	7.6-7.9	485	Hickory.....	0.74-0.84	49
Iron, steel.....	7.8-7.9	490	Locust.....	0.73	46
Iron, spiegel-eisen.....	7.5	468	Maple, hard.....	0.68	43
Iron, ferro-silicon.....	6.7-7.3	437	Maple, white.....	0.53	33
Iron ore, hematite.....	5.2	325	Oak, chestnut.....	0.86	54
Iron ore, hematite in bank.....		160-180	Oak, live.....	0.95	59
Iron ore, hematite loose.....		130-160	Oak, red, black.....	0.65	41
Iron ore, limonite.....	3.6-4.0	237	Oak, white.....	0.74	46
Iron ore, magnetite.....	4.9-5.2	315	Pine, Oregon.....	0.51	32
Iron slag.....	2.5-3.0	172	Pine, red.....	0.48	30
Lead.....	11.37	710	Pine, white.....	0.41	26
Lead ore, galena.....	7.3-7.6	465	Pine, yellow, long-leaf.....	0.70	44
Manganese.....	7.2-8.0	475	Pine, yellow, short-leaf.....	0.61	38
Manganese ore, pyrolusite.....	3.7-4.6	259	Poplar.....	0.48	30
Mercury.....	13.6	849	Redwood, California.....	0.42	26
Nickel.....	8.9-9.2	565	Spruce, white, black.....	0.40-0.46	27
Nickel, monel metal.....	8.8-9.0	556	Walnut, black.....	0.61	38
Platinum, cast-hammered.....	21.1-21.5	1330	Walnut, white.....	0.41	26
Silver, cast-hammered.....	10.4-10.6	656	Moisture Contents:		
Tin, cast-hammered.....	7.2-7.5	459	Seasoned timber 15 to 20%..		
Tin ore, cassiterite.....	6.4-7.0	418	Green timber up to 50%....		
Zinc, cast-rolled.....	6.9-7.2	440	Various Liquids		
Zinc ore, blende.....	3.9-4.2	253	Alcohol, 100%.....	0.79	49
Various Solids			Acids, muriatic 40%.....	1.20	75
Cereals, oats, bulk.....		32	Acids, nitric 91%.....	1.50	94
Cereals, barley, bulk.....		39	Acids, sulphuric 87%.....	1.80	112
Cereals, corn, rye, bulk.....		48	Lye, soda 66%.....	1.70	106
Cereals, wheat, bulk.....		48	Oils, vegetable.....	0.91-0.94	58
Hay and Straw, bales.....		20	Oils, mineral, lubricants.....	0.90-0.93	57
Cotton, Flax, Hemp.....	1.47-1.50	93	Water, 4°C, max. density.....	1.0	62.428
Fats.....	0.90-0.97	58	Water, 100°C.....	0.9584	59.830
Flour, loose.....	0.40-0.50	28	Water, ice.....	0.88-0.92	56
Flour, pressed.....	0.70-0.80	47	Water, snow, fresh fallen.....	.125	8
Glass, common.....	2.40-2.60	156	Water, sea water.....	1.02-1.03	64
Glass, plate or crown.....	2.45-2.72	161	Gases, Air = 1		
Glass, crystal.....	2.90-3.00	184	Air, 0°C, 760 mm.....	1.0	.08071
Leather.....	0.86-1.02	59	Ammonia.....	0.5920	.0478
Paper.....	0.70-1.15	58	Carbon dioxide.....	1.5291	.1234
Potatoes, piled.....		42	Carbon monoxide.....	0.9673	.0781
Rubber, caoutchouc.....	0.92-0.96	59	Gas, illuminating.....	0.35-0.45	.028-.036
Rubber goods.....	1.0-2.0	94	Gas, natural.....	0.47-0.48	.038-.039
Salt, granulated, piled.....		48	Hydrogen.....	0.0693	.00559
Saltpeter.....		67	Nitrogen.....	0.9714	.0784
Starch.....	1.53	96	Oxygen.....	1.1056	.0892
Sulphur.....	1.93-2.07	125			
Wool.....	1.32	82			

The specific gravities of solids and liquids refer to water at 4°C., those of gases to air at 0°C. and 760 mm pressure. The weights per cubic foot are derived from average specific gravities, except where stated that weights are for bulk, heaped or loose material, etc.

SPECIFIC GRAVITIES AND WEIGHTS

Substance	Specific Gravity	Weight, Pounds per Cu. Ft.	Substance	Specific Gravity	Weight, Pounds per Cu. Ft.
Ashlar Masonry			Minerals		
Granite, syenite, gneiss.....	2.3-3.0	165	Asbestos.....	2.1-2.8	153
Limestone, marble.....	2.3-2.8	160	Barytes.....	4.50	281
Sandstone, bluestone.....	2.1-2.4	140	Basalt.....	2.7-3.2	184
Mortar Rubble Masonry			Bauxite.....	2.55	159
Granite, syenite, gneiss.....	2.2-2.8	155	Borax.....	1.7-1.8	109
Limestone, marble.....	2.2-2.6	150	Chalk.....	1.8-2.6	137
Sandstone, bluestone.....	2.0-2.2	130	Clay, marl.....	1.8-2.6	137
Dry Rubble Masonry			Dolomite.....	2.9	181
Granite, syenite, gneiss.....	1.9-2.3	130	Feldspar, orthoclase.....	2.5-2.6	159
Limestone, marble.....	1.9-2.1	125	Gneiss, serpentine.....	2.4-2.7	159
Sandstone, bluestone.....	1.8-1.9	110	Granite, syenite.....	2.5-3.1	175
Brick Masonry			Greenstone, trap.....	2.8-3.2	187
Pressed brick.....	2.2-2.3	140	Gypsum, alabaster.....	2.3-2.8	159
Common brick.....	1.8-2.0	120	Hornblende.....	3.0	187
Soft brick.....	1.5-1.7	100	Limestone, marble.....	2.5-2.8	165
Concrete Masonry			Magnesite.....	3.0	187
Cement, stone, sand.....	2.2-2.4	144	Phosphate rock, apatite.....	3.2	200
Cement, slag, etc.....	1.9-2.3	130	Porphyry.....	2.6-2.9	172
Cement cinder, etc.....	1.5-1.7	100	Pumice, natural.....	0.37-0.90	40
Various Building Mat'l			Quartz, flint.....	2.5-2.8	165
Ashes, cinders.....	40-45		Sandstone, bluestone.....	2.2-2.5	147
Cement, portland, loose.....	90		Shale, slate.....	2.7-2.9	175
Cement, portland, set.....	2.7-3.2	183	Soapstone, talc.....	2.6-2.8	169
Lime, gypsum, loose.....	53-64		Stone, Quarried, Piled		
Mortar, set.....	1.4-1.9	103	Basalt, granite, gneiss.....	96
Slags, bank slag.....	67-72		Limestone, marble, quartz.....	95
Slags, bank screenings.....	98-117		Sandstone.....	82
Slags, machine slag.....	96		Shale.....	92
Slags, slag sand.....	49-55		Greenstone, hornblende.....	107
Earth, etc., Excavated			Bituminous Substances		
Clay, dry.....	63		Asphaltum.....	1.1-1.5	81
Clay, damp, plastic.....	110		Coal, anthracite.....	1.4-1.7	97
Clay and gravel, dry.....	100		Coal, bituminous.....	1.2-1.5	84
Earth, dry, loose.....	76		Coal, lignite.....	1.1-1.4	78
Earth, dry, packed.....	95		Coal, peat, turf, dry.....	0.65-0.85	47
Earth, moist, loose.....	78		Coal, charcoal, pine.....	0.28-0.44	23
Earth, moist, packed.....	96		Coal, charcoal, oak.....	0.47-0.57	33
Earth, mud, flowing.....	108		Coal, coke.....	1.0-1.4	75
Earth, mud, packed.....	115		Graphite.....	1.9-2.3	131
Riprap, limestone.....	80-85		Paraffine.....	0.87-0.91	56
Riprap, sandstone.....	90		Petroleum.....	0.87	54
Riprap, shale.....	105		Petroleum, refined.....	0.79-0.82	50
Sand, gravel, dry, loose.....	90-105		Petroleum, benzine.....	0.73-0.75	46
Sand, gravel, dry, packed.....	100-120		Petroleum, gasoline.....	0.66-0.69	42
Sand, gravel, dry, wet.....	118-120		Pitch.....	1.07-1.15	69
Excavations in Water			Tar, bituminous.....	1.20	75
Sand or gravel.....	60		Coal and Coke, Piled		
Sand or gravel and clay.....	65		Coal, anthracite.....	47-58
Clay.....	80		Coal, bituminous, lignite.....	40-54
River mud.....	90		Coal, peat, turf.....	20-26
Soil.....	70		Coal, charcoal.....	10-14
Stone riprap.....	65		Coal, coke.....	23-32

The specific gravities of solids and liquids refer to water at 4°C., those of gases to air at 0°C. and 760 mm pressure. The weights per cubic foot are derived from average specific gravities, except where stated that weights are for bulk, heaped or loose material, etc.

PROPERTIES OF AMERICAN STANDARD YARD LUMBER AND TIMBER SIZES

NATIONAL LUMBER MANUFACTURERS ASSOCIATION

Nominal Size	American Standard Dressed Size	Area of Section A = bd	Weight per Lineal foot	Moment of Inertia $I = \frac{bd^3}{12}$	Section Modulus $S = \frac{bd^2}{6}$	Nominal Size	American Standard Dressed Size	Area of Section A = bd	Weight per Lineal foot	Moment of Inertia $I = \frac{bd^3}{12}$	Section Modulus $S = \frac{bd^2}{6}$
Inches	Inches	Sq. In.	Pounds			Inches	Inches	Sq. In.	Pounds		
2×4	1½×3½	5.89	1.6	6.45	3.56	10×20	9½×19½	185.25	51.4	5870.05	602.06
2×6	1½×5½	9.14	2.5	24.10	8.57	10×22	9½×21½	204.25	56.7	7867.81	731.89
2×8	1½×7½	12.19	3.4	57.13	15.32	10×24	9½×23½	223.25	62.0	10274.06	874.39
2×10	1½×9½	15.44	4.3	116.09	24.44	10×26	9½×25½	242.25	67.3	13126.81	1029.56
2×12	1½×11½	18.69	5.2	205.94	35.82	10×28	9½×27½	261.25	72.5	16465.24	1197.39
2×14	1½×13½	23.62	6.5	333.15	49.36	10×30	9½×29½	280.25	77.8	20323.79	1377.89
2×16	1½×15½	25.18	7.0	504.24	65.07						
2×18	1½×17½	28.43	7.9	725.71	82.94						
2×20	1½×19½	31.69	8.8	1004.05	102.98						
						12×12	11½×11½	132.25	36.7	1457.50	253.47
						12×14	11½×13½	155.25	43.1	2357.85	349.31
						12×16	11½×15½	178.25	49.5	3568.70	460.48
						12×18	11½×17½	201.25	55.9	5136.49	586.98
						12×20	11½×19½	224.25	62.3	7105.90	728.81
3×4	2½×3½	9.51	2.6	10.42	5.75	12×22	11½×21½	247.25	68.7	9524.24	885.98
3×6	2½×5½	14.76	4.2	38.93	13.84	12×24	11½×23½	270.25	75.0	12437.08	1058.47
3×8	2½×7½	19.68	5.7	92.28	24.60	12×26	11½×25½	293.25	81.4	15890.42	1246.31
3×10	2½×9½	24.93	7.2	187.55	39.48	12×28	11½×27½	316.25	87.8	19932.58	1449.47
3×12	2½×11½	30.18	8.8	332.69	57.86	12×30	11½×29½	339.25	94.2	24602.61	1667.97
3×14	2½×13½	35.43	10.3	538.21	79.73						
3×16	2½×15½	40.68	11.3	814.60	105.11						
3×18	2½×17½	45.94	12.8	1172.36	133.98						
3×20	2½×19½	51.19	14.2	1622.00	166.36						
						14×14	13½×13½	182.25	50.6	2767.92	410.06
						14×16	13½×15½	209.25	58.1	4189.36	540.56
						14×18	13½×17½	236.25	65.6	6029.29	689.06
						14×20	13½×19½	263.25	73.1	8341.73	855.56
						14×22	13½×21½	290.25	80.6	11180.67	1040.06
4×4	3½×3½	13.14	3.6	14.38	7.94	14×24	13½×23½	317.25	88.1	14600.10	1242.56
4×6	3½×5½	20.39	5.7	53.76	19.11	14×26	13½×25½	344.25	95.6	18654.04	1463.06
4×8	3½×7½	27.18	7.5	127.44	33.98	14×28	13½×27½	371.25	103.1	23398.73	1701.56
4×10	3½×9½	34.43	9.6	258.99	54.52	14×30	13½×29½	398.25	110.6	28881.42	1958.06
4×12	3½×11½	41.68	11.6	459.42	79.90						
4×14	3½×13½	48.93	13.6	743.23	110.11						
4×16	3½×15½	56.18	15.6	1124.90	145.15						
4×18	3½×17½	63.43	17.6	1618.96	185.02						
4×20	3½×19½	70.69	19.6	2239.88	229.73						
						16×16	15½×15½	240.25	66.7	4809.98	620.64
						16×18	15½×17½	271.25	75.3	6922.49	791.14
						16×20	15½×19½	302.25	83.9	9577.50	982.31
						16×22	15½×21½	333.25	92.5	12837.00	1194.14
6×6	5½×5½	30.25	8.4	76.25	27.73	16×24	15½×23½	364.25	101.2	16763.00	1426.64
6×8	5½×7½	41.25	11.4	193.35	51.56	16×26	15½×25½	395.25	109.8	21417.50	1759.81
6×10	5½×9½	52.25	14.5	329.96	82.73	16×28	15½×27½	426.25	118.4	26863.78	1963.64
6×12	5½×11½	63.25	17.5	497.06	121.23	16×30	15½×29½	457.25	127.0	33159.98	2248.14
6×14	5½×13½	74.25	20.6	1127.66	167.06						
6×16	5½×15½	85.25	23.6	1706.76	220.22						
6×18	5½×17½	96.25	26.7	2456.36	280.73						
6×20	5½×19½	107.25	29.8	3398.46	348.56	18×18	17½×17½	306.25	85.0	7815.73	893.23
6×22	5½×21½	118.25	32.8	4555.05	423.73	18×20	17½×19½	341.25	94.8	10813.33	1109.06
						18×22	17½×21½	376.25	104.5	14493.43	1348.23
						18×24	17½×23½	411.25	114.2	18926.02	1610.72
8×8	7½×7½	56.25	15.6	263.67	70.31	18×26	17½×25½	446.25	123.9	24181.11	1896.56
8×10	7½×9½	71.25	19.8	535.85	112.81	18×28	17½×27½	481.25	133.7	30331.62	2205.72
8×12	7½×11½	86.25	23.9	950.55	165.31	18×30	17½×29½	516.25	143.4	37438.79	2538.22
8×14	7½×13½	101.25	28.0	1537.73	227.81						
8×16	7½×15½	116.25	32.0	2327.42	300.31						
8×18	7½×17½	131.25	36.4	3349.60	382.81	20×20	19½×19½	380.25	105.6	12049.49	1235.81
8×20	7½×19½	146.25	40.6	4634.30	475.31	20×22	19½×21½	419.25	116.4	16149.86	1502.31
8×22	7½×21½	161.25	44.8	6211.48	577.81	20×24	19½×23½	458.25	127.3	21089.04	1794.81
8×24	7½×23½	176.25	48.9	8111.17	690.31	20×26	19½×25½	497.25	138.1	26944.73	2113.31
						20×28	19½×27½	536.25	148.9	33798.17	2457.81
						20×30	19½×29½	575.25	159.8	41717.61	2828.31
10×10	9½×9½	90.25	25.0	678.75	142.89						
10×12	9½×11½	109.25	30.3	1204.01	209.39	24×24	23½×23½	552.25	153.4	25414.96	2162.97
10×14	9½×13½	128.25	35.6	1947.78	288.56	24×26	23½×25½	599.25	166.4	32471.80	2546.81
10×16	9½×15½	147.25	40.9	2948.04	380.39	24×28	23½×27½	646.25	179.5	40731.06	2916.97
10×18	9½×17½	166.25	46.1	4242.80	484.89	24×30	23½×29½	693.25	192.5	50274.98	3408.47

The weights given above are based on assumed average weight of 40 lbs. per cubic foot.

SAFE LOAD IN POUNDS PER SQUARE INCH OF CROSS-SECTIONAL AREA

SQUARE AND RECTANGULAR TIMBER COLUMNS

DRY LOCATIONS

Species of Lumber	American Standard Grade	*Ratio of Length to Least Dimension (l/d)											
		10& less	l/d 12	l/d 14	l/d 16	l/d 18	l/d 20	l/d 25	l/d 30	l/d 35	l/d 40	l/d 50	l/d 50
		lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
Ash, Commercial White	Select	1100	1076	1055	1023	978	913	658					
	Common	880	868	857	840	818	784	647	457	336	257	164	
Cedar, Western Red; Fir, Balsam	Select	700	686	674	656	629	592	438					
	Common	560	553	547	538	524	505	425	304	224	171	110	
Cedar, Northern and Southern White	Select	550	540	530	516	496	468	351					
	Common	440	435	430	423	412	398	338	244	179	137	88	
Chestnut; Pine, Northern White, Idaho White, Sugar, Calif. White, and Pondosa	Select	750	733	718	695	663	617	438					
	Common	600	591	583	572	556	532	434	304	224	171	110	
Cypress, Southern; Larch, Western	Select	1100	1063	1030	981	909	810						
	Common	880	861	843	818	781	729	526	365	268	206	132	
Douglas Fir (Coast Region); Pine, Southern Yellow; Beech; Birch, Yellow and Sweet; Maple, Sugar	**Dense } Select	1285	1251	1222	1176	1112	1022	702					
	Select	1175	1149	1127	1093	1045	975	702	487	358	274	175	
	Common	880	870	861	847	826	796	675					
Douglas Fir (Rky. Mtn. Region); Spruce, Red, White, Sitka; Norway Pine; Alaska Cedar; Elm, Slippery and White; Sycamore; Gum, Red and Black; Tupelo	Select	800	786	774	753	726	688	526					
	Common	640	632	627	617	602	582	500	365	268	206	132	
Hemlock, West Coast	Select	900	885	872	852	823	783	614					
	Common	720	712	706	696	680	660	573	426	313	240	153	
Hemlock, Eastern; Fir, Commercial White	Select	700	689	678	664	641	611	482					
	Common	560	554	549	542	530	515	449	335	246	188	121	
Oak, White and Red	Select	1000	982	967	943	908	860	658					
	Common	800	790	783	771	753	728	625	457	336	257	164	
Redwood	Select	1000	972	947	910	856	781						
	Common	800	786	773	754	726	688	526	365	268	206	132	
Spruce, Englemann	Select	600	586	574	556	530	494	351					
	Common	480	473	466	457	444	426	347	244	179	137	88	
Tamarack	Select	1000	976	955	923	877	817	570					
	Common	800	788	777	761	737	706	566	396	291	223	142	

SAFE LOADS in compression parallel to grain for timber columns shall not exceed in pounds per square inch the values given in the above table for the respective species, grade, and ratio of unsupported length to least dimension, (l/d).

No column shall be used in which the unsupported length is more than 50 times the least diameter. l and d must be figured in the same unit of measurement.

ALLOWABLE UNIT STRESSES FOR STRUCTURAL LUMBER AND TIMBER**ALL SIZES, DRY LOCATIONS**

Species of Timber	American Standard Grade	Allowable Unit Stress in Pounds per Square Inch				
		Bending Stress		Compression Stress		Modulus of Elasticity (All Locations)
		In Extreme Fibre	Horizontal Shear All Locations	Parallel to Grain	Perpendicular to Grain	
Cedar, Western Red	Select Common	900 720	80 64	700 560	200	1000000
Cedar, Northern and Southern White	Select Common	750 600	70 56	550 440	175	800000
Cedar, Port Orford	Select Common	1100 880	90 72	900 720	250	1200000
Cedar, Alaska	Select Common	1100 880	90 72	800 640	250	1200000
Cypress, Southern	Select Common	1300 1040	100 80	1100 880	350	1200000
Douglas Fir, Coast Region (Western Washington and Oregon)	Dense Select Select Common	1750 1600 1200	105 90 72	1285 1175 880	380 345 325	1600000
Douglas Fir, Rocky Mountain Region	Select Common	1100 880	85 68	800 640	275	1200000
Fir, Balsam	Select Common	900 720	70 56	700 560	150	1000000
Fir, Golden, Noble, Silver, White (Commercial White)	Select Common	1100 880	70 56	700 560	300	1100000
Hemlock, West Coast	Select Common	1300 1040	75 60	900 720	300	1400000
Hemlock, Eastern	Select Common	1100 880	70 56	700 560	300	1100000
Larch, Western	Select Common	1200 960	100 80	1100 880	325	1300000
Oak, Commercial White and Red	Select Common	1400 1120	125 100	1000 800	500	1500000
Pine, Southern Yellow	Dense Select Select Common	1750 1600 1200	128 110 88	1285 1175 880	380 345 325	1600000
Pine, Calif., Idaho and No. White, Lodgepole, Ponderosa, Sugar, Westn. Yellow	Select Common	900 720	85 68	750 600	250	1000000
Pine, Norway	Select Common	1100 880	85 68	800 640	300	1200000
Redwood	Select Common	1200 960	70 56	1000 800	250	1200000
Spruce, Red, White, Sitka	Select Common	1100 880	85 68	800 640	250	1200000
Spruce, Englemann	Select Common	750 600	70 56	600 480	175	800000
Tamarack, Eastern	Select Common	1200 960	95 76	1000 800	300	1300000

The allowable working stresses given above are taken from recommendations of the Forest Products Laboratory of the Department of Agriculture at Madison, Wisconsin, for use in dry locations. The grades for which stresses are given are for dimension lumber and timber equivalent in quality to the American Standards for Structural Material as published by the Bureau of Standards, U. S. Department of Commerce, in Simplified Practice Recommendation No. 16. These grades and stresses have been adopted by the American Railway Engineering Association, accepted by the American Society for Testing Materials, and are recommended by the Building Code Committee of the Department of Commerce. All computations to determine the required size of lumber members should be based on the net cross sectional area or actual size.

ALLOWABLE UNIT STRESSES FOR STRUCTURAL LUMBER AND TIMBER

USED IN LOCATIONS USUALLY WET

Species	Grade	Allowable Unit Stress in Pounds per Square Inch					
		Bending Stress			Compression Stress		Modulus of Elasticity
		In Extreme Fibre		Horizontal Shear	Parallel to Grain	Perpendicular to Grain	
		Joist and Plank Sizes 4" and less in thickness	Beam and Stringer Sizes 5" & thicker				
Cedar, Western Red	Select Common	670 570	750 600	80 64	650 520	125	1000000
Cedar, Northern & Southern White	Select Common	530 450	70 56	100	800000
Cedar, Port Orford	Select Common	800 680	900 720	90 72	750 600	150	1200000
Cedar, Alaska	Select Common	800 680	90 72	150	1200000
Cypress, Southern	Select Common	800 680	100 80	225	1200000
Douglas Fir, Coast Region (Western Washington and Oregon)	Dense Select Select Common	1050 950 750	1165 1065 800	105 90 72	990 905 680	235 215 200	1600000
Douglas Fir, Rocky Mountain Region	Select Common	620 530	700 560	85 68	700 560	200	1200000
Fir, Balsam	Select Common	530 450	70 56	100	1000000
Fir, Golden, Noble, Silver, White (Commercial White)	Select Common	710 600	70 56	200	1100000
Hemlock, West Coast	Select Common	800 680	900 720	75 60	800 640	200	1400000
Hemlock, Eastern	Select Common	710 600	70 56	200	1100000
Larch, Western	Select Common	800 680	900 720	100 80	800 640	200	1300000
Pine, Southern	Dense Select Select Common	1050 950 750	1165 1065 800	128 110 88	990 905 680	235 215 200	1600000
Pine, Calif., Idaho and No. White, Lodgepole, Ponderosa and Sugar	Select Common	670 570	85 68	125	1000000
Pine, Norway	Select Common	710 600	85 68	150	1200000
Redwood	Select Common	710 600	800 640	70 56	750 600	125	1200000
Spruce, Red, White, Sitka	Select Common	710 600	800 640	85 68	650 520	125	1200000
Spruce, Englemann	Select Common	440 370	70 56	100	800000
Tamarack, Eastern	Select Common	800 680	95 76	200	1300000

The strength of wood is influenced largely by its moisture content, and therefore by the moisture conditions of service, which have an important bearing also on decay and checking. The allowable working stresses given above are taken from recommendations of the Forest Products Laboratory of the Department of Agriculture at Madison, Wisconsin, for use in locations where the lumber will be usually wet.

The grades for which stresses are given are for dimension lumber and timber equivalent in quality to the American Standards for Structural Material as published by the Bureau of Standards, U. S. Department of Commerce, in Simplified Practice Recommendation No. 16. These grades and stresses have been adopted by the American Railway Engineering Association, accepted by the American Society for Testing Materials, and are recommended by the Building Code Committee of the Department of Commerce.

All computations to determine the required size of lumber members should be based on the net cross sectional area or actual size.

CONTENTS OF STORAGE WAREHOUSES

Material	Weights per Cubic Foot of Space, Pounds	Height of Pile Feet	Weights per Square Foot of Floor Pounds	Recommended Live Loads, Pounds per Square Foot
Building Materials				
Asbestos.....	50	6	300	
Bricks, Building.....	45	6	270	
Bricks, Fire Clay.....	75	6	450	
Cement, Natural.....	59	6	354	300
Cement, Portland.....	73	6	438	to
Gypsum.....	50	6	300	400
Lime and Plaster.....	53	5	265	
Tiles.....	50	6	300	
Woods, bulk.....	45	6	270	
Drugs, Paints, Oil, Etc.				
Alum, Pearl, in barrels.....	33	6	198	
Bleaching Powder, in hogsheads.....	31	3½	102	
Blue Vitriol, in barrels.....	45	5	226	
Glycerine, in cases.....	52	6	312	
Linseed Oil, in barrels.....	36	6	216	
Linseed Oil, in iron drums.....	45	4	180	
Logwood Extract, in boxes.....	70	5	350	
Rosin, in barrels.....	48	6	288	200
Shellac, Gum.....	38	6	228	to
Soaps.....	50	6	300	300
Soda Ash, in hogsheads.....	62	2¾	167	
Soda, Caustic, in iron drums.....	88	3¾	294	
Soda, Silicate, in barrels.....	53	6	318	
Sulphuric Acid.....	60	1½	100	
Toilet Articles.....	35	6	210	
Varnishes.....	55	6	330	
White Lead Paste, in cans.....	174	3½	610	
White, Lead, dry.....	86	4¾	408	
Red Lead and Litharge, dry.....	132	3¾	495	
Dry Goods, Cotton, Wool, Etc.				
Burlap, in bales.....	43	6	258	
Carpets and Rugs.....	30	6	180	
Coir Yarn, in bales.....	33	8	264	
Cotton, in bales, American.....	30	8	240	
Cotton, in bales, Foreign.....	40	8	320	
Cotton Bleached Goods, in cases.....	28	8	224	
Cotton Flannel, in cases.....	12	8	96	
Cotton Sheeting, in cases.....	23	8	184	
Cotton Yarn, in cases.....	25	8	200	200
Excelsior, compressed.....	19	8	152	to
Hemp, Italian, compressed.....	22	8	176	250
Hemp, Manila, compressed.....	30	8	240	
Jute, compressed.....	41	8	328	
Linen Damask, in cases.....	50	5	250	
Linen Goods, in cases.....	30	8	240	
Linen Towels, in cases.....	40	6	240	
Silk and Silk Goods.....	45	8	360	
Sisal, compressed.....	21	8	168	
Tow, compressed.....	29	8	232	
Wool, in bales, compressed.....	48			
Wool, in bales, not compressed.....	13	8	104	
Wool, Worsted, in cases.....	27	8	216	

CONTENTS OF STORAGE WAREHOUSES

Material	Weights per Cubic Foot of Space, Pounds	Height of Pile Feet	Weights per Square Foot of Floor Pounds	Recommended Live Loads, Pounds per Square Foot
Groceries, Wines, Liquors, Etc.				
Beans, in bags.....	40	8	320	
Beverages.....	40	8	320	
Canned Goods, in cases.....	58	6	348	
Cereals.....	45	8	360	
Cocoa.....	35	8	280	
Coffee, Roasted, in bags.....	33	8	264	
Coffee, Green, in bags.....	39	8	312	
Dates, in cases.....	55	6	330	
Figs, in cases.....	74	5	370	
Flour, in barrels.....	40	5	200	
Fruits, Fresh.....	35	8	280	250
Meat and Meat Products.....	45	6	270	to
Milk, Condensed.....	50	6	300	300
Molasses, in barrels.....	48	5	240	
Rice, in bags.....	58	6	348	
Sal Soda, in barrels.....	46	5	230	
Salt, in bags.....	70	5	350	
Soap Powder, in cases.....	38	8	304	
Starch, in barrels.....	25	6	150	
Sugar, in barrels.....	43	5	215	
Sugar, in cases.....	51	6	306	
Tea, in chests.....	25	8	200	
Wines and Liquors, in barrels.....	38	6	228	
Hardware, Etc.				
Automobile Parts.....	40	8	320	
Chain.....	100	6	600	
Cutlery.....	45	8	360	
Door Checks.....	45	6	270	
Electrical Goods and Machinery.....	40	8	320	
Hinges.....	64	6	384	
Locks, in cases, packed.....	31	6	186	
Machinery, Light.....	20	8	160	300
Plumbing, Fixtures.....	30	8	240	to
Plumbing, Supplies.....	55	6	330	400
Sash Fasteners.....	48	6	288	
Screws.....	101	6	606	
Shafting Steel.....	125			
Sheet Tin, in boxes.....	278	2	556	
Tools, Small, Metal.....	75	6	450	
Wire Cables, on reels.....			425	
Wire, Insulated Copper, in coils.....	63	5	315	
Wire, Galvanized Iron, in coils.....	74	4½	333	
Wire, Magnet, on spools.....	75	6	450	
Miscellaneous				
Automobile Tires.....	30	6	180	
Automobiles, uncrated.....	8		64	
Books (solidly packed).....	65	6	390	
Furniture.....	20			
Glass and Chinaware, in crates.....	40	8	320	
Hides and Leather, in bales.....	20	8	160	
Hides, Buffalo, in bundles.....	37	8	296	
Leather and Leather Goods.....	40	8	320	
Paper, Newspaper, and Strawboards.....	35	6	210	
Paper, Writing and Calendars.....	60	6	360	
Rope, in coils.....	32	6	192	
Rubber, Crude.....	50	8	400	
Tobacco, bales.....	35	8	280	

CORRUGATED SHEETS

DIMENSIONS

Corrugations				Sheets		Length of Sheet in Inches	Area in Sq. Feet of One Sheet			Number of Sheets in 100 Sq. Feet		
Width in Inches		Depth in Inches	Number per Sheet	Full Sheet Width	Covering Width		Corrugations			Corrugations		
Nominal	Actual						5"	2', 2 1/2' 3"	5/8" 1 1/4"	5"	2', 2 1/2' 3"	5/8" 1 1/4"
5	5	7/8	6	28	25	60	11.67	10.83	10.42	8.57	9.23	9.60
3	3	9/16	9	26	24	72	14.00	13.00	12.50	7.14	7.69	8.00
*2 1/2	2 3/4	1 1/2	10 1/2	27 1/2	24	84	16.33	15.17	14.58	6.12	6.59	6.86
2 1/2	2 3/4	1 1/2	10	26	24	96	18.67	17.33	16.67	5.36	5.77	6.00
2	2	7/16	13	26	24	108	21.00	19.50	18.75	4.76	5.13	5.33
1 1/4	1 1/4	3/8	20	25	23 3/4	120	23.33	21.67	20.83	4.29	4.62	4.80
5/8	5/8	3/16	40	25	24 3/8	144	28.00	26.00	25.00	3.57	3.85	4.00

*Sizes given are for 27 1/2" width.

5, 6, 7, 8, 9 and 10 feet are Standard lengths. Maximum length is 12 ft. except for 5/8".

WEIGHTS

Pounds per 100 Square Feet

Painted Sheets

Corrugations	Thickness, United States Standard Gage															
	10	12	14	16	18	20	21	22	23	24	25	26	27	28	29	
5	...	470	336	269	215	162	148	135	122	108	95	81	75	68	..	
3	...	472	338	270	216	163	149	136	122	109	95	82	75	68	..	
*2 1/2	615	478	342	274	219	165	151	137	124	110	97	83	76	69	..	
2 1/2	607	472	338	270	216	163	149	136	122	109	95	82	75	68	..	
2	270	216	163	149	136	122	109	95	82	75	68	..	
1 1/4	169	155	141	127	113	99	85	78	71	..	
5/8	113	99	85	78	71	..	

Galvanized Sheets

Corrugations	Thickness, United States Standard Gage															
	10	12	14	16	18	20	21	22	23	24	25	26	27	28	29	
5	...	486	352	285	231	178	164	151	137	124	111	97	90	84	77	
3	...	488	353	286	232	178	165	151	138	125	111	98	91	84	77	
*2 1/2	631	494	358	290	235	181	167	153	140	126	113	99	92	85	78	
2 1/2	623	488	353	286	232	178	165	151	138	125	111	98	91	84	77	
2	286	232	178	165	151	138	125	111	98	91	84	77	
1 1/4	186	172	158	144	130	116	102	95	88	81	
5/8	130	116	102	95	88	81	

The weights given in the above tables are for actual dimensions and do not include allowances for end or side laps.

NUMBER OF SQUARE FEET REQUIRED

2 1/2" Standard Sheets to cover Area of 100 Square Feet

Side Lap	End Lap in Inches					
	1	2	3	4	5	6
Number of Corrugations	109	111	112	113	114	116
1 1/2	116	117	118	120	121	122
2	123	124	126	127	129	130

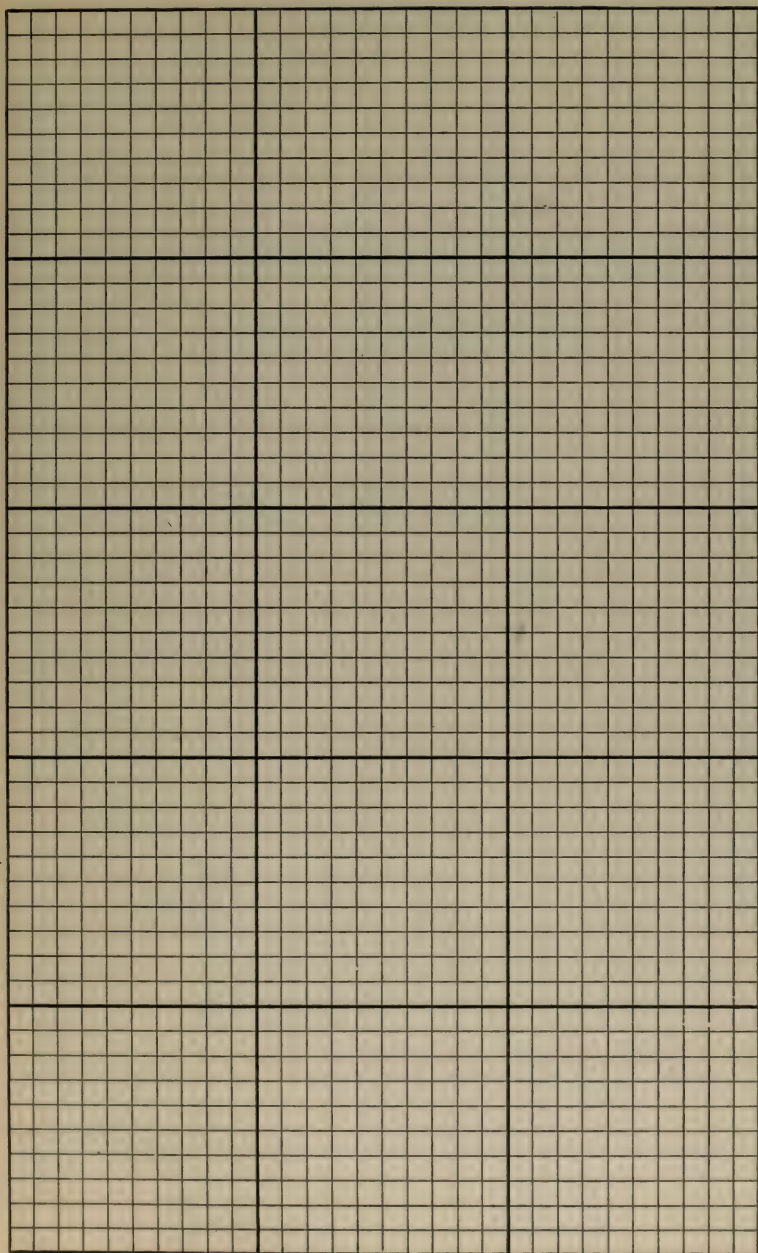
The above table is based on the use of standard widths of sheets 96 inches long.

If longer or shorter sheets are used the number of square feet given will vary accordingly.

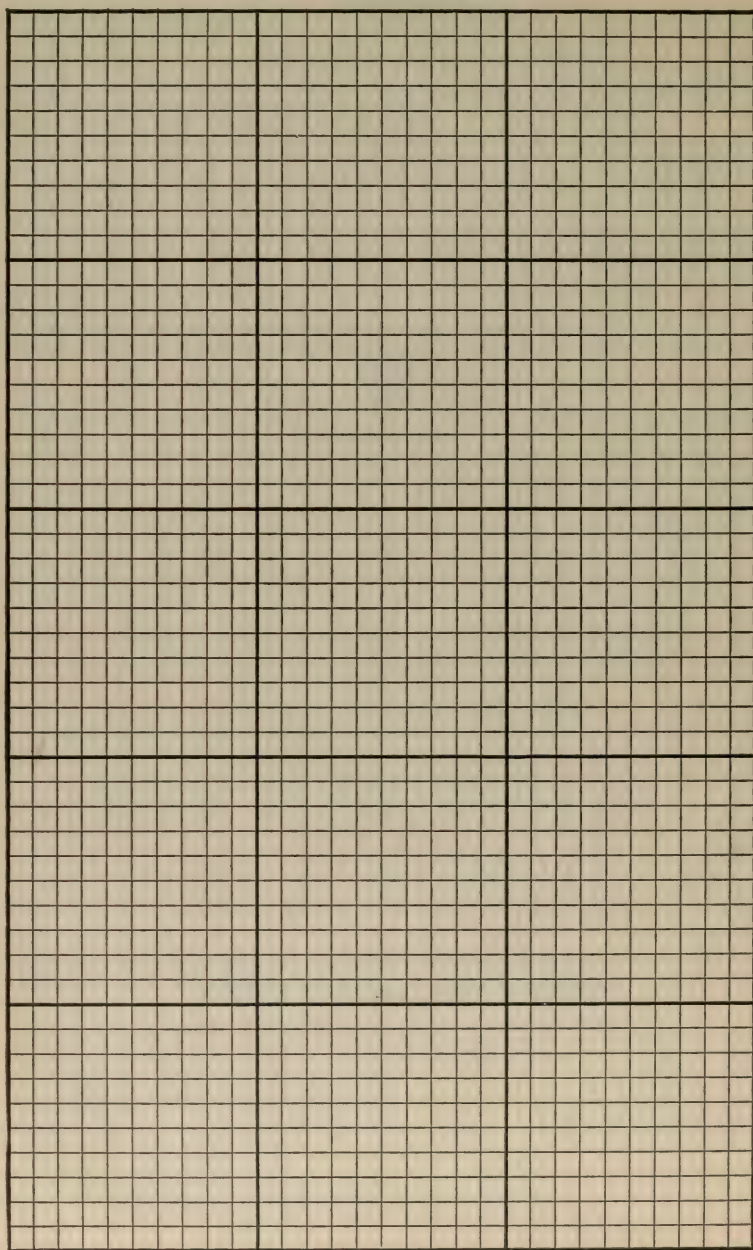
Laps:— In standard roof construction one and one-half corrugations are allowed for lap in the width of the sheet and six inches in the length.

In standard siding construction one corrugation is allowed for lap in the width of the sheet and four inches in the length.

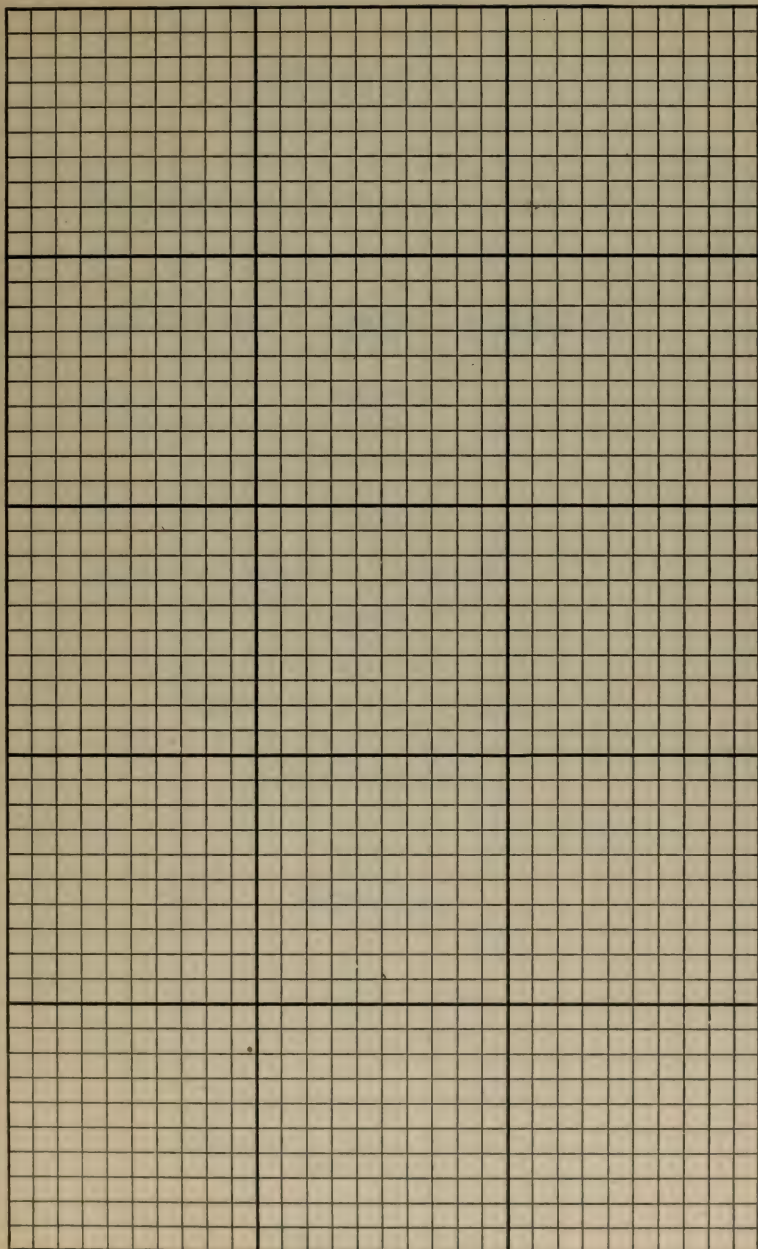
NOTES and DIAGRAMS



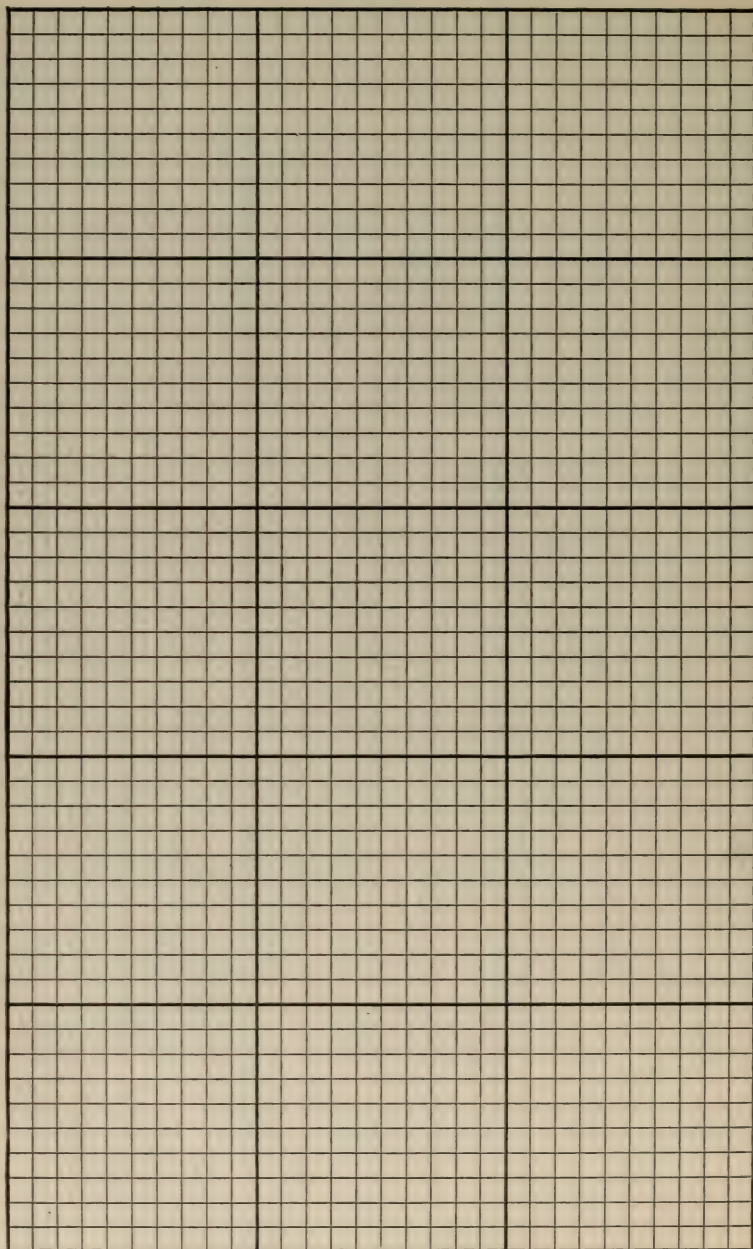
NOTES and DIAGRAMS



NOTES and DIAGRAMS



NOTES and DIAGRAMS



Part IV

Structural Shapes and Details

Explanation of Specification Formulae

Angles

Channels

Beams

American Standard

Bethlehem

Carnegie

Miscellaneous Beam Sections

Beam Summary

Columns

Bethlehem

Carnegie

Plate and Angle

Plate and Channel

Miscellaneous Sections

Base Plates

Rivets and Bolts

A. I. S. C. SPECIFICATION FORMULAE

In 1923 the American Institute of Steel Construction undertook the work of promoting uniform practice in the industry, and in order that its efforts would not be interpreted as being unduly influenced by commercial interests it selected a committee from among the leading talent in the academic, engineering and architectural professions to prepare a Standard Specification on the Design, Fabrication, and Erection of Structural Steel. This committee represented a combined experience of approximately one hundred and fifty years in an industry which is not more than thirty-five years old. The personnel was as follows:

GEORGE F. SWAIN: M. Am Soc C E—M. Am Soc M E—M. Inst C E
M. A R E A—Past President, A S C E—Professor
of Civil Engineering, Harvard University

MILO S. KETCHUM: M. Am Soc C E—M. A R E A—Dean of the College
of Engineering, and Director of the Engineering
Experiment Station of the University of Illinois

E. R. GRAHAM: of Graham, Anderson, Probst & White, Architects,
Chicago, Ill.

W. J. THOMAS: M. Am Soc C E—Chief Engineer, Geo. B. Post &
Sons, Architects, N. Y.

WILBUR J. WATSON: M. Am Soc C E—M. A R E A—President, Watson
Engineering Company, Cleveland, Ohio

It was recognized in their deliberations that the misleading term of "factor of safety" was more the subject of the application of any recommended unit stress than the unit stress itself. They did not undertake to define the qualities and property of steel, which is a proper function of the American Society for Testing Materials, but restricted themselves to a definition of the uses of steel in connection with building construction.

On the following pages is a mathematical explanation of the development of the various formulae recommended in the Specification for the proper reduction of working stresses. The diagram showing various column formulae indicates that a wide difference of opinion has existed on the proper consideration of this subject.

Part IV

Section 1

Explanation of A. I. S. C. Specification Formulae

Beams

Web Shear and Stiffeners

Laterally Unsupported Flanges

Columns

Rivet Stresses

A. I. S. C. Connection Angles

BEAMS—ALLOWABLE STRESSES**(A. I. S. C. Specification)**

All parts of the structure shall be so proportioned that the sum of the maximum static stresses in pounds per sq. in. shall not exceed the following:—

Shearing

On the gross area of the webs of beams and girders, where h , the height between flanges in inches, is not more than 60 times t , the thickness of the web in inches. 12000

On the gross area of the webs of beams and girders if the web is not stiffened where h , the height between flanges in inches, is more than 60 times t , the thickness of the web, the maximum shear per

$$\text{square inch, } \frac{V}{A} \text{ shall not exceed } \frac{18000}{1 + \frac{h^2}{7200t^2}}$$

In which V is the total shear, and A is gross area of web in square inches.

Stiffeners

Stiffeners shall be required on the webs of rolled beams and plate girders at the ends and at points of concentrated loads, and at other points where h the clear distance between flanges is greater than $85t\sqrt{18000(A/V)-1}$, in which t is the thickness of the web. When stiffeners are required, the distance in inches between them shall not be greater than $85t\sqrt{18000(A/V)-1}$, or not greater than 6 feet. When h is greater than 60 times t the thickness of the web of a plate girder, stiffeners shall be required at distances not greater than 6 feet apart. Stiffeners under or over concentrated loads shall be proportioned to distribute such loads into the web.

BEAMS—WEB SHEAR AND STIFFENERS

The development of formulae appearing in the Specification on this subject is based upon the accepted theory that the vertical shear in the webs of beams and girders may be properly resolved at 45° to the axis of the beam or girder, or at right angles to each other. Numerous tests have been made on beams and girders in which they have been loaded beyond their elastic limit with the result that the mill surface of the material has been broken down along the lines on which the interior material has been distorted. These lines have been photographed and confirm the theory exactly. They indicate that the webs of rolled beams act as multiple lattice trusses, and that riveted plate and angle girders act as pin connected trusses. These strain lines show the stresses acting at exactly 45° to the neutral axis. If the web of a beam or girder

is to fail by buckling this failure would of course develop as a result of the compression stresses acting at 45° to the axis of the girder; and the length of the column would be the square root of $2h^2$ where h is the height between flanges. Over a long period it has been established that until this height is more than 60 times the thickness of the web, there is no danger from buckling. The formula representing the crippling strength of the web is developed as follows:

f_c = average intensity of the allowable compression stress equal 18,000 #

f_s = average intensity of the vertical shear per square inch on the gross section of the web equals 12,000 #

l = length of the compression fibre at 45° between the stiffeners or the flanges, whichever is the smaller.

A = gross area of the web in square inches

V = gross vertical shear on the web

h = distance between flanges or stiffeners, whichever is the smaller

t = thickness of the web

r = least radius of gyration of the web

Therefore, $r = t/\sqrt{12}$ and $l = \sqrt{2h^2}$

The column formula applied to the web of a girder would then be

$$f_s = \frac{f_c}{1 + \frac{l^2}{cr^2}} = \frac{f_c}{1 + \frac{h^2}{c_1 t^2}}$$

c is a constant applying when the ratio l/r is used, and c_1 is a corresponding constant applying when h/t is used.

Solving this equation for h^2/t^2 we have,

$$\frac{h^2}{t^2} = c_1 \left(\frac{f_c}{f_s} - 1 \right)$$

It is now necessary to determine the value of the constant c_1 . Conceding the fact that stiffeners are not needed inside the points where h/t equals 60, we may substitute in this formula and get,

$$3600 = c_1 \left(\frac{18000}{12000} - 1 \right)$$

and solving this we have,

$$c_1 = 7200$$

The column formula for web crippling then becomes,

$$\frac{V}{A} = \frac{18000}{1 + \frac{h^2}{7200 t^2}}$$

and solving this, we have,

$$h = 85 t \sqrt{18000 \frac{A}{V} - 1}$$

By this analysis and treatment of the webs of beams and girders, we are enabled to so space the stiffeners on a web $\frac{1}{2}$ " thick as to give it the same resistance to buckling as a web 1" thick would have. It is, of course, obvious that we cannot make the shear of a $\frac{1}{2}$ " web equivalent to the shear of a 1" web; but we have taken the subject out of the empirical treatment and placed it on a rational basis.

On the opposite page is a chart devised to eliminate the necessity of calculations in finding the allowable vertical shear in the webs of beams and girders, and it also gives the proper spacing of web stiffeners.

The oblique lines through the points on the line which is the scale representing web thickness in inches all pass through zero. These lines intersect verticals from the base line giving the scale of h . The horizontal lines from this intersection give the ratio h/t on the left of the chart and where this horizontal line crosses the curve, gives the allowable shear per square inch in the web, which is read at the top of the chart. By reversing the process, the proper distance between stiffeners is given.

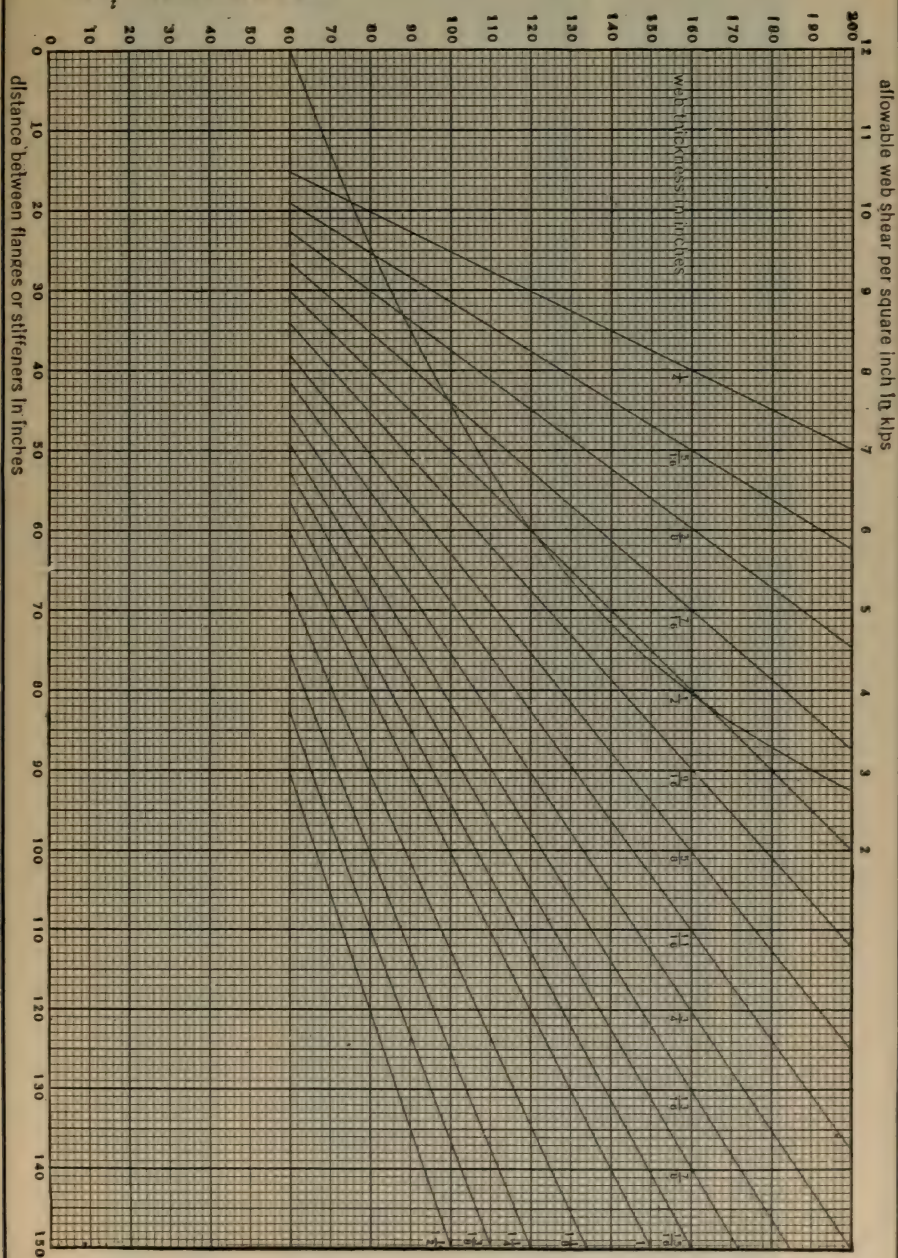
Example:—

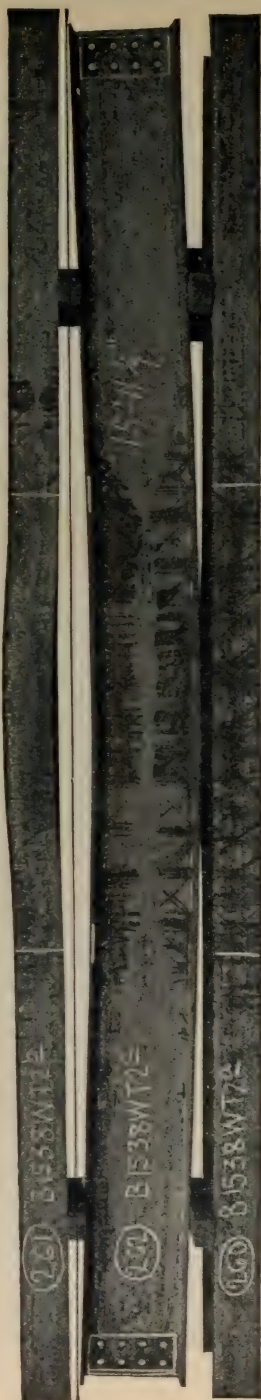
9000 pounds per square inch shear is permitted when h/t equals 85; and if t is $\frac{1}{2}$ inch $h = 42$ inches, which is the maximum distance between stiffeners if the distance between flanges is more than 42 inches.

Below is given the allowable shear per square inch for various ratios of h/t .

h/t	V/A	h/t	V/A	h/t	V/A	h/t	V/A
60	12000	74	10224	87	8775	100	7535
61	11868	75	10105	88	8672	105	7111
62	11734	76	9988	89	8571	110	6722
63	11604	77	9871	90	8471	115	6345
64	11473	78	9756	91	8372	120	6000
65	11343	79	9642	92	8274	125	5678
66	11215	80	9529	93	8177	130	5378
67	11087	81	9418	94	8082	135	5097
68	10961	82	9308	95	7988	140	4836
69	10835	83	9199	96	7895	145	4592
70	10711	84	9091	97	7803	150	4364
71	10587	85	8984	98	7712	155	4151
72	10465	86	8880	99	7623	160	3951
73	10344						

WEB SHEAR AND STIFFENERS CHART

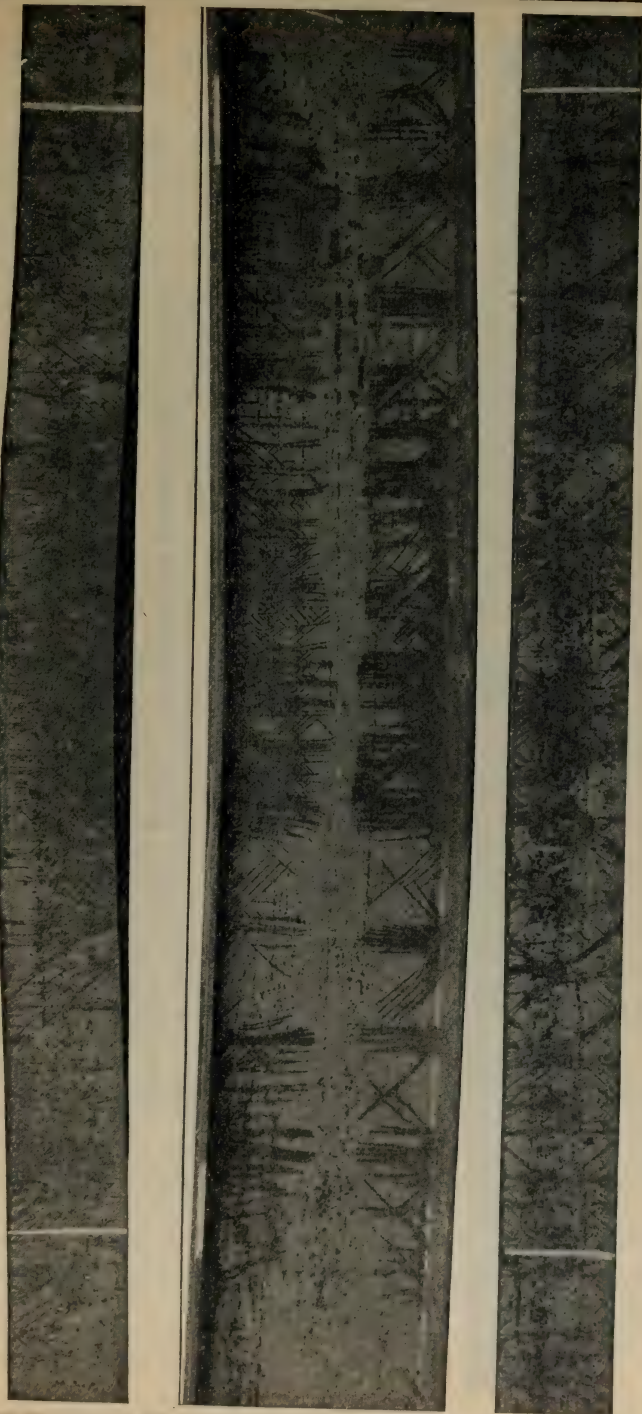
ratio $\frac{h}{t}$. h and t both in inches.



The above illustration is a picture of a 15 inch—38 pound beam 15 feet—11 $\frac{3}{4}$ inches long which has been loaded at the third points as indicated by the white marks.

There is a picture of a top and bottom flange shown from which it will be seen that the failure was due to buckling of the compression flange. The line drawn above the beam indicates the permanent set; and the lines on the web are the strain lines which are shown more clearly on an enlarged cut on the next page.

No paint was used on any of these beams, and the cracks in the mill scale are the result of strains beyond the elastic limit of the material.



Enlarged photo of web stress shown on the opposite page.



The above illustration is a picture of a plate and angle girder 27 feet $11\frac{1}{2}$ inches long, fabricated from a $30 \times \frac{3}{8}$ inch web plate; and flange angles $6 \times 4 \times \frac{3}{4}$ for the top flange and $6 \times 4 \times \frac{1}{2}$ for the bottom flange.

The loads were applied at the third points over the stiffeners and the line drawn above the beam shows the permanent set after the girder was removed from the testing machine. Strain lines are plainly visible radiating at exactly 45° from the various rivets.

BEAMS—ALLOWABLE STRESSES**(A. I. S. C. Specification)**

All parts of the structure shall be so proportioned that the sum of the maximum static stresses in pounds per sq. in. shall not exceed the following:—

Bending

On extreme fibres of rolled shapes, and built up sections, net section, if lateral deflection is prevented. 18000

When the unsupported length l exceeds 15 times b , the width of the compression flange, the stress in pounds per sq. in. in the latter shall not exceed

$$1 + \frac{20000}{2000b^2} l^2$$

The laterally unsupported length of beams and girders shall not exceed 40 times b the width of the compression flange.

BEAMS—LATERALLY UNSUPPORTED FLANGES

The question of the stresses in laterally unsupported flanges is of vital importance in the proper design of beams and girders. It is recognized of course, that this flange stress does not exist as uniform through the full length of a beam or girder flange, and is therefore properly entitled to somewhat higher unit stresses than the direct use of the column formula would permit. Practice over many years has established that it should be unnecessary to reduce the allowable stress in the compression flange until the length of this unsupported flange is more than 15 times its width. On this basis the 18,000 pound unit stress is permitted up to the point where l/b is 15, and is reduced by the column formula curve beyond this point. The constant in the denominator of this curve is determined as in the other two formulae by drawing a curve which starts at 20,000 and passes through 18,000 at $15 l/b$.

The A. I. S. C. Specification has, in the treatment of this subject, eliminated a large part of the empirical formulae which have existed in the past. It might be advocated that a straight line formula would as satisfactorily answer the purpose, but it should be remembered that such a straight line formula does not contain any factor which can be interpreted as representing failure by flexure. In addition to this, the use of any formula depends upon the engineer having before him the tabulated properties of the sections to be used, and if this tabulation is necessary in the straight line formula, it would be just as consistent to carry the calculations one stage further and give the allowable unit stress, thus eliminating the chances of errors in calculation.

On the page opposite is given a chart for determining the per cent of the allowable uniform load which various compression flanges may carry if laterally unsupported. The maximum allowable load is that which produces a flange stress of 18000 pounds per square inch on the beam or girder when laterally supported. The formula is,

$$f_c = \frac{20000}{1 + \frac{l^2}{2000 b^2}}$$

In which

f_c = allowable compression stress in pounds per square inch:

l = unsupported length of the compression flange in inches.

b = width of the flange in inches.

The oblique lines pass through the flange width scale given in inches and zero.

These lines intersect verticals from the span given in feet. The horizontal line from this intersection gives the ratio l/b on the left of the chart; and where this horizontal line crosses the percentage line, is the per cent of a laterally supported beam load which the same beam will carry if laterally unsupported.

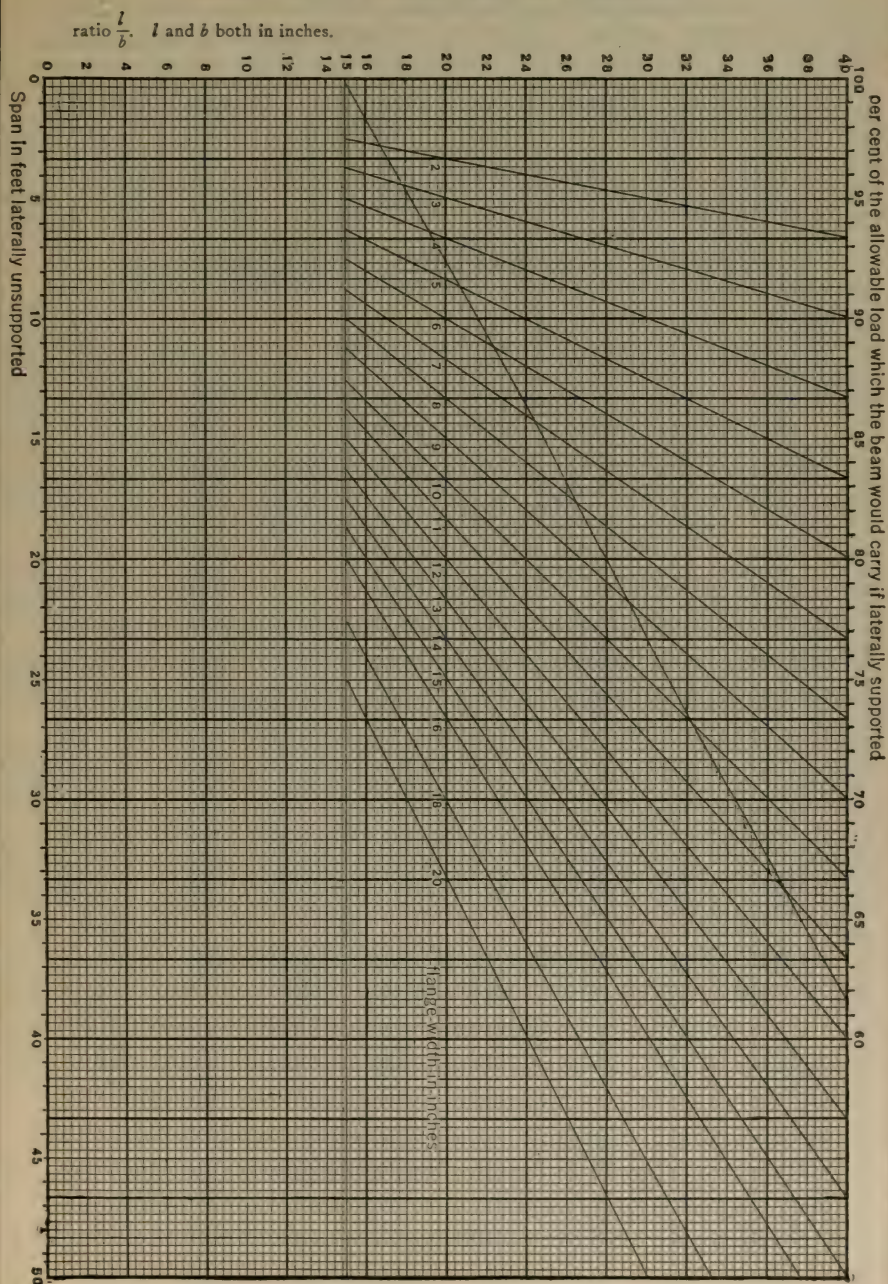
Example:—

A flange 6 inches wide on a laterally unsupported span of 15 feet has l/b equal to 30, and it will carry 76½% of the load of the same beam if it is laterally supported. The chart also gives the spans where the reduction of flange stress is required, and the maximum spans for laterally unsupported flanges.

A table giving the allowable flange stress and percentage of fixed beam loads for beams with laterally unsupported flanges is given on the page immediately following the chart.



LATERALLY UNSUPPORTED FLANGES



BEAMS AND GIRDERS WITH LATERALLY UNSUPPORTED FLANGES

ALLOWABLE STRESS, IN POUNDS PER SQ. INCH, IN EXTREME FIBRE FOR VARIOUS RATIOS OF l/b

$\frac{l}{b}$	Fibre Stress	$\frac{l}{b}$	Fibre Stress	$\frac{l}{b}$	Fibre Stress	$\frac{l}{b}$	Fibre Stress	$\frac{l}{b}$	Fibre Stress
15.0	18000	20.0	16667	25.0	15238	30.0	13793	35.0	12403
16.0	17730	21.0	16387	26.0	14948	31.0	13509	36.0	12136
17.0	17475	22.0	16103	27.0	14657	32.0	13228	37.0	11873
18.0	17212	23.0	15817	28.0	14368	33.0	12949	38.0	11614
19.0	16942	24.0	15528	29.0	14080	34.0	12674	39.0	11360
								40.0	11111

PERCENTAGE OF FIXED BEAM LOADS FOR VARIOUS RATIOS OF l/b

$\frac{l}{b}$	%	$\frac{l}{b}$	%	$\frac{l}{b}$	%	$\frac{l}{b}$	%	$\frac{l}{b}$	%
15.0	100.00	20.0	92.58	25.0	84.65	30.0	76.63	35.0	68.90
15.1	99.74	20.1	92.43	25.1	84.49	30.1	76.47	35.1	68.76
15.2	99.61	20.2	92.28	25.2	84.33	30.2	76.31	35.2	68.61
15.3	99.47	20.3	92.13	25.3	84.17	30.3	76.15	35.3	68.46
15.4	99.33	20.4	91.97	25.4	84.01	30.4	75.99	35.4	68.31
15.5	99.19	20.5	91.82	25.5	83.85	30.5	75.84	35.5	68.16
15.6	99.06	20.6	91.66	25.6	83.69	30.6	75.68	35.6	68.01
15.7	98.93	20.7	91.50	25.7	83.53	30.7	75.52	35.7	67.86
15.8	98.78	20.8	91.35	25.8	83.37	30.8	75.36	35.8	67.72
15.9	98.64	20.9	91.19	25.9	83.20	30.9	75.21	35.9	67.57
16.0	98.50	21.0	91.04	26.0	83.04	31.0	75.05	36.0	67.42
16.1	98.36	21.1	90.88	26.1	82.88	31.1	74.89	36.1	67.27
16.2	98.22	21.2	90.72	26.2	82.72	31.2	74.74	36.2	67.13
16.3	98.08	21.3	90.56	26.3	82.55	31.3	74.58	36.3	66.98
16.4	97.94	21.4	90.41	26.4	82.39	31.4	74.42	36.4	66.83
16.5	97.80	21.5	90.25	26.5	82.23	31.5	74.26	36.5	66.69
16.6	97.65	21.6	90.09	26.6	82.07	31.6	74.11	36.6	66.54
16.7	97.51	21.7	89.93	26.7	81.91	31.7	73.95	36.7	66.39
16.8	97.37	21.8	89.78	26.8	81.75	31.8	73.79	36.8	66.25
16.9	97.23	21.9	89.62	26.9	81.59	31.9	73.64	36.9	66.11
17.0	97.08	22.0	89.46	27.0	81.43	32.0	73.48	37.0	65.96
17.1	96.94	22.1	89.30	27.1	81.27	32.1	73.33	37.1	65.82
17.2	96.80	22.2	89.14	27.2	81.11	32.2	73.17	37.2	65.67
17.3	96.65	22.3	88.98	27.3	80.94	32.3	73.02	37.3	65.53
17.4	96.50	22.4	88.82	27.4	80.78	32.4	72.86	37.4	65.38
17.5	96.35	22.5	88.66	27.5	80.62	32.5	72.71	37.5	65.24
17.6	96.21	22.6	88.51	27.6	80.46	32.6	72.55	37.6	65.09
17.7	96.06	22.7	88.35	27.7	80.30	32.7	72.40	37.7	64.95
17.8	95.92	22.8	88.19	27.8	80.14	32.8	72.25	37.8	64.81
17.9	95.77	22.9	88.03	27.9	79.98	32.9	72.09	37.9	64.67
18.0	95.62	23.0	87.87	28.0	79.82	33.0	71.94	38.0	64.52
18.1	95.47	23.1	87.71	28.1	79.66	33.1	71.78	38.1	64.38
18.2	95.33	23.2	87.55	28.2	79.50	33.2	71.63	38.2	64.24
18.3	95.17	23.3	87.39	28.3	79.34	33.3	71.48	38.3	64.09
18.4	95.02	23.4	87.23	28.4	79.18	33.4	71.32	38.4	63.96
18.5	94.87	23.5	87.07	28.5	79.02	33.5	71.17	38.5	63.81
18.6	94.72	23.6	86.91	28.6	78.86	33.6	71.02	38.6	63.67
18.7	94.57	23.7	86.75	28.7	78.69	33.7	70.87	38.7	63.53
18.8	94.43	23.8	86.59	28.8	78.53	33.8	70.72	38.8	63.39
18.9	94.27	23.9	86.43	28.9	78.38	33.9	70.56	38.9	63.25
19.0	94.12	24.0	86.27	29.0	78.22	34.0	70.41	39.0	63.11
19.1	93.97	24.1	86.11	29.1	78.06	34.1	70.26	39.1	62.97
19.2	93.82	24.2	85.94	29.2	77.90	34.2	70.11	39.2	62.83
19.3	93.66	24.3	85.78	29.3	77.74	34.3	69.96	39.3	62.69
19.4	93.51	24.4	85.62	29.4	77.58	34.4	69.80	39.4	62.55
19.5	93.36	24.5	85.46	29.5	77.42	34.5	69.65	39.5	62.42
19.6	93.20	24.6	85.30	29.6	77.26	34.6	69.50	39.6	62.27
19.7	93.05	24.7	85.14	29.7	77.10	34.7	69.35	39.7	62.14
19.8	92.90	24.8	84.98	29.8	76.94	34.8	69.21	39.8	62.00
19.9	92.75	24.9	84.81	29.9	76.78	34.9	69.05	40.0	61.72

 l = the unsupported length, in inches, of the compression flange. b = the width of the flange in inches.

COLUMNS—ALLOWABLE STRESSES**(A. I. S. C. Specification)**

All parts of the structure shall be so proportioned that the sum of the maximum static stresses in pounds per sq. in. shall not exceed the following:—

Compression

Rolled Steel, on short lengths or where lateral deflection is prevented.....18000

On gross section of columns.....
$$1 + \frac{l^2}{18000r^2}$$

with a maximum of.....15000

In which l is the unsupported length of the column, and r is the corresponding least radius of gyration of the section, both in inches.

For main compression members, the ratio l/r shall not exceed 120, and for bracing and other secondary members, 200.

COLUMNS

One of the apparent defects in most curves representing column failures is the lack of consideration of the fact that steel in compression fails by one of three processes depending upon the ratio of slenderness. These three types of failure may be described as bearing, transverse crippling and flexure. Bearing failures occur in short specimens which can hardly be classed as columns in the usual meaning of the term, since a failure by bearing is evidenced by a lateral flow of the metal. It is of course, true that the physical evidence of bearing exists in all columns to the extent that the specimen is shortened and the area is increased by the lateral flow of the metal. As the ratio of slenderness increases, the action of bearing merges into a combination of shear and bearing on a plane inclined to the axis of the column, and this combination will be referred to as transverse crippling, which corresponds very closely to what is considered shear in the web of a beam or girder. Pure shear rarely exists in construction.

When the ratio of slenderness is small, and the specimen very short, the angle of the plane on which transverse failure occurs, is nearly at right angles to the direction of the compression stress, and the dominant condition of failure is bearing. This condition exists up to where l/r is approximately 25. As the length increases, the angle of this plane of failure changes, the bearing stress decreases, and the shearing increases until the plane is 45° to the axis of stress, and at this point the intensity of shear is one-half the axial stress, or direct compression. Failure in columns does not occur on this 45° plane, but when the

angle between the axial stress and the plane is approximately 35° to 40° , and is the result of a combination of shear and bearing, referred to as crippling.

Professor Charles E. Greene in his book on Structural Mechanics (1897) analyzes conditions of transverse shear, and by experiment found that in granular material, such as cast iron, the angle of the plane of failure was about 35° to the axis. Due to the ductile properties of steel, complete fracture cannot be obtained in this type of failure. If failure by transverse crippling is sufficiently complete, the column folds up about the part where primary failure started instead of bowing from end to end as will occur when the failure is one of flexure. It may, however, occur that in the primary failure by crippling, the resulting eccentricity may cause the failure to merge into a flexural condition, and bow from end to end although the primary condition was one of crippling. This will explain why columns sometimes fail by flexure against the axis of their maximum strength in bending.

An examination of many column tests shows that failure by transverse crippling dominates until the ratio of slenderness l/r is about 80 and sometimes more than 100. If it were possible to eliminate eccentricity, including metallurgical and mechanical inequalities both as regards the straightness of the column, and the application of the load, all columns would fail at practically uniform stress by transverse crippling. The elimination of mechanical and metallurgical eccentricities being impossible in commercial practice, means that when such eccentricities become sufficient, the columns will not fail by crippling, but by flexure; and to be consistent the formula for this flexure type of failure must include a factor representing flexure.

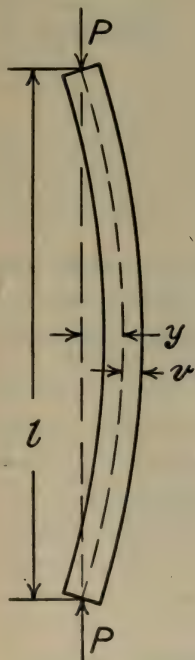
The American Institute of Steel Construction's Specification considers columns as resisting crippling (at 15,000 pounds per square inch), where l/r is 60 or less, and reduces the allowable working stress by a flexure formula where l/r is more than 60.

Confirming the uniformity with which columns fail under conditions of transverse crippling, the following records of test are given from which it will be seen that the strength corresponds to the yield point of the material.

Soft Steel 1" Thick			Medium Steel 2" Thick		
Length	l/r	Ultimate Stress per sq. in.	Length	l/r	Ultimate Stress per sq. in.
12'0"	40.5	38,700	12'0"	38	43,800
12'0"	40.5	38,000	12'0"	38	45,000
12'0"	40.5	37,700	12'0"	38	45,000
24'0"	81	38,600	24'0"	76	42,000
24'0"	81	37,600	24'0"	76	42,500
24'0"	81	36,600	24'0"	76	43,600

While the point at which failure by flexure due to metallurgical and mechanical eccentricity is empirical, and starts somewhere about where l/r is 80, the Specification is based on failures by transverse crippling ending where l/r is 60, and beyond this reduces the allowable stress by a flexure formula which prevents an appreciable increase in the unknown initial eccentricity.

Such a formula for determining the maximum working stress should be obtained by combining the stress per square inch due to direct compression, and the stress per square inch due to flexure, making the sum of these two equal the maximum allowable stress. In connection with the diagram attached hereto:



l = length of the column in inches.

y = maximum deflection in inches from the line of action of the compression stress.

v = distance in inches of the extreme fibre from the axis of the section through its center of gravity.

P = total load in compression.

A = area of the column in square inches.

I = moment of inertia of the column cross section $= Ar^2$

S = section modulus of the column $= \frac{I}{v} = \frac{Ar^2}{v}$,

r = radius of gyration of the column cross section.

f = maximum allowable stress intensity per square in.

The intensity of stress per square inch due to direct compression is then equal $\frac{P}{A}$.

The bending moment due to direct compression is $P y$.

The stress per sq. in. due to bending is $\frac{Py}{S} = \frac{Pyv}{Ar^2}$.

Then combining the stress per square inch from direct compression with the stress per square inch due to bending, we have,

$$f = \frac{P}{A} + \frac{Pyv}{Ar^2} = \frac{P}{A} \left(1 + \frac{yv}{r^2} \right)$$

and solving this, we have

$$\frac{P}{A} = \frac{f}{1 + \frac{yv}{r^2}}$$

$$\frac{P}{A} = \frac{f}{1 + \frac{y v}{r^2}}$$

This formula must be correct within the elastic limit of the material if our theory of flexure is sound. It cannot, however, be used in this form because y is unknown. It is, however, known that as l increases y will also increase. Also yv is a distance times a distance in which v is a constant. To retain the consistency of the equation in replacing the quantity yv , we must have it include a distance times a distance; and as l is the distance, regulating the variation in y , we may properly introduce cl^2 to replace the quantity yv . In this factor c includes the constant v , and the unknown ratio of l to y . Substituting the quantity cl^2 , we have the Rankine formula.

$$\frac{P}{A} = \frac{f}{1 + \frac{cl^2}{r^2}}$$

This substitution above referred to is reasonable, for as v increases, other things being equal, y must decrease, and as l increases y must increase in a greater ratio. If the length of the column increases while the cross section and v remain the same, clearly y would increase in a greater ratio.

It may be said that this formula contains one inherent inaccuracy, namely, that c should really be a variable increasing with P . It is not practical to make c a variable for designing purposes, and furthermore, the exact law of its variation has not been determined. The purpose of reducing the working stress is to make the variation of c so small that it is negligible; it is therefore assumed a constant for practical purposes, and in this connection the use of the formula is limited for primary columns between the points $60 l/r$ and $120 l/r$; and for secondary members from $120 l/r$ to $200 l/r$. The determination of the constant in the denominator of this formula is as follows:

The maximum allowable stress in compression is 18000 pounds, and at $60 l/r$ the maximum allowable working stress has been fixed at 15000 lbs.

From this we derive the equation,

$$15000 = \frac{18000}{1 + \frac{cl^2}{r^2}}$$

Substituting 60 for l/r , we have

$$15000 = \frac{18000}{1 + 3600 c}$$

Solving this, we have

$$c = \frac{1}{18000}$$

and our formula then becomes,

$$\frac{P}{A} = f = \frac{18000}{1 + \frac{l^2}{18000r^2}}$$

This provides a reduction in stress per square inch over the range in which the column is considered as failing through flexure.

It might be advocated that a straight line formula could be devised to give practically the same reductions for flexural conditions as the curve, but a comparative analysis of the two shows that the straight line is mathematically inconsistent. The straight line formula is,

$$\frac{P}{A} = f - \frac{cl}{r} \text{ or } f = \frac{P}{A} + \frac{cl}{r}$$

In the development of our formula we found f equal to the sum of the direct load stress and the bending stress, or,

$$f = \frac{P}{A} + \frac{P y v}{A r^2}$$

From these formulae we have,

$$\frac{P y v}{A r^2} = \frac{cl}{r}$$

In this we find that cl/r of the straight line formula is equal to the bending stress in our formula. This is not consistent, since on the left we have a stress per square inch times a ratio and on the right a constant times a ratio.

Furthermore, solving for y , we have,

$$y = \frac{clAr}{Pv}$$

In this we find that y would increase if either A or r were increased, which is the reverse of actual conditions; also if P were increased, y would decrease, which is absurd.

The claim that a straight line formula is easier to operate is based upon the assumption that the operator has memorized the tables of radius of gyration and if he has not, the tabulation might consistently be carried one step further giving the unit stress and eliminating the chances for errors in computation.

On the page opposite is a chart which is devised to eliminate the necessity of tedious mathematical calculations to determine the allowable working stress in columns of various lengths.

The oblique lines through the points on the scale of radius of gyration in inches all pass through zero. These lines intersect verticals from the base where the length of the column is shown in feet. The horizontal line at the point of this intersection gives the ratio of l/r on the left of the chart. The line which is the scale of radius of gyration in inches is so located that the length of the column in feet is converted to inches and divided by the radius of gyration which is read on its scale. Where the horizontal line from the ratio of l/r intersects the column formula curve, the allowable stress per square inch in the column is read at the top of the chart.

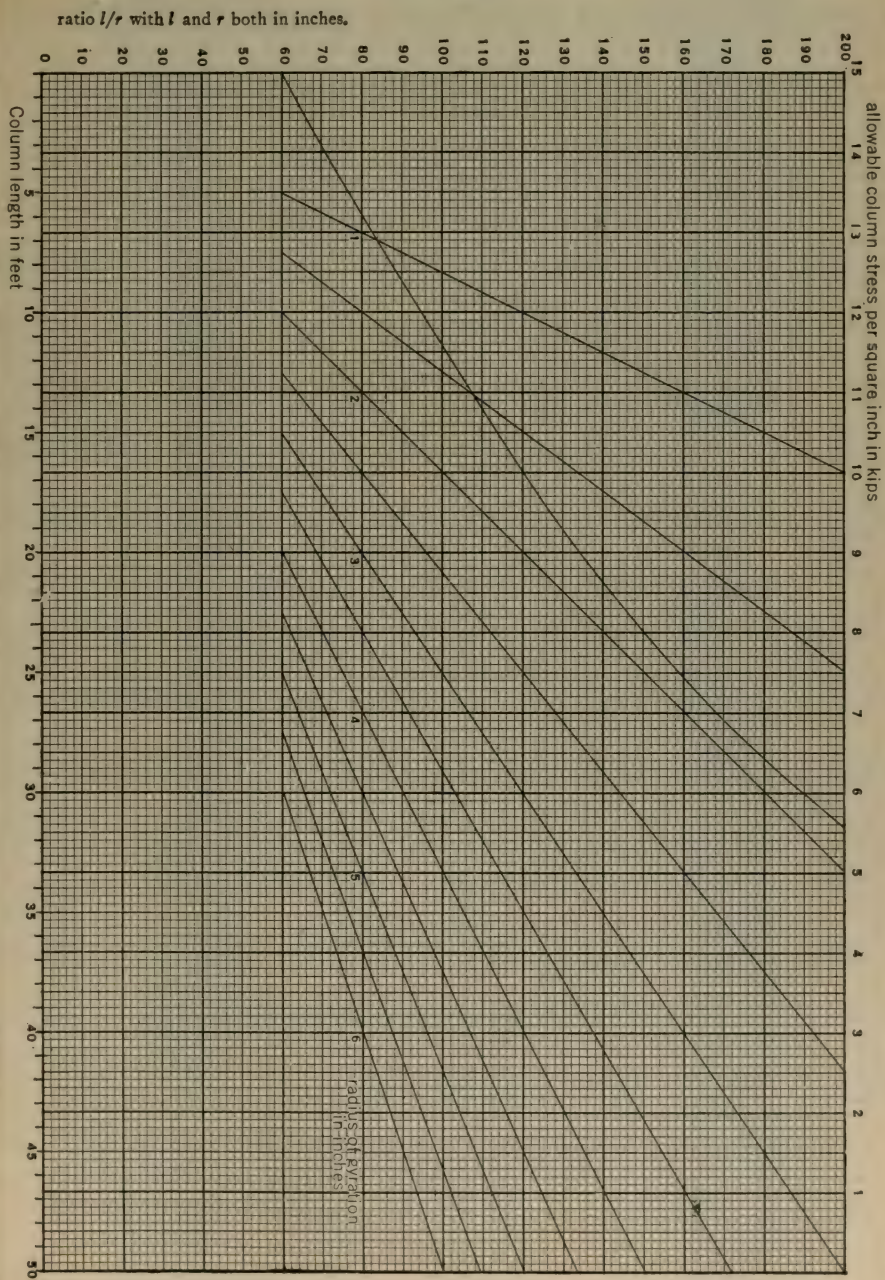
Example:—

The oblique line representing r equal to 3 inches crosses the vertical line representing a column 27 feet long at a horizontal line showing the ratio l/r to be 108. This horizontal line crosses the curve at a point which shows the stress to be 10,900 pounds per square inch.

A table giving the allowable working stress per square inch for ratios of l/r ranging from 60 to 200 is given on the page immediately following the chart.



COLUMNS



ALLOWABLE WORKING STRESS FOR COLUMNS. VARIOUS RATIOS $\frac{1}{r}$

$\frac{1}{r}$	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79
0	15000	14916	14832	14748	14663	14578	14493	14407	14321	14235	14148	14062	13975	13888	13801	13714	13627	13540	13453	13366
.1	14992	14908	14824	14740	14655	14570	14484	14398	14312	14226	14139	14053	13966	13879	13792	13705	13618	13531	13444	13357
.2	14983	14899	14815	14731	14646	14561	14476	14390	14304	14218	14131	14045	13958	13871	13784	13697	13610	13523	13436	13349
.3	14974	14891	14807	14723	14638	14553	14467	14381	14295	14209	14122	14036	13949	13862	13775	13688	13601	13514	13427	13340
.4	14966	14882	14798	14714	14629	14544	14459	14373	14287	14200	14114	14027	13940	13853	13766	13679	13592	13505	13418	13331
.5	14958	14874	14790	14706	14621	14536	14450	14364	14278	14192	14105	14018	13932	13845	13758	13671	13584	13497	13410	13323
.6	14950	14866	14782	14697	14612	14527	14441	14355	14269	14183	14096	14010	13923	13836	13749	13662	13575	13488	13401	13314
.7	14941	14857	14773	14688	14604	14519	14433	14347	14261	14174	14088	14001	13914	13827	13740	13653	13566	13479	13392	13305
.8	14933	14849	14765	14680	14595	14510	14424	14338	14252	14165	14079	13992	13905	13818	13731	13644	13557	13470	13383	13296
.9	14924	14840	14756	14671	14587	14502	14416	14330	14244	14157	14071	13984	13897	13810	13723	13636	13549	13462	13375	13288
$\frac{1}{r}$	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99
0	13279	13192	13105	13018	12931	12844	12758	12672	12585	12500	12414	12328	12243	12158	12073	11989	11905	11821	11737	11654
.1	13270	13183	13096	13009	12922	12835	12749	12663	12577	12491	12405	12320	12235	12150	12065	11981	11897	11813	11729	11646
.2	13262	13175	13088	13001	12914	12827	12741	12655	12568	12483	12397	12311	12226	12141	12056	11972	11888	11804	11720	11637
.3	13253	13166	13079	12992	12905	12818	12732	12646	12560	12474	12388	12303	12218	12133	12048	11964	11880	11796	11712	11629
.4	13244	13157	13070	12983	12896	12810	12724	12637	12551	12466	12380	12294	12209	12124	12039	11955	11871	11787	11704	11621
.5	13236	13149	13062	12975	12888	12801	12715	12629	12543	12457	12371	12286	12201	12116	12031	11947	11863	11779	11696	11613
.6	13227	13140	13053	12966	12879	12792	12706	12620	12534	12448	12362	12277	12192	12107	12023	11939	11855	11771	11687	11604
.7	13218	13131	13044	12957	12870	12784	12698	12612	12526	12440	12354	12269	12184	12099	12014	11930	11846	11762	11679	11596
.8	13209	13122	13035	12948	12861	12775	12689	12601	12515	12431	12345	12260	12175	12090	12006	11922	11838	11754	11671	11588
.9	13201	13114	13027	12940	12853	12767	12681	12594	12509	12423	12337	12252	12167	12082	11997	11913	11829	11745	11662	11579
$\frac{1}{r}$	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119
0	11571	11489	11407	11325	11244	11163	11082	11002	10922	10843	10764	10686	10608	10530	10453	10376	10300	10224	10149	10074
.1	11563	11481	11399	11317	11236	11155	11074	10994	10914	10835	10756	10678	10600	10522	10445	10368	10292	10217	10142	10067
.2	11555	11473	11391	11309	11228	11147	11066	10986	10906	10827	10748	10670	10592	10515	10438	10361	10285	10209	10134	10059
.3	11546	11464	11382	11301	11220	11139	11058	10978	10898	10819	10741	10663	10585	10507	10430	10353	10277	10202	10127	10052
.4	11538	11456	11374	11293	11212	11131	11050	10970	10890	10811	10733	10655	10577	10499	10422	10346	10270	10194	10119	10044
.5	11530	11448	11366	11285	11204	11123	11042	10962	10883	10804	10725	10647	10569	10492	10415	10338	10262	10187	10112	10037
.6	11522	11440	11358	11276	11195	11114	11034	10954	10875	10796	10717	10639	10561	10484	10407	10330	10254	10179	10104	10030
.7	11514	11432	11350	11268	11187	11106	11026	10946	10867	10788	10709	10631	10553	10476	10399	10323	10247	10172	10097	10022
.8	11505	11423	11341	11260	11179	11098	11018	10938	10859	10780	10702	10624	10546	10468	10391	10315	10239	10164	10089	10015
.9	11497	11415	11333	11252	11171	11090	11010	10930	10851	10772	10694	10616	10538	10461	10384	10308	10232	10157	10082	10007
$\frac{1}{r}$	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0	10000	9926	9853	9780	9708	9636	9565	9494	9424	9354	9284	9215	9146	9078	9011	8944	8878	8812	8747	8682
.5	9963	9890	9817	9744	9672	9601	9530	9459	9389	9319	9250	9181	9112	9045	8978	8911	8845	8780	8715	8650
$\frac{1}{r}$	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159
0	8617	8553	8489	8426	8364	8302	8241	8180	8120	8060	8000	7941	7882	7824	7767	7710	7653	7597	7541	7486
.5	8585	8521	8458	8395	8333	8272	8211	8150	8090	8030	7971	7912	7853	7796	7739	7682	7625	7569	7514	7459
$\frac{1}{r}$	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179
0	7431	7377	7323	7270	7217	7164	7112	7060	7009	6958	6908	6858	6808	6759	6711	6663	6615	6568	6521	6475
.5	7404	7350	7297	7244	7191	7138	7086	7034	6984	6933	6883	6833	6784	6735	6687	6639	6592	6545	6498	6452
$\frac{1}{r}$	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199
0	6429	6383	6338	6293	6248	6204	6160	6117	6074	6031	5989	5947	5905	5864	5823	5783	5743	5703	5664	5625
.5	6400	6356	6311	6267	6224	6181	6139	6096	6053	6011	5968	5926	5885	5844	5803	5763	5723	5684	5645	5606

PRIMARY MEMBERS

SECONDARY MEMBERS ONLY

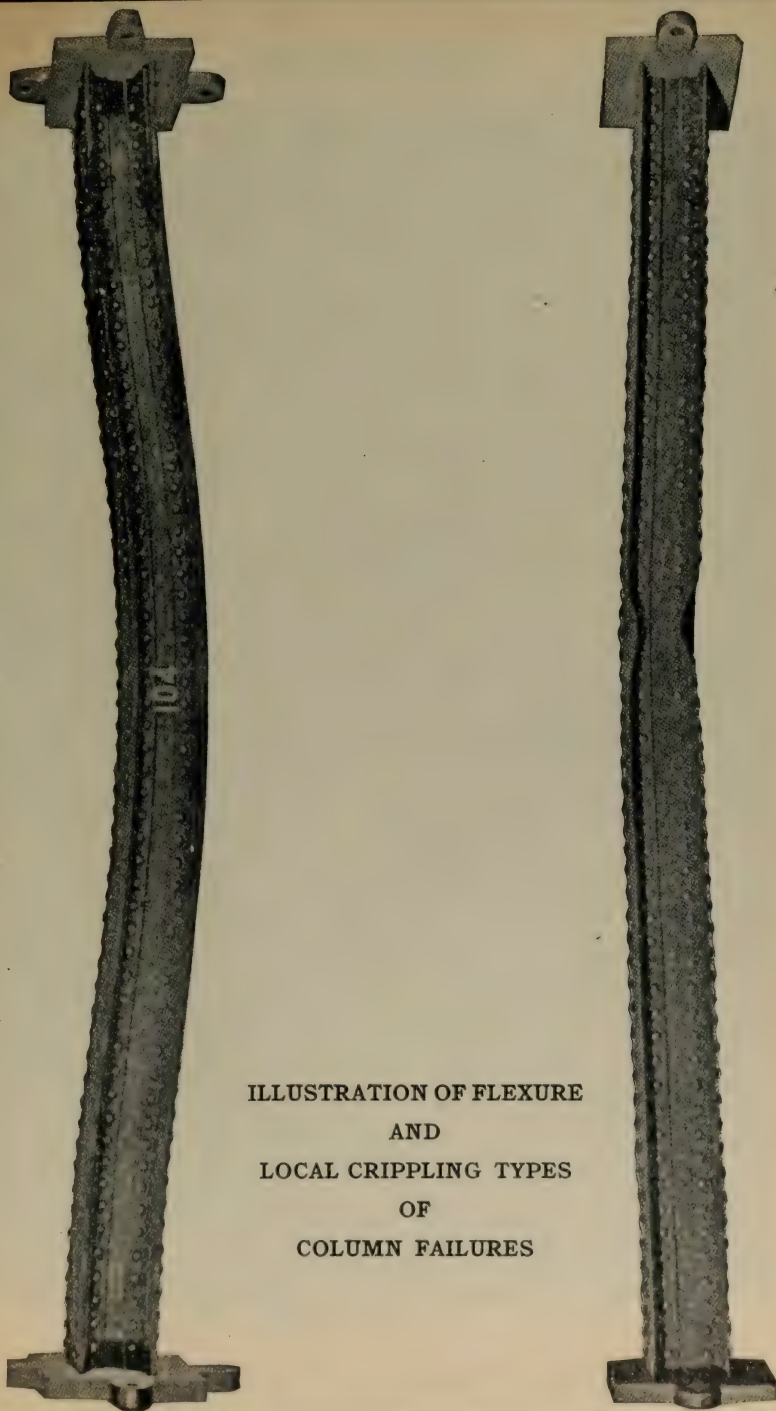
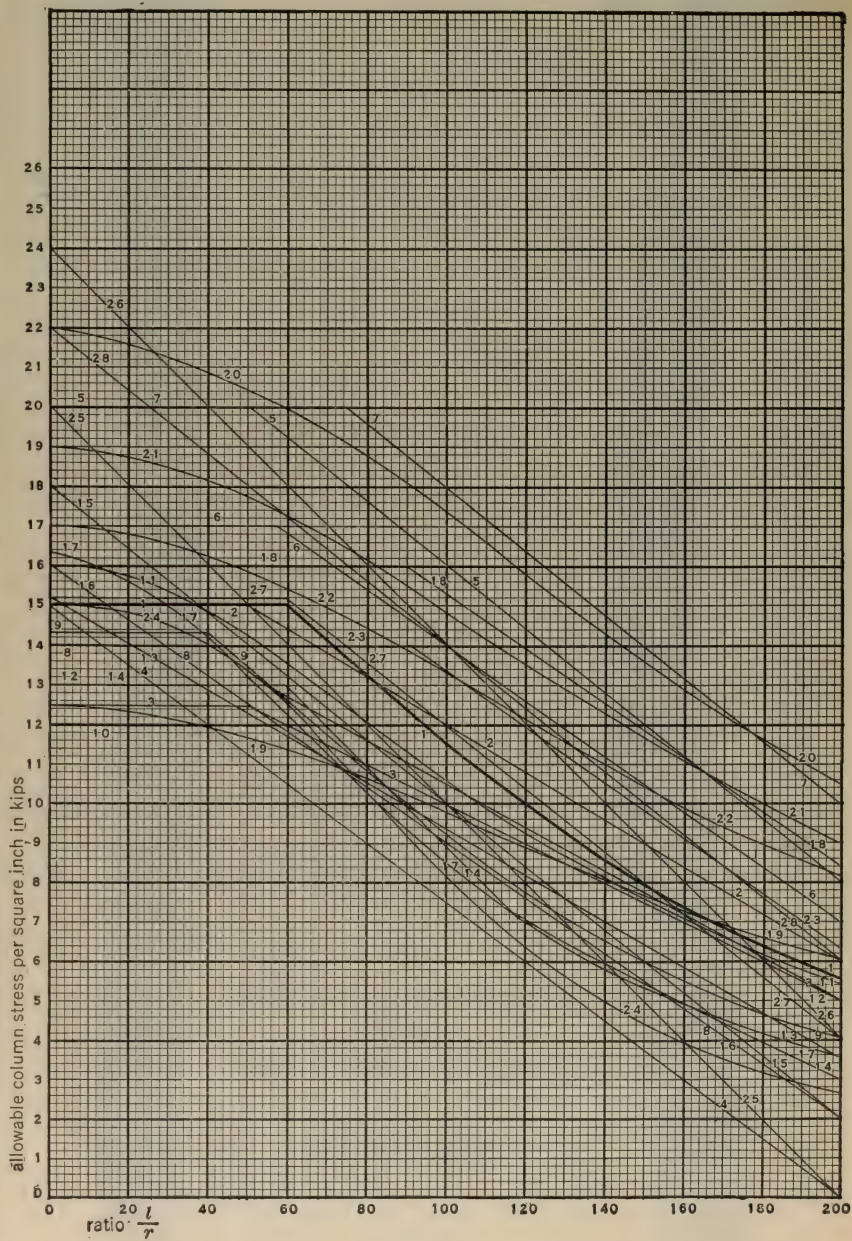


ILLUSTRATION OF FLEXURE
AND
LOCAL CRIPPLING TYPES
OF
COLUMN FAILURES

COLUMN DIAGRAMS



COLUMN DIAGRAMS

On the page opposite there is a diagram illustrating twenty-eight (28) different column formulae, including that of the American Institute of Steel Construction which is shown as the heavy line.

Since the rolling mills began publishing handbooks about thirty-five years ago based on a 16,000 pound unit stress, an endless number of column formulae have been devised to give the allowable working stresses under different ratios of slenderness.

The diagrams clearly illustrate that the basic unit stress is not a consistent index of the so called factor of safety.

Below is given a key to the chart with the various formulae which are represented.

1. A. I. S. C.: 15000 to 60 l/r : beyond 60 $l/r = \frac{18,000}{1 + \frac{l^2}{18,000r^2}}$
2. Am. Bridge 1922: 18000—60 l/r with max. 15000
3. A. R. E. A. design Ry. Bridge: 15000—50 l/r with max. 12500
4. A. R. E. A. electrical spec.: 15000—75 l/r
5. A. R. E. A. existing Ry. Bridge O. H. Steel: 24000—80 l/r with max. 20000
6. A. R. E. A. existing Ry. Bridge Besm. Steel: 21000—70 l/r with max. 17000
7. A. R. E. A. existing Buildings: 26000 — 80 l/r with max. 20000
8. A. R. E. A. 1920 Ry. Bridges: 16000—70 l/r with max. 14000
9. A. S. C. E. Highway Bridge: $\frac{16,000}{1 + \frac{l^2}{13,500r^2}}$ with max. at 40 l/r
10. Boston 1919: 12000 to 80 l/r : 20000—100 l/r above 80 l/r
11. Boston 1918: $\frac{16,000}{1 + \frac{l^2}{20,000r^2}}$
12. Bethlehem Steel: 16000—55 l/r with max. 13000
13. N. Y. City: 15200—58 l/r prior to 1915. 16000—70 l/r
14. Carnegie straight lines: 13000 to 50 l/r : 7000 at 120 l/r : 3000 at 200 l/r
J. & L. Chicago etc. use No. 8
15. Omaha: 18000—80 l/r
16. N. Y. C. Ry.: 16000—70 l/r with max. 15000
Can. Eng. Std. Assn. Ry. Bridges—Use No. 3
17. Philadelphia: $\frac{16,000}{1 + \frac{l^2}{11,000r^2}}$
18. Canton Boiler: 16000 to 90 l/r above which 21400—60 l/r

$$19. \text{ Cambria-Gordon: } \frac{12,500}{1 + \frac{l^2}{36,000r^2}}$$

$$20. \text{ Osborn Highway: } \frac{22,000}{1 + \frac{l^2}{36,000r^2}}$$

$$21. \text{ Osborn Elect. Ry.: } \frac{19,000}{1 + \frac{l^2}{36,000r^2}}$$

$$22. \text{ Osborn Steam Ry.: } \frac{17,000}{1 + \frac{l^2}{36,000r^2}}$$

23. Chicago Bridge & Iron: 20300—70 l/r : max. 14000

$$24. \text{ Cleveland: } S = \frac{P}{A} \left[1 + \left(\frac{ec}{r^2} + \frac{3}{10} \right) \text{Sec. } \frac{l}{Kr} \sqrt{\frac{FP}{AE}} \right]$$

25. Blackwells Island Bridge Ordinary loading: 20000—100 l/r

26. Blackwells Island Bridge Congested loading: 24000—100 l/r

27. Present Quebec Bridge combined loads exclusive of secondary stresses:
20000—80 l/r with max. 15200

28. Present Quebec Bridge All combined loads inclusive of secondary stresses:
22000—80 l/r .

RIVETS AND BOLTS

For many years there has been a considerable variation in the working stresses allowed in rivets, and careful thought was given this important subject. Engineers have long recognized that more complete conditions of bearing exist on plates and sections, which are enclosed on both sides, than can exist on outside plates or sections where the rivet acts as a cantilever. Rational provision is made for this in our Specification and it will permit a more consistent and economical development of stresses. Tests which have been recently made clearly indicate the truth of what many engineers have believed regarding the friction between riveted surfaces being greater than the usually allowed working stress in the rivets.

The Specification also properly classifies rivets as power or hand driven instead of field or shop driven.

Power driven rivets are those driven by pneumatic tools, whether in the shop or field. Hand driven rivets are those driven without the use of pneumatic equipment.

CONNECTION ANGLES

The use of the Standard Web Connection Angle for supporting the end reactions of beams and girders is based on the assumption that the beam or girder has been proportioned, and will act as a simple beam. If uniformly loaded a simple beam has its maximum bending moment and deflection at the center of the span.

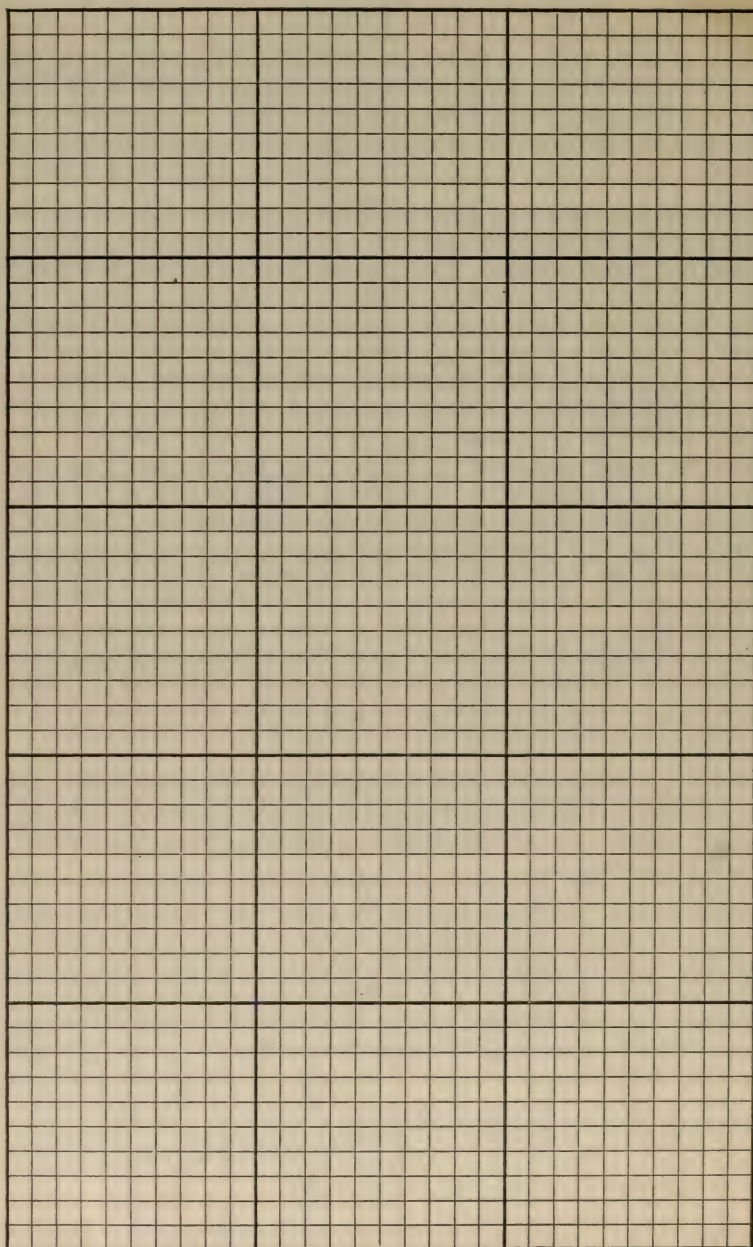
The deflection curve for a uniformly loaded simple span beam is a parabola, and where it supports a plastered ceiling the maximum deflection due to live load is limited to $1/360$ of the span. The maximum bending moment of a uniformly loaded simple span beam occurs at the center. The maximum bending moment of a uniformly loaded fixed end beam occurs at the supports and is double the moment of the fixed end span at the center. For beams with the same loading and the same length of span the maximum bending moment of the fixed end beam is two-thirds of the maximum moment of the simple span beam. It is obviously impossible to consider a pair of web connection angles capable of changing the simple span beam to one with fixed ends. Where there is a deflection of $1/360$ of the span due to uniform loading, the ends of the beam will no longer be perpendicular to the original axis of the beam, but will move through an angle of about $0^{\circ} 38'$, causing bending in the outstanding legs of the connection angles between the rivets and the heel of the angles. This movement in the outstanding legs of the angles will be the same for all thicknesses of angles so long as the beam acts as a simple span, and the unit stress resulting from this bending in the angles will be proportional to the thickness of the material which is bent. That is, the relative unit stresses in angles $\frac{3}{8}"$ thick and $\frac{1}{2}"$ thick is as 3 is to 4, and, for the same deflection, the unit stress in a $\frac{1}{2}"$ angle is 1.33 times the unit stress in a $\frac{3}{8}"$ angle.

The proper thickness for connection angles for simple spans is therefore the minimum which will develop the bearing value of the rivets used in shear. For $\frac{3}{4}"$ power driven rivets this thickness is between $\frac{5}{16}"$ and $\frac{3}{8}"$, and the $\frac{3}{8}"$ thickness is therefore used.

It has been the standard of the industry to keep the center to center distance between rivets in the outstanding angle legs $5\frac{1}{2}"$ by varying the gage in the outstanding legs of the angles to offset the different thickness of beam webs. This variation in the outstanding leg gage is by sixteenths of an inch, which is so inconspicuous in angles with equal legs that in shop assembling the web leg and the outstanding leg are often interchanged unless extreme care is used, resulting in errors which are expensive to correct in the field. To obviate this and speed up shop assembling, the standard connection is made $4" \times 3\frac{1}{2}" \times \frac{3}{8}"$ with the $3\frac{1}{2}"$ leg and a $2\frac{1}{4}"$ gage always on the beam web. The $2\frac{1}{4}"$ gage in the leg against the web is sufficient to permit ignoring the allowable cutting tolerance of $\frac{3}{8}"$ over or under the ordered length of the beam.

The $4" \times 3\frac{1}{2}" \times \frac{3}{8}"$ is a more desirable angle for stock as it is more adaptable to other uses than the $4" \times 4" \times \frac{1}{2}"$ angle previously used.

NOTES and DIAGRAMS



Part IV

Section 2

Angles

Dimensions and Technical Functions

Tensile Values

Allowable Total Loads

by


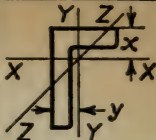
A. I. S. C. Specification

for

One Angle Struts

Two Angle Struts

Angles used as Beams

	STANDARD ANGLES																	
	SIZES					AREAS												
	TECHNICAL FUNCTIONS																	
	Size in Inches	Thick- ness	Weight per Foot	Area in Sq. In.	AXES													
					X - X				Y - Y				Z - Z					
					l	S	r	x	l	S	r	y	r					
★ 1¾ × 1¾		⅛	1.44	0.42	0.13	0.10	0.55	0.48	0.35				
		⅜	2.12	0.62	0.18	0.14	0.54	0.51	0.34				
		½	2.77	0.81	0.23	0.19	0.53	0.53	0.34				
		⅝	1.65	0.48	0.19	0.13	0.63	0.55	0.40				
★ 2 × 2		⅜	2.44	0.72	0.27	0.19	0.62	0.57	0.39				
		½	3.19	0.94	0.35	0.25	0.61	0.59	0.39				
		⅝	3.92	1.15	0.42	0.30	0.60	0.61	0.39				
		¾	1.86	0.55	0.35	0.20	0.80	0.74	0.20	0.13	0.61	0.49	0.43					
★ 2½ × 2		⅜	2.75	0.81	0.51	0.29	0.79	0.76	0.29	0.20	0.60	0.51	0.43					
		½	3.62	1.06	0.65	0.38	0.78	0.79	0.37	0.25	0.59	0.54	0.42					
		⅝	4.50	1.31	0.79	0.47	0.78	0.81	0.45	0.31	0.58	0.56	0.42					
		¾	2.08	0.61	0.38	0.20	0.79	0.67	0.50				
★ 2½ × 2½		⅜	3.07	0.90	0.55	0.30	0.78	0.69	0.49				
		½	4.1	1.19	0.70	0.39	0.77	0.72	0.49				
		⅝	5.0	1.47	0.85	0.48	0.76	0.74	0.49				
		¾	5.9	1.73	0.98	0.57	0.75	0.76	0.48				
3 × 2½		⅛	4.5	1.31	1.17	0.56	0.95	0.91	0.74	0.40	0.75	0.66	0.53					
		⅜	5.6	1.62	1.42	0.69	0.94	0.93	0.90	0.49	0.74	0.68	0.53					
		½	6.6	1.92	1.66	0.81	0.93	0.96	1.04	0.58	0.74	0.71	0.52					
		⅝	7.6	2.22	1.88	0.93	0.92	0.98	1.18	0.66	0.73	0.73	0.52					
3 × 3		⅛	4.9	1.44	1.24	0.58	0.93	0.84	0.59				
		⅜	6.1	1.78	1.51	0.71	0.92	0.87	0.59				
		½	7.2	2.11	1.76	0.83	0.91	0.89	0.58				
		⅝	8.3	2.43	1.99	0.95	0.91	0.91	0.58				
3½ × 2½		½	9.4	2.75	2.22	1.07	0.90	0.93	0.58				
		⅜	4.9	1.44	1.80	0.75	1.12	1.11	0.78	0.41	0.74	0.61	0.54					
		⅝	6.1	1.78	2.19	0.93	1.11	1.14	0.94	0.50	0.73	0.64	0.54					
		¾	7.2	2.11	2.56	1.09	1.10	1.16	1.09	0.59	0.72	0.66	0.54					
3½ × 3½		⅝	8.3	2.43	2.91	1.26	1.09	1.18	1.23	0.68	0.71	0.68	0.54					
		¾	9.4	2.75	3.24	1.41	1.09	1.20	1.36	0.76	0.70	0.70	0.53					
		⅝	7.2	2.09	2.45	0.98	1.08	0.99	0.69				
		¾	8.5	2.48	2.87	1.15	1.07	1.01	0.68				
4 × 3		¾	9.8	2.87	3.26	1.32	1.07	1.04	0.68				
		⅝	11.1	3.25	3.64	1.49	1.06	1.06	0.68				
		¾	12.4	3.62	3.99	1.65	1.05	1.08	0.68				
		⅝	13.6	3.98	4.33	1.81	1.04	1.10	0.68				
4 × 3½		⅝	7.2	2.09	3.38	1.23	1.27	1.26	1.65	0.73	0.89	0.76	0.65					
		¾	8.5	2.48	3.96	1.46	1.26	1.28	1.92	0.87	0.88	0.78	0.64					
		¾	9.8	2.87	4.52	1.68	1.25	1.30	2.18	0.99	0.87	0.80	0.64					
		½	11.1	3.25	5.05	1.89	1.25	1.33	2.42	1.12	0.86	0.83	0.64					
4 × 4		½	12.4	3.62	5.55	2.09	1.24	1.35	2.66	1.23	0.86	0.85	0.64					
		⅝	13.6	3.98	6.03	2.30	1.23	1.37	2.87	1.35	0.85	0.87	0.64					
		⅝	7.7	2.25	3.56	1.26	1.26	1.18	2.55	0.99	1.07	0.93	0.73					
		¾	9.1	2.67	4.18	1.49	1.25	1.21	2.99	1.17	1.06	0.96	0.73					
5 × 3		¾	10.6	3.09	4.76	1.72	1.24	1.23	3.40	1.35	1.05	0.98	0.72					
		½	11.9	3.50	5.32	1.94	1.23	1.25	3.79	1.52	1.04	1.00	0.72					
		⅝	13.3	3.90	5.86	2.15	1.23	1.27	4.17	1.68	1.03	1.02	0.72					
		¾	14.7	4.30	6.37	2.35	1.22	1.29	4.49	1.83	1.02	1.04	0.72					
5 × 3½		¾	16.0	4.68	6.86	2.56	1.21	1.32	4.86	2.00	1.02	1.07	0.72					
		⅝	17.3	5.06	7.32	2.75	1.20	1.34	5.18	2.15	1.01	1.09	0.72					
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 4		¾	11.3	3.31	4.97	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 4½		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 5		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 5½		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 6		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 6½		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 7		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 8		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 9		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 10		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 11		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 12		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 14		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21	1.21	0.78				
		¾	15.7	4.61	6.66	2.40	1.20	1.23	0.77				
5 × 16		¾	17.1	5.03	7.17	2.61	1.19	1.25	0.77				
		⅝	18.5	5.44	7.66	2.81	1.19	1.27	0.77				
		¾	8.2	2.40	3.71	1.29	1.24	1.12	0.79				
		⅝	9.8	2.86	4.36	1.52	1.23	1.14	0.79				
5 × 18		¾	11.3	3.31	4.94	1.75	1.23	1.16	0.78				
		½	12.8	3.75	5.56	1.97	1.22	1.18	0.78				
		⅝	14.3	4.18	6.12	2.19	1.21											

STANDARD ANGLES

SIZES
WEIGHTS — AREAS
TECHNICAL FUNCTIONS



Size in Inches	Thick- ness	Weight per Foot	Area in Sq. In.	AXES											
				X - X				Y - Y				Z - Z			
				l	S	r	x	l	S	r	y	l	S	r	z
5 × 3½	5/16	8.7	2.56	6.60	1.94	1.61	1.59	2.72	1.02	1.03	0.84	0.77			
	3/8	10.4	3.05	7.78	2.29	1.60	1.61	3.18	1.21	1.02	0.86	0.76			
	7/16	12.0	3.53	8.90	2.64	1.59	1.63	3.63	1.39	1.01	0.88	0.76			
	1/2	13.6	4.00	9.99	2.99	1.58	1.66	4.05	1.56	1.01	0.91	0.75			
	9/16	15.2	4.47	11.03	3.32	1.57	1.68	4.45	1.73	1.00	0.93	0.75			
	5/8	16.8	4.92	12.03	3.65	1.56	1.70	4.83	1.90	0.99	0.95	0.75			
	11/16	18.3	5.37	12.99	3.97	1.56	1.72	5.20	2.06	0.98	0.97	0.75			
	3/4	19.8	5.81	13.92	4.28	1.55	1.75	5.55	2.22	0.98	1.00	0.75			
	7/8	21.3	6.25	14.83	4.59	1.54	1.77	5.89	2.37	0.97	1.01	0.75			
	1	22.8	6.68	15.72	4.89	1.53	1.79	6.22	2.51	0.96	1.02	0.75			
6 × 3½	3/8	11.7	3.42	12.86	3.24	1.94	2.04	3.34	1.23	0.99	0.79	0.77			
	7/16	13.5	3.97	14.76	3.75	1.93	2.06	3.81	1.41	0.98	0.81	0.76			
	1/2	15.3	4.50	16.59	4.24	1.92	2.08	4.25	1.59	0.97	0.83	0.76			
	9/16	17.1	5.03	18.37	4.72	1.91	2.11	4.67	1.77	0.96	0.86	0.75			
	5/8	18.9	5.55	20.08	5.19	1.90	2.13	5.08	1.94	0.96	0.88	0.75			
	11/16	20.6	6.06	21.74	5.65	1.89	2.15	5.47	2.11	0.95	0.90	0.75			
	3/4	22.4	6.56	23.34	6.10	1.89	2.18	5.84	2.27	0.94	0.93	0.75			
	13/16	24.0	7.06	24.89	6.55	1.88	2.20	6.20	2.43	0.94	0.95	0.75			
	7/8	25.7	7.55	26.39	6.98	1.87	2.22	6.55	2.59	0.93	0.97	0.75			
	1	27.4	8.03	27.83	7.39	1.86	2.24	6.89	2.74	0.92	0.99	0.75			
6 × 4	3/8	12.3	3.61	13.47	3.32	1.93	1.94	4.90	1.60	1.17	0.94	0.88			
	7/16	14.3	4.18	15.46	3.83	1.92	1.96	5.60	1.85	1.16	0.96	0.87			
	1/2	16.2	4.75	17.40	4.33	1.91	1.99	6.27	2.08	1.15	0.99	0.87			
	9/16	18.1	5.31	19.26	4.83	1.90	2.01	6.91	2.31	1.14	1.01	0.87			
	5/8	20.0	5.86	21.07	5.31	1.90	2.03	7.52	2.54	1.13	1.03	0.86			
	11/16	21.8	6.40	22.82	5.78	1.89	2.06	8.11	2.76	1.13	1.06	0.86			
	3/4	23.6	6.94	24.51	6.25	1.88	2.08	8.68	2.97	1.12	1.08	0.86			
	13/16	25.4	7.47	26.15	6.70	1.87	2.10	9.23	3.18	1.11	1.10	0.86			
	7/8	27.2	7.98	27.73	7.15	1.86	2.12	9.75	3.39	1.11	1.12	0.86			
	1	29.0	8.48	29.26	7.58	1.85	2.14	10.26	3.59	1.10	1.14	0.86			
6 × 6	3/8	14.9	4.36	15.39	3.53	1.88	1.64	1.19			
	7/16	17.2	5.06	17.68	4.07	1.87	1.66	1.19			
	1/2	19.6	5.75	19.91	4.61	1.86	1.68	1.18			
	9/16	21.9	6.43	22.07	5.14	1.85	1.71	1.18			
	5/8	24.2	7.11	24.16	5.66	1.84	1.73	1.17			
	11/16	26.5	7.78	26.19	6.17	1.83	1.75	1.17			
	3/4	28.7	8.44	28.15	6.66	1.83	1.78	1.17			
	13/16	31.0	9.09	30.06	7.15	1.82	1.80	1.17			
	7/8	33.1	9.73	31.92	7.63	1.81	1.82	1.16			
	15/16	35.3	10.37	33.72	8.11	1.80	1.84	1.16			
1	37.4	11.00	35.46	8.57	1.80	1.86	1.16				
7 × 3½	3/8	13.0	3.80	19.62	4.34	2.27	2.48	3.47	1.25	0.96	0.73	0.76			
	7/16	15.0	4.40	22.56	5.01	2.26	2.50	3.95	1.44	0.95	0.75	0.76			
	1/2	17.0	5.00	25.41	5.68	2.25	2.53	4.41	1.62	0.94	0.78	0.75			
	9/16	19.1	5.59	28.18	6.34	2.25	2.55	4.86	1.80	0.93	0.80	0.75			
	5/8	21.0	6.17	30.86	6.96	2.24	2.57	5.28	1.97	0.93	0.82	0.75			
	11/16	23.0	6.75	33.47	7.60	2.23	2.60	5.69	2.14	0.92	0.85	0.74			
	3/4	24.9	7.31	35.99	8.22	2.22	2.62	6.08	2.31	0.91	0.87	0.74			
	13/16	26.8	7.87	38.45	8.83	2.21	2.64	6.46	2.48	0.91	0.89	0.74			
	7/8	28.7	8.42	40.82	9.42	2.20	2.66	6.83	2.64	0.90	0.91	0.74			
	15/16	30.5	8.97	43.13	10.00	2.19	2.69	7.18	2.80	0.89	0.94	0.74			
1	32.3	9.50	45.37	10.58	2.19	2.71	7.53	2.96	0.89	0.96	0.74				
8 × 6	7/16	20.2	5.93	39.23	7.07	2.57	2.45	19.25	4.23	1.80	1.45	1.30			
	1/2	23.0	6.75	44.31	8.02	2.56	2.47	21.68	4.79	1.79	1.47	1.30			
	9/16	25.7	7.56	49.26	8.95	2.55	2.50	24.04	5.34	1.78	1.50	1.30			
	5/8	28.5	8.36	54.10	9.87	2.54	2.52	26.33	5.88	1.77	1.52	1.29			
	11/16	31.2	9.15	58.82	10.77	2.54	2.54	28.56	6.40	1.77	1.54	1.29			
	3/4	33.8	9.94	63.42	11.67	2.53	2.56	30.72	6.92	1.76	1.56	1.28			
	13/16	36.5	10.72	67.92	12.55	2.52	2.59	32.82	7.44	1.75	1.59	1.28			
	7/8	39.1	11.48	72.32	13.41	2.51	2.61	34.86	7.94	1.74	1.61	1.28			
	15/16	41.7	12.25	76.59	14.27	2.50	2.63	36.85	8.43	1.73	1.63	1.28			
	1	44.2	13.00	80.78	15.11	2.49	2.65	38.78	8.92	1.73	1.65	1.28			
8 × 8	1/2	26.4	7.75	48.65	8.37	2.51	2.19	1.59			
	9/16	29.6	8.68	54.09	9.34	2.50	2.21	1.58			
	5/8	32.7	9.61	59.43	10.30	2.49	2.23	1.58			
	11/16	35.8	10.53	64.64	11.25	2.48	2.25	1.58			
	3/4	38.9	11.44	69.74	12.18	2.47	2.28	1.57			
	13/16	42.0	12.34	74.72	13.11	2.46	2.30	1.57			
	7/8	45.0	13.23	79.58	14.02	2.45	2.32	1.56			
	15/16	48.1	14.12	84.34	14.91	2.44	2.34	1.56			
	1	51.0	15.00	88.98	15.80	2.44	2.37	1.56			
	1 1/16	54.0	15.87	93.53	16.67	2.43	2.39	1.56			
1 1/8	56.9	16.73	97.97	17.53	2.42	2.41	1.55				

STANDARD
ANGLES

NET AREAS AND TENSILE VALUES OF ONE ANGLE IN KIPS
TENSION AT 18000 POUNDS PER SQUARE INCH
TO DEVELOP VALUES BELOW, ANGLES MUST BE ATTACHED BY BOTH LEGS

Size in Inches	Thick- ness	1/2" RIVET		5/8" RIVET		3/4" RIVET				7/8" RIVET			
		1 HOLE OUT		1 HOLE OUT		1 HOLE OUT		2 HOLES OUT		1 HOLE OUT		2 HOLES OUT	
		Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value
★ 1 3/4 × 1 3/4	1/8 3/16 1/4	.342 .503 .654	6.16 9.05 11.77										
★ 2 × 2	1/8 3/16 1/4 5/16	.402 .593 .784 .955	7.24 10.67 14.11 17.19	.386 .569 .752 .916	6.95 10.24 13.54 16.49								
★ 2 1/2 × 2	1/8 3/16 1/4 5/16	.472 .693 .904 1.115	8.50 12.47 16.27 20.07	.456 .669 .872 1.076	8.21 12.04 15.70 19.37	.646 .841 1.037	11.63 15.14 18.66						
★ 2 1/2 × 2 1/2	1/8 3/16 1/4 5/16 3/8	.532 .783 1.034 1.275 1.496	9.58 14.09 18.61 22.95 26.93	.516 .759 1.002 1.236 1.448	9.29 13.66 18.04 22.25 26.06	.736 .971 1.197 1.402	13.25 17.48 21.55 25.24	.572 .752 .924 1.074	10.30 13.54 16.63 19.33				
3 × 2 1/2	1/4 5/16 3/8 7/16	1.154 1.425 1.686 1.937	20.77 25.65 30.35 34.87	1.122 1.386 1.638 1.882	20.20 24.95 29.48 33.88	1.091 1.347 1.592 1.827	19.64 24.25 28.66 32.89	.872 1.074 1.264 1.444	15.70 19.33 22.75 25.99				
3 × 3	1/4 5/16 3/8 7/16 1/2	1.252 1.546 1.828 2.102 2.375	22.54 27.83 32.90 37.84 42.75	1.221 1.507 1.782 2.047 2.312	21.98 27.13 32.08 36.85 41.62	1.002 1.234 1.454 1.664 1.875	18.04 22.21 26.17 29.95 33.75				
3 1/2 × 2 1/2	1/4 5/16 3/8 7/16 1/2	1.252 1.546 1.828 2.102 2.375	22.54 27.83 32.90 37.84 42.75	1.221 1.507 1.782 2.047 2.312	21.98 27.13 32.08 36.85 41.62	1.002 1.234 1.454 1.664 1.875	18.04 22.21 26.17 29.95 33.75				
3 1/2 × 3 1/2	5/16 3/8 7/16 1/2 9/16 5/8	1.817 2.152 2.487 2.812 3.128 3.433	32.71 38.74 44.77 50.62 56.30 61.79	1.544 1.824 2.104 2.375 2.636 2.886	27.79 32.83 37.87 42.75 47.45 51.95	1.777 2.105 2.432 2.750 3.057 3.355	31.99 37.89 43.78 49.50 55.03 60.39	1.466 1.730 1.994 2.250 2.494 2.730	26.39 31.14 35.89 40.50 44.89 49.14
4 × 3	5/16 3/8 7/16 1/2 9/16 5/8	1.817 2.152 2.487 2.812 3.128 3.433	32.71 38.74 44.77 50.62 56.30 61.79	1.544 1.824 2.104 2.375 2.636 2.886	27.79 32.83 37.87 42.75 47.45 51.95	1.777 2.105 2.432 2.750 3.057 3.355	31.99 37.89 43.78 49.50 55.03 60.39	1.466 1.730 1.994 2.250 2.494 2.730	26.39 31.14 35.89 40.50 44.89 49.14
4 × 3 1/2	5/16 3/8 7/16 1/2 9/16 5/8 11/16 3/4	1.977 2.342 2.707 3.062 3.408 3.753 4.078 4.404	35.59 42.16 48.73 55.12 61.34 67.55 73.40 79.27	1.704 2.014 2.324 2.624 2.916 3.206 3.476 3.748	30.67 36.25 41.83 47.23 52.49 57.71 62.57 67.46	1.938 2.295 2.652 3.000 3.337 3.675 3.992 4.310	34.88 41.31 47.74 54.00 60.07 66.15 71.86 77.58	1.626 1.920 2.214 2.500 2.774 3.050 3.304 3.560	29.27 34.56 39.85 45.00 49.93 54.90 59.47 64.08
4 × 4	5/16 3/8 7/16 1/2 9/16 5/8 11/16 3/4	2.127 2.532 2.927 3.312 3.688 4.063 4.428 4.784	38.29 45.58 52.69 59.62 66.38 73.13 79.70 86.11	1.854 2.204 2.544 2.874 3.196 3.516 3.826 4.128	33.37 39.67 45.79 51.73 57.53 63.29 68.87 74.30	2.087 2.485 2.872 3.250 3.617 3.985 4.342 4.690	37.57 44.73 51.70 58.50 65.11 71.73 78.16 84.42	1.774 2.110 2.434 2.750 3.054 3.360 3.654 3.940	31.93 37.98 43.81 49.50 54.97 60.48 65.77 70.92
5 × 3	5/16 3/8 7/16 1/2 9/16 5/8 11/16 3/4	2.127 2.532 2.927 3.312 3.688 4.063 4.428 4.784	38.29 45.58 52.69 59.62 66.38 73.13 79.70 86.11	1.854 2.204 2.544 2.874 3.196 3.516 3.826 4.128	33.37 39.67 45.79 51.73 57.53 63.29 68.87 74.30	2.087 2.485 2.872 3.250 3.617 3.985 4.342 4.690	37.57 44.73 51.70 58.50 65.11 71.73 78.16 84.42	1.775 2.110 2.435 2.750 3.055 3.360 3.655 3.940	31.95 37.98 43.83 49.50 54.99 60.48 65.79 70.92

★Angles are classified as in Bar Size when their greatest dimension is less than 3 inches.

NET AREAS AND TENSILE VALUES OF ONE ANGLE IN KIPS

TENSION AT 18000 POUNDS PER SQUARE INCH

TO DEVELOP VALUES BELOW, ANGLES MUST BE ATTACHED BY BOTH LEGS

STANDARD
ANGLES

Size in Inches	Thick- ness	¾" RIVET				½" RIVET				1" RIVET			
		1 HOLE OUT		2 HOLES OUT		1 HOLE OUT		2 HOLES OUT		1 HOLE OUT		2 HOLES OUT	
		Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value	Net Area	Tens. Value
5 × 3½	5/16	2.287	41.17	2.014	36.25	2.248	40.46	1.936	34.85				
	3/8	2.722	49.00	2.394	43.09	2.675	48.15	2.300	41.40				
	7/16	3.147	56.65	2.764	49.75	3.092	55.66	2.654	47.77				
	1/2	3.562	64.12	3.124	56.23	3.500	63.00	3.000	54.00				
	9/16	3.978	71.60	3.486	62.75	3.907	70.33	3.344	60.19				
	11/16	4.373	78.71	3.826	68.87	4.295	77.31	3.670	66.06				
6 × 3½	3/8	4.768	85.82	4.166	74.99	4.682	84.28	3.994	71.89				
	7/16	5.154	92.77	4.498	80.96	5.060	91.08	4.310	77.58				
	1/2	3.092	55.66	2.764	49.75	3.045	54.81	2.670	48.06				
	5/8	3.587	64.57	3.204	57.67	3.532	63.58	3.095	55.71				
	3/4	4.062	73.12	3.624	65.23	4.000	72.00	3.500	63.00				
	7/8	4.538	81.68	4.046	72.83	4.467	80.41	3.905	70.29				
6 × 4	5/16	5.003	90.05	4.456	80.21	4.925	88.65	4.300	77.40				
	3/8	5.458	98.24	4.856	87.41	5.372	96.70	4.685	84.33				
	7/16	5.904	106.27	5.248	94.46	5.810	104.58	5.060	91.08				
	1/2	6.349	114.28	5.638	101.48	6.247	112.45	5.435	97.83				
	5/8	6.784	122.11	6.018	108.32	6.675	120.15	5.800	104.40				
	3/4	3.282	59.08	2.954	53.17	3.235	58.23	2.860	51.48	3.188	57.38	2.766	49.79
6 × 6	7/16	3.797	68.35	3.414	61.45	3.742	67.36	3.304	59.47	3.688	66.38	3.196	57.53
	1/2	4.312	77.62	3.874	69.73	4.250	76.50	3.750	67.50	4.187	75.37	3.624	65.23
	5/8	4.818	86.72	4.326	77.87	4.747	85.45	4.184	75.31	4.677	84.19	4.044	72.79
	3/4	5.313	95.63	4.766	85.79	5.235	94.23	4.610	82.98	5.157	92.84	4.454	80.17
	7/8	5.798	104.36	5.196	93.53	5.712	102.82	5.024	90.43	5.627	101.29	4.854	87.37
	1	6.284	113.11	5.628	101.30	6.190	111.42	5.440	97.92	6.096	109.73	5.252	94.54
7 × 3½	5/16	6.759	121.66	6.048	108.86	6.657	119.83	5.844	105.19	6.556	118.01	5.642	101.56
	3/8	7.214	129.85	6.448	116.06	7.105	127.89	6.230	112.14	6.996	125.93	6.012	108.22
	7/16	4.032	72.58	3.704	66.67	3.985	71.73	3.610	64.98	3.938	70.88	3.516	63.29
	1/2	4.677	84.19	4.294	77.29	4.622	83.20	4.184	75.31	4.568	82.22	4.076	73.37
	5/8	5.312	95.62	4.874	87.73	5.250	94.50	4.750	85.50	5.187	93.37	4.624	83.23
	3/4	5.938	106.88	5.446	98.03	5.867	105.61	5.304	95.47	5.797	104.35	5.164	92.95
7 × 4	7/8	6.563	118.13	6.016	108.29	6.485	116.73	5.860	105.48	6.407	115.33	5.704	102.67
	1	7.178	129.20	6.576	118.37	7.092	127.66	6.404	115.27	7.007	126.13	6.234	112.21
	5/16	7.784	140.11	7.128	128.30	7.690	138.42	6.940	124.92	7.596	136.73	6.752	121.54
	3/8	8.379	150.82	7.668	138.02	8.277	148.99	7.464	134.35	8.176	147.17	7.262	130.72
	7/16	8.964	161.35	8.198	147.56	8.855	159.39	7.980	143.64	8.746	157.43	7.762	139.72
	1/2	9.547	172.50	8.682	156.88	8.562	168.78	8.494	152.89	9.315	167.67	8.260	148.68
8 × 3½	5/8	10.121	183.59	9.146	165.83	9.027	177.81	8.000	162.00	9.875	177.75	8.750	157.50
	3/4	3.472	62.50	3.144	56.59	3.425	61.65	3.050	54.90	3.378	60.80	2.956	53.21
	7/16	4.017	72.31	3.634	65.41	3.962	71.32	3.524	63.43	3.908	70.34	3.416	61.49
	1/2	4.562	82.12	4.124	74.23	4.500	81.00	4.000	72.00	4.437	79.87	3.874	69.73
	5/8	5.098	91.76	4.606	82.91	5.027	90.49	4.464	80.35	4.957	89.23	4.324	77.83
	3/4	5.623	101.21	5.076	91.37	5.545	99.81	4.920	88.56	5.467	98.41	4.764	85.75
8 × 4	7/8	6.148	110.66	5.546	99.83	6.062	109.12	5.374	96.73	5.977	107.59	5.204	93.67
	1	6.654	119.77	5.998	107.96	6.560	118.08	5.810	104.58	6.466	116.39	5.622	101.20
	5/16	7.159	128.86	6.448	116.06	7.057	127.03	6.244	112.39	6.956	125.21	6.042	108.76
	3/8	7.654	137.77	6.888	123.98	7.545	135.81	6.670	120.06	7.436	133.85	6.452	116.14
	7/16	8.148	146.88	7.282	130.98	7.167	140.88	6.292	126.29	7.184	140.88	6.312	122.49
	1/2	8.642	156.00	7.766	140.88	7.685	148.88	6.810	134.10	7.696	148.88	6.810	134.10
8 × 6	5/8	9.136	165.83	8.146	147.56	8.062	155.62	7.170	134.10	8.080	148.88	7.170	134.10
	3/4	9.630	175.00	8.618	156.88	8.537	164.88	7.644	140.88	8.562	156.88	7.644	140.88
	7/8	10.121	183.59	9.146	165.83	9.027	177.81	8.000	162.00	9.875	177.75	8.750	157.50
	1	10.615	192.77	9.612	175.00	9.527	184.00	8.500	170.00	10.375	184.00	9.250	170.00
	5/16	7.312	131.62	6.674	123.73	7.250	130.50	6.750	121.50	7.187	129.37	6.624	119.23
	3/8	8.188	147.38	7.496	138.53	8.117	146.11	7.554	135.97	8.047	144.85	7.414	133.45
8 × 8	7/16	9.063	163.13	8.316	153.29	8.985	161.73	8.360	150.48	8.907	160.33	8.204	147.67
	1/2	9.928	178.70	9.162	167.87	9.842	177.16	9.154	164.77	9.757	175.63	8.984	161.71
	5/8	10.784	194.11	10.128	182.30	10.690	192.42	9.940	178.92	10.596	190.73	9.752	175.54
	3/4	11.629	209.32	10.918	196.52	11.527	207.49	10.714	192.85	11.426	205.67	10.512	189.22
	7/8	12.464	224.35	11.698	210.56	12.355	222.39	11.480	206.64	12.246	220.43	11.262	202.72
	1	13.300	239.38	12.532	224.67	13.182	237.28	12.244	220.39	13.065	235.17	12.010	216.18



STRUTS OF ONE ANGLE

ALLOWABLE CONCENTRIC LOADS IN KIPS

Values given are for Least Radius of Gyration which is about Axis Z-Z.
Loads to right of heavy vertical line are for Secondary Members ONLY.

Size in Inches	Thick-ness	Weight per foot	Area in Sq. In.	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET											
					2	3	4	5	6	7	8	9	10	11	12	
1 3/4 x 1 3/4	1/8	1.44	0.42	0.35	6.0	4.8	3.7	2.9								
	3/16	2.12	0.62	0.34	8.7	6.9	5.3	4.1								
	1/4	2.77	0.81	0.34	11.4	9.0	6.9	5.3								
2 x 2	1/8	1.65	0.48	0.40	7.2	6.0	4.8	3.8	3.1							
	3/16	2.44	0.72	0.39	10.7	8.8	7.0	5.7	4.5							
	1/4	3.19	0.94	0.39	14.0	11.5	9.2	7.4	5.8							
	5/16	3.92	1.15	0.39	17.1	14.1	11.2	9.1	7.2							
2 1/2 x 2	1/8	1.86	0.55	0.43	8.3	7.1	5.8	4.8	3.9	3.2						
	3/16	2.75	0.81	0.43	12.2	10.5	8.6	7.0	5.7	4.7						
	1/4	3.62	1.06	0.42	15.9	13.5	11.1	8.9	7.2	5.9						
	5/16	4.50	1.31	0.42	19.7	16.7	13.7	11.0	8.9	7.3						
2 1/2 x 2 1/2	1/8	2.08	0.61	0.50	9.2	8.5	7.3	6.1	5.1	4.3	3.6					
	3/16	3.07	0.90	0.49	13.5	12.5	10.6	8.8	7.4	6.1	5.2					
	1/4	4.1	1.19	0.49	17.9	16.5	14.0	11.7	9.7	8.1	6.8					
	5/16	5.0	1.47	0.49	22.1	20.4	17.3	14.4	12.0	10.0	8.5					
	3/8	5.9	1.73	0.48	26.0	23.7	20.0	16.7	13.8	11.5						
3 x 2 1/2	1/4	4.5	1.31	0.53	19.7	18.8	16.2	13.8	11.6	9.8	8.4					
	5/16	5.6	1.62	0.53	24.3	23.2	20.0	17.0	14.4	12.2	10.3					
	3/8	6.6	1.92	0.52	28.8	27.3	23.4	19.9	16.7	14.1	11.9					
	7/16	7.6	2.22	0.52	33.3	31.6	27.1	23.0	19.4	16.3	13.8					
3 x 3	1/4	4.9	1.44	0.59	21.6	21.5	19.0	16.5	14.2	12.2	10.5	9.1				
	3/8	6.1	1.78	0.59	26.7	26.5	23.4	20.3	17.5	15.1	13.0	11.2				
	7/16	7.2	2.11	0.58	31.7	31.3	27.5	23.8	20.5	17.5	15.1	13.0				
	1/2	8.3	2.43	0.58	36.5	36.0	31.7	27.4	23.6	20.2	17.4	14.9				
	1/2	9.4	2.75	0.58	41.3	40.8	35.9	31.0	26.7	22.9	19.6	16.9				
3 1/2 x 2 1/2	1/4	4.9	1.44	0.54	21.6	20.8	18.0	15.4	13.0	11.1	9.4	8.0				
	3/8	6.1	1.78	0.54	26.7	26.7	22.3	19.0	16.1	13.7	11.6	9.9				
	7/16	7.2	2.11	0.54	31.7	30.4	26.4	22.5	19.1	16.2	13.8	11.8				
	1/2	8.3	2.43	0.54	36.5	35.1	30.4	26.0	22.0	18.7	15.9	13.6				
	1/2	9.4	2.75	0.53	41.3	39.4	34.0	28.9	24.4	20.7	17.5					
3 1/2 x 3 1/2	5/16	7.2	2.09	0.69	31.4	31.4	29.6	26.5	23.4	20.6	18.1	15.9	14.0	12.4		
	3/8	8.5	2.48	0.68	37.2	37.2	35.0	31.2	27.5	24.2	21.2	18.6	16.3	14.4		
	7/16	9.8	2.87	0.68	43.1	43.1	40.5	36.1	31.8	28.0	24.5	21.5	18.9	16.7		
	1/2	11.1	3.25	0.68	48.8	48.8	45.8	40.9	36.0	31.7	27.8	24.4	21.4	18.9		
	5/8	12.4	3.62	0.68	54.3	54.3	51.0	45.5	40.1	35.3	30.9	27.2	23.9	21.1		
4 x 3	5/8	13.6	3.98	0.68	59.7	59.7	56.1	50.0	44.1	38.8	34.0	29.9	26.2	23.2		
	5/16	7.2	2.09	0.65	31.4	31.4	28.9	25.5	22.4	19.5	17.0	14.8	13.0			
	3/8	8.5	2.48	0.64	37.2	37.2	34.0	30.0	26.2	22.8	19.8	17.3	15.1			
	7/16	9.8	2.87	0.64	43.1	43.1	39.4	34.7	30.3	26.4	23.0	20.0	17.5			
	1/2	11.1	3.25	0.64	48.8	48.8	44.6	39.3	34.4	29.9	26.0	22.7	19.8			
4 x 3 1/2	1/2	12.4	3.62	0.64	54.3	54.3	49.6	43.8	38.3	33.3	29.0	25.2	22.1			
	5/8	13.6	3.98	0.64	59.7	59.7	54.6	48.1	42.1	36.6	31.8	27.7	24.3			
	5/16	7.7	2.25	0.73	33.8	33.8	32.6	29.5	26.3	23.3	20.7	18.3	16.2	14.4	12.8	
	3/8	9.1	2.67	0.73	40.1	40.1	38.7	35.0	31.2	27.7	24.5	21.7	19.2	17.1	15.2	
	7/16	10.6	3.09	0.72	46.4	46.4	44.6	40.1	35.8	31.7	28.0	24.7	21.9	19.4	17.2	
	1/2	11.9	3.50	0.72	52.5	52.5	50.5	45.5	40.5	35.9	31.7	28.0	24.8	22.0	19.5	
	5/8	13.3	3.90	0.72	58.5	58.5	56.3	50.7	45.1	40.0	35.3	31.2	27.6	24.5	21.8	
4 x 4	5/8	14.7	4.30	0.72	64.5	64.5	62.1	55.9	49.8	44.1	39.0	34.4	30.4	27.0	24.0	
	1 1/16	16.0	4.68	0.72	70.2	70.2	67.6	60.8	54.1	48.0	42.4	37.4	33.1	29.4	26.1	
	3/4	17.3	5.06	0.72	75.9	75.9	73.1	65.7	58.5	51.9	45.8	40.5	35.8	31.8	28.2	
	5/16	8.2	2.40	0.79	36.0	36.0	35.9	32.7	29.6	26.5	23.7	21.2	18.9	16.9	15.2	
	3/8	9.8	2.86	0.79	42.9	42.9	42.7	39.0	35.2	31.6	28.3	25.3	22.6	20.2	18.1	
	7/16	11.3	3.31	0.78	49.7	49.7	49.2	44.9	40.4	36.2	32.3	28.9	25.7	23.0	20.6	
	1/2	12.8	3.75	0.78	56.3	56.3	55.8	50.8	45.8	41.1	36.6	32.7	29.1	26.1	23.3	
5 x 3	5/16	14.3	4.18	0.78	62.7	62.7	62.2	56.6	51.1	45.8	40.8	36.4	32.5	29.1	26.0	
	3/8	15.7	4.61	0.77	69.2	69.2	68.2	62.1	55.9	50.0	44.5	39.6	35.3	31.5	28.2	
	7/16	17.1	5.03	0.77	75.5	75.5	74.4	67.7	61.0	54.5	48.4	43.3	38.8	34.4	30.8	
	1 1/16	18.5	5.44	0.77	81.6	81.6	80.5	73.2	65.9	59.0	52.6	46.8	41.7	37.2	33.3	
	5/16	8.2	2.40	0.66	36.0	36.0	33.4	29.6	26.0	22.8	19.8	17.4	15.2	13.4		
	3/8	9.8	2.86	0.65	42.9	42.9	39.5	34.9	30.6	26.7	23.3	20.3	17.8			
	7/16	11.3	3.31	0.65	49.7	49.7	45.7	40.4	35.4	30.9	26.9	23.5	20.6			
5 x 3 1/2	1/2	12.8	3.75	0.65	56.3	56.3	51.8	45.8	40.1	35.0	30.5	26.6	23.3			
	3/8	14.3	4.18	0.65	62.7	62.7	57.8	51.1	44.7	39.0	34.0	29.7	26.0			
	5/16	15.7	4.61	0.64	69.2	69.2	63.2	55.7	48.7	42.4	36.9	32.1	28.1			
	3/8	17.1	5.03	0.64	75.5	75.5	69.0	60.8	53.2	46.3	40.2	35.1	30.7			
	1 1/16	18.5	5.44	0.64	81.6	81.6	74.6	65.8	57.5	50.0	43.5	37.9	33.2			
	5/16	8.2	2.40	0.66	36.0	36.0	33.4	29.6	26.0	22.8	19.8	17.4	15.2	13.4		
	3/8	9.8	2.86	0.65	42.9	42.9	39.5	34.9	30.6	26.7	23.3	20.3	17.8			
5 x 4	7/16	11.3	3.31	0.65	49.7	49.7	45.7	40.4	35.4	30.9	26.9	23.5	20.6			
	1/2	12.8	3.75	0.65	56.3	56.3	51.8	45.8	40.1	35.0	30.5	26.6	23.3			
	3/8	14.3	4.18	0.65	62.7	62.7	57.8	51.1	44.7	39.0	34.0	29.7	26.0			
	5/16	15.7	4.61	0.64	69.2	69.2	63.2	55.7	48.7	42.4	36.9	32.1	28.1			
	3/8	17.1	5.03	0.64	75.5	75.5	69.0	60.8	53.2	46.3	40.2	35.1	30.7			
	1 1/16	18.5	5.44	0.64	81.6	81.6	74.6	65.8	57.5	50.0	43.5	37.9	33.2			
	5/16	8.2	2.40	0.66	36.0	36.0	33.4	29.6	26.0	22.8	19.8	17.4	15.2	13.4		
5 x 4 1/2	3/8	9.8	2.86	0.65	42.9	42.9	39.5	34.9	30.6	26.7	23.3	20.3	17.8			
	7/16	11.3	3.31	0.65	49.7	49.7	45.7	40.4	35.4	30.9	26.9	23.5	20.6			
	1/2	12.8	3.75	0.65	56.3	56.3	51.8	45.8	40.1	35.0	30.5	26.6	23.3			
	3/8	14.3	4.18	0.65	62.7	62.7	57.8	51.1	44.7	39.0	34.0	29.7	26.0			
	5/16	15.7	4.61	0.64	69.2	69.2	63.2	55.7	48.7	42.4	36.9	32.1	28.1			
	3/8	17.1	5.03	0.64	75.5	75.5	69.0	60.8	53.2	46.3	40.2	35.1	30.7			
	1 1/16	18.5	5.44	0.64	81.6	81.6	74.6	65.8	57.5	50.0	43.5	37.9	33.2			

STRUTS OF ONE ANGLE

ALLOWABLE CONCENTRIC LOADS IN KIPS

Values given are for Least Radius of Gyration which is about Axis Z - Z.

Loads to right of heavy vertical line are for Secondary Members ONLY.



Size in Inches	Thick- ness	Weight per foot	Area Sq. Inches	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET																	
					3	4	5	6	7	8	10	12	14	16	18	20	22					
5 × 3½	5/16	8.7	2.56	0.77	38	38	34	31	28	25	20	16										
	3/8	10.4	3.05	0.76	46	45	41	37	33	29	23	18										
	7/16	12.0	3.53	0.76	53	52	47	42	38	34	27	21										
	1/2	13.6	4.00	0.75	60	59	53	48	42	38	30	24										
	9/16	15.2	4.47	0.75	67	66	59	53	47	42	33	26										
	5/8	16.8	4.92	0.75	74	72	65	59	52	46	37	29										
	11/16	18.3	5.37	0.75	81	79	71	64	57	51	40	32										
	3/4	19.8	5.81	0.75	87	85	77	69	62	55	43	34										
6 × 3½	3/8	11.7	3.42	0.77	51	51	46	41	37	33	26	21										
	7/16	13.5	3.97	0.76	60	58	53	48	43	38	30	24										
	1/2	15.3	4.50	0.76	68	66	60	54	48	43	34	27										
	9/16	17.1	5.03	0.75	75	74	67	60	53	47	37	30										
	5/8	18.9	5.55	0.75	83	81	74	66	59	52	41	33										
	11/16	20.6	6.06	0.75	91	89	80	72	64	57	45	36										
	3/4	22.4	6.56	0.75	98	96	87	78	70	62	49	39										
	13/16	24.0	7.06	0.75	106	103	94	84	75	67	52	42										
6 × 4	3/8	12.3	3.61	0.88	54	54	52	47	43	39	32	26										
	7/16	14.3	4.18	0.87	63	63	60	55	50	45	37	30	24									
	1/2	16.2	4.75	0.87	71	71	68	62	56	51	42	34	28									
	9/16	18.1	5.31	0.87	80	80	76	69	63	57	46	38	31									
	5/8	20.0	5.86	0.86	88	88	83	76	69	62	51	41	34									
	11/16	21.8	6.40	0.86	96	96	91	83	75	68	55	45	37									
	3/4	23.6	6.94	0.86	104	104	98	90	82	74	60	49	40									
	13/16	25.4	7.47	0.86	112	112	106	97	88	79	65	53	43									
6 × 6	3/8	14.9	4.36	1.19	65	65	65	65	61	58	50	43	37	32	28							
	7/16	17.2	5.06	1.19	76	76	76	76	71	67	58	51	43	37	32							
	1/2	19.6	5.75	1.18	86	86	86	86	81	76	66	57	49	42	36							
	9/16	21.9	6.43	1.18	96	96	96	96	90	85	73	63	54	47	40							
	5/8	24.2	7.11	1.17	107	107	107	106	99	93	81	69	60	51	44							
	11/16	26.5	7.78	1.17	117	117	117	116	109	102	88	76	65	56	48							
	3/4	28.7	8.44	1.17	127	127	127	126	118	111	96	82	71	61	52							
	13/16	31.0	9.09	1.17	136	136	136	135	127	119	103	89	76	66	57							
7 × 3½	3/8	13.0	3.80	0.76	57	56	51	46	41	36	29	23										
	7/16	15.0	4.40	0.76	66	65	59	53	47	42	33	26										
	1/2	17.0	5.00	0.75	75	73	66	60	53	47	37	30										
	9/16	19.1	5.59	0.75	84	82	74	67	59	53	42	33										
	5/8	21.0	6.17	0.75	93	90	82	73	65	58	46	36										
	11/16	23.0	6.75	0.74	101	98	89	80	71	63	49	39										
	3/4	24.9	7.31	0.74	110	107	96	86	77	68	54	42										
	13/16	26.8	7.87	0.74	118	115	104	93	83	73	58	46										
8 × 6	3/8	13.0	3.80	0.76	57	56	51	46	41	36	29	23										
	7/16	15.0	4.40	0.76	66	65	59	53	47	42	33	26										
	1/2	17.0	5.00	0.75	75	73	66	60	53	47	37	30										
	9/16	19.1	5.59	0.75	84	82	74	67	59	53	42	33										
	5/8	21.0	6.17	0.75	93	90	82	73	65	58	46	36										
	11/16	23.0	6.75	0.74	101	98	89	80	71	63	49	39										
	3/4	24.9	7.31	0.74	110	107	96	86	77	68	54	42										
	13/16	26.8	7.87	0.74	118	115	104	93	83	73	58	46										
8 × 8	3/8	13.0	3.80	0.76	57	56	51	46	41	36	29	23										
	7/16	15.0	4.40	0.76	66	65	59	53	47	42	33	26										
	1/2	17.0	5.00	0.75	75	73	66	60	53	47	37	30										
	9/16	19.1	5.59	0.75	84	82	74	67	59	53	42	33										
	5/8	21.0	6.17	0.75	93	90	82	73	65	58	46	36										
	11/16	23.0	6.75	0.74	101	98	89	80	71	63	49	39										
	3/4	24.9	7.31	0.74	110	107	96	86	77	68	54	42										
	13/16	26.8	7.87	0.74	118	115	104	93	83	73	58	46										

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO EQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

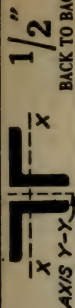
BACK TO BACK

Size	Thickness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
		Area	Weight	X-X	Y-Y	Unsuperscribed Length in Feet										Unsuperscribed Length in Feet																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																							
						3	4	5	6	7	8	9	10	12	14	16	18	20	6	7	8	9	10	12	14	16	18	20	22	24	26																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																								
2½ × 2½	⅜	1.80	6.1	.78	1.18	27	27	24	22	20	18	16	14	11</

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO EQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.



Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																
		Area	Weight	X-X	Y-Y	Unsupported Length in Feet										Unsupported Length in Feet																
						3	4	5	6	7	8	9	10	12	14	16	18	20	6	7	8	9	10	12	14	16	18	20	22	24	26	
2½ × 2½	⅜	1.80	6.1	.78	1.22	27	27	24	22	20	18	16	14	11	27	26	24	23	21	18	16	14	12	10	20	22	24	26
	¼	2.38	8.2	.77	1.24	36	35	32	29	26	23	21	18	15	36	34	32	30	28	24	21	18	16	14	12	10	20	
	⅝	2.94	10.0	.76	1.25	44	43	39	35	32	28	25	22	18	44	42	40	37	35	30	26	23	20	17	14	12	10	
	¾	3.46	11.8	.75	1.26	52	51	46	41	37	33	29	26	20	52	50	47	44	42	36	31	27	24	21	18	16	14	
3 × 3	¼	2.88	9.8	.93	1.43	43	43	42	39	36	33	30	27	22	18	43	41	39	37	35	29	26	23	20	18	16	14	12	
	⅝	3.56	12.2	.92	1.45	53	53	52	48	44	40	36	33	27	23	53	52	49	46	41	37	32	29	25	23	20	18	16	
	¾	4.22	14.4	.91	1.46	63	63	61	56	52	47	43	39	32	26	63	61	58	55	50	44	39	34	31	27	24	21	18	
	⅞	4.86	16.6	.91	1.47	73	73	71	65	59	54	49	45	37	30	73	71	67	64	57	51	45	40	35	31	28	25	23	
3½ × 3½	⅝	4.18	14.4	1.08	1.65	63	63	63	60	56	52	48	45	38	32	63	63	63	61	58	53	48	43	39	35	31	28	25	
	¾	4.96	17.0	1.07	1.66	74	74	74	71	67	62	57	53	45	38	32	74	74	74	72	69	63	57	51	46	41	37	34	30
	⅞	5.74	19.6	1.07	1.67	86	86	86	83	77	71	66	61	52	44	37	86	86	86	84	80	73	66	60	54	48	43	39	35
	1	6.50	22.2	1.06	1.68	98	98	98	93	87	80	74	68	58	49	41	98	98	98	95	91	83	75	68	61	55	49	44	40
4 × 4	⅞	7.24	24.8	1.05	1.69	109	109	109	103	96	89	82	76	64	54	46	109	109	109	106	102	93	84	76	68	61	55	50	45
	1	7.96	27.2	1.04	1.70	119	119	119	113	105	97	90	82	69	59	50	119	119	119	117	112	102	93	84	76	68	61	55	50
	1 ⅛	8.72	29.8	1.24	1.85	72	72	72	72	69	65	61	57	49	43	37	32	72	72	72	70	65	59	54	49	45	41	37	34
	1 ¼	9.50	32.2	1.23	1.86	86	86	86	82	77	72	67	62	53	45	38	86	86	86	83	77	71	65	59	53	49	44	40	
6 × 6	1 ½	10.30	39.2	1.23	1.87	99	99	99	99	95	89	83	78	68	59	51	44	99	99	99	97	90	82	75	69	62	57	51	47
	1 ⅝	11.50	43.8	1.35	2.70	193	193	193	193	193	188	173	159	145	132	120	108	193	193	193	193	190	181	171	161	151	142	133	
	1 ¾	12.86	48.4	1.34	2.71	213	213	213	213	213	207	191	175	160	145	132	120	213	213	213	213	213	210	200	189	178	168	158	148
	1 ⅞	14.22	53.0	1.83	2.71	233	233	233	233	233	233	226	208	191	174	158	143	120	233	233	233	233	233	231	219	207	195	183	172
8 × 8	2	15.56	57.4	1.83	2.73	253	253	253	253	253	253	246	226	207	189	171	156	120	253	253	253	253	250	239	226	212	200	188	176
	2 ⅛	16.88	62.0	1.82	2.74	273	273	273	273	273	273	264	244	222	202	184	167	143	273	273	273	273	271	257	243	229	216	203	190
	2 ¼	18.18	66.2	1.81	2.75	292	292	292	292	292	292	282	259	237	216	196	177	156	292	292	292	292	290	276	261	246	232	218	204
	2 ½	19.46	70.6	1.80	2.76	311	311	311	311	311	311	300	275	252	229	207	188	171	311	311	311	311	311	310	294	279	263	247	232
10 × 10	2 ⅝	20.74	74.8	1.80	2.77	330	330	330	330	330	330	330	318	292	267	243	220	199	330	330	330	330	330	329	316	297	283	267	252
	2 ¾	22.00	79.2	1.81	2.78	350	350	350	350	350	350	350	338	312	286	260	235	215	350	350	350	350	350	349	336	317	302	286	270
	3	23.33	84.0	1.80	2.79	369	369	369	369	369	369	369	356	330	304	278	253	229	369	369	369	369	368	355	336	321	305	289	273
	3 ⅛	24.66	88.8	1.79	2.80	388	388	388	388	388	388	388	375	349	323	297	272	247	388	388	388	388	388	387	374	359	343	327	311
12 × 12	3 ¼	26.00	93.6	1.78	2.81	407	407	407	407	407	407	407	394	368	342	316	291	266	407	407	407	407	407	406	393	378	362	346	330
	3 ½	27.33	98.4	1.77	2.82	426	426	426	426	426	426	426	413	387	361	335	310	285	426	426	426	426	426	425	412	397	381	365	349
	3 ¾	28.66	102.0	1.76	2.83	445	445	445	445	445	445	445	432	406	380	354	329	304	445	445	445	445	445	444	431	416	400	384	368
	4	30.00	107.6	1.75	2.84	464	464	464	464	464	464	464	451	425	399	373	348	323	464	464	464	464	464	463	450	435	419	403	387
14 × 14	4 ⅛	31.33	112.2	1.74	2.85	483	483	483	483	483	483	483	470	444	418	392	367	342	483	483	483	483	483	482	469	454	438	422	406
	4 ¼	32.66	116.8	1.73	2.86	502	502	502	502	502	502	502	489	463	437	411	386	361	502	502	502	502	502	501	488	473	457	441	425
	4 ½	34.00	121.0	1.72	2.87	521	521	521	521	521	521	521	508	482	456	430	405	380	521	521	521	521	521	520	507	492	476	460	444
	4 ⅝	35.33	125.6	1.71	2.88	540	540	540	540	540	540	540	527	501	475	449	424	399	540	540	540	540	540	539	526	510	494	478	462

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

SHORT LEGS BACK TO BACK

BACK TO BACK

Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																
		Area	Weight	X-X	Y-Y	Unsupported Length in Feet										Unsupported Length in Feet																
						3	4	5	6	7	8	9	10	12	14	16	6	7	8	9	10	12	14	16								
2½ × 2	3/16	1.62	5.5	.60	1.24	24	22	19	16	14	12	10	9
	1/4	2.12	7.2	.59	1.25	32	28	24	21	18	15	13	
	5/16	2.62	9.0	.58	1.26	39	34	30	25	22	19	16	
3 × 2½	1/4	2.62	9.0	.75	1.45	39	38	35	31	28	25	22	20	16	
	5/16	3.24	11.2	.74	1.46	49	47	43	38	34	30	27	24	20	
	3/8	3.84	13.2	.74	1.48	58	56	51	45	40	36	32	28	22	
3½ × 2½	1/4	4.42	15.2	.73	1.49	66	64	58	52	46	41	36	32	25	
	5/16	5.50	18.8	.70	1.76	83	78	70	62	55	48	43	38	
	3/8	6.58	22.2	.72	1.73	93	88	80	72	64	56	49	43	38	
4 × 3	1/2	7.60	27.2	.85	1.98	119	119	112	102	93	84	75	68	55	45	
	5/8	9.10	31.6	.86	1.97	138	138	130	120	110	100	91	82	72	62	54	46	40	36	32	28	25	22	19	17	15	13	11	10	9	8	
	3/4	10.12	34.6	1.01	1.93	152	152	144	134	124	114	104	95	86	77	68	60	52	46	41	36	32	28	25	22	19	17	15	13	11	10	
4 × 3½	5/8	10.12	34.6	1.01	1.93	152	152	144	134	124	114	104	95	86	77	68	60	52	46	41	36	32	28	25	22	19	17	15	13	11	10	
	3/4	11.62	39.6	.98	2.48	174	174	166	156	146	136	126	116	106	97	87	78	70	62	54	46	40	36	32	28	25	22	19	17	15		
	5/16	12.12	41.6	1.02	2.40	188	188	180	170	160	150	140	130	120	110	100	91	82	74	66	58	50	44	38	32	28	25	22	19	17	15	
5 × 3	3/8	12.12	41.6	1.02	2.40	188	188	180	170	160	150	140	130	120	110	100	91	82	74	66	58	50	44	38	32	28	25	22	19	17	15	
	1/2	14.72	49.6	1.01	2.43	212	212	204	194	184	174	164	154	144	134	124	114	104	95	86	78	70	62	54	46	40	36	32	28	25	22	
	5/8	16.72	57.6	1.00	2.44	232	232	224	214	204	194	184	174	164	154	144	134	124	114	104	95	86	78	70	62	54	46	40	36	32	28	
5 × 3½	3/4	18.72	65.6	.99	2.45	252	252	244	234	224	214	204	194	184	174	164	154	144	134	124	114	104	95	86	78	70	62	54	46	40	36	
	5/16	19.72	69.6	1.00	2.45	268	268	260	250	240	230	220	210	200	190	180	170	160	150	140	130	120	110	100	91	82	74	66	58	50	44	
	3/4	21.72	77.6	.98	2.48	288	288	280	270	260	250	240	230	220	210	200	190	180	170	160	150	140	130	120	110	100	91	82	74	66	58	

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

SHORT LEGS BACK TO BACK

BACK TO BACK



Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																	
		Area	Weight	X-X	Y-Y	4	5	6	7	8	9	10	11	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40					
6 × 3½	¾	6.84	23.4	.99	2.95	103	102	95	88	81	74	68	57	47	40	103	100	95	90	85	81	76	72	67	63	60	56	53	50	
	7/16	7.94	27.0	.98	2.96	119	118	110	102	93	85	78	65	54	46	119	116	110	105	99	94	88	83	78	74	70	66	62	58	
	½	9.00	30.6	.97	2.97	135	133	124	114	105	98	90	77	64	51	135	131	125	119	113	106	100	95	89	84	79	74	70	66	
	5/8	10.06	34.2	.96	2.99	151	149	138	127	116	106	97	80	67	56	151	147	140	133	126	119	113	106	100	94	89	84	79	74	
	¾	11.10	37.8	.96	3.00	167	164	152	140	128	117	107	89	74	62	167	163	155	147	140	132	125	118	111	105	99	93	87	82	
	1 1/8	12.12	41.2	.95	3.01	182	179	165	152	139	127	116	96	80	182	178	170	161	153	145	137	129	122	115	108	102	96	90	
6 × 4	¾	13.12	44.8	.94	3.03	197	193	178	164	149	136	124	102	85	197	193	184	175	166	157	149	140	132	125	118	111	105	99	93	
	7/16	14.12	48.0	.94	3.04	212	207	192	176	161	147	133	110	92	212	208	199	189	179	169	160	152	143	135	127	120	113	107	101	
	½	15.10	51.4	.93	3.05	227	221	204	187	171	155	141	117	97	227	223	213	202	192	182	172	162	153	145	136	129	121	114	107	
	5/8	7.22	24.6	1.17	2.87	108	107	101	95	88	82	71	60	52	45	108	104	99	94	88	83	78	74	69	65	61	58	54	51	
	¾	8.36	28.6	1.16	2.88	125	124	117	109	102	95	81	69	59	50	125	121	115	109	103	97	91	86	81	76	71	67	63	59	
	1 1/8	9.50	32.4	1.15	2.90	142	142	140	132	124	115	107	92	78	67	58	143	138	131	124	117	110	104	98	92	87	81	77	72	68
7 × 3½	¾	10.62	36.2	1.14	2.91	159	159	157	147	137	127	119	102	87	74	64	159	154	146	139	131	124	117	110	103	97	91	86	81	76
	7/16	11.72	40.0	1.13	2.92	176	176	172	162	150	139	130	111	94	81	70	176	170	162	153	145	137	129	122	114	108	101	95	90	84
	½	12.80	43.6	1.13	2.94	192	192	188	176	164	153	142	121	103	88	76	192	186	177	168	159	150	142	134	126	118	111	105	99	93
	5/8	13.88	47.2	1.12	2.95	208	208	203	190	177	165	153	130	111	95	81	208	202	193	183	173	163	154	145	137	129	121	114	107	101
	¾	14.94	50.8	1.11	2.96	224	224	218	204	190	176	163	139	118	101	87	224	218	208	197	186	176	166	157	148	139	131	123	116	109
	1 1/8	15.96	54.4	1.11	2.97	239	239	233	218	203	188	174	148	126	108	93	239	233	222	211	200	189	178	168	158	149	140	132	124	117
8 × 6	¾	7.60	26.0	.96	3.50	114	112	104	96	88	80	73	61	51	42	114	114	113	108	104	99	95	91	86	82	78	74	70	67	
	7/16	8.80	30.0	.95	3.51	132	130	120	111	101	92	84	69	58	132	132	131	126	122	115	110	105	100	95	90	86	82	78	
	½	10.00	34.0	.94	3.53	150	147	135	125	114	104	94	79	65	150	150	149	143	137	131	126	120	114	109	103	98	93	89	
	5/8	11.18	38.2	.93	3.54	168	163	151	139	126	115	105	86	72	168	168	167	160	154	147	141	134	128	122	116	110	105	100	
	¾	12.34	42.0	.93	3.55	185	180	167	153	140	127	115	95	79	185	185	184	177	170	163	155	148	141	135	128	122	116	110	
	1 1/8	13.50	46.0	.92	3.57	203	197	181	166	152	138	125	103	85	203	203	202	194	186	178	171	163	155	148	141	134	127	121	
7 × 3½	¾	14.62	49.8	.91	3.58	219	212	195	179	163	148	134	110	91	219	219	219	211	202	194	185	177	169	161	153	145	138	132	
	5/8	15.74	53.6	.91	3.59	236	228	210	192	175	159	144	119	98	236	236	236	227	218	209	200	190	182	173	165	157	149	142	
	¾	16.84	57.4	.90	3.60	253	243	224	204	186	168	153	125	103	253	253	253	243	233	224	214	204	195	186	177	168	160	153	
	1 1/8	17.94	61.0	.89	3.62	269	258	237	216	196	178	161	132	108	269	269	269	260	249	239	229	219	209	199	189	180	172	163	
	½	19.00	64.6	.89	3.63	285	273	251	229	208	188	170	139	115	285	285	285	273	264	253	242	232	221	211	201	191	182	173	
	5/8	7.60	26.0	.96	3.50	114	112	104	96	88	80	73	61	51	42	114	114	113	108	104	99	95	91	86	82	78	74	70	67	
7 × 3½	7/16	8.80	30.0	.95	3.51	132	130	120	111	101	92	84	69	58	132	132	131	126	122	115	110	105	100	95	90	86	82	78	
	½	10.00	34.0	.94	3.53	150	147	135	125	114	104	94	79	65	150	150	149	143	137	131	126	120	114	109	103	98	93	89	
	5/8	11.18	38.2	.93	3.54	168	163	151	139	126	115	105	86	72	168	168	167	160	154	147	141	134	128	122	116	110	105	100	
	¾	12.34	42.0	.93	3.55	185	180	167	153	140	127	115	95	79	185	185	184	177	170	163	155	148	141	135	128	122	116	110	
	1 1/8	13.50	46.0	.92	3.57	203	197	181	166	152	138	125	103	85	203	203	202	194	186	178	171	163	155	148	141	134	127	121	
	¾	14.62	49.8	.91	3.58	219	212	195	179	163	148	134	110	91	219	219	219	211	202	194	185	177	169	161	153	145	138	132	
7 × 3½	5/8	15.74	53.6	.91	3.59	236	228	210	192	175	159	144	119	98	236	236	236	227	218	209	200	190	182	173	165	157	149	142	
	¾	16.84	57.4	.90	3.60	253	243	224	204	186	168	153	125	103	253	253	253	243	233	224	214	204	195	186	177	168	160	153	
	1 1/8	17.94	61.0	.89	3.62	269	258	237	216	196	178	161	132	108	269	269	269	260	249	239	229	219	209	199	189	180	172	163	
	½	19.00	64.6	.89	3.63	285	273	251	229	208	188	170	139	115	285	285	285	273	264	253	242	232	221	211	201	191	182	173	
	5/8	7.60	26.0	.96	3.50	114	112	104	96	88	80	73	61	51	42	114	114	113	108	104	99	95	91	86	82	78	74	70	67	
	7/16	8.80	30.0	.95	3.51	132	130	120	111	101	92	84	69	58	132	132	131	126	122	115	110	105	100	95	90	86	82	78	
8 × 6	½	10.00	34.0	.94	3.53	150	147	135	125	114	104	94	79	65	150	150	149	143	137	131	126	120	114	109	103	98	93	89	
	5/8	11.18	38.2	.93	3.54	168	163	151	139	126	115	105	86	72	168	168	167	160	154	147	141	134	128	122	116	110	105	100	
	¾	12.34	42.0	.93	3.55	185	180	167	153	140	127	115	95	79	185	185	184	177	170	163	155	148	141	135	128	122	116	110	
	1 1/8	13.50	46.0	.92	3.57	203	197	181	166	152	138	125	103	85	203	203	202	194	186	178	171	163	155	148	141	134	127	121	
	¾	14.62	49.8	.91	3.58	219	212	195	179	163	148	134	110	91	219	219	219	211	202	194	185	177	169	161	153	145	138	132	
	5/8	15.74	53.6	.91	3.59	236	228	210	192	175	159	144	119	98	236	236	236	227	218	209	200	190	182	173	165	157	149	142	
8 × 6	¾	16.84	57.4	.90	3.60	253	243	224	204	186	168	153	125																				

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

LONG LEGS BACK TO BACK

BACK TO BACK

Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																	
		Area	Weight	X-X	Y-Y	Unsupported Length in Feet										Unsupported Length in Feet																	
						4	5	6	7	8	9	10	12	14	16	18	20	22	4	5	6	7	8	9	10	12	14	16	18	20	22		
2 1/2 x 2	3/16	1.62	5.5	.79	.92	24	22	20	18	16	14	13	10	24	24	22	20	18	17	15	12	10		
	1/4	2.12	7.2	.78	.93	32	29	26	23	21	19	17	13	32	31	29	26	24	22	20	16	14		
	5/16	2.62	9.0	.78	.95	39	36	32	29	26	23	20	16	39	39	36	33	30	27	25	21	17		
3 x 2 1/2	1/4	2.62	9.0	.95	1.13	39	36	33	30	28	25	20	17	39	39	38	36	34	31	29	25	21	18	16	
	5/16	3.34	11.2	.94	1.14	49	48	44	40	37	34	31	25	21	49	49	48	45	42	39	36	31	26	23	19	
	3/8	3.84	13.2	.93	1.16	58	56	52	48	43	40	36	30	25	58	58	57	53	50	47	43	37	32	27	24	
3 1/2 x 2 1/2	7/16	4.62	16.6	1.09	1.12	73	70	66	61	57	52	44	38	32	26	73	73	71	67	62	58	53	46	39	33	29	
	1/2	5.30	18.8	1.09	1.13	83	80	75	69	64	59	50	43	36	31	83	83	81	76	71	66	61	52	44	38	33	
	5/8	6.00	22.2	1.25	1.33	98	98	94	88	83	77	67	58	51	44	38	98	98	96	91	86	81	71	62	54	47	42	37	...	
4 x 3	1/2	7.24	24.8	1.24	1.35	109	109	104	98	92	86	75	65	56	49	42	109	109	107	102	96	91	80	70	61	54	47	42	37	
	5/8	7.96	27.2	1.23	1.36	119	119	114	107	100	94	81	70	61	53	46	119	119	118	112	106	100	88	78	68	60	52	46	...	
	3/4	8.50	29.6	1.22	1.37	129	129	123	115	108	101	87	75	65	56	49	129	129	129	129	123	117	110	97	86	77	69	62	55	
4 x 3 1/2	1/2	9.36	32.0	1.21	1.60	140	140	133	125	117	109	94	81	70	61	53	140	140	140	140	140	140	135	129	117	105	95	85	76	68
	5/8	10.12	34.6	1.20	1.63	152	152	143	134	126	117	101	87	75	65	57	152	152	152	152	152	146	140	127	115	103	92	83	74	
	3/4	10.88	37.0	1.55	1.61	163	163	163	161	154	147	132	118	106	94	84	75	163	163	163	163	159	151	142	134	117	102	89	78	68	
5 x 3	1/2	12.50	43.8	1.58	1.62	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183	183		
	5/8	13.26	46.6	1.57	1.61	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193	193		
	3/4	14.02	49.4	1.56	1.60	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203	203		
5 x 3 1/2	1/2	15.00	51.0	1.54	1.59	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213	213		
	5/8	15.76	53.8	1.53	1.58	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223	223		
	3/4	16.52	56.6	1.52	1.57	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233	233		

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

BACK TO BACK



AXIS Y-Y

AXIS X-X

Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X												AXIS Y - Y												
		Area	Weight	X-X	Y-Y	Unsupervised Length in Feet												Unsupervised Length in Feet												
						9	10	12	14	16	18	20	22	24	26	28	30	6	7	8	9	10	12	14	16	18	20	22	24	26
6 × 3½	¾	6.84	23.4	1.94	1.39	103	102	94	87	80	73	67	61	55	50	46	...	103	102	97	92	87	77	68	60	53	46	41
	7/16	7.94	27.0	1.93	1.40	119	118	109	101	92	84	77	70	64	58	53	...	119	119	113	107	102	90	79	70	62	54	48
	½	9.06	30.6	1.92	1.41	135	133	123	114	104	95	87	79	72	66	60	...	135	135	129	122	116	103	91	80	70	62	55
	9/16	10.06	34.2	1.91	1.42	151	148	138	127	116	106	96	88	80	73	67	...	151	151	144	137	130	115	102	90	79	70	62
	5/8	11.10	37.8	1.90	1.43	167	164	152	139	127	116	106	96	88	80	73	...	167	167	160	152	144	128	113	100	88	78	69
	11/16	12.12	41.2	1.89	1.45	182	178	165	152	139	126	115	105	95	87	79	...	182	182	175	167	158	141	125	110	98	87	77
6 × 4	¾	7.22	24.6	1.89	1.46	197	193	179	164	150	137	125	113	103	94	86	...	197	197	190	181	172	153	136	120	107	94	84
	7/16	8.36	28.6	1.88	1.48	212	207	192	176	161	147	133	121	110	101	92	...	212	212	206	196	186	167	148	131	116	103	92
	½	9.50	32.4	1.87	1.49	227	221	205	188	172	156	142	129	117	107	97	...	227	227	221	211	200	179	159	141	125	111	99
	9/16	10.62	36.2	1.91	1.62	108	107	99	91	84	77	70	64	58	53	48	...	108	108	104	100	95	81	73	65	59	53	47
	5/8	11.72	40.0	1.90	1.63	125	124	115	106	97	88	81	73	67	61	56	...	125	125	121	116	110	95	85	76	68	61	55
	11/16	12.80	43.6	1.89	1.65	143	140	130	120	110	100	91	83	76	69	63	...	143	143	138	133	127	110	98	88	79	71	64
7 × 3½	¾	13.88	47.2	1.88	1.66	159	156	145	133	122	111	101	92	84	77	70	...	159	159	153	148	143	122	110	98	88	80	72
	7/16	14.94	50.8	1.89	1.67	176	173	160	147	135	123	112	102	93	85	77	...	176	176	170	164	158	135	122	109	98	88	80
	½	15.96	54.4	1.87	1.68	192	188	174	160	146	134	121	111	101	92	84	...	192	192	187	180	174	150	136	123	110	98	87
	9/16	17.00	58.0	1.86	1.69	208	204	188	173	158	144	131	119	108	99	90	...	208	208	202	195	187	161	146	131	118	106	96
	5/8	18.06	61.0	1.87	1.70	224	219	202	186	170	155	141	128	116	106	96	...	224	224	218	211	202	174	158	142	128	115	104
	11/16	19.12	64.6	1.86	1.71	239	233	215	198	181	164	149	136	123	112	102	...	239	239	232	225	216	187	169	152	137	124	112
7 × 3½	¾	7.60	26.0	2.27	1.33	114	114	112	105	98	91	84	78	72	67	62	...	114	112	106	100	94	83	72	63	55	49	43
	7/16	8.80	30.0	2.26	1.34	132	132	129	121	113	105	97	90	83	77	71	...	132	130	123	116	110	96	85	74	65	57	50
	½	10.00	34.0	2.25	1.35	150	150	147	137	128	119	110	102	94	87	80	...	150	148	141	133	125	110	97	85	74	65	58
	9/16	11.18	38.2	2.25	1.36	168	168	164	154	143	133	123	114	105	97	90	...	168	166	158	149	140	124	109	96	84	74	65
	5/8	12.34	42.0	2.24	1.37	185	185	181	169	158	146	135	125	116	107	99	...	185	184	175	165	156	138	121	106	93	82	72
	11/16	13.50	46.0	2.23	1.39	203	203	197	185	172	160	148	137	126	116	107	...	203	202	192	182	172	152	134	118	104	92	81
8 × 6	¾	14.62	49.8	2.22	1.40	219	219	213	200	186	173	160	147	136	125	116	...	219	219	209	198	187	166	146	129	113	100	88
	7/16	15.74	53.6	2.21	1.41	236	236	229	215	200	185	171	158	146	134	124	...	236	236	225	214	202	179	158	140	123	109	96
	½	16.84	57.4	2.20	1.42	253	253	246	229	213	197	183	168	155	143	132	...	253	253	242	229	217	193	170	150	133	117	104
	9/16	17.94	61.0	2.19	1.44	269	269	260	243	226	210	194	179	165	152	140	...	269	269	259	246	233	208	184	162	144	127	113
	5/8	19.00	64.6	2.19	1.45	285	285	276	258	240	222	205	189	174	161	148	...	285	285	275	261	248	221	196	173	153	136	121
	11/16	20.96	69.0	2.18	1.46	301	301	290	271	252	234	216	199	183	167	151	...	301	301	290	271	252	234	216	199	183	167	151

LOADS BY A. I. S. C. SPECIFICATION

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES $\frac{1}{2}$ "

BACK TO BACK

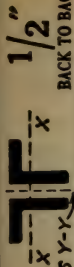
4X/5 Y-Y

LOADS TO RIGHT OF HEAVY VERTICAL LINES ARE FOR SECONDARY MEMBERS ONLY.

SHORT LEGS BACK TO BACK

Size	Thick- ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y																
		Area	Weight	X-X	Y-Y	Unsupported Length in Feet										Unsupported Length in Feet																
6 × 3½	¾	6.84	23.4	.99	3.00	103	102	95	88	81	74	68	57	47	40	103	100	96	91	86	81	77	73	68	64	61	57	54	51	
	7/16	7.94	27.0	.98	3.01	119	118	110	102	93	85	78	65	54	46	119	116	111	105	100	94	89	84	80	75	71	66	63	59	
	½	9.00	30.6	.97	3.02	135	133	124	114	105	98	87	73	61	51	135	132	126	120	114	108	102	96	91	85	80	76	71	67	
	9/16	10.06	34.2	.96	3.04	151	149	138	127	116	106	97	80	67	56	151	148	141	135	128	121	114	108	102	96	90	85	80	76	
	5/8	11.10	37.8	.96	3.05	167	164	152	140	128	117	107	89	74	62	167	164	156	149	141	134	126	119	113	106	100	94	89	84	
	11/16	12.12	41.2	.95	3.06	182	179	165	152	139	127	116	96	80	182	179	171	163	154	146	138	131	123	116	110	104	98	92	
6 × 4	¾	13.12	44.8	.94	3.08	197	193	178	164	149	136	124	102	85	197	194	186	177	168	159	150	142	134	127	120	113	107	100	
	13/16	14.12	48.0	.94	3.09	212	207	192	176	161	147	133	110	92	212	209	200	190	181	171	162	153	145	137	129	121	115	109	
	7/8	15.10	51.4	.93	3.10	227	221	204	187	171	155	141	117	97	227	224	214	204	194	184	174	164	155	147	138	131	123	117	
	¾	7.22	24.6	1.17	2.92	108	108	107	101	95	88	82	71	60	52	45	108	105	100	95	89	84	79	75	70	66	62	59	55	52
	7/16	8.36	28.6	1.16	2.93	125	125	124	117	109	102	95	81	69	59	50	125	121	115	110	104	98	92	87	82	77	72	68	64	60
	½	9.50	32.4	1.15	2.95	142	142	140	132	124	115	107	92	78	67	58	142	139	132	125	118	112	105	99	94	88	83	78	73	69
7 × 3½	9/16	10.62	36.2	1.14	2.96	159	159	157	147	137	127	119	102	87	74	64	159	155	148	140	133	126	118	111	105	99	93	88	82	78
	5/8	11.72	40.0	1.13	2.97	176	176	172	162	150	139	130	111	94	81	70	176	171	163	155	147	139	131	123	116	110	103	97	91	86
	11/16	12.80	43.6	1.13	2.98	192	192	188	176	164	153	142	121	103	88	76	191	187	178	169	161	152	143	135	127	120	113	106	100	94
	¾	13.88	47.2	1.12	2.99	208	208	203	190	177	165	153	130	111	95	81	208	203	194	184	174	165	156	147	138	131	123	116	109	102
	13/16	14.94	50.8	1.11	3.00	224	224	218	204	190	176	163	139	118	101	87	224	219	209	198	188	178	168	159	149	141	133	125	118	111
	7/8	15.96	54.4	1.11	3.02	239	239	233	218	203	188	174	148	126	108	93	239	235	225	214	202	191	180	170	161	151	143	134	127	120
8 × 6	¾	7.60	26.0	.96	3.55	114	112	104	96	88	80	73	61	51	42	114	112	113	109	105	100	96	90	87	83	79	75	71	68	65
	7/16	8.80	30.0	.95	3.56	132	130	120	111	101	92	84	69	58	132	132	131	127	121	116	111	106	101	96	92	87	83	79	75
	½	10.00	34.0	.94	3.58	150	147	135	125	114	104	94	78	65	150	150	150	144	138	133	127	121	115	110	105	99	95	90	86
	9/16	11.18	38.2	.93	3.59	168	163	151	139	126	115	105	86	72	168	168	168	161	155	148	142	135	129	124	117	112	106	101	
	5/8	12.34	42.0	.93	3.60	185	180	167	153	140	127	115	95	79	185	185	185	178	171	164	157	150	143	136	130	123	117	112	107
	11/16	13.50	46.0	.92	3.61	203	197	181	166	152	138	125	103	85	203	203	203	195	187	180	172	164	156	149	142	135	129	123	117
8 × 6	¾	14.62	49.8	.91	3.63	219	212	195	179	163	148	134	111	91	219	219	219	212	203	195	187	178	170	162	155	147	140	133	126
	13/16	15.74	53.6	.91	3.64	236	228	210	192	175	159	144	119	98	236	236	236	228	219	210	201	192	184	175	167	159	151	144	137
	7/8	16.84	57.4	.90	3.65	253	243	224	204	186	168	153	125	103	253	253	253	244	235	225	216	206	197	188	179	170	162	155	148
	15/16	17.94	61.0	.89	3.67	269	258	237	216	196	178	161	132	108	269	269	269	261	251	241	230	220	210	201	191	182	174	166	158
	¾	19.00	64.6	.89	3.68	285	273	251	229	208	188	170	139	115	285	285	285	277	266	255	244	234	223	213	203	194	185	176	167
	7/16	11.86	40.4	1.80	3.73	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	178	
8 × 6	½	13.50	46.0	1.79	3.74	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	202	
	9/16	15.12	51.4	1.78	3.75	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	227	
	5/8	16.72	57.0	1.77	3.76	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	251	
	¾	18.30	62.4	1.77	3.77	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275	275
	11/16	19.88	67.0	1.76	3.78	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298	298
	13/16	21.44	73.0	1.75	3.79	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322	322
8 × 6	7/8	22.96	78.2	1.74	3.81	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344	344
	15/16	24.50	83.4	1.73	3.81	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368	368
	¾	26.00	88.4	1.73	3.82	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390	390
	11/16	27.50	93.4	1.73	3.82	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412	412
	¾	29.00	98.4	1.73	3.82	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434	434
	13/16	30.50	103.4	1.73	3.82	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456	456

LOADS BY A. I. S. C. SPECIFICATION



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR STRUTS OF TWO UNEQUAL ANGLES

Loads to right of heavy vertical lines are for Secondary Members ONLY.

LONG LEGS BACK TO BACK

BACK TO BACK

LOADS BY A. I. S. C. SPECIFICATION

Size	Thick-ness	Two Angles		Radius of Gyration		AXIS X - X										AXIS Y - Y															
		Area	Weight	X-X	Y-Y	9	10	12	14	16	18	20	22	24	26	28	30	6	7	8	9	10	12	14	16	18	20	22	24	26	28
6 × 3½	¾	6.84	23.4	1.94	1.43	103	102	94	87	80	73	67	61	55	50	46	...	103	103	99	94	89	79	70	62	54	48	43			
	7/16	7.94	27.0	1.93	1.44	119	118	109	101	92	84	77	70	64	58	53	...	119	119	115	109	103	92	81	72	64	56	50			
	½	9.00	30.6	1.92	1.46	135	133	123	114	104	95	87	79	72	66	60	...	135	135	131	124	118	105	93	83	73	65	58			
	5/8	10.06	34.2	1.91	1.47	151	148	138	127	116	106	96	88	80	73	67	...	151	151	146	139	132	118	105	93	82	73	65			
	11/16	11.10	37.8	1.90	1.48	167	164	152	139	127	116	106	96	88	80	73	...	167	167	162	154	146	131	116	103	92	81	72	65		
6 × 4	¾	12.12	41.2	1.89	1.49	182	178	165	152	139	126	115	105	95	87	79	...	182	182	177	169	160	144	128	113	101	89	80			
	13/16	13.12	44.8	1.89	1.51	197	193	179	164	150	137	125	113	103	94	86	...	197	197	193	184	175	157	140	124	111	98	88			
	½	14.12	48.0	1.88	1.52	212	207	192	176	161	147	133	121	110	101	92	...	212	212	208	199	189	170	151	135	120	107	95			
	5/8	15.10	51.4	1.87	1.53	227	221	205	188	172	156	142	129	117	107	97	...	227	227	223	213	203	182	163	145	129	115	102			
	¾	16.06	54.4	1.86	1.54	242	235	219	202	186	170	155	141	128	116	106	96	...	242	242	238	228	218	200	181	164	148	132	119	107	
7 × 3½	¾	7.60	26.0	2.27	1.37	114	114	112	105	98	91	84	78	72	67	62	57	114	113	108	102	96	85	75	65	58	51	45			
	7/16	8.80	30.0	2.26	1.38	132	132	129	121	113	105	97	90	83	77	71	66	132	131	125	118	112	99	87	77	67	59	52			
	½	10.00	34.0	2.25	1.39	150	150	147	137	128	119	110	102	94	87	80	74	150	150	144	135	127	113	99	87	77	68	60			
	5/8	11.18	38.2	2.25	1.41	168	168	164	154	143	133	123	114	105	97	90	83	168	168	160	152	144	128	113	99	87	77	68			
	11/16	12.34	42.0	2.24	1.42	185	185	181	169	158	146	136	125	116	107	99	91	185	185	177	168	159	141	125	110	97	86	76			
7 × 3½	¾	13.50	46.0	2.23	1.43	203	203	197	185	172	160	148	137	126	116	107	99	203	203	194	185	175	155	138	121	107	95	84			
	13/16	14.62	49.8	2.22	1.45	219	219	213	200	186	173	160	147	136	125	116	107	219	219	212	201	191	170	151	133	118	104	93			
	½	15.74	53.6	2.21	1.46	236	236	229	215	200	185	171	158	146	134	124	115	236	236	228	217	206	184	163	144	128	113	101			
	5/8	16.84	57.4	2.20	1.47	253	253	245	229	213	197	183	168	155	143	132	122	253	253	245	233	221	198	176	156	138	122	109			
	11/16	17.94	61.0	2.19	1.49	269	269	260	243	226	210	194	179	165	152	140	129	269	269	262	250	237	213	189	168	149	132	118			
8 × 6	¾	19.00	64.6	2.19	1.50	285	285	276	258	240	222	205	189	174	161	148	137	285	285	278	266	252	226	202	179	159	141	126			
	13/16	20.16	68.4	2.18	1.51	301	301	291	272	254	236	218	201	186	172	159	147	301	301	294	282	268	243	218	195	175	157	140			
	½	21.30	72.4	2.17	1.52	317	317	306	287	268	249	230	212	196	181	167	154	317	317	310	298	284	259	234	211	191	173	156			
	5/8	22.56	76.4	2.16	1.53	333	333	321	302	282	263	244	225	208	193	178	165	333	333	326	314	300	275	250	225	204	186				
	11/16	23.84	80.4	2.15	1.54	349	349	337	317	297	277	258	238	220	204	189	175	349	349	342	330	316	291	266	241	220	202				
8 × 6	¾	24.30	83.4	2.14	1.55	365	365	353	333	313	292	272	252	234	216	200	185	365	365	358	346	332	307	282	257	235	217				
	13/16	25.12	84.4	2.13	1.56	381	381	369	349	329	308	287	267	248	230	213	200	381	381	374	362	348	323	298	273	251	233				
	½	26.40	88.4	2.12	1.57	397	397	385	365	345	324	303	282	263	245	227	214	397	397	390	378	364	339	314	289	267	249				
	5/8	27.60	92.4	2.11	1.58	413	413	401	381	361	340	319	298	279	261	243	229	413	413	406	394	380	355	330	305	283	265				
	11/16	28.80	96.4	2.10	1.59	429	429	417	397	377	356	335	314	293	275	257	243	429	429	422	410	396	371	346	321	300					

ALLOWABLE UNIFORM LOAD IN KIPS FOR STANDARD ANGLES USED AS BEAMS

Position	Angle		Coef. of Strength	Length in Span in feet. Laterally supported.												
	Size	Thick- ness		Weight per foot	3	4	5	6	7	8	9	10	11	12	13	14
Equal Legs	$2\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{4}$ $\frac{5}{16}$	4.1 5.0	4719 5795	1.57 1.93	1.18 1.45	.94 1.16	.79 .97	.67 .83	.59 .72	.52 .64	.47 .58	.43 .53			
	3×3	$\frac{1}{4}$ $\frac{5}{16}$	4.9 6.1	6889 8507	2.30 2.84	1.72 2.13	1.38 1.70	1.15 1.42	.98 1.22	.86 1.06	.77 .95	.69 .85	.63 .77	.57 .71		
	$3\frac{1}{2} \times 3\frac{1}{2}$	$\frac{5}{16}$ $\frac{3}{8}$	7.2 8.5	11713 13831	3.90 4.61	2.93 3.46	2.34 2.77	1.95 2.31	1.67 1.98	1.46 1.73	1.30 1.54	1.17 1.38	1.06 1.26	.98 1.15		
	4×4	$\frac{5}{16}$ $\frac{3}{8}$	8.2 9.8	15458 18294	5.15 6.10	3.86 4.57	3.09 3.66	2.58 3.05	2.21 2.61	1.93 2.29	1.72 2.03	1.55 1.83	1.41 1.66	1.29 1.52	1.19 1.41	
	6×6	$\frac{3}{8}$ $\frac{1}{2}$	14.9 19.6	42358 55305	14.12 18.44	10.59 13.83	8.47 11.06	7.06 9.22	6.05 7.90	5.29 6.91	4.71 6.15	4.24 5.53	3.85 5.03	3.53 4.62	3.26 4.25	3.03 3.95
	Long Leg Up	$3 \times 2\frac{1}{2}$	$\frac{1}{4}$ $\frac{5}{16}$	4.5 5.6	6718 8231	2.24 2.74	1.68 2.06	1.34 1.65	1.12 1.37	.96 1.18	.84 1.03	.75 .91	.67 .82	.61 .75		
$3\frac{1}{2} \times 2\frac{1}{2}$		$\frac{1}{4}$ $\frac{5}{16}$	4.9 6.1	9038 11136	3.01 3.71	2.26 2.78	1.81 2.23	1.51 1.86	1.29 1.59	1.13 1.39	1.00 1.24	.90 1.11	.82 1.01	.75 1.23		
4×3		$\frac{5}{16}$ $\frac{3}{8}$	7.2 8.5	14802 17471	4.93 5.82	3.70 4.37	2.96 3.49	2.47 2.91	2.11 2.50	1.85 2.18	1.64 1.94	1.48 1.75	1.35 1.59	1.23 1.46	1.14 1.34	
$4 \times 3\frac{1}{2}$		$\frac{5}{16}$ $\frac{3}{8}$	7.7 9.1	15149 17978	5.05 5.99	3.79 4.49	3.03 3.60	2.52 3.00	2.16 2.57	1.89 2.25	1.68 2.00	1.51 1.80	1.38 1.63	1.26 1.50	1.17 1.38	
5×3		$\frac{5}{16}$ $\frac{3}{8}$	8.2 9.8	22626 26800	7.54 8.93	5.66 6.70	4.53 5.36	3.77 4.47	3.23 3.83	2.83 3.35	2.51 2.98	2.26 2.68	2.06 2.44	1.89 2.23	1.74 2.06	1.62 1.91
$5 \times 3\frac{1}{2}$		$\frac{5}{16}$ $\frac{3}{8}$	8.7 10.4	23226 27540	7.74 9.18	5.81 6.89	4.65 5.51	3.87 4.59	3.32 3.93	2.90 3.44	2.58 3.06	2.32 2.75	2.11 2.50	1.94 2.30	1.79 2.12	1.66 1.97
Short Leg Up	6×4	$\frac{3}{8}$ $\frac{1}{2}$	12.3 16.2	39813 52070	13.27 17.36	9.95 13.02	7.96 10.41	6.64 8.68	5.69 7.44	4.98 6.51	4.42 5.79	3.98 5.21	3.62 4.73	3.32 4.34	3.06 4.01	2.84 3.72
	$3 \times 2\frac{1}{2}$	$\frac{1}{4}$ $\frac{5}{16}$	4.5 5.6	4826 5934	1.61 1.98	1.21 1.48	.96 1.19	.80 .99	.69 .85	.60 .74	.54 .66	.48 .59	.44 .54			
	$3\frac{1}{2} \times 2\frac{1}{2}$	$\frac{1}{4}$ $\frac{5}{16}$	4.9 6.1	4952 6064	1.65 2.02	1.24 1.52	.99 1.21	.83 1.01	.71 .87	.62 .76	.55 .67	.50 .61	.45 .55	.41 .51		
	4×3	$\frac{5}{16}$ $\frac{3}{8}$	7.2 8.5	8839 10378	2.95 3.46	2.21 2.59	1.77 2.08	1.47 1.73	1.26 1.48	1.10 1.30	.98 1.15	.88 1.04	.80 .94	.74 .86	.68 .80	
	$4 \times 3\frac{1}{2}$	$\frac{5}{16}$ $\frac{3}{8}$	7.7 9.1	11907 14126	3.97 4.71	2.98 3.53	2.38 2.83	1.98 2.35	1.70 2.02	1.49 1.77	1.32 1.57	1.19 1.41	1.08 1.28	.99 1.18	.92 1.09	
	5×3	$\frac{5}{16}$ $\frac{3}{8}$	8.2 9.8	9052 10643	3.02 3.55	2.26 2.66	1.81 2.13	1.51 1.77	1.29 1.52	1.13 1.33	1.01 1.18	.91 1.06	.82 .97	.75 .89	.70 .82	
	$5 \times 3\frac{1}{2}$	$\frac{5}{16}$ $\frac{3}{8}$	8.7 10.4	12271 14454	4.09 4.82	3.07 3.61	2.45 2.89	2.05 2.41	1.75 2.06	1.53 1.81	1.36 1.61	1.23 1.45	1.12 1.31	1.02 1.20	.94 1.11	
	6×4	$\frac{3}{8}$ $\frac{1}{2}$	12.3 16.2	19216 24997	6.41 8.33	4.80 6.25	3.84 5.00	3.20 4.17	2.75 3.57	2.40 3.12	2.14 2.78	1.92 2.50	1.75 2.22	1.60 2.08	1.48 1.92	1.37 1.79

For Loads for Spans not tabulated divide the Coefficient of Strength by the Span in feet.

LOADS BY A. I. S. C. SPECIFICATION

Part IV

Section 3

American Standard Channels

Dimensions

Technical Functions

Allowable Total Loads

by

A. I. S. C. Specification

Connection Angles

Usual Stock Sizes	
Depth	Weight
3"	4.1#
4	5.4
5	6.7
6	8.2
7	9.8
8	11.5
9	13.4
10	15.3
12	20.7
15	33.9

3"

STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds

P is Minimum Span in feet uniformly loaded to cause V

W is Maximum Load on one Standard Connection

Q is Minimum Span in feet, uniformly loaded to cause W

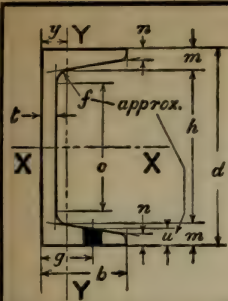
W is Weight of one Standard Connection including Angles and Web Rivets

y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange

Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"		3	3	3	Live Load Deflection must not exceed 1-360 of the Span. Total Def. x Live Load Live Load Def. = Tabular Load		
Wt. per foot..		4.1	5.0	6.0			
Area, sq. in. .		1.19	1.46	1.75			
b"		1.41	1.50	1.60			
t.....		.170	.258	.356			
h.....		2.246	2.246	2.246			
m.....		.377	.377	.377			
n.....		.170	.170	.170			
f.....		.270	.270	.270			
c.....		1.789	1.789	1.789			
g.....		7/8	7/8	7/8			
u.....		1/4	1/4	1/4			
AXES	X-X	l.....	1.6	1.8	2.1		
		S.....	1.07	1.2	1.4		
		r.....	1.17	1.12	1.08		
	Y-Y	l.....	0.20	0.25	0.31		
		S.....	0.21	0.24	0.27		
		r.....	0.41	0.41	0.42		
y.....		0.44	0.44	0.46			
Coef. Str.		12800	14400	16800	Total Deflection in Inches for Maximum Load; laterally fixed beam.		
Max.Mom. # %		19200	21600	25200			
V.....		6100	9300	12800			
P.feet.....		1.05	.77	.66			
W.....		7700	11600	11900			
Q.feet.....		.83	.62	.71			
w.lbs.....		5	5	5			
Rivet dia.....		1/2	1/2	1/2			
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free		
	1	12.2	12.2	14.4	14.4	16.8	16.8
	2	6.4	6.3	7.2	7.1	8.4	8.4
	3	4.3	3.7	4.8	4.1	5.6	5.0
	4	3.2	2.3	3.6	2.6	4.2	3.2
	5	2.6	..	2.9	1.8	3.4	2.2
	6	2.1	..	2.4	..	2.8	..
	7	1.8	..	2.1	..	2.4	..
	8	1.6	..	1.8	..	2.1	..
	9	1.4	..	1.6	..	1.9	..
	10	1.3	..	1.4	..	1.7	..
	11	1.2	..	1.3	..	1.5	..
	12	1.1	..	1.2	..	1.4	..
	13	1.0	..	1.1	..	1.3	..
	14	0.9	..	1.0	..	1.2	..
	15	0.8	..	1.0	..	1.1	..



STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets
 y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange.
 Allowable concentrated center loads are 50% and their deflections 80% of those shown



Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.										Total Deflection in inches for Maximum Load; laterally fixed beam.		Total Def. × Live Load Tabular Load	
Span feet		Laterally		Laterally		Laterally		Total Deflection must not exceed 1-360 of the Span.		Live Load Deflection must not exceed 1-360 of the Span.		Live Load Def. = Total Def. × Live Load Tabular Load	
		fixed	free	fixed	free	fixed	free						
Depth = d" Wt. per foot.. Area, sq. in.. b" t.. h.. m.. n.. f.. c.. g.. u.. AXES I.. S.. r.. Y-Y I.. S.. r.. y.. Coef. Str.. Max. Mom. % V.. P. feet.. W.. Q. feet.. w. lbs.. Rivet dia.. Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	4	4	4	4	4	4	4	4	4	4	4	4	4
	5.4	6.25	7.25	5.4	6.25	7.25	5.4	6.25	7.25	5.4	6.25	7.25	5.4
	1.56	1.82	2.12	1.56	1.82	2.12	1.56	1.82	2.12	1.56	1.82	2.12	1.56
	1.58	1.65	1.72	1.58	1.65	1.72	1.58	1.65	1.72	1.58	1.65	1.72	1.58
	.180	.247	.320	.180	.247	.320	.180	.247	.320	.180	.247	.320	.180
	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174	3.174
	.413	.413	.413	.413	.413	.413	.413	.413	.413	.413	.413	.413	.413
	.180	.180	.180	.180	.180	.180	.180	.180	.180	.180	.180	.180	.180
	.280	.280	.280	.280	.280	.280	.280	.280	.280	.280	.280	.280	.280
	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700	2.700
	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"	1"
	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16
	3.8	4.1	4.5	3.8	4.1	4.5	3.8	4.1	4.5	3.8	4.1	4.5	3.8
	1.9	2.05	2.25	1.9	2.05	2.25	1.9	2.05	2.25	1.9	2.05	2.25	1.9
	1.56	1.50	1.47	1.56	1.50	1.47	1.56	1.50	1.47	1.56	1.50	1.47	1.56
0.32	0.38	0.44	0.32	0.38	0.44	0.32	0.38	0.44	0.32	0.38	0.44	0.32	
0.29	0.32	0.35	0.29	0.32	0.35	0.29	0.32	0.35	0.29	0.32	0.35	0.29	
0.45	0.45	0.46	0.45	0.45	0.46	0.45	0.45	0.46	0.45	0.45	0.46	0.45	
0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	0.46	
22800	24600	27000	22800	24600	27000	22800	24600	27000	22800	24600	27000	22800	
34200	36900	40500	34200	36900	40500	34200	36900	40500	34200	36900	40500	34200	
8600	11900	15400	8600	11900	15400	8600	11900	15400	8600	11900	15400	8600	
1.33	1.03	0.88	1.33	1.03	0.88	1.33	1.03	0.88	1.33	1.03	0.88	1.33	
8100	11100	11900	8100	11100	11900	8100	11100	11900	8100	11100	11900	8100	
1.41	1.11	1.13	1.41	1.11	1.13	1.41	1.11	1.13	1.41	1.11	1.13	1.41	
5	5	5	5	5	5	5	5	5	5	5	5	5	
1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	1/2	
17.2	17.2	23.8	23.8	27.0	27.0	17.2	17.2	23.8	23.8	27.0	27.0	17.2	
11.4	11.4	12.3	12.3	13.5	13.5	11.4	11.4	12.3	12.3	13.5	13.5	11.4	
7.6	6.7	8.2	7.3	9.0	8.3	7.6	6.7	8.2	7.3	9.0	8.3	7.6	
5.7	4.3	6.2	4.8	6.7	5.4	5.7	4.3	6.2	4.8	6.7	5.4	5.7	
4.6	3.0	4.9	3.4	5.4	3.7	4.6	3.0	4.9	3.4	5.4	3.7	4.6	
3.8	..	4.1	..	4.5	..	3.8	..	4.1	..	4.5	..	3.8	
3.3	..	3.5	..	3.8	..	3.3	..	3.5	..	3.8	..	3.3	
2.9	..	3.1	..	3.4	..	2.9	..	3.1	..	3.4	..	2.9	
2.5	..	2.7	..	3.0	..	2.5	..	2.7	..	3.0	..	2.5	
2.3	..	2.5	..	2.7	..	2.3	..	2.5	..	2.7	..	2.3	
2.1	..	2.2	..	2.5	..	2.1	..	2.2	..	2.5	..	2.1	
1.9	..	2.1	..	2.3	..	1.9	..	2.1	..	2.3	..	1.9	
1.8	..	1.9	..	2.1	..	1.8	..	1.9	..	2.1	..	1.8	
1.6	..	1.8	..	1.9	..	1.6	..	1.8	..	1.9	..	1.6	
1.5	..	1.6	..	1.8	..	1.5	..	1.6	..	1.8	..	1.5	

5"

STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds

P is Minimum Span in feet uniformly loaded to cause V

W is Maximum Load on one Standard Connection

Q is Minimum Span in feet, uniformly loaded to cause W

w is Weight of one Standard Connection including Angles and Web Rivets

y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange

Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"	5	5	5	Live Load Deflection must not exceed 1-300 of the Span. Total Def. x Live Load Live Load Def. = Tabular Load	
Wt. per foot...	6.7	9.0	11.5		
Area, sq. in...	1.95	2.63	3.36		
b"	1.75	1.89	2.03		
t.....	.190	.325	.472		
h.....	4.100	4.100	4.100		
m.....	.450	.450	.450		
n.....	.190	.190	.190		
f.....	.290	.290	.290		
c.....	3.609	3.609	3.609		
g.....	1 1/8	1 1/8	1 1/8		
u.....	5/16	5/16	5/16		
AXES	X-X	I.....	7.4	8.8	10.4
		S.....	2.96	3.52	4.16
		r.....	1.95	1.83	1.76
	Y-Y	I.....	0.48	0.64	0.82
		S.....	0.38	0.45	0.54
		r.....	0.50	0.49	0.49
Coef. Str.....		35500	42200	49900	
Max. Mom. #		53300	63400	74900	
V.....		11400	19500	28500	
P. feet.....		1.56	1.08	0.88	
W.....		8600	11900	11900	
Q. feet.....		2.07	1.77	2.10	
w. lbs.....		6	6	6	
Rivet dia.....		1/2	1/2	1/2	

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; laterally fixed beam.
		fixed	free	fixed	free	fixed	free	
	1	22.8	22.8	39.0	39.0	49.2	49.2	.033 .059 .093
	2	17.8	17.8	21.1	21.1	24.9	24.9	
	3	11.8	10.9	14.0	13.2	16.6	15.6	
	4	8.9	7.2	10.5	8.8	12.5	10.4	
	5	7.1	5.0	8.4	6.2	10.0	7.4	
	6	5.9	..	7.0	4.5	8.3	5.3	.134 .182 .238 .302 .372
	7	5.1	..	6.0	..	7.1	..	
	8	4.4	..	5.3	..	6.2	..	
	9	3.9	..	4.7	..	5.5	..	
	10	3.6	..	4.2	..	5.0	..	
	11	3.2	..	3.8	..	4.5	..	.450 .537 .630 .730 .838
	12	3.0	..	3.5	..	4.2	..	
	13	2.7	..	3.2	..	3.8	..	
	14	2.5	..	3.0	..	3.6	..	
	15	2.4	..	2.8	..	3.3	..	
	16	2.2	..	2.6	..	3.1	..	.955 1.08 1.20 1.34 1.49
	17	2.1	..	2.5	..	2.9	..	
	18	2.0	..	2.3	..	2.8	..	
	19	1.9	..	2.2	..	2.6	..	
	20	1.8	..	2.1	..	2.5	..	

STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets
 y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown

6"



Depth = d"		6	6	6	6				
Wt. per foot...		8.2	10.5	13.0	15.5				
Area, sq. in...		2.39	3.07	3.81	4.54				
b"		1.92	2.03	2.16	2.28				
t.....		.200	.314	.437	.559				
h.....		5.026	5.026	5.026	5.026				
m.....		.487	.487	.487	.487				
n.....		.200	.200	.200	.200				
f.....		.300	.300	.300	.300				
c.....		4.518	4.518	4.518	4.518				
g.....		1 1/8	1 1/8	1 3/8	1 3/8				
u.....		5/16	3/8	3/8	3/8				
AXES	X-X	1.....	13.0	15.1	17.3	19.5			
		S.....	4.33	5.03	5.77	6.5			
	Y-Y	1.....	0.70	0.87	1.1	1.3			
		S.....	0.50	0.57	0.65	0.73			
		r.....	0.54	0.53	0.53	0.53			
		v.....	0.52	0.50	0.52	0.55			
Coef. Str.....		52000	60400	69200	78000				
Max.Mom. # "		78000	90200	103800	117000				
V.....		14400	22600	31500	40200				
P, feet.....		1.81	1.34	1.10	.97				
W.....		9000	11900	11900	11900				
Q, feet.....		2.89	2.54	2.91	3.28				
w, lbs.....		6	6	6	6				
Rivet dia.....		5/8	5/8	5/8	5/8				
Uniform Load in Kips, as fixed by shear or flexure, whichever is generally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free	
		fixed	free	fixed	free	fixed	free	fixed	free
	1	28.8	28.8	15.2	15.2	33.0	33.0	78.0	78.0
	2	26.0	26.0	30.2	30.2	34.6	34.6	39.0	39.0
	3	17.3	16.4	20.1	19.3	23.1	22.5	26.0	25.7
	4	13.0	11.0	15.1	13.1	17.3	15.4	19.5	18.1
	5	10.4	7.8	12.1	9.4	13.8	11.0	15.6	12.9
	6	8.7	5.7	10.1	6.9	11.5	8.3	13.0	9.6
	7	7.4	..	8.6	..	9.9	..	11.1	7.3
	8	6.5	..	7.6	..	8.7	..	9.8	..
	9	5.8	..	6.7	..	7.7	..	8.7	..
	10	5.2	..	6.0	..	6.9	..	7.8	..
	11	4.7	..	5.5	..	6.3	..	7.1	..
	12	4.3	..	5.0	..	5.8	..	6.5	..
	13	4.0	..	4.6	..	5.4	..	6.0	..
	14	3.7	..	4.3	..	5.0	..	5.6	..
	15	3.5	..	4.0	..	4.6	..	5.2	..
	16	3.3	..	3.8	..	4.3	..	4.9	..
	17	3.1	..	3.6	..	4.1	..	4.6	..
	18	2.9	..	3.4	..	3.8	..	4.3	..
	19	2.7	..	3.2	..	3.6	..	4.1	..
	20	2.6	..	3.0	..	3.5	..	3.9	..
	21	2.5	..	2.9	..	3.3	..	3.7	..
	22	2.4	..	2.7	..	3.1	..	3.5	..
	23	2.3	..	2.6	..	3.0	..	3.4	..
24	2.2	..	2.5	..	2.9	..	3.3	..	
25	2.1	..	2.4	..	2.8	..	3.1	..	

Live Load Deflection must not exceed 1-360 of the Span.

Total Def. × LiveLoad Tabular Load

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Total Deflection in
 inches for Maximum
 Load; laterally fixed
 beam.

Live Load Deflection must not exceed
 1-360 of the Span.
 $\text{Live Load Def.} = \frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

7"

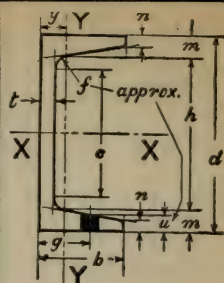


STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets
 y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown



Depth = d"		7	7	7	7	7	Total Deflection must not exceed 1-360 of the Span. Total Def. × LiveLoad LiveLoad Def. = <div>Tabular Load</div>			
Wt. per foot...		9.8	12.25	14.75	17.25	19.75				
Area, sq. in.		2.85	3.58	4.32	5.05	5.79				
b"		2.09	2.19	2.30	2.40	2.51				
t		.210	.314	.419	.524	.629				
h		5.954	5.954	5.954	5.954	5.954				
n		.523	.523	.523	.523	.523				
m		.210	.210	.210	.210	.210				
f		.310	.310	.310	.310	.310				
c		5.429	5.429	5.429	5.429	5.429				
u		1 1/4	1 1/4	1 1/4	1 1/2	1 1/2				
g		3/8	3/8	7/16	7/16	7/16				
AXES	X X	I.....	21.1	24.1	27.1	30.1	33.1			
		S.....	6.03	6.88	7.74	8.60	9.46			
		T.....	2.72	2.59	2.51	2.44	2.39			
	Y Y	I.....	0.98	1.2	1.4	1.6	1.8			
S.....		0.63	0.71	0.79	0.86	0.96				
T.....		0.59	0.58	0.57	0.56	0.56				
V.....		0.55	0.53	0.53	0.55	0.58				
Coef. Str.		72300	82600	92900	103200	113500	Total Deflection in inches for Maximum Load, laterally fixed beam.			
Max. Mom. #		108500	123900	139400	154800	170200				
V.....		17600	25500	35200	44000	52800				
P.....		2.05	1.56	1.32	1.17	1.07				
W.....		9500	11900	11900	11900	11900				
Q.....		3.81	3.47	3.90	4.34	4.77				
w.....		6	6	6	6	6				
Rivet dia.....		5/8	5/8	5/8	5/8	5/8				
Allowable Uniform Load in Kips, as fixed by span or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient Strength by the Span in feet.	Span feet	Laterally fixed	free	Laterally fixed	free	Laterally fixed		free	Laterally fixed	free
	1	35.2	35.2	52.8	52.8	70.4		70.4	88.0	88.0
2	35.2	35.2	41.3	41.3	46.4	46.4		51.6	51.6	
3	24.1	23.3	27.5	26.9	31.0	30.7	34.4	34.4		
4	18.1	15.9	20.7	18.5	23.2	21.2	25.8	23.9		
5	14.5	11.2	16.5	13.4	18.6	15.4	20.6	17.4		
6	12.1	8.5	13.8	10.0	15.5	11.1	17.2	13.3		
7	10.3	6.4	11.8	7.6	13.3	8.9	14.7	10.1		
8	9.0	..	10.3	..	11.6	..	12.9	8.0		
9	8.0	..	9.2	..	10.3	..	11.5	..		
10	7.2	..	8.3	..	9.3	..	10.3	..		
11	6.6	..	7.5	..	8.4	..	9.4	..		
12	6.0	..	6.9	..	7.7	..	8.6	..		
13	5.5	..	6.4	..	7.1	..	7.9	..		
14	5.1	..	5.9	..	6.6	..	7.4	..		
15	4.8	..	5.5	..	6.2	..	6.9	..		
16	4.5	..	5.2	..	5.8	..	6.5	..		
17	4.3	..	4.9	..	5.5	..	6.1	..		
18	4.0	..	4.6	..	5.2	..	5.7	..		
19	3.8	..	4.3	..	4.9	..	5.4	..		
20	3.6	..	4.1	..	4.6	..	5.2	..		
21	3.4	..	3.9	..	4.4	..	4.9	..		
22	3.3	..	3.8	..	4.2	..	4.7	..		
23	3.1	..	3.6	..	4.0	..	4.4	..		
24	3.0	..	3.4	..	3.9	..	4.3	..		
25	2.9	..	3.3	..	3.7	..	4.1	..		

Allowable Uniform Load in Kips, as fixed by given or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS


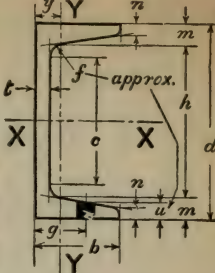
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 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets
 y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange
 Deflection concentrated center loads are 50% and their deflections 80% of those shown

8"



Depth = d"		8		8		8		8		8		Live Load Deflection must not exceed 1-360 of the Span. Total Def. × Live Load Tabular Load	
Wt. per foot...		11.50		13.75		16.25		18.75		21.25			
Area, sq. in.		3.36		4.02		4.76		5.49		6.23			
b"		2.26		2.34		2.44		2.53		2.62			
t		.220		.303		.395		.487		.579			
h		6.880		6.880		6.880		6.880		6.880			
m		.560		.560		.560		.560		.560			
n		.220		.220		.220		.220		.220			
f		.320		.320		.320		.320		.320			
c		6.338		6.338		6.338		6.338		6.338			
g		1 3/8		1 3/8		1 1/2		1 1/2		1 1/2			
u		3/8		3/8		7/16		7/16		7/16			
AXES	X-X	I	32.3	35.8	39.8	43.7	47.6	Total Deflection in Inches for Maximum Load, laterally fixed beam.					
		S <td>8.08</td> <td>8.95</td> <td>9.95</td> <td>10.92</td> <td>11.9</td>	8.08	8.95	9.95	10.92	11.9						
	r	3.10	2.99	2.89	2.82	2.77							
	Y-Y	I	1.3	1.5	1.8	2.0	2.2						
Y-Y	S	.79	.86	.94	1.0	1.1							
		r	.63	.62	.61	.60	.60						
	y	.58	.56	.56	.57	.59							
	Coef. Str.		96900	107400	119400	131100	142800	Total Deflection in Inches for Maximum Load, laterally fixed beam.					
Max. Mom. #		145400	161100	179100	196700	214200							
V		21100	29100	37900	46800	55600							
P. feet		2.30	1.80	1.58	1.40	1.28							
W		19800	23800	23800	23800	23800							
Q. feet		2.45	2.26	2.51	2.75	3.00							
w. lbs.		13	13	13	13	13							
Rivet dia.		3/4	3/4	3/4	3/4	3/4							
Allowable Uniform Load in Kips, as fixed by shear or flexure whichever is least For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free		Laterally fixed	Laterally free			
		fixed	free	fixed	free	fixed	free		fixed	free			
	1	42.2	42.2	58.2	58.2	75.8	75.8	93.6	93.6	.021 .037 .058			
	2	12.2	42.2	53.7	53.7	59.7	59.7	55.6	65.6				
	3	32.3	31.9	35.8	35.6	39.8	39.8	43.7	43.7				
	4	24.2	22.0	26.9	24.7	29.8	27.7	32.8	30.9				
	5	19.4	15.9	21.5	18.0	23.9	20.4	26.3	22.8				
	6	16.1	12.0	17.9	13.5	19.9	15.4	21.9	17.3	23.8		19.2	.084 .114 .149 .189 .233
	7	13.8	9.0	15.3	10.3	17.1	12.0	18.7	13.4	20.4		15.0	
	8	12.1	..	13.4	..	14.9	9.3	16.4	10.6	17.9		11.9	
	9	10.8	..	11.9	..	13.3	..	14.5	..	15.9		..	
	10	9.7	..	10.7	..	11.9	..	13.1	..	14.3		..	
	11	8.8	..	9.8	..	10.8	..	11.9	..	13.0		..	.281 .335 .394 .456 .524
	12	8.1	..	8.9	..	9.9	..	10.9	..	11.9		..	
	13	7.5	..	8.3	..	9.1	..	10.1	..	11.0		..	
	14	6.9	..	7.7	..	8.5	..	9.3	..	10.2		..	
	15	6.5	..	7.2	..	7.9	..	8.7	..	9.5		..	
	16	6.1	..	6.8	..	7.4	..	8.2	..	8.9		..	.596 .674 .754 .840 .931
	17	5.7	..	6.4	..	7.0	..	7.7	..	8.4		..	
	18	5.4	..	6.0	..	6.6	..	7.3	..	7.9		..	
19	5.1	..	5.7	..	6.3	..	6.9	..	7.5	..			
20	4.8	..	5.4	..	6.0	..	6.6	..	7.1	..			
21	4.6	..	5.1	..	5.7	..	6.2	..	6.8	..	1.03 1.13 1.25 1.34 1.46		
22	4.4	..	4.9	..	5.4	..	6.0	..	6.5	..			
23	4.2	..	4.7	..	5.2	..	5.7	..	6.2	..			
24	4.0	..	4.5	..	5.0	..	5.5	..	6.0	..			
25	3.9	..	4.3	..	4.8	..	5.2	..	5.7	..			

<div>9"</div> <div></div>		<div>STANDARD CHANNELS</div> <div>DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS</div> <div>I is Moment of Inertia S is Section Modulus r is Radius of Gyration V is Maximum Web Shear in Pounds P is Minimum Span in feet uniformly loaded to cause V W is Maximum Load on one Standard Connection Q is Minimum Span in feet, uniformly loaded to cause W w is Weight of one Standard Connection including Angles and Web Rivets y is Distance in inches between Center of Gravity and back of Channel</div> <div>Rivet given is maximum diameter in flange Allowable concentrated center loads are 50% and their deflections 80% of those shown</div>				<div></div>				
Depth = d"		9	9	9	9	Live Load Deflection must not exceed 1-360 of the Span. LiveLoadDef. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$				
Wt. per foot		13.4	15.0	20.0	25.0					
Area, sq. in.		3.89	4.39	5.86	7.33					
b"		2.43	2.49	2.65	2.81					
t		.230	.285	.448	.612					
h		7.806	7.806	7.806	7.806					
m		.597	.597	.597	.597					
g		.230	.230	.230	.230					
f		.330	.330	.330	.330					
c		7.247	7.247	7.247	7.247					
u		1 $\frac{3}{16}$	1 $\frac{3}{8}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$					
r		$\frac{7}{16}$	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{1}{2}$					
AXES	X-X	I	47.3	50.7	60.6	70.5				
		S	10.51	11.27	13.47	15.66				
		r	3.49	3.40	3.22	3.10				
	Y-Y	I	1.8	1.9	2.4	3.0				
S		0.97	1.0	1.2	1.4					
r		.67	.67	.65	.64					
y		.61	.59	.59	.61					
Coef. Str.		126100	135200	161600	188000	Total Deflection in inches for Maximum Load; laterally fixed beam.				
Max.Mom.#		189200	202800	242400	282000					
V		24800	30800	48500	66100					
P, feet		2.54	2.19	1.67	1.42					
W		20700	23800	23800	23800					
Q, feet		3.05	2.84	3.39	3.95					
w, lbs.		13	13	13	13					
Rivet dia.		$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$					
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally fixed	Laterally fixed	Laterally fixed					
		fixed	free	fixed	free					
	1	49.6	49.6	51.6	61.6	97.0	97.0	132	132	
	2	49.6	49.6	61.6	61.6	80.8	80.8	94.0	94.0	
	3	42.0	42.0	45.1	45.1	53.9	53.9	62.7	62.7	.019
	4	31.5	29.3	33.8	31.7	40.4	38.6	47.0	45.5	.033
	5	25.2	21.5	27.0	23.2	32.3	28.6	37.6	34.1	.052
	6	21.0	16.2	22.5	17.6	26.9	21.8	31.3	26.2	.074
	7	18.0	12.5	19.4	13.7	23.1	17.1	26.9	20.6	.101
	8	15.8	9.9	16.9	10.7	20.2	13.6	23.5	16.5	.132
	9	14.0	..	15.0	..	18.0	..	21.0	13.4	.168
	10	12.6	..	13.5	..	16.2	..	18.8	..	.207
	11	11.5	..	12.3	..	14.7	..	17.1	..	.250
	12	10.5	..	11.3	..	13.5	..	15.7	..	.298
	13	9.7	..	10.4	..	12.4	..	14.5	..	.350
	14	9.0	..	9.7	..	11.5	..	13.4	..	.406
	15	8.4	..	9.0	..	10.8	..	12.5	..	.466
	16	7.9	..	8.4	..	10.2	..	11.8	..	.530
	17	7.4	..	8.0	..	9.5	..	11.1	..	.599
	18	7.0	..	7.5	..	9.0	..	10.4	..	.670
	19	6.6	..	7.1	..	8.5	..	9.9	..	.747
	20	6.3	..	6.8	..	8.1	..	9.4	..	.828
21	6.0	..	6.4	..	7.7	..	9.0	..	.912	
22	5.7	..	6.1	..	7.3	..	8.5	..	1.00	
23	5.5	..	5.9	..	7.0	..	8.2	..	1.10	
24	5.3	..	5.6	..	6.7	..	7.8	..	1.19	
25	5.0	..	5.4	..	6.5	..	7.5	..	1.29	

STANDARD CHANNELS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and Web Rivets
y is Distance in inches between Center of Gravity and back of Channel

Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"	12	12	12	12	12	
Wt. per foot...	20.7	25.0	30.0	35.0	40.0	
Area, sq. in. . .	6.03	7.32	8.79	10.26	11.73	
b"	2.94	3.05	3.17	3.29	3.42	
t.....	.280	.387	.510	.632	.755	
h.....	10.554	10.554	10.554	10.554	10.554	
m.....	.723	.723	.723	.723	.723	
n.....	.280	.280	.280	.280	.280	
f.....	.380	.380	.380	.380	.380	
c.....	9.910	9.910	9.910	9.910	9.910	
g.....	13/4	13/4	13/4	2	2	
u.....	1/2	1/2	1/2	5/8	5/8	
AXES	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
Coef. Str.	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
Max. Mom. %	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
V.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
P. feet.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
W.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
Q. feet.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
w. lbs.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75
Rivet dia.....	I.....	128.1	143.5	161.2	178.8	196.5
		21.35	23.92	26.87	29.8	32.75
		4.61	4.43	4.28	4.18	4.09
	S.....	3.9	4.5	5.2	5.9	6.6
		1.7	1.9	2.1	2.3	2.5
		.81	.79	.77	.76	.75

Live Load Deflection must not exceed 1-360 of the Span.
Live Load Def. = Total Def. × Live Load Tabular Load

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
1	81	81	111	111	147	147	182	182	217	217		
	81	81	111	111	147	147	179	179	197	197		
2	81	81	96	96	108	108	119	119	131	131		.014
	64	63	72	71	81	80	89	89	98	98		
3	51	47	57	53	65	61	72	68	79	76		.025
	43	37	48	42	54	47	60	53	66	60		
4	37	29	41	33	46	38	51	43	56	48		.039
	32	23	36	27	40	31	45	35	49	39		
5	28	19	32	22	36	25	40	29	44	32		.056
	26	...	29	18	32	21	36	24	39	27		
6	23	...	26	...	29	...	33	...	36	23		.076
	21	...	24	...	27	...	30	...	33	...		
7	20	...	22	...	25	...	28	...	30099
	18	...	21	...	23	...	26	...	28	...		
8	17	...	19	...	22	...	24	...	26126
	16	...	18	...	20	...	22	...	25	...		
9	15	...	17	...	19	...	21	...	23155
	14	...	16	...	18	...	20	...	22	...		
10	13	...	15	...	17	...	19	...	21188
	13	...	14	...	16	...	18	...	20	...		
11	12	...	14	...	15	...	17	...	19223
	12	...	13	...	15	...	16	...	18	...		
12	11	...	13	...	14	...	16	...	17263
	11	...	12	...	13	...	15	...	16	...		
13	10	...	12	...	13	...	14	...	16304
	10	...	11	...	12	...	14	...	15	...		
14	10	...	11	...	12	...	14	...	15341
	10	...	11	...	12	...	14	...	15	...		
15	10	...	11	...	12	...	14	...	15398
	10	...	11	...	12	...	14	...	15	...		
16	10	...	11	...	12	...	14	...	15449
	10	...	11	...	12	...	14	...	15	...		
17	10	...	11	...	12	...	14	...	15503
	10	...	11	...	12	...	14	...	15	...		
18	10	...	11	...	12	...	14	...	15560
	10	...	11	...	12	...	14	...	15	...		
19	10	...	11	...	12	...	14	...	15621
	10	...	11	...	12	...	14	...	15	...		
20	10	...	11	...	12	...	14	...	15684
	10	...	11	...	12	...	14	...	15	...		
21	10	...	11	...	12	...	14	...	15751
	10	...	11	...	12	...	14	...	15	...		
22	10	...	11	...	12	...	14	...	15822
	10	...	11	...	12	...	14	...	15	...		
23	10	...	11	...	12	...	14	...	15894
	10	...	11	...	12	...	14	...	15	...		
24	10	...	11	...	12	...	14	...	15970
	10	...	11	...	12	...	14	...	15	...		
25	10	...	11	...	12	...	14	...	15	...		1.050
	10	...	11	...	12	...	14	...	15	...		
26	10	...	11	...	12	...	14	...	15	...		
	10	...	11	...	12	...	14	...	15	...		

Part IV

Section 4

American Standard Beams

Dimensions

Technical Functions


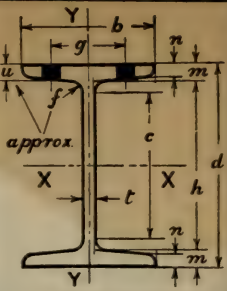
Allowable Total Loads
by

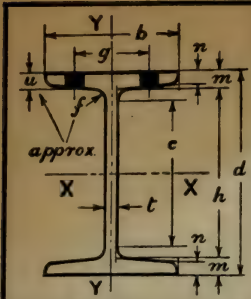
A. I. S. C. Specification

Allowable End Reactions

Standard Connection Angles

Usual Stock Sizes	
Depth	Weight
3"	5.7 *
4	7.7
5	10.0
6	12.5
7	15.3
8	18.4
9	21.8
10	25.4
12	31.8
15	42.9
18	54.7
20	65.4
24	79.9

3" 		STANDARD BEAMS				
		DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS				
		I is Moment of Inertia S is Section Modulus r is Radius of Gyration V is Maximum Web Shear in Pounds P is Minimum Span in feet uniformly loaded to cause V R is Allowable End Reaction for 3 3/8" bearing. For details see page of Allowable End Reactions W is Maximum Load on one Standard Connection Q is Minimum Span in feet, uniformly loaded to cause W w is Weight of one Standard Connection including Angles and Web Rivets				
		Rivet given is maximum diameter in flange Allowable concentrated center loads are 50% and their deflections 80% of those shown				
Depth = d"		3	3	3	Live Load Deflection must not exceed 1-360 of the Span. Total Def. × Live Load Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$	
Wt. per foot...		5.7	6.5	7.5		
Area, sq. in....		1.64	1.88	2.17		
b"		2.33	2.41	2.51		
t		.170	.251	.349		
h		2.300	2.300	2.300		
m		.350	.350	.350		
n		.170	.170	.170		
f		.270	.270	.270		
c		1.843	1.843	1.843		
s		1 1/2	1 1/2	1 1/2	Live Load Deflection in inches for Maximum Load; laterally fixed beam.	
u		5/16	5/16	5/16		
AXES	I.....	2.5	2.7	2.9		
	S.....	1.67	1.80	1.93		
	r.....	1.23	1.19	1.15		
Y-Y	I.....	0.46	0.51	0.59		
	S.....	0.40	0.43	0.47		
	r.....	0.53	0.52	0.52		
Coef. Str.....		20000	21600	23200		
Max. Mom. " #		30000	32400	34800		
V.....		6100	9000	12600		
P. feet.....		1.64	1.20	0.92		
R.....		6100	9000	12600		
W.....		7650	11300	11900		
Q. feet.....		1.31	0.96	0.97		
w. lbs.....		5	5	5		
Rivet dia.....		3/8	3/8	3/8		
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam load not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		
		fixed	free	fixed	free	
	1	12.2	12.2	18.0	18.0	
	2	10.0	10.0	10.8	10.8	
	3	6.7	6.6	7.2	7.2	
	4	5.0	4.6	5.4	5.0	
	5	4.0	3.3	4.3	3.6	
	6	3.3	2.5	3.6	2.8	
	7	2.9	1.9	3.1	2.1	
	8	2.5	..	2.7	1.7	
	9	2.2	..	2.4	..	
	10	2.0	..	2.2	..	
	11	1.8	..	2.0	..	
	12	1.7	..	1.8	..	
	13	1.5	..	1.7	..	
	14	1.4	..	1.5	..	
	15	1.3	..	1.4	..	



STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown

4"

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Total Deflection in inches for Maximum Load; laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	
1	18.2	18.2	24.2	24.2	31.2	31.2	38.4	38.4		
2	18.0	18.0	18.9	18.9	20.1	20.1	21.3	21.3		.019
3	12.0	12.0	12.6	12.6	13.4	13.4	14.2	14.2		.042
4	9.0	8.6	9.5	9.1	10.1	10.0	10.7	10.4		.074
5	7.2	6.4	7.6	6.8	8.0	7.2	8.5	7.7		.116
6	6.0	4.9	6.3	5.2	6.7	5.6	7.1	6.0		.168
7	5.1	3.8	5.4	4.1	5.7	4.4	6.1	4.7		.228
8	4.5	3.0	4.7	3.2	5.0	3.5	5.3	3.8		.298
9	4.0	...	4.2	2.6	4.5	2.9	4.7	3.1		.378
10	3.6	...	3.8	...	4.0	...	4.3465
11	3.3	...	3.4	...	3.7	...	3.9562
12	3.0	...	3.1	...	3.4	...	3.6670
13	2.8	...	2.9	...	3.1	...	3.3787
14	2.6	...	2.7	...	2.9	...	3.0912
15	2.4	...	2.5	...	2.7	...	2.8	...		1.05

Depth = d" Wt. per foot. Area, sq. in. b" t h n f c u	4 7.7 2.21 2.66 .190 3.208 .396 .190 .29 2.717 1½ 5/16	4 8.5 2.46 2.72 .253 3.208 .396 .190 .29 2.717 1½ 5/16	4 9.5 2.76 2.80 .326 3.208 .396 .190 .29 2.717 1½ 5/16	4 10.5 3.05 2.87 .400 3.208 .396 .190 .29 2.717 1½ 5/16	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = Total Def. × Live Load Tabular Load
AXES						
Y-Y	I	6.0	6.3	6.7	7.1	
	S	3.0	3.15	3.35	3.55	
	r	1.64	1.60	1.56	1.52	
X-X	I	0.77	0.83	0.91	1.0	
	S	0.58	0.61	0.65	0.70	
	r	0.59	0.58	0.58	0.57	
Coef. Str.	36000	37800	40200	42600		
Max. Mom. #	54000	56700	60300	63900		
V	9100	12100	15600	19200		
P. feet	1.98	1.56	1.29	1.11		
R	9100	12100	15600	19200		
W	8550	11400	11900	11900		
Q. feet	2.11	1.66	1.69	1.79		
w. lbs.	5	5	5	5		
Rivet dia.	½	½	½	½		

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"	5	5	5	Live Load Deflection must not exceed 1-360 of the Span.	Total Def. \times Live Load Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
Wt. per foot...	10.0	12.25	14.75				
Area, sq. in...	2.87	3.56	4.29	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
b"	3.00	3.14	3.28				
t	.210	.347	.494	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
h	4.114	4.114	4.114				
m	.443	.443	.443	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
n	.210	.210	.210				
f	.31	.31	.31	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
c	3.589	3.589	3.589				
g	$1\frac{3}{4}$	$1\frac{3}{4}$	$1\frac{3}{4}$	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$		
u	$\frac{3}{8}$	$\frac{3}{8}$	$\frac{3}{8}$				
AXES	X-X	I	12.1	13.5	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$	
	X-X	S	4.84	5.40			
	X-X	r	2.05	1.95			
Y-Y	Y-Y	I	1.2	1.4	Live Load Deflection must not exceed 1-360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$	
	Y-Y	S	0.82	0.91			
	Y-Y	r	0.65	0.63			
Coef. Str.	58100	64860	72000	Total Deflection in Inches for Maximum Load; laterally fixed beam.			
Max. Mom. #	87120	97200	108000				
V	12600	20800	29600	Total Deflection in Inches for Maximum Load; laterally fixed beam.			
P. feet	2.30	1.56	1.22				
R	12600	20800	29600	Total Deflection in Inches for Maximum Load; laterally fixed beam.			
W	9450	11900	11900				
Q. feet	3.07	2.73	3.03	Total Deflection in Inches for Maximum Load; laterally fixed beam.			
w. lbs.	6	6	6				
Rivet dia.	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	Total Deflection in Inches for Maximum Load; laterally fixed beam.			
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Total Deflection in Inches for Maximum Load; laterally fixed beam.	
		fixed	free	fixed	free		
	1	25.2	25.2	41.6	41.6		.033
	2	25.2	25.2	32.4	32.4		
	3	19.4	19.4	21.6	21.6		
	4	14.5	14.5	16.2	16.1		
	5	11.6	10.7	13.0	12.2		
	6	9.7	8.4	10.8	9.5		.134
	7	8.3	6.6	9.3	7.6		
	8	7.3	5.4	8.1	6.1		
	9	6.5	4.4	7.2	5.0		
	10	5.8	...	6.5	4.2		
	11	5.3	...	5.9450
	12	4.8	...	5.4	...		
	13	4.5	...	5.0	...		
	14	4.2	...	4.6	...		
	15	3.9	...	4.3	...		
	16	3.6	...	4.1955
	17	3.4	...	3.8	...		
	18	3.2	...	3.6	...		
	19	3.1	...	3.4	...		
	20	2.9	...	3.2	...		

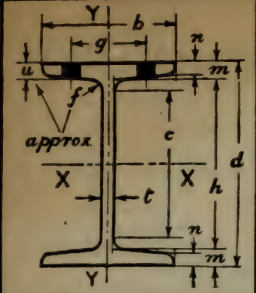
STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 R is Allowable End Reaction for 3/4" bearing. For details see page of Allowable End Reactions
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown

6"
 I



Depth = d"	6	6	6
Wt. per foot...	12.5	14.75	17.25
Area, sq. in...	3.61	4.29	5.02
b"	3.33	3.44	3.57
t	.230	.343	.465
h	5.024	5.024	5.024
m	.488	.488	.488
n	.230	.230	.230
f	.33	.33	.33
c	4.465	4.465	4.465
g	2	2	2
u	3/8	3/8	3/8
AXES			
X-X	1	21.8	23.8
S	7.27	7.93	8.67
r	2.46	2.36	2.28
Y-Y	1	1.8	2.1
S	1.1	1.2	1.3
r	.72	.69	.68
Coef. Str.	87200	95200	104000
Max. Mom. #	130800	142800	156000
V	16600	24700	34500
P. feet	2.63	1.93	1.51
R	16600	24700	34500
W	10350	11900	11900
Q. feet	4.21	4.00	4.37
w. lbs.	6	6	6
Rivet dia.	5/8	5/8	5/8

Live Load Deflection must not exceed 1-360 of the Span.
 Live Load Def. = Total Def. × Live Load
 Tabular Load

Total Deflection in inches for Maximum Load, laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		
		fixed	free	fixed	free	fixed	free	fixed	free	
	2	33.2	33.2	47.6	47.6	52.0	52.0			
	3	29.1	29.1	31.7	31.7	34.7	34.7			.028
	4	21.8	21.8	23.8	23.8	26.0	26.0			.050
	5	17.4	16.6	19.0	18.3	20.8	20.2			.078
	6	14.5	13.1	15.9	14.5	17.3	16.0			.112
	7	12.5	10.5	13.6	11.6	14.9	13.0			.152
	8	10.9	8.5	11.9	9.5	13.0	10.6			.198
	9	9.7	7.1	10.6	7.9	11.6	8.9			.252
	10	8.7	5.9	9.5	6.6	10.4	7.4			.310
	11	7.9	5.0	8.7	5.6	9.5	6.3			.375
	12	7.3	...	7.9	...	8.7447
	13	6.7	...	7.3	...	8.0525
	14	6.2	...	6.8	...	7.4608
	15	5.8	...	6.3	...	6.9698
	16	5.5	...	6.0	...	6.5795
	17	5.1	...	5.6	...	6.1898
	18	4.8	...	5.3	...	5.8	...			1.01
	19	4.6	...	5.0	...	5.5	...			1.12
	20	4.4	...	4.8	...	5.2	...			1.24
	21	4.2	...	4.5	...	5.0	...			1.37
	22	4.0	...	4.3	...	4.7	...			1.51
	23	3.8	...	4.1	...	4.5	...			1.64
	24	3.6	...	4.0	...	4.3	...			1.79
	25	3.5	...	3.8	...	4.2	...			1.94

7"

STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds

P is Minimum Span in feet uniformly loaded to cause V

R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions

W is Maximum Load on one Standard Connection

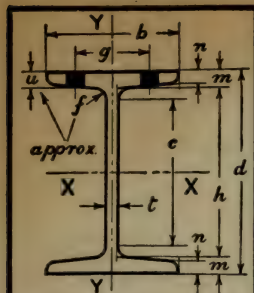
Q is Minimum Span in feet, uniformly loaded to cause W

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange

Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"	7	7	7	Live Load Deflection must not exceed 1-360 of the Span. Total Def. x Live Load Live Load Def. = Tabular Load		
Wt. per foot..	15.3	17.5	20.0			
Area, sq. in...	4.43	5.09	5.83			
b"	3.66	3.76	3.86			
t	.250	.345	.450			
h	5.936	5.936	5.936			
m	.534	.534	.534			
n	.250	.250	.250			
f	.35	.35	.35			
c	5.339	5.339	5.339			
g	2¼	2¼	2¼	Live Load Deflection in inches for Maximum Load; laterally fixed beam.		
u	⅜	⅜	⅜			
AXES	X-X	I.....	36.2	38.9	41.9	
		S.....	10.34	11.11	11.97	
		r.....	2.86	2.77	2.68	
Y-Y	I.....	I.....	2.7	2.9	3.1	
		S.....	1.5	1.6	1.6	
		r.....	0.78	0.76	0.74	
Coef. Str.....		124100	133400	143700		
Max.Mom. #		186200	200100	215500		
V.....		21000	29000	37800		
P. feet.....		2.95	2.30	1.90		
R.....		19700	27200	35400		
W.....		11250	11900	11900		
Q. feet.....		5.52	5.60	6.04		
w. lbs.....		6	6	6		
Rivet dia.....		⅝	⅝	⅝		
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed free		Laterally fixed free		
	2	42.0	42.0	58.0	58.0	
	3	41.4	41.4	44.5	44.5	
	4	31.0	31.0	33.4	33.4	
	5	24.8	24.3	26.7	26.3	
	6	20.7	19.3	22.2	20.9	
	7	17.7	15.6	19.1	17.0	
	8	15.5	12.8	16.7	14.0	
	9	13.8	10.7	14.8	11.6	
	10	12.4	9.0	13.3	9.8	
	11	11.3	7.6	12.1	8.3	
	12	10.3	6.4	11.1	7.1	
	13	9.5	...	10.3	...	
	14	8.9	...	9.5	...	
	15	8.3	...	8.9	...	
	16	7.7	...	8.3	...	
	17	7.3	...	7.8	...	
	18	6.9	...	7.4	...	
	19	6.5	...	7.0	...	
	20	6.2	...	6.7	...	
	21	5.9	...	6.4	...	
	22	5.6	...	6.1	...	
	23	5.4	...	5.8	...	
	24	5.2	...	5.6	...	
	25	5.0	...	5.3	...	



STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 R is Allowable End Reaction for 3/4" bearing. For details see page of Allowable End Reactions
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown

8"

Depth = d"	8	8	8	8
Wt. per foot..	18.4	20.5	23.0	25.5
Area, sq. in...	5.34	5.97	6.71	7.43
b"	4.00	4.08	4.17	4.26
t"	.270	.349	.441	.532
c"	6.838	6.838	6.838	6.838
m"	.581	.581	.581	.581
n"	.270	.270	.270	.270
r"	.37	.37	.37	.37
f"	6.211	6.211	6.211	6.211
g"	2 1/4	2 1/4	2 1/4	2 1/4
h"	7 1/16	7 1/16	7 1/16	7 1/2
AXES	I	S	r	I
X-X	56.9	60.2	64.2	68.1
Y-Y	14.22	15.05	16.05	17.02
	3.26	3.18	3.09	3.03
	3.8	4.0	4.4	4.7
	1.9	2.0	2.1	2.2
	0.84	0.82	0.81	0.80
Coef. Str.	170700	180600	192600	204300
Max. Mom. #	256100	270900	288900	306450
V	25900	33500	42300	51100
P. feet	3.30	2.70	2.28	2.00
R	22300	28800	36400	43900
W	23800	23800	23800	23800
Q. feet	3.59	3.79	4.05	4.29
w. lbs.	13	13	13	13
Rivet dia.	3/4	3/4	3/4	3/4

Live Load Deflection must not exceed 1-360 of the Span.
 Live Load Def. = Total Def. × Live Load
 Tabular Load

Total Deflection in inches for Maximum Load; laterally fixed beam.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Total Deflection in inches for Maximum Load; laterally fixed beam.
	fixed	free	fixed	free	fixed	free	fixed	free	
2	51.8	51.8	67.0	67.0	84.6	84.6			
3	51.8	51.8	60.2	60.2	64.2	64.2	68.1	68.1	.037
4	42.7	42.7	45.2	45.2	48.2	48.2	51.1	51.1	.058
5	34.1	34.1	36.1	36.1	38.5	38.5	40.9	40.9	
6	28.5	27.2	30.1	28.9	32.1	31.0	34.1	33.1	.084
7	24.4	22.2	25.8	23.7	27.5	25.4	29.2	27.2	.114
8	21.3	18.4	22.6	19.7	24.1	21.2	25.5	22.6	.149
9	19.0	15.5	20.1	16.5	21.4	17.8	22.7	19.1	.189
10	17.1	13.1	18.1	14.0	19.3	15.2	20.4	16.2	.233
11	15.5	11.1	16.4	11.9	17.5	13.0	18.6	14.0	.281
12	14.2	9.6	15.1	10.3	16.1	11.2	17.0	12.0	.335
13	13.1	8.3	13.9	8.9	14.8	9.7	15.7	10.4	.394
14	12.2	...	12.9	...	13.8	...	14.6	9.1	.456
15	11.4	...	12.0	...	12.8	...	13.6524
16	10.7	...	11.3	...	12.0	...	12.8596
17	10.0	...	10.6	...	11.3	...	12.0674
18	9.5	...	10.0	...	10.7	...	11.4754
19	9.0	...	9.5	...	10.1	...	10.8840
20	8.5	...	9.0	...	9.6	...	10.2931
21	8.1	...	8.6	...	9.2	...	9.7	...	1.03
22	7.8	...	8.2	...	8.8	...	9.3	...	1.13
23	7.4	...	7.9	...	8.4	...	8.9	...	1.23
24	7.1	...	7.5	...	8.0	...	8.5	...	1.34
25	6.8	...	7.2	...	7.7	...	8.2	...	1.46

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for 3 1/2" bearing. For details see page of Allowable End Reactions
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their deflections 80% of those shown

Depth = d"	9	9	9	9	Live Load Deflection must not exceed 1/360 of the Span. Total Def. x Live Load Live Load Def = Tabular Load	
Wt. per foot...	21.8	25.0	30.0	35.0		
Area, sq. in...	6.32	7.28	8.76	10.22		
b"	4.33	4.44	4.60	4.76		
t	.290	.397	.561	.724		
h	7.746	7.746	7.746	7.746		
m	.627	.627	.627	.627		
n	.290	.290	.290	.290		
f	.39	.39	.39	.39		
c	7.085	7.085	7.085	7.085		
u	2 1/2	2 1/2	2 1/2	2 1/2		
	1/2	1/2	1/2	1/2		
AXES	X-X	I	84.9	91.4	101.4	111.3
		S	18.87	20.31	22.53	24.73
		r	3.67	3.54	3.40	3.30
Y-Y	I	5.2	5.6	6.4	7.3	
		S	2.4	2.5	2.8	3.0
		r	0.90	0.88	0.85	0.84
Coef. Str.	226400	243700	270400	296800	Total Deflection in Inches for Maximum Load: laterally fixed beam	
Max. Mom. #	33960	36560	40360	44520		
V	31360	42900	60660	78200		
P. feet	3.62	2.84	2.23	1.90		
R	25000	34200	48400	62400		
W	23800	23800	23800	23800		
Q. feet	4.76	5.12	5.68	6.24		
w. lbs.	13	13	13	13		
Rivet dia.	3/4	3/4	3/4	3/4		

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		
	3	62.6	62.6	81.2	81.2	90.1	90.1	98.9	98.9	
	4	56.6	56.6	60.9	60.9	67.6	67.6	74.2	74.2	
	5	45.3	45.3	48.7	48.7	54.1	54.1	59.4	59.4	
	6	37.7	36.8	40.6	39.9	45.1	44.7	49.5	49.4	
	7	32.3	30.2	34.8	32.8	38.6	36.7	42.4	40.7	
	8	28.3	25.2	30.5	27.5	33.8	30.8	37.1	34.2	
	9	25.2	21.4	27.1	23.2	30.0	26.1	33.0	29.2	
	10	22.6	18.1	24.4	19.9	27.0	22.4	29.7	25.0	
	11	20.6	15.6	22.2	17.1	24.6	19.3	27.0	21.7	
	12	18.9	13.5	20.3	14.8	22.5	16.8	24.7	18.8	
	13	17.4	11.7	18.7	12.9	20.8	14.7	22.8	16.5	
	14	16.2	...	17.4	11.3	19.3	12.9	21.2	14.5	
	15	15.1	...	16.2	...	18.0	11.3	19.8	12.8	
	16	14.2	...	15.2	...	16.9	...	18.6	...	
	17	13.3	...	14.3	...	15.9	...	17.5	...	
	18	12.6	...	13.5	...	15.0	...	16.5	...	
	19	11.9	...	12.8	...	14.2	...	15.6	...	
	20	11.3	...	12.2	...	13.5	...	14.8	...	
	21	10.8	...	11.6	...	12.9	...	14.1	...	
	22	10.3	...	11.1	...	12.3	...	13.5	...	
	23	9.8	...	10.6	...	11.8	...	12.9	...	
	24	9.4	...	10.2	...	11.3	...	12.4	...	
	25	9.1	...	9.7	...	10.8	...	11.9	...	

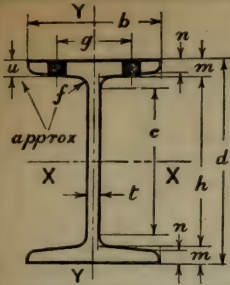
STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds
 P is Minimum Span in feet uniformly loaded to cause V
 R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions
 W is Maximum Load on one Standard Connection
 Q is Minimum Span in feet, uniformly loaded to cause W
 w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
 Allowable concentrated center loads are 50% and their deflections 80% of those shown

10"



Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.										Total Deflection in inches for Maximum Load; laterally fixed beam.
Span feet	Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free			
3	74.4	74.4	106	106	116	116	126	126		.030 .047 .067 .091 .119 .151 .186
4	73.3	73.3	80.1	80.1	87.5	87.5	94.8	94.8		
5	58.6	58.6	64.1	64.1	70.0	70.0	75.8	75.8		
6	48.8	48.4	53.4	53.4	58.3	58.3	63.2	63.2		
7	41.9	40.0	45.8	44.1	50.0	48.5	54.2	53.0		
8	36.6	33.6	40.1	37.1	43.7	40.9	47.4	44.7	.119 .151 .186	
9	32.6	28.6	35.6	31.6	38.9	34.9	42.1	38.2		
10	29.3	24.5	32.0	27.1	35.0	30.0	37.9	32.9		
11	26.6	21.1	29.1	23.5	31.8	26.0	34.5	28.7		
12	24.4	18.4	26.7	20.5	29.2	22.8	31.6	25.1		
13	22.5	16.0	24.6	17.9	26.9	19.9	29.2	22.1	.315 .365 .419	
14	20.9	14.1	22.9	15.8	25.0	17.6	27.1	19.5		
15	19.5	12.4	21.4	14.0	23.3	15.6	25.3	17.3		
16	18.3	...	20.0	12.3	21.9	13.9	23.7	15.4		
17	17.2	...	18.8	...	20.6	...	22.3	...		
18	16.3	...	17.8	...	19.4	...	21.1603 .672 .745	
19	15.4	...	16.9	...	18.4	...	20.0	...		
20	14.7	...	16.0	...	17.5	...	19.0	...		
21	14.0	...	15.3	...	16.7	...	18.1	...		
22	13.3	...	14.6	...	15.9	...	17.2	...		
23	12.7	...	13.9	...	15.2	...	16.5986 1.07 1.16	
24	12.2	...	13.4	...	14.6	...	15.8	...		
25	11.7	...	12.8	...	14.0	...	15.2	...		

12"

I

STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for 3 1/2" bearing. For details see page of Allowable End Reactions
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their deflection 80% of those shown

Depth = d"	12	12	12	12	12	12		
Wt. per foot...	31.8	35.0	40.8	45.0	50.0	55.0		
Area, sq. in...	9.26	10.20	11.84	13.10	14.57	16.04		
b"	5.00	5.08	5.25	5.36	5.48	5.60		
t...	.350	.428	.460	.565	.687	.810		
h...	10.524	10.524	10.282	10.282	10.282	10.282		
n...	.738	.738	.859	.859	.859	.859		
f...	.350	.350	.460	.460	.460	.460		
c...	.45	.45	.56	.56	.56	.56		
g...	9.762	9.762	9.333	9.333	9.333	9.333		
u...	3"	3"	3"	3"	3 1/2"	3 1/2"		
	3/16	3/16	3/4	3/4	3/4	3/4		
AXES	X-X	I...	215.8	227.0	268.9	284.1	301.6	319.3
		S...	35.97	37.83	44.82	47.35	50.27	53.22
	Y-Y	r...	4.83	4.72	4.77	4.66	4.55	4.46
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	X-X	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
	Y-Y	I...	9.5	10.0	13.8	14.8	16.0	17.3
		S...	3.8	3.9	5.3	5.5	5.8	6.2
Coef. Str.	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
Max.Mom."	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
V...	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
P, feet...	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
R...	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
W...	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
Q, feet...	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
w, lbs.	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04
Rivet dia.	X-X	r...	1.01	0.99	1.08	1.06	1.05	1.04
		I...	9.5	10.0	13.8	14.8	16.0	17.3
	Y-Y	S...	3.8	3.9	5.3	5.5	5.8	6.2
		r...	1.01	0.99	1.08	1.06	1.05	1.04

Live Load Deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. × Live Load
Tabular Load

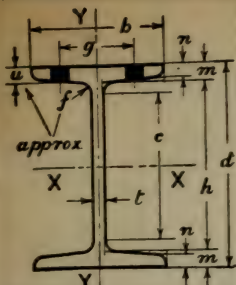
Span feet	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally fixed/free	Laterally
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STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and Web Rivets

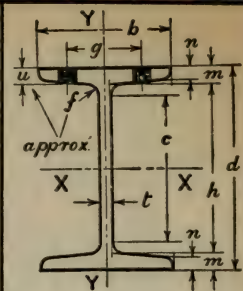
Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their
deflections 80% of those shown



15"



Depth = d" Wt. per foot Area, sq. in. b" t. h. m. n. l. c. g. u.	15		15		15		15		15		15		15		15		Total Deflection must not exceed 1-360 of the Span. Total Def. × Live Load Live Load Def. = Tabular Load	
	42.9 12.49 5.50 .410 13.332 .834 .410 .51 12.468 3½ 5⁄8	45.0 13.12 5.54 .452 13.332 .834 .410 .51 12.468 3½ 5⁄8	50.0 14.59 5.64 .550 13.332 .834 .410 .51 12.468 3½ 5⁄8	55.0 16.06 5.74 .648 13.332 .834 .410 .51 12.468 3½ 5⁄8	60.8 17.68 6.00 .590 12.918 1.041 .590 .69 11.749 7⁄8	65.0 18.91 6.08 .672 12.918 1.041 .590 .69 11.749 7⁄8	70.0 20.38 6.18 .770 12.918 1.041 .590 .69 11.749 7⁄8	75.0 21.85 6.28 .868 12.918 1.041 .590 .69 11.749 7⁄8										
AXES X-X Y-Y	I..... S..... r.....	441.8 58.91 5.95 14.6 5.3 1.08	453.6 60.48 5.88 15.0 5.4 1.07	481.1 64.15 5.74 16.0 5.7 1.05	508.7 67.83 5.63 17.0 5.9 1.03	609.0 81.20 5.87 26.0 8.7 1.21	632.1 84.28 5.78 27.2 8.9 1.20	659.6 87.95 5.69 28.8 9.3 1.19	687.2 91.63 5.61 30.6 9.8 1.18									
	Coef. Str. Max. Mom. # V P. feet. R. W. Q. feet. W. lbs. Rivet dia.	706900 1060300 73800 4.79 43800 36900 9.58 19 ¾	725800 1088600 81400 4.46 49200 40700 8.92 19 ¾	769800 1154600 99000 3.89 59800 47700 8.07 19 ¾	813900 1220900 116600 3.49 70500 47700 8.53 19 ¾	974400 1461600 106200 4.59 64200 47700 10.21 19 ¾	1011400 1517000 121000 4.18 73100 47700 10.60 19 ¾	1055400 1583000 138600 3.81 83700 47700 11.06 19 ¾	1099500 1649300 156200 3.52 94400 47700 11.53 19 ¾									
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Total Deflection in Inches for Maximum Load; laterally fixed beam.
	4	148	148	165	163	192	192	204	204	212	212	242	242	264	264	275	275	
	5	141	141	145	154	154	154	163	163	195	195	202	202	211	211	220	220	
	6	118	118	121	121	128	128	136	136	162	162	169	169	176	176	183	183	
	7	101	100	104	104	110	110	116	116	139	139	145	145	151	151	157	157	
	8	88	85	91	88	96	93	102	99	122	120	126	124	132	131	137	136	
	9	79	74	81	76	86	81	90	85	108	103	112	108	117	113	122	118	
	10	71	64	73	66	77	70	81	75	97	90	101	94	106	99	110	103	
	11	64	55	66	57	70	61	74	65	89	80	92	83	96	87	100	91	
	12	59	49	60	50	64	54	68	57	81	70	84	73	88	77	92	81	
13	54	43	56	45	59	47	63	51	75	62	78	65	81	68	85	72		
14	50	38	52	40	55	42	58	45	70	56	72	58	75	61	79	65		
15	47	34	48	35	51	38	54	40	65	50	67	52	70	55	73	58		
16	44	30	45	31	48	34	51	36	61	45	63	46	66	50	69	52		
17	42	28	43	28	45	30	48	33	57	40	59	42	62	45	65	47		
18	39	24	40	25	43	28	45	29	54	36	56	39	59	41	61	43		
19	37	...	38	...	41	...	43	27	51	33	53	35	56	37	58	39		
20	35	...	36	...	38	...	41	...	49	30	51	32	53	34	55	38		
21	34	...	35	...	37	...	39	...	46	...	48	...	50	...	52	...		
22	32	...	33	...	35	...	37	...	44	...	46	...	48	...	50	...		
23	31	...	32	...	33	...	35	...	42	...	44	...	46	...	48	...		
24	29	...	30	...	32	...	34	...	41	...	42	...	44	...	46	...		
25	28	...	29	...	31	...	33	...	39	...	40	...	42	...	44	...		
26	27	...	28	...	30	...	31	...	37	...	39	...	41	...	42	...		
27	26	...	27	...	29	...	30	...	36	...	37	...	39	...	41	...		
28	25	...	26	...	27	...	29	...	35	...	36	...	38	...	39	...		
29	24	...	25	...	27	...	28	...	34	...	35	...	36	...	38	...		
30	24	...	24	...	26	...	27	...	32	...	34	...	35	...	37	...		

18"		STANDARD BEAMS																
		DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS																
I is Moment of Inertia S is Section Modulus r is Radius of Gyration V is Maximum Web Shear in Pounds P is Minimum Span in feet uniformly loaded to cause V R is Allowable End Reaction for 3 3/4" bearing. For details see page of Allowable End Reactions W is Maximum Load on one Standard Connection Q is Minimum Span in feet, uniformly loaded to cause W w is Weight of one Standard Connection including Angles and Web Rivets																		
Rivet given is maximum diameter in flange Allowable concentrated center loads are 50% and their deflections 80% of those shown																		
Depth = d"	18	18	18	18	18	18	18	18	18	18	18	18	Total Deflection must not exceed 1-360 of the Span. Live Load Def. = Total Def. × Live Load Tabular Load					
Wt. per foot..	54.7	60.0	65.0	70.0	75.6	80.0	85.0	90.0										
Area, sq. in..	15.94	17.50	18.98	20.46	22.04	23.34	24.81	26.29										
b"	6.00	6.09	6.17	6.25	7.00	7.07	7.15	7.24										
t..	.460	.547	.629	.711	.560	.632	.714	.796										
h..	16.156	16.156	16.156	16.156	15.610	15.610	15.610	15.610										
m..	.922	.922	.922	.922	1.195	1.195	1.195	1.195										
n..	.460	.460	.460	.460	.659	.659	.659	.659										
f..	.56	.56	.56	.56	.66	.66	.66	.66										
c..	15.207	15.207	15.207	15.207	14.492	14.492	14.492	14.492										
g..	3 3/4	3 3/4	3 3/4	3 3/4	4"	4"	4"	4"										
u..	3 3/4	3 3/4	3 3/4	3 3/4	1"	1"	1"	1"										
AXES	I..	795.5	837.8	877.7	917.5	1141.8	1176.8	1216.6	1256.5									
	S..	88.39	93.09	97.53	101.94	126.87	130.76	135.18	139.61									
	r..	7.07	6.92	6.80	6.70	7.20	7.10	7.00	6.91									
	I..	21.2	22.3	23.4	24.5	46.3	47.9	49.8	51.9									
Y-Y	I..	7.1	7.3	7.6	7.8	13.2	13.6	14.0	14.3									
	S..	1.15	1.13	1.11	1.09	1.45	1.43	1.42	1.40									
	r..																	
	I..																	
Coef. Str.	1060700	1117100	1170300	1223300	1522400	1569100	1622100	1675300										
Max.Mom." #	1591000	1675600	1755400	1835000	2283600	2353600	2433200	2513000										
V..	99400	118200	135900	153600	121000	136500	154200	171900										
P..	5.34	4.73	4.31	3.98	6.29	5.75	5.26	4.88										
R..	52800	65600	75500	85300	67200	75800	85700	95500										
W..	41400	47700	47700	47700	47700	47700	47700	47700										
Q..	12.81	11.71	12.27	12.82	15.96	16.45	17.00	17.56										
w, lbs.	19	19	19	19	19	19	19	19										
Rivet dia.	7/8	7/8	7/8	7/8	7/8	7/8	7/8	7/8										
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Total Deflection in inches for Maximum Load; laterally fixed beam.				
	6	177	177	186	186	195	195	204	204	242	242	262	262					
	7	152	152	160	160	167	167	175	175	218	218	224	224					
	8	133	131	140	138	146	145	153	152	190	190	196	196					
	9	118	113	124	119	130	125	136	132	169	168	174	173					
	10	106	98	112	104	117	109	122	114	152	147	157	152					
	11	96	86	102	92	106	96	111	100	138	130	143	135					
	12	88	76	93	81	98	86	102	90	127	116	131	121					
	13	82	68	86	72	90	76	94	80	117	104	121	108					
	14	76	61	80	64	84	68	87	71	109	94	112	97					
	15	71	54	74	57	78	61	82	64	102	85	105	88					
	16	66	49	70	52	73	55	76	57	95	77	98	80					
	17	62	44	66	47	69	50	72	52	90	70	92	72					
	18	59	40	62	42	65	45	68	47	85	64	87	66					
	19	56	36	59	39	62	41	64	43	80	58	83	61					
	20	53	33	56	35	59	37	61	39	76	53	78	55					
	21	51	...	53	...	56	...	58	...	73	49	75	51					
	22	48	...	51	...	53	...	56	...	69	45	71	47					
	23	46	...	49	...	51	...	53	...	66	41	68	43					
	24	44	...	47	...	49	...	51	...	63	...	65	...					
	25	42	...	45	...	47	...	49	...	61	...	63	...					
	26	41	...	43	...	45	...	47	...	59	...	60	...					
	27	39	...	41	...	43	...	45	...	56	...	58	...					
	28	38	...	40	...	42	...	44	...	54	...	56	...					
	29	37	...	39	...	40	...	42	...	52	...	54	...					
	30	35	...	37	...	39	...	41	...	51	...	52	...					
	31	34	...	36	...	38	...	39	...	49	...	51	...					
	32	33	...	35	...	37	...	38	...	48	...	49	...					
	33	32	...	34	...	35	...	37	...	46	...	48	...					
	34	31	...	33	...	34	...	36	...	45	...	46	...					
	35	30	...	32	...	33	...	35	...	44	...	45	...					
	36	29	...	31	...	32	...	34	...	42	...	44	...					

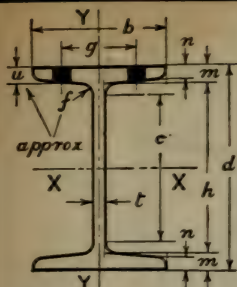
STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds
P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see
page of Allowable End Reactions
W is Maximum Load on one Standard Connection
Q is Minimum Span in feet, uniformly loaded to cause W
w is Weight of one Standard Connection including Angles and
Web Rivets.

Rivet given is maximum diameter in flange
Allowable concentrated center loads are 50% and their
deflections 80% of those shown

20"
I

[illegible]

LOADS BY A. I. S. C. SPECIFICATION

24''



STANDARD BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds
D is Minimum Span in feet uniformly

P is Minimum Span in feet uniformly loaded to cause V
R is Allowable End Reaction for 3 1/2" bearing For det

K is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions

W is Maximum Load on one Standard

Q is Minimum Span in feet uniformly loaded to c

w is Weight of one Standard Connection including Angle

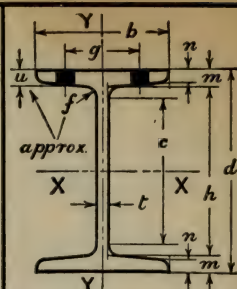
Web Rivets

Rivet given is maxim

Rivet given is maximum diameter in flange

Allowable concentrated center loads are 50% and their

Allowable concentrated center deflections 80% of those shown

[illegible]

ALLOWABLE END REACTIONS FOR AMERICAN STANDARD BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight Per Foot	Web t.	Unit Stress in Buckling	Reaction R For $3\frac{1}{2}"$ Bearing	Min. Span For $3\frac{1}{2}"$ Bearing	Reaction R For $5\frac{1}{2}"$ Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to Develop V.
5	10.00	.210	15000	12600	2.30	12600	3150	12600	2.75
	12.25	.347	"	20800	1.56	20800	5205	20800	"
	14.75	.494	"	29600	1.22	29600	7410	29600	"
6	12.50	.230	15000	16600	2.63	16600	3450	16600	3.31
	14.75	.343	"	24700	1.93	24700	5145	24700	3.30
	17.25	.465	"	34500	1.51	34500	6975	34500	3.45
7	15.30	.250	15000	19700	3.15	21000	3750	21000	3.85
	17.50	.345	"	27200	2.45	29000	5175	29000	"
	20.00	.450	"	35400	2.03	37800	6750	37800	"
8	18.40	.270	15000	22300	3.83	25900	4050	25900	4.39
	20.50	.349	"	28800	3.13	33500	5235	33500	"
	23.00	.441	"	36400	2.65	42300	6615	42300	"
	25.50	.532	"	43900	2.33	51100	7980	51100	4.40
9	21.80	.290	15000	25000	4.52	31300	4350	31300	4.95
	25.00	.397	"	34200	3.56	42900	5955	42900	"
	30.00	.561	"	48400	2.79	60600	8415	60600	"
	35.00	.724	"	62400	2.38	78200	10860	78200	"
10	25.40	.310	15000	27900	5.25	37200	4650	37200	5.50
	30.00	.447	"	40200	3.98	53600	6705	53600	"
	35.00	.594	"	53500	3.27	71300	8910	71300	"
	40.00	.741	"	66700	2.84	88900	11115	88900	"
12	31.80	.350	15000	34100	6.32	44600	5250	50400	6.60
	35.00	.428	"	41700	5.44	54600	6420	61600	"
	40.80	.460	"	44900	5.99	58700	6900	66200	"
	45.00	.565	"	55100	5.16	72000	8475	81400	6.60
	50.00	.687	"	67000	4.50	87600	10305	98900	"
15	55.00	.810	"	79000	4.04	103300	12150	116600	"
	42.90	.410	14730	43800	8.07	55900	6035	73800	8.47
	45.00	.452	15000	49200	7.38	62700	6780	81400	8.25
	50.00	.550	"	59800	6.43	76300	8250	99000	"
	55.00	.648	"	70500	5.77	89900	9720	116600	"
	60.80	.590	15000	64200	7.59	81900	8850	106200	8.25
	65.00	.672	"	73100	6.92	93200	10080	121000	"
18	70.00	.770	"	83700	6.30	106800	11550	138600	"
	75.00	.868	"	94400	5.82	120400	13020	156200	"
	54.70	.460	14350	52800	10.07	66000	6600	99400	10.55
	60.00	.547	15000	65600	8.51	82100	8205	118200	9.90
	65.00	.629	"	75500	7.75	94400	9435	135900	"
	70.00	.711	"	85300	7.17	106700	10665	153600	"
	75.60	.560	15000	67200	11.33	84000	8400	121000	9.90
20	80.00	.632	"	75800	10.35	94800	9480	136500	"
	85.00	.714	"	85700	9.47	107100	10710	154200	"
	90.00	.796	"	95500	8.78	119400	11940	171900	"
	65.40	.500	14210	60400	11.63	74600	7105	120000	11.88
	70.00	.567	14910	71900	10.14	88800	8450	136100	11.11
	75.00	.641	15000	81700	9.28	101000	9615	153800	11.00
	81.40	.600	"	76500	11.50	94500	9000	144000	"
24	85.00	.653	15000	83300	10.82	102800	9795	156700	11.00
	90.00	.726	"	92600	10.05	114300	10890	174200	"
	95.00	.800	"	102000	9.41	126000	12000	192000	"
	100.00	.873	"	111300	8.88	137500	13095	209500	"
	79.90	.500	13010	61800	16.89	74800	6505	144000	16.10
	85.00	.563	13820	73900	14.61	89500	7780	162100	14.84
	90.00	.624	14450	85700	13.02	103700	9015	179700	13.94
24	95.00	.686	14950	97400	11.81	117900	10255	197600	13.26
	100.00	.747	15000	106400	11.14	128900	11205	215000	13.19
	105.90	.625	14450	85800	16.38	104400	9030	180000	13.93
	110.00	.675	14870	95400	15.04	115400	10035	194400	13.37
	115.00	.737	15000	105000	14.00	127100	11055	212300	13.20
	120.00	.798	"	113700	13.24	137700	11970	229800	13.20

The beam web is treated as a column with fixed ends, having an effective length l of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

CONNECTION ANGLES FOR AMERICAN STANDARD BEAMS

DIMENSIONS, WEIGHTS, AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

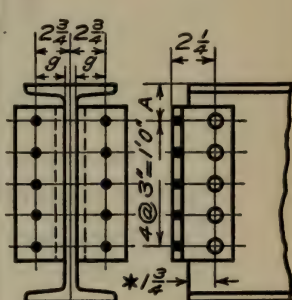
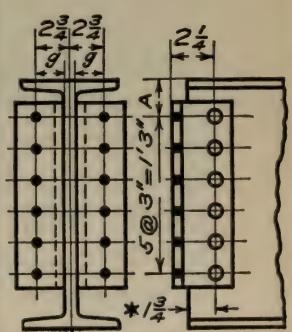
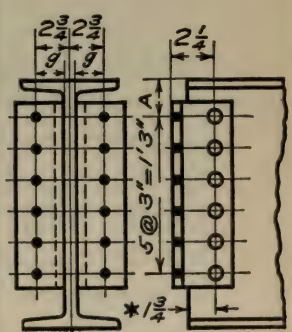
Beam		Connection Value			Framing Distance C	Connection Angles				Weight inc. Web Rivets	Connection Details.
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length			
			Power Driven Rivets	Unfin- ished Bolts							
3"	5.7	7650	11930	8840	1/8	IC. 5.11	2 11/16	6" x 4" x 3/8" 0' — 2' Long	5 lbs.		
	6.5	11296	"	"	3/16	IC. 5.10	2 5/8				
	7.5	15706	"	"	1/4	IC. 5.9	2 9/16				
4"	7.7	8550	11930	8840	3/16	IC. 5.10	2 5/8	6" x 4" x 3/8" 0' — 2' Long	6 lbs.		
	8.5	11390	"	"	3/16	IC. 5.10	2 5/8				
	9.5	14670	"	"	1/4	IC. 5.9	2 9/16				
10.5	18000	"	"	1/4	IC. 5.9	2 9/16					
5"	10.0	9450	11930	8840	3/16	IC. 6.10	2 5/8	6" x 4" x 3/8" 0' — 2 1/2' Long	6 lbs.		
	12.25	15620	"	"	1/4	IC. 6.9	2 9/16				
	14.75	22230	"	"	5/16	IC. 6.8	2 1/2				
6"	12.5	10350	11930	8840	3/16	IC. 6.10	2 5/8	6" x 4" x 3/8" 0' — 2 1/2' Long	6 lbs.		
	14.75	15440	"	"	1/4	IC. 6.9	2 9/16				
	17.25	20930	"	"	5/16	IC. 6.8	2 1/2				
7"	15.3	11250	11930	8840	3/16	IC. 6.10	2 5/8	6" x 4" x 3/8" 0' — 2 1/2' Long	6 lbs.		
	17.5	15530	"	"	1/4	IC. 6.9	2 9/16				
	20.0	20250	"	"	5/16	IC. 6.8	2 1/2				
8"	18.4	24300	23860	17670	3/16	IC.13.10	2 5/8	6" x 4" x 3/8" 0' — 5 1/2' Long	13 lbs.		
	20.5	31410	"	"	1/4	IC.13.9	2 9/16				
	23.0	39690	"	"	5/16	IC.13.8	2 1/2				
	25.5	47720	"	"	5/16	IC.13.8	2 1/2				
9"	21.8	26100	23860	17670	3/16	IC.13.10	2 5/8	6" x 4" x 3/8" 0' — 5 1/2' Long	13 lbs.		
	25.0	35730	"	"	1/4	IC.13.9	2 9/16				
	30.0	47720	"	"	3/8	IC.13.8	2 1/2				
	35.0	"	"	"	7/16	IC.13.6	2 3/8				
10"	25.4	27900	23860	17670	1/4	IC.13.10	2 5/8	6" x 4" x 3/8" 0' — 5 1/2' Long	13 lbs.		
	30.0	40230	"	"	5/16	IC.13.8	2 1/2				
	35.0	47720	"	"	3/8	IC.13.7	2 7/16				
	40.0	"	"	"	7/16	IC.13.6	2 3/8				
12"	31.8	31500	23860	17670	1/4	IC.13.9	2 9/16	6" x 4" x 3/8" 0' — 5 1/2' Long	19 lbs.		
	35.0	38520	"	"	1/4	IC.13.9	2 9/16				
	40.8	41400	"	"	5/16	IC.13.8	2 1/2				
	45.0	47720	"	"	3/8	IC.13.7	2 7/16				
	50.0	"	"	"	7/16	IC.13.6	2 3/8				
	55.0	"	"	"	1/2	IC.13.6	2 3/8				
15"	42.9	36900	47720	35340	1/4	IC.19.9	2 9/16	4" x 3 1/2" x 3/8" 0' — 11 1/2' Long	19 lbs.		
	45.0	40680	"	"	5/16	IC.19.8	2 1/2				
	50.0	47720	"	"	5/16	IC.19.8	2 1/2				
	55.0	"	"	"	3/8	IC.19.7	2 7/16				
	60.8	47720	47720	35340	3/8	IC.19.7	2 7/16				
	65.0	"	"	"	3/8	IC.19.7	2 7/16				
	70.0	"	"	"	7/16	IC.19.6	2 3/8				
	75.0	"	"	"	1/2	IC.19.5	2 5/16				
18"	54.7	41400	47720	35340	5/16	IC.19.8	2 1/2	4" x 3 1/2" x 3/8" 0' — 11 1/2' Long	19 lbs.		
	60.0	47720	"	"	5/16	IC.19.8	2 1/2				
	65.0	"	"	"	3/8	IC.19.7	2 7/16				
	70.0	"	"	"	7/16	IC.19.6	2 3/8				
	75.6	47720	47720	35340	3/8	IC.19.8	2 1/2				
	80.0	"	"	"	3/8	IC.19.7	2 7/16				
	85.0	"	"	"	7/16	IC.19.6	2 3/8				
	90.0	"	"	"	7/16	IC.19.6	2 3/8				

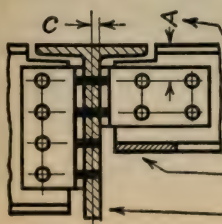
LOADS BY A. I. S. C. SPECIFICATION

CONNECTION ANGLES FOR AMERICAN STANDARD BEAMS

DIMENSIONS, WEIGHTS AND WORKING LOADS.

3/4" POWER DRIVEN RIVETS.

Beam		Connection Value			Framing Distance C	Connection Angles				Connection Details.
Depth	Weight per foot	Web	Outstanding Single Shear			A.I.S.C. Mark	Gage	Size and Length	Weight inc. Web Rivets	
			Power Driven Rivets	Unfin-ished Bolts						
20'	65.4	56250	59650	44180	5/16	IC.25.8	2 1/2	4" x 3 1/2" x 3/8" 1' — 2 1/2" Long	25 lbs.	
	70.0	59650	"	"	3/8	IC.25.7	2 7/16			
	75.0	"	"	"	3/8	IC.25.7	2 7/16			
	81.4	"	"	"	3/8	IC.25.7	2 7/16			
	85.0	59650	59650	44180	3/8	IC.25.7	2 7/16			
	90.0	"	"	"	7/16	IC.25.6	2 3/8			
24'	95.0	"	"	"	7/16	IC.25.6	2 3/8	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.	
	100.0	"	"	"	1/2	IC.25.5	2 5/16			
	79.9	67500	71580	53020	5/16	IC.30.8	2 1/2			
	85.0	71580	"	"	3/8	IC.30.7	2 7/16			
	90.0	"	"	"	3/8	IC.30.7	2 7/16			
	95.0	"	"	"	7/16	IC.30.7	2 7/16			
24'	100.0	71580	71580	53020	7/16	IC.30.6	2 3/8	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.	
	105.9	"	"	"	3/8	IC.30.7	2 7/16			
	110.0	"	"	"	3/8	IC.30.7	2 7/16			
	115.0	"	"	"	7/16	IC.30.6	2 3/8			
	120.0	"	"	"	7/16	IC.30.6	2 3/8			



*Layer-out starts with this dimension at left end of beam. With beams ordered one inch short, as usual in standard shop practice, this leaves sufficient end distance or clearance at right end, in case of full allowable 3/8" underrun or 3/8" overrun in beam lengths.

When A = 3" all beams and channels from 24" 100 lb. to 5" inclusive, can be framed opposite with tops flush.

When A = 3 1/4" all beams and channels from 24" 120 lb. to 6" inclusive, excepting 8", can be framed opposite with tops flush.

Flange must be cut away as shown, for field riveting, on all beams (excepting 5" and 8") framing opposite a larger beam which has a different size standard connection.

Minimum Web required to develop Single Shearing Value is .33"

Minimum Web required to develop Double Shearing Value is .53"

BEAM SUMMARY

Pages 361—367

The beam summary affords the quickest and easiest method of selecting the most economical beam section to use for any total continuous uniformly distributed load and any span in feet.

A.I.S.C. CONNECTION ANGLES

The A. I. S. C. mark on drawings gives useful information without further reference to a connection angle chart. The figures, immediately following the Institute's symbol IC, are the weight of the connection, including the web rivets, and the last figures are the number of sixteenths of an inch greater than 2" in the gauge of the outstanding legs. Thus, connection angles IC.49.7 weigh 49 pounds, including web rivets, and the gauge in the outstanding leg is $2\frac{7}{16}$ ". A further discussion on the A. I. S. C. connection angle appears on page 227.

Part IV

Section 5

BETHLEHEM BEAM SECTIONS

Dimensions—Technical Functions

Allowable Total Loads by A. I. S. C. Specification

Allowable End Reactions—Standard Connection Angles

Usual Stock Sizes					
Depth	Weight	Depth	Weight	Depth	Weight
8"	17.5 *	16"	40.0 *	26"	91.0 *
9"	20.5 *	18"	49.0 *	28"	97.0 *
10"	23.5 *	20"	59.5 *	30"	121.0 *
12"	28.0 *	22"	62.5 *	33"	135.0 *
14"	33.0 *	24"	73.5 *	36"	155.0 *
15"	38.5 *				

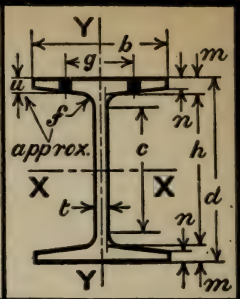
Manufacturers Section Index											
Sec. Index	Depth	Weight				Sec. Index	Depth	Weight			
B 8	8"	17.5	19.0			B 20	20"	56.0	59.5	62.0	64.5
B 9	9"	20.5	22.0			B 20a	20"	68.5	73.0	78.0	
B 10	10"	21.0	23.5	26.0	28.5	B 22	22"	54.5	58.0	62.5	67.5
B 12	12"	25.0	28.0	31.5	36.0	B 22a	22"	77.0	83.0	89.0	96.5
B 12a	12"	40.0	44.0	48.5		B 24	24"	70.0	73.5	79.5	
B 14	14"	30.0	33.0	37.5	42.0	B 24a	24"	84.5	90.5		
B 15	15"	36.0	38.5	40.0	42.5	B 24b	24"	95.5	99.5	104.5	
B 15a	15"	46.0	50.5	54.5	59.5	B 26	26"	81.0	85.5	91.0	98.0
B 15b	15"	71.5				B 28	28"	85.0	91.0	97.0	104.0
B 16	16"	35.0	40.0	45.0	50.0			112.0	119.0	133.0	
B 16a	16"	56.5	60.5	66.0	71.5	B 30	30"	110.0	115.0	121.0	129.0
B 18	18"	47.0	49.0	52.0	54.5			137.0	149.0	163.0	
B 18a	18"	59.0	64.5	69.0	74.0	B 33	33"	125.0	135.0	143.0	165.0
						B 36	36"	147.0	155.0	164.0	173.0

8"
B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets
Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".	8.00	8.06
Wt. per foot.	17.5	19.0
Area, Sq. In..	5.20	5.68
b".	5.250	5.270
t".	.250	.270
h".	7.164	7.164
m".	.418	.448
n".	.210	.240
f".	.30	.30
c".	6.625	6.625
g".	2¼	2¼
u".	11.32	¾

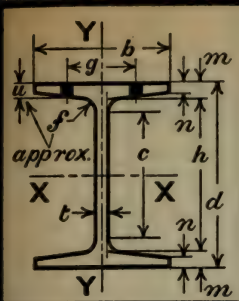
A X E S	X-X	I....	57.7	63.7
		S....	14.43	15.81
		r....	3.33	3.35
Y-Y		I....	6.39	7.20
		S....	2.44	2.73
		r....	1.11	1.13

Coef. Str....	173100	189700
Max. Mom. *#	259700	284500
V.....	24000	26100
P.....	3.61	3.63
R.....	20600	22300
W.....	22500	23900
Q.....	3.85	3.97
w. lbs....	13	13
Rivet dia....	¾	¾

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. × Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		
		fixed	free	fixed	free	
	2	48.0	48.0	52.2	52.2	
	3	48.0	48.0	52.2	52.2	
	4	43.3	43.3	47.4	47.4	.037
	5	34.6	34.6	38.0	38.0	.058
	6	28.9	28.9	31.6	31.6	.084
	7	24.7	24.3	27.1	26.7	.114
	8	21.6	20.6	23.7	22.6	.149
	9	19.2	17.6	21.1	19.4	.189
	10	17.3	15.2	19.0	16.8	.233
	11	15.7	13.3	17.2	14.6	.281
	12	14.4	11.6	15.8	12.8	.335
	13	13.3	10.3	14.6	11.3	.394
	14	12.4	9.1	13.6	10.0	.456
	15	11.5	8.0	12.6	8.8	.524
	16	10.8	7.2	11.9	8.0	.596
	17	10.2	6.5	11.2	7.1	.674



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.

9"
B

Depth = d".		9.00	9.06
Wt. per foot.		20.5	22.0
Area, Sq. In..		6.09	6.51
b.....		5.500	5.510
t.....		.250	.260
h.....		8.062	8.062
m.....		.469	.499
n.....		.250	.280
f.....		.30	.30
c.....		7.500	7.500
g.....		2½	2½
u.....		¾	13/32
AXES			
X-X	I....	86.5	93.9
X-X	S....	19.22	20.73
X-X	r....	3.77	3.80
Y-Y	I....	8.54	9.42
Y-Y	S....	3.10	3.42
Y-Y	r....	1.18	1.20
Coef. Str....		230700	248700
Max. Mom. %		346000	373100
V.....		27000	28300
P, feet..		4.27	4.39
R.....		21300	22400
W.....		22500	23400
Q, feet..		5.13	5.31
w, lbs....		13	13
Rivet dia....		¾	¾
Total Deflection in inches for Maximum Load; Laterally fixed beam.		.052	
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.		.074	
Span feet		.101	
3		.132	
4		.168	
5		.207	
6		.250	
7		.298	
8		.350	
9		.406	
10		.466	
11		.530	
12		.599	
13		.670	
14		.747	
15			
16			
17			
18			
19			

10"
B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

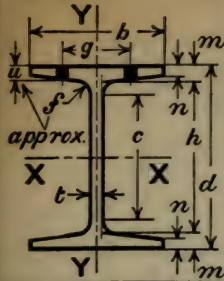
I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3 1/4" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.

Depth = d".	9.90	10.00	10.09	10.19	Live Load deflection must not exceed 1/360 of the Span.
Wt. per foot.	21.0	23.5	26.0	28.5	
Area, Sq. In..	6.28	6.96	7.68	8.41	
b".	5.740	5.750	5.770	5.785	
t.	.240	.250	.270	.285	
h.	8.972	8.972	8.972	8.972	
m.	.464	.514	.559	.609	
n.	.235	.285	.330	.380	
f.	.30	.30	.30	.30	
c.	8.375	8.375	8.375	8.375	
g.	23/4	23/4	23/4	23/4	
u.	11/32	13/32	15/32	1/2	
AXES	I....	108.1	123.2	137.9	154.1
	S....	21.84	24.64	27.33	30.25
	r....	4.15	4.21	4.24	4.28
Y-Y	I....	9.30	10.9	12.5	14.2
	S....	3.24	3.80	4.33	4.92
	r....	1.22	1.25	1.28	1.30

Coef. Str.	262100	295700	328000	362900	Total Deflection in inches for Maximum Load: Laterally fixed beam.
Max. Mom. "M	393100	443500	492000	544400	
V.....	28500	30000	32700	34800	
P. feet..	4.60	4.93	5.02	5.21	
R.....	20200	21300	23700	25400	
W.....	21600	22500	23900	23900	
Q. feet..	6.07	6.57	6.86	7.59	
w. lbs....	13	13	13	13	
Rivet dia.	3/4	3/4	3/4	3/4	

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load: Laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	
3	57.0	57.0	60.0	60.0	65.4	65.4	69.6	69.6	.047	
	4	57.0	57.0	60.0	60.0	65.4	65.4	69.6		69.6
	5	52.4	52.4	59.1	59.1	65.4	65.4	69.6		69.6
	6	43.7	43.7	49.3	49.3	54.7	54.7	60.5		60.5
	7	37.5	37.5	42.2	42.2	46.9	46.9	51.8		51.8
8	32.8	32.0	37.0	36.1	41.0	40.0	45.4	44.3	.119	
	9	29.1	27.5	32.9	31.1	36.4	34.4	40.3		38.1
	10	26.2	23.9	29.6	27.0	32.8	30.0	36.3		33.2
	11	23.8	20.9	26.9	23.6	29.8	26.2	33.0		29.1
	12	21.9	18.5	24.6	20.8	27.3	23.1	30.2		25.6
13	20.2	16.4	22.7	18.4	25.2	20.5	27.9	22.7	.315	
	14	18.7	14.5	21.1	16.4	23.4	18.3	25.9		20.2
	15	17.5	13.0	19.7	14.7	21.9	16.4	24.2		18.1
	16	16.4	11.7	18.5	13.2	20.5	14.7	22.7		16.3
	17	15.4	10.5	17.4	11.9	19.3	13.2	21.3		14.6
18	14.6	9.5	16.4	10.7	18.2	11.9	20.2	13.2	.603	
	19	13.8	8.6	15.6	9.7	17.3	10.8	19.1		11.9
	20	13.1	...	14.8	...	16.4	...	18.2		...
	21	12.5	...	14.1	...	15.6	...	17.3		...
										.821



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3 1/2" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets
Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.

12"
B

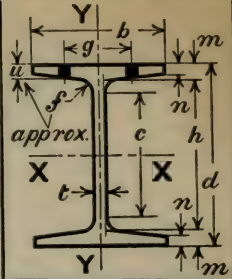
Depth = d"		11.88	12.00	12.12	12.25	12.00	12.12	12.25	Total Deflection must not exceed 1/360 of the Span.	
Wt. per foot.		25.0	28.0	31.5	36.0	40.0	44.0	48.5		
Area, Sq. In.		7.44	8.28	9.36	10.58	11.80	12.97	14.28		
b"		6.495	6.500	6.525	6.555	6.750	6.780	6.815		
t		.240	.245	.270	.300	.330	.360	.395	Live Load Def. = Total Def. x Live Load Tabular Load	
h		10.900	10.900	10.900	10.900	10.530	10.530	10.530		
n		.490	.550	.610	.675	.735	.795	.860		
n		.230	.290	.350	.415	.468	.528	.593		
f		.35	.35	.35	.35	.40	.40	.40	Live Load Def. = Total Def. x Live Load Tabular Load	
c		10.250	10.250	10.250	10.250	9.750	9.750	9.750		
g		3"	3"	3"	3"	3"	3"	3"		
u		3/8	7/16	1/2	9/16	23/32	25/32	27/32		
A X E S	I	185.1	213.6	245.7	281.8	301.2	335.1	373.2	Total Deflection in inches for Maximum Load; Laterally fixed beam.	
	S	31.16	35.60	40.54	46.01	50.20	55.30	60.93		
	r	4.99	5.08	5.12	5.16	5.05	5.08	5.11		
	I	13.6	16.4	19.4	22.7	27.6	31.1	35.1		
Y - Y	S	4.19	5.04	5.93	6.93	8.18	9.18	10.29	Total Deflection in inches for Maximum Load; Laterally fixed beam.	
	r	1.35	1.41	1.44	1.46	1.53	1.55	1.57		
	I	373900	427200	486500	552100	602400	663600	731200		
	Max. Mom. °	560900	640800	729800	828100	903600	995300	1096700		
V		34200	35300	39300	44100	47500	52400	58100	Total Deflection in inches for Maximum Load; Laterally fixed beam.	
P		5.47	6.05	6.19	6.26	6.34	6.33	6.29		
R		19900	20500	23800	27800	31700	35300	38900		
W		21600	22100	23860	23860	23860	23860	23860		
Q		8.66	9.67	10.18	11.55	12.60	13.88	15.30	Total Deflection in inches for Maximum Load; Laterally fixed beam.	
w		13	13	13	13	13	13	13		
Rivet dia.		3/4	3/4	3/4	3/4	3/4	3/4	3/4		
Span feet		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	
3		68	68	71	71	79	79	88	88	.056
4		68	68	71	71	79	79	88	88	
5		68	68	71	71	79	79	88	88	
6		62	62	71	71	79	79	88	88	.076
7		53	53	61	61	70	70	79	79	
8		47	47	53	53	61	61	69	69	
9		42	41	47	46	54	53	61	60	.099
10		37	35	43	41	49	47	55	52	
11		34	31	39	36	44	41	50	46	
12		31	28	36	32	41	37	46	41	.126
13		29	25	33	28	37	32	42	36	
14		27	22	31	26	35	29	39	33	
15		25	20	28	22	32	26	37	30	.155
16		23	18	27	21	30	23	35	27	
17		22	16	25	19	29	22	32	24	.188
18		21	15	24	17	27	19	31	22	
19		20	14	22	15	26	18	29	20	
20		19	13	21	14	24	16	28	19	.223
21		18	11	20	13	23	15	26	17	
22		17	...	19	...	22	...	25	...	
23		16	...	19	...	21	...	24263
24		16	...	18	...	20	...	23	...	
25		15	...	17	...	19	...	22	...	
26	304
27		
28		
29	341
30		
31		
32	398
33		
34		
35	449
36		
37		
38	503
39		
40		
41	560
42		
43		
44	621
45		
46		
47	684
48		
49		
50	751
51		
52		
53	822
54		
55		
56	894
57		
58		
59	970
60		
61		

14"
B

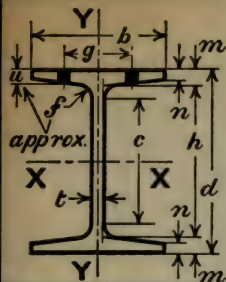
BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets
Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.										Total Deflection in inches for Maximum Load; Laterally fixed beam.
Span feet	Laterally		Laterally		Laterally		Laterally			
	fixed	free	fixed	free	fixed	free	fixed	free		
5	88.2	88.2	89.0	89.0	103	103	116	116		
6	85.0	85.0	89.0	89.0	103	103	116	116		
7	72.8	72.8	81.9	81.9	93.2	93.2	105	105		
8	63.7	63.7	71.6	71.6	81.5	81.5	91.9	91.9		
9	56.7	55.8	63.7	62.7	72.5	71.5	81.7	80.7	.108	
10	51.0	49.0	57.3	55.0	65.2	62.7	73.5	70.7	.133	
11	46.4	43.3	52.1	48.6	59.3	55.4	66.8	62.5	.161	
12	42.5	38.5	47.8	43.3	54.4	49.4	61.3	55.7	.192	
13	39.2	34.4	44.1	38.7	50.2	44.1	56.6	49.9	.225	
14	36.4	30.9	40.9	34.7	46.6	39.7	52.5	44.8	.261	
15	34.0	27.9	38.2	31.3	43.5	35.8	49.0	40.4	.299	
16	31.9	25.2	35.8	28.3	40.8	32.4	46.0	36.6	.341	
17	30.0	22.9	33.7	25.7	38.4	29.4	43.2	33.2	.384	
18	28.3	20.8	31.8	23.4	36.2	26.7	40.8	30.2	.431	
19	26.8	19.0	30.2	21.4	34.3	24.4	38.7	27.6	.480	
20	25.5	17.4	28.7	19.5	32.6	22.3	36.8	25.3	.532	
21	24.3	15.9	27.3	17.9	31.1	20.5	35.0	23.1	.587	
22	23.2	14.6	26.0	16.4	29.6	18.7	33.4	21.2	.644	
23	22.2	...	24.9	...	28.4	...	32.0704	
24	21.3	...	23.9	...	27.2	...	30.6766	
25	20.4	...	22.9	...	26.1	...	29.4831	
26	19.6	...	22.0	...	25.1	...	28.3899	
27	18.9	...	21.2	...	24.2	...	27.2969	
28	18.2	...	20.5	...	23.3	...	26.3	...	1.043	
29	17.6	...	19.8	...	22.5	...	25.4	...	1.119	
30	17.0	...	19.1	...	21.7	...	24.5	...	1.197	



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds.
 P is Minimum Span in feet, uniformly loaded to cause V .
 R is Allowable End Reaction for $3\frac{1}{2}$ bearing. For details see page of Allowable End Reactions.
 W is Maximum Load on one Standard Connection.
 Q is Minimum Span in feet, uniformly loaded to cause W .
 w is Weight of one Standard Connection including Angles and Web Rivets
 Rivet given is Maximum Diameter in flange.
 Allowable concentrated center loads are 50% and their deflections 80% of those shown.

15"
B

Depth = d".	14.91	15.00	15.03	15.09	14.75	14.88	15.00	15.12	15.00
Wt. per foot.	36.0	38.5	40.0	42.5	46.0	50.5	54.5	59.5	71.5
Area, Sq. In.	10.61	11.37	11.80	12.50	13.63	14.84	16.05	17.49	21.04
b".	6.740	6.750	6.765	6.785	6.955	6.975	7.000	7.040	7.500
t".	.280	.290	.305	.325	.365	.385	.410	.450	.520
h".	13.662	13.662	13.662	13.662	13.250	13.250	13.250	13.250	12.848
m".	.624	.669	.684	.714	.750	.815	.875	.935	1.076
n".	.355	.400	.415	.445	.475	.540	.600	.660	.785
f".	.40	.40	.40	.40	.50	.50	.50	.50	.60
c".	12.875	12.875	12.875	12.875	12.375	12.375	12.375	12.375	11.750
g".	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$
u".	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$
AXES									
I... X-X	410.9	447.6	463.3	492.0	508.2	563.3	617.0	676.2	799.5
S... X-X	55.12	59.68	61.65	65.21	68.91	75.71	82.27	89.44	106.60
r... X-X	6.22	6.27	6.27	6.27	6.11	6.16	6.20	6.22	6.16
I... Y-Y	21.7	24.1	25.1	26.9	30.8	34.7	38.6	42.8	60.9
S... Y-Y	6.45	7.15	7.42	7.93	8.85	9.96	11.0	12.2	16.2
r... Y-Y	1.43	1.46	1.46	1.47	1.50	1.53	1.55	1.56	1.70
Coef. Str.	661400	716200	739800	782500	826900	908500	987200	1073300	1279200
Max. Mom. %	992100	1074200	1109700	1173700	1240300	1362800	1480800	1610000	1918800
P. feet.	50100	52200	55000	58900	64600	68700	73800	81700	93600
R. feet.	6.60	6.86	6.73	6.64	6.40	6.61	6.69	6.57	6.83
Q. feet.	24800	26200	28400	31300	37400	40100	43800	48900	56600
W. lbs.	25200	26100	27500	29300	32900	34700	36900	40500	46800
Q. feet.	13.12	13.72	13.45	13.35	12.57	13.09	13.38	13.25	13.67
w. lbs.	19	19	19	19	19	19	19	19	19
Rivet dia.	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$

deflection must not exceed
 $\frac{1}{360}$ of the Span.
 Total Def. \times Live Load
 Tabular Load
 Live Load
 Live Load Def. = Total Def.

	Span feet	Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Laterally fixed free		Total Deflection inches for Maximum Load; Laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free			
Coefficient of Strength by the Span in feet.	4	100	100	104	104	110	110	118	118	129	129	137	137	148	148	163	163	187	187	.061 .079 .101 .124 .150 .179 .210 .243 .279 .318 .359 .402 .448 .497 .547 .601 .651 .715 .776 .839 .905 .973 1.040 1.120
	5	100	100	104	104	110	110	118	118	129	129	137	137	148	148	163	163	187	187	
	6	100	100	104	104	110	110	118	118	129	129	137	137	148	148	163	163	187	187	
	7	94	94	102	102	106	106	112	112	118	118	130	130	141	141	153	153	183	183	
	8	83	83	90	90	92	92	98	98	103	103	114	114	123	123	134	134	160	160	
	9	73	72	80	79	82	81	87	86	92	91	101	100	110	109	119	118	142	142	
	10	66	63	72	69	74	71	78	75	83	80	91	88	99	96	107	104	128	126	
	11	60	56	65	61	67	63	71	66	75	71	83	78	90	85	98	93	116	112	
	12	55	50	60	54	62	56	65	59	69	63	76	70	82	75	89	82	107	100	
	13	51	45	55	48	57	50	60	53	64	57	70	62	76	68	83	74	98	90	
Coefficient of Strength by the Span in feet.	14	47	40	51	43	53	45	56	48	59	51	65	56	71	61	77	67	91	81	
	15	44	36	48	39	49	40	52	43	55	46	61	51	66	55	72	60	85	73	
	16	41	32	45	36	46	36	49	39	52	42	57	46	62	50	67	54	80	67	
	17	39	30	42	32	43	33	46	35	49	38	53	41	58	45	63	49	75	61	
	18	37	27	40	29	41	30	43	32	46	34	50	38	55	41	60	45	71	56	
	19	35	25	38	27	39	28	41	29	44	32	48	35	52	38	56	41	67	51	
	20	33	22	36	24	37	25	39	27	41	29	45	31	49	34	54	38	64	47	
	21	32	21	34	22	35	23	37	24	39	26	43	29	47	32	51	35	61	43	
	22	30	19	33	21	34	21	36	23	38	25	41	27	45	29	49	32	58	40	
	23	29	...	31	...	32	...	34	...	36	22	39	24	43	27	47	30	56	37	
Coefficient of Strength by the Span in feet.	24	28	...	30	...	31	...	33	...	35	...	38	...	41	...	45	...	53	34	
	25	27	...	29	...	30	...	31	...	33	...	36	...	40	...	43	...	51	31	
	26	25	...	28	...	28	...	30	...	32	...	35	...	38	...	41	...	49	...	
	27	25	...	27	...	27	...	29	...	31	...	34	...	37	...	40	...	47	...	
	28	24	...	26	...	26	...	28	...	30	...	32	...	35	...	38	...	46	...	
	29	23	...	25	...	25	...	27	...	29	...	31	...	34	...	37	...	44	...	
	30	22	...	24	...	25	...	26	...	28	...	30	...	33	...	36	...	43	...	
	31	21	...	23	...	24	...	25	...	27	...	29	...	31	...	34	...	41	...	
	32	20	...	22	...	23	...	24	...	26	...	28	...	30	...	33	...	40	...	
	33	19	...	21	...	22	...	23	...	25	...	27	...	29	...	32	...	39	...	

16"

B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

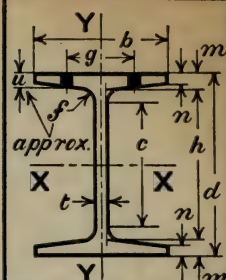
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

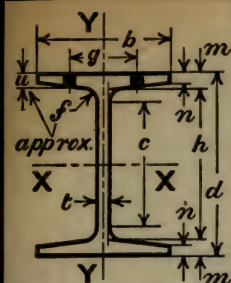
Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Depth = d".	15.81	16.00	16.12	16.25	15.88	16.00	16.12	16.25	Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. × Live Load Tabular Load
	Wt. per foot.	35.0	40.0	45.0	50.0	56.5	60.5	66.0	71.5	
	Area, Sq. In.	10.29	11.83	13.26	14.78	16.63	17.89	19.40	21.07	
	b".	7.240	7.250	7.285	7.320	8.485	8.500	8.530	8.565	
	t.....	.285	.295	.330	.365	.375	.390	.420	.455	
	h.....	14.704	14.704	14.704	14.704	14.248	14.248	14.248	14.248	
	m.....	.553	.648	.708	.773	.816	.876	.936	1.001	
	n.....	.263	.358	.418	.483	.479	.539	.599	.664	
	f.....	.40	.40	.40	.40	.50	.50	.50	.50	
	c.....	14.000	14.000	14.000	14.000	13.375	13.375	13.375	13.375	
g.....	33/4	33/4	33/4	33/4	33/4	33/4	33/4	33/4		
u.....	13/32	1/2	9/16	5/8	11/16	3/4	13/16	7/8		
AXES	X-X	I.....	435.8	526.2	594.5	669.0	742.3	812.1	888.4	Live Load deflection must not exceed 1/360 of the Span.
	X-X	S.....	55.13	65.78	73.76	82.34	93.49	101.51	110.22	
	X-X	r.....	6.51	6.67	6.69	6.73	6.68	6.74	6.77	
Y-Y	Y-Y	I.....	21.4	27.6	31.9	36.6	57.8	64.3	71.2	Live Load Def. = Total Def. × Live Load Tabular Load
	Y-Y	S.....	5.92	7.61	8.75	10.01	13.6	15.1	16.7	
	Y-Y	r.....	1.44	1.53	1.55	1.57	1.86	1.90	1.92	
Rivet dia.	Coef. Str.	661500	789300	885100	988100	1121900	1218100	1322700	1437800	Total Deflection in inches for Maximum Load; Laterally fixed beam.
	Max. Mom. *	992300	1184000	1327700	1482100	1682800	1827200	1984000	2156700	
	V.....	54100	56600	63800	71200	71500	74900	81200	88700	
	P, feet..	6.11	6.97	6.94	6.94	7.85	8.13	8.14	8.11	
	R.....	25400	26700	31900	37100	39000	41100	45500	50600	
	W.....	25700	25700	28800	32400	33800	35100	37800	41000	
	Q, feet..	12.87	15.36	15.37	15.25	16.60	17.35	17.50	17.53	
	w, lbs.	19	19	19	19	19	19	19	19	
	Rivet dia.	7/8	7/8	7/8	7/8	7/8	7/8	7/8	7/8	
	Span	Span	Laterally		Laterally		Laterally		Laterally	
feet		fixed	free	fixed	free	fixed	free	fixed	free	
6	108	108	113	113	128	128	142	142	143	.116
	7	95	95	113	113	126	126	141	141	
	8	83	83	99	99	111	111	124	124	
	9	74	74	88	88	98	98	110	110	
	10	66	65	79	77	89	87	99	97	
11	60	57	72	69	81	77	90	86	102	.141
	12	55	51	66	61	74	69	82	76	
	13	51	46	61	55	68	61	76	69	
	14	47	41	56	49	63	55	71	62	
	15	44	37	53	45	59	50	66	56	
16	41	34	49	40	55	45	62	51	70	.298
	17	39	31	46	37	52	42	58	46	
	18	37	28	44	34	49	38	55	43	
	19	35	26	42	31	47	35	52	39	
	20	33	24	40	29	44	32	49	35	
21	32	22	38	26	42	29	47	33	53	.513
	22	30	20	36	24	40	27	45	30	
	23	29	19	34	22	39	25	43	28	
	24	28	17	33	21	37	23	41	26	
	25	27	...	32	...	35	...	40	...	
26	25	...	30	...	34	...	38	...	43	.787
	27	25	...	29	...	33	...	37	...	
	28	24	...	28	...	32	...	35	...	
	29	23	...	27	...	31	...	34	...	
	30	22	...	26	...	30	...	33	...	



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

18"
B

Depth = d". Wt. per foot. Area, Sq. In.	17.94 47.0 13.90	18.00 49.0 14.44	18.06 52.0 15.34	18.12 54.5 16.06	17.75 59.0 17.48	17.88 64.5 18.97	18.00 69.0 20.38	18.12 74.0 21.79								
	b..... t..... h..... m..... n..... f..... c..... g..... u.....	7.495 .325 16.532 .704 .405 .40 15.750 3 3/4 9 1/16	7.500 .330 16.532 .734 .435 .40 15.750 3 3/4 19 1/32	7.525 .355 16.532 .764 .465 .40 15.750 3 3/4 5 7/8	7.540 .370 16.532 .794 .495 .40 15.750 3 3/4 21 1/32	8.710 .380 16.136 .807 .460 .50 15.250 4" 21 1/32	8.730 .400 16.136 .872 .525 .50 15.250 4" 23 1/32	8.750 .420 16.136 .932 .585 .50 15.250 4" 25 1/32	8.770 .440 16.136 .992 .645 .50 15.250 4" 27 1/32							
	AXES															
	X-X	I..... S..... r.....	764.1 85.18 7.42	802.8 89.20 7.46	851.7 94.32 7.45	896.1 98.91 7.47	960.3 108.20 7.41	1059.7 118.53 7.47	1153.7 128.19 7.53	1249.2 137.88 7.57						
	Y-Y	I..... S..... r.....	34.0 9.06 1.56	36.1 9.64 1.58	38.7 10.3 1.59	41.1 10.9 1.60	60.7 13.9 1.86	68.4 15.7 1.90	75.6 17.3 1.93	82.9 18.9 1.95						
	Coef. Str..... Max. Mom. *" V..... P. feet..... R..... W..... Q. feet..... w. lbs..... Rivet dia.....	1022200 1533300 70000 7.30 31000 36600 13.96 25 7/8	1070400 1605600 71300 7.51 31800 37100 14.43 25 7/8	1131800 1697700 76900 7.36 35800 39900 14.18 25 7/8	1186900 1780300 80500 7.37 38200 41600 14.27 25 7/8	1298400 1947600 80900 8.02 40200 42800 15.17 25 7/8	1422400 2133600 85800 8.29 43100 45000 15.80 25 7/8	1538300 2307400 90700 8.48 46300 47300 16.26 25 7/8	1654600 2481800 95700 8.64 49500 49500 16.71 25 7/8							
	Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Total Deflection in inches for Maximum Load; Laterally fixed beam.			
		6	140	140	143	143	154	154	161	161	162	172		181	191	191
		7	140	140	143	143	154	154	161	161	162	172		181	181	191
		8	128	128	134	134	141	141	148	148	162	172		181	181	191
9		114	114	119	119	126	126	132	132	144	144	158		171	184	
10		102	100	107	105	113	111	119	117	130	130	142		154	165	
11		93	89	97	93	103	99	108	104	118	118	129		140	150	
12		85	80	89	83	94	88	99	93	108	106	119		116	128	
13		79	72	82	75	87	80	91	83	100	96	109		104	118	
14		73	65	76	68	81	72	85	76	93	87	102		96	110	
15	68	59	71	61	75	65	79	68	87	80	95	87	103			
16	64	54	67	56	71	60	74	62	81	72	89	80	96			
17	60	49	63	51	67	54	70	57	76	66	84	73	90			
18	57	45	59	46	63	50	66	52	72	61	79	67	85			
19	54	41	56	43	60	46	62	47	68	56	75	62	81			
20	51	37	54	40	57	42	59	44	65	52	71	57	77			
21	49	35	51	36	54	38	57	41	62	47	68	53	73			
22	47	32	49	34	51	35	54	37	59	45	65	50	70			
23	44	29	47	31	49	33	52	35	56	41	62	46	67			
24	43	28	45	29	47	30	49	31	54	39	59	42	64			
25	41	...	43	27	45	28	47	29	52	36	57	40	62			
26	39	...	41	...	44	...	46	...	50	34	55	37	59			
27	38	...	40	...	42	...	44	...	48	32	53	35	57			
28	37	...	38	...	40	...	42	...	46	29	51	33	55			
29	35	...	37	...	39	...	41	...	45	28	49	30	53			
30	34	...	36	...	38	...	40	...	43	...	47	...	51			
31	33	...	35	...	37	...	38	...	42	...	46	...	50			
32	32	...	33	...	35	...	37	...	41	...	44	...	48			
33	31	...	32	...	34	...	36	...	39	...	43	...	47			
34	30	...	31	...	33	...	35	...	38	...	42	...	45			
35	29	...	31	...	32	...	34	...	37	...	41	...	44			

20"
B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

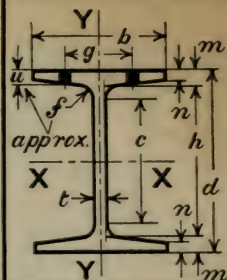
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d", Wt. per foot. Area, Sq. In.	19.88	20.00	20.06	20.12	19.88	20.00	20.09	
	56.0	59.5	62.0	64.5	68.5	73.0	78.0	
	16.51	17.47	18.25	18.93	20.12	21.58	22.98	
	8.000	8.000	8.015	8.025	8.855	8.875	8.905	
	.375	.375	.390	.400	.410	.430	.460	
	18.392	18.392	18.392	18.392	18.136	18.136	18.136	
	.744	.804	.834	.864	.872	.932	.977	
	.425	.485	.515	.545	.520	.580	.625	
	.45	.45	.45	.45	.55	.55	.55	
	17.625	17.625	17.625	17.625	17.125	17.125	17.125	
4"	4"	4"	4"	4"	4"	4"		
19 ³²	21 ³²	11 ¹⁶	23 ³²	23 ³²	25 ³²	27 ³²		
AXES	I	1086.1	1181.5	1239.8	1295.1	1366.0	1485.0	1585.5
	S	109.27	118.15	123.61	128.74	137.42	148.50	157.84
	r	8.11	8.22	8.24	8.27	8.24	8.30	8.31
Y-Y	I	43.5	48.6	51.5	54.3	71.0	78.5	84.7
	S	10.9	12.2	12.9	13.5	16.0	17.7	19.0
	r	1.62	1.67	1.68	1.69	1.88	1.91	1.92
Coef. Str.	1311200	1417800	1483300	1544800	1649100	1782000	1894100	
Max. Mom. %	1966800	2126700	2225000	2317300	2473600	2673000	2841100	
V	89500	90900	93900	96600	97800	103200	110900	
P, feet	7.33	7.88	7.90	8.00	8.43	8.63	8.54	
R	39100	38900	41500	43200	45100	48400	53500	
W	42200	42200	43900	45000	46200	48400	51800	
Q, feet	15.54	16.80	16.89	17.17	17.85	18.41	18.28	
w, lbs.	25	25	25	25	25	25	25	
Rivet dia.	7/8	7/8	7/8	7/8	7/8	7/8	7/8	
Total Deflection in inches for Maximum Load; Laterally fixed beam.								
	Live Load Def. = Total Def. x Live Load Tabular Load							

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free			
6	179	179	180	180	188	188	193	193	196	196	206	206	222	222		
8	164	164	177	177	185	185	193	193	196	196	206	206	222	222		
10	131	131	142	142	148	148	154	154	165	165	178	178	189	189	.093	
11	119	116	129	126	135	132	140	137	150	150	162	162	172	172	.113	
12	109	104	118	113	124	119	129	124	137	134	149	146	158	155	.134	
13	101	94	109	102	114	106	119	111	127	122	139	132	146	141	.158	
14	94	86	101	92	106	97	110	100	118	111	127	120	135	127	.183	
15	87	77	95	84	99	88	103	91	110	101	119	110	126	116	.210	
16	82	71	89	77	93	80	97	84	103	93	111	100	118	106	.239	
17	77	65	83	70	87	73	91	76	97	85	105	92	111	98	.270	
18	73	59	79	64	82	67	86	70	92	79	99	85	105	90	.302	
19	69	55	75	59	78	62	81	64	87	73	94	79	100	84	.336	
20	66	51	71	54	74	57	77	59	83	67	89	72	95	78	.373	
21	62	46	68	50	71	53	74	55	79	62	85	67	90	71	.411	
22	60	43	64	46	67	48	70	50	75	58	81	62	86	66	.451	
23	57	40	62	43	64	45	67	47	72	54	77	58	82	62	.493	
24	55	37	59	40	62	42	64	43	69	50	74	54	79	58	.537	
25	52	34	57	37	59	39	62	41	66	47	71	50	76	54	.582	
26	50	32	55	35	57	36	59	37	63	43	69	47	73	50	.630	
27	49	...	53	...	55	...	57	...	61	41	66	44	70	47	.679	
28	47	...	51	...	53	...	55	...	59	38	64	41	68	44	.736	
29	45	...	49	...	51	...	53	...	57	36	61	38	65	41	.783	
30	44	...	47	...	49	...	51	...	55	...	59	...	63838	
31	42	...	46	...	48	...	50	...	53	...	57	...	61895	
32	41	...	44	...	46	...	48	...	52	...	56	...	59954	
33	40	...	43	...	45	...	47	...	50	...	54	...	57	...	1.01	
34	39	...	42	...	44	...	45	...	49	...	52	...	56	...	1.08	
35	38	...	41	...	42	...	44	...	47	...	51	...	54	...	1.14	
36	36	...	39	...	41	...	43	...	46	...	50	...	53	...	1.21	
37	35	...	38	...	40	...	42	...	45	...	48	...	51	...	1.28	

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

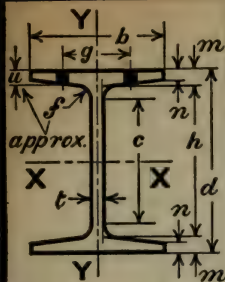
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets.

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%.

and their deflections 80% of those shown.

22"
B

Depth = d".	21.75	21.88	22.00	22.12	22.25	21.88	22.00	22.12	22.25
Wt. per foot.	54.5	58.0	62.5	67.5	73.0	77.0	83.0	89.0	96.5
Area, Sq. In.	16.04	17.14	18.38	19.84	21.51	22.74	24.51	26.28	28.38
b".	8.490	8.490	8.500	8.520	8.545	9.220	9.250	9.280	9.320
t.360	.360	.370	.390	.415	.425	.455	.485	.525
h.	20.424	20.424	20.424	20.424	20.424	20.010	20.010	20.010	20.010
m.663	.728	.788	.848	.913	.935	.995	1.055	1.120
n.325	.390	.450	.510	.575	.569	.629	.689	.754
f.50	.50	.50	.50	.50	.55	.55	.55	.55
c.	19.500	19.500	19.500	19.500	19.500	19.000	19.000	19.000	19.000
g.	4"	4"	4"	4"	4"	4"	4"	4"	4"
u.	$\frac{1}{2}$	$\frac{9}{16}$	$\frac{5}{8}$	$\frac{11}{16}$	$\frac{3}{4}$	$\frac{25}{32}$	$\frac{27}{32}$	$\frac{29}{32}$	$\frac{31}{32}$
AXES									
I.	1232.6	1363.9	1495.4	1637.5	1796.7	1866.7	2026.5	2188.6	2373.7
S.	113.34	124.67	135.95	148.06	161.50	170.63	184.23	197.88	213.37
r.	8.77	8.92	9.02	9.08	9.14	9.06	9.09	9.13	9.15
V.	42.2	48.9	55.2	61.8	69.1	87.0	95.8	104.8	115.1
S.	9.95	11.5	13.0	14.5	16.2	18.9	20.7	22.6	24.7
r.	1.62	1.69	1.73	1.76	1.79	1.96	1.98	2.00	2.01
Coef. Str.	1360100	1496000	1631300	1776700	1938000	2047600	2210700	2374600	2560400
Max. Mom. *	2040200	2244100	2447000	2665000	2907000	3073000	3316100	3561900	3840600
V.	94000	94500	97700	103500	110800	111600	120100	128700	140200
P. feet.	7.23	7.92	8.35	8.58	8.75	9.17	9.20	9.23	9.13
R.	36000	36000	37700	41300	45800	47700	53000	58400	65400
W.	48600	48600	49980	52680	56060	57400	61400	65500	70900
Q. feet.	13.99	15.39	16.32	16.86	17.29	17.84	18.00	18.13	18.06
w. lbs.	30	30	30	30	30	30	30	30	30
Rivet dia.	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$

deflection must not exceed
 $\frac{1}{360}$ of the Span.
Total Def. \times Live Load
Tabular Load

Total Deflection in
inches for Maximum
Load; Laterally fixed
beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the
Coefficient of Strength by the Span in feet.

Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free
6	188	188	189	189	195	195	207	207	222	222	223	223	240	240	257	257	280	280		
8	170	170	187	187	195	195	207	207	222	222	223	223	240	240	257	257	280	280		
10	136	136	150	150	163	163	178	178	194	194	205	205	221	221	237	237	256	256		
12	113	110	125	121	136	132	148	144	162	158	171	169	184	182	198	196	213	211	.122	
14	97	90	107	99	117	109	127	118	138	128	146	139	158	151	170	162	183	175	.166	
16	85	75	94	83	102	90	111	98	121	107	128	117	138	126	148	135	160	147	.217	
18	76	64	83	70	91	76	99	83	108	91	114	99	123	107	132	115	142	124	.274	
20	68	54	75	60	82	65	89	71	97	77	102	85	111	92	119	99	128	107	.339	
21	65	50	71	55	78	60	85	66	92	71	98	79	105	85	113	92	122	99	.373	
22	62	46	68	51	74	55	81	61	88	66	93	73	101	80	110	86	116	92	.410	
23	59	42	65	47	71	52	77	56	84	61	89	68	96	74	103	79	111	86	.448	
24	57	40	62	44	68	48	74	52	81	57	85	64	92	69	99	74	107	80	.488	
25	54	37	60	41	65	44	71	49	78	54	82	60	88	64	95	69	102	75	.529	
26	52	35	58	39	63	42	68	45	75	50	79	56	85	60	91	65	99	70	.572	
27	50	32	55	35	60	39	66	43	72	47	76	52	82	56	88	61	95	66	.617	
28	49	31	53	33	58	36	63	39	69	43	73	49	79	53	85	57	91	61	.664	
29	47	...	52	...	56	...	61	...	67	...	71	46	76	49	82	53	88	58	.712	
30	45	...	50	...	54	...	59	...	65	...	68	43	74	47	79	50	85	54	.762	
31	44	...	48	...	53	...	57	...	63	...	66	...	71	...	77	...	83	51	.813	
32	43	...	47	...	51	...	56	...	61	...	64	...	69	...	74	...	80867	
33	41	...	45	...	49	...	54	...	59	...	62	...	67	...	72	...	78927	
34	40	...	44	...	48	...	52	...	57	...	60	...	65	...	70	...	75979	
35	39	...	43	...	47	...	51	...	55	...	59	...	63	...	68	...	73	...	1.04	
36	38	...	42	...	45	...	49	...	54	...	57	...	61	...	66	...	71	...	1.10	
38	36	...	39	...	43	...	47	...	51	...	54	...	58	...	63	...	67	...	1.22	
40	34	...	37	...	41	...	44	...	48	...	51	...	55	...	59	...	64	...	1.35	
42	32	...	36	...	39	...	42	...	46	...	49	...	53	...	57	...	61	...	1.49	
44	31	...	34	...	37	...	40	...	44	...	47	...	50	...	54	...	58	...	1.64	
46	30	...	33	...	35	...	39	...	42	...	45	...	48	...	51	...	54	...	1.79	

24"
B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

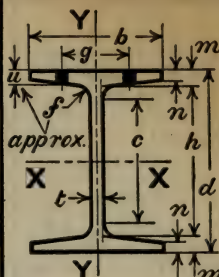
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d". Wt. per foot. Area, Sq. In.. b". t". h". m". n". f". c". g". u".	23.88 70.0 20.62 9.000 .395 22.242 .819 .460 .50 21.375 4" 21 ¹ / ₂ "	24.00 73.5 21.70 9.000 .395 22.242 .879 .520 .50 21.375 4" 23 ¹ / ₃₂ "	24.09 79.5 23.35 9.035 .430 22.242 .924 .565 .50 21.375 4" 25 ¹ / ₃₂ "	24.00 84.5 24.97 9.500 .460 22.106 .947 .570 .55 21.125 4" 13 ¹ / ₁₆ "	24.12 90.5 26.47 9.515 .475 22.106 1.007 .630 .55 21.125 4" 27 ¹ / ₃₂ "	23.91 95.5 28.05 9.730 .505 21.822 1.044 .660 .60 20.750 5 ¹ / ₂ " 13 ¹ / ₁₆ "	24.00 99.5 29.40 9.750 .525 21.822 1.089 .705 .60 20.750 5 ¹ / ₂ " 7 ⁷ / ₈ "	24.09 104.5 30.88 9.775 .550 21.822 1.134 .750 .60 20.750 5 ¹ / ₂ " 29 ¹ / ₃₂ "	Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. × Live Load Tabular Load										
	A X E S	1954.1 163.66 9.74	2108.8 175.73 9.86	2266.7 188.19 9.85	2405.7 200.48 9.82	2588.2 214.61 9.89	2692.7 225.24 9.80	2841.3 236.78 9.83		2997.3 248.84 9.85									
	Y-Y	67.4 15.0 1.81	74.7 16.6 1.86	81.2 18.0 1.87	95.8 20.2 1.96	104.9 22.1 1.99	117.1 24.1 2.04	124.9 25.6 2.06		132.9 27.2 2.07									
	Coef. Str.	1963900	2108800	2258200	2405700	2575300	2702800	2841300		2986100									
	Max. Mom. %	2945900	3163200	3387300	3608600	3863000	4054200	4262000		4479100									
	V.	113200	113800	124300	132500	137500	144900	151200		159000									
	P. feet..	8.67	9.27	9.08	9.08	9.36	9.33	9.40		9.39									
	R.	42000	41800	48400	54100	56800	62700	66600		71400									
	W.	53300	53300	58100	62100	64100	68200	70900		71600									
	Q. feet..	18.42	19.78	19.43	19.37	20.09	19.82	20.04		20.85									
w. lbs..	30	30	30	30	30	30	30	30											
Rivet dia..	7/8"	7/8"	7/8"	7/8"	7/8"	7/8"	7/8"	7/8"											
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.	
		feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed		free
	6	226	226	228	228	249	249	265	265	275	275	290	290	302	302	318	318		
	8	226	226	228	228	249	249	265	265	275	275	290	290	302	302	318	318		
	10	196	196	211	211	226	226	241	241	258	258	270	270	284	284	299	299		
	12	164	162	176	173	188	185	201	200	215	214	225	225	237	237	249	249		
	14	140	132	151	143	161	152	172	165	184	177	193	187	203	197	213	206		
	16	123	111	132	120	141	128	150	138	161	149	169	157	178	166	187	174		
	18	109	94	117	101	125	108	134	118	143	126	150	134	158	141	166	148		
	20	98	80	105	86	113	93	120	101	129	109	135	115	142	121	149	127		
	21	94	75	100	80	108	86	114	94	123	101	129	107	135	113	142	118		
	22	89	69	96	75	103	80	109	87	117	94	123	100	129	105	136	111		
	23	85	64	92	69	98	74	105	82	112	88	117	93	124	98	130	103		
	24	82	60	88	65	94	69	100	76	107	82	113	87	118	91	124	96		
	25	79	56	84	60	90	64	96	71	103	76	108	81	114	86	119	90		
	26	76	53	81	56	87	61	93	67	99	72	104	76	109	80	115	85		
	27	73	49	78	53	84	57	89	63	95	67	100	71	105	75	111	80		
	28	70	46	75	49	81	53	86	59	92	63	97	68	101	70	107	75		
	29	68	43	73	46	78	50	83	55	89	59	93	63	98	67	103	70		
	30	66	41	70	43	75	47	80	52	86	56	90	59	95	63	100	66		
31	63	...	68	...	73	...	78	49	83	52	87	56	92	59	96	62			
32	61	...	66	...	71	...	75	...	81	...	84	52	89	56	93	58			
33	60	...	64	...	68	...	73	...	78	...	82	...	86	...	90	...			
34	58	...	62	...	66	...	71	...	76	...	79	...	84	...	88	...			
35	56	...	60	...	65	...	69	...	74	...	77	...	81	...	85	...			
36	55	...	59	...	63	...	67	...	72	...	75	...	79	...	83	...			
38	52	...	55	...	59	...	63	...	68	...	71	...	75	...	79	...			
40	49	...	53	...	56	...	60	...	64	...	68	...	71	...	75	...			
42	47	...	50	...	54	...	57	...	61	...	64	...	68	...	71	...			
44	45	...	48	...	51	...	55	...	59	...	61	...	65	...	68	...			
46	43	...	46	...	49	...	52	...	56	...	59	...	62	...	65	...			
48	41	...	44	...	47	...	50	...	54	...	56	...	59	...	62	...			

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

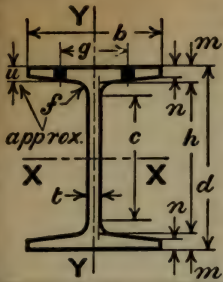
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.

26" B



Depth = d".	25.78	25.88	26.00	26 12
Wt. per foot.	81.0	85.5	91.0	98.0
Area, Sq. In..	23.90	25.11	26.76	28.69
b".	9.470	9.480	9.500	9.530
t".	.440	.450	.470	.500
h".	24.036	24.036	24.036	24.036
m".	.872	.922	.982	1.042
n".	.495	.545	.605	.665
f".	.55	.55	.55	.55
c".	23.00	23.00	23.00	23.00
g".	5 1/2	5 1/2	5 1/2	5 1/2
u".	21 3/2	11 1/6	3 1/4	13 1/6
A X E S				
I....	2600.1	2772.5	2993.1	3231.2
S....	201.71	214.26	230.24	247.41
r....	10.43	10.51	10.58	10.61
I....	84.3	91.7	100.9	110.6
S....	17.8	19.3	21.2	23.2
r....	1.88	1.91	1.94	1.96

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Coef. Str....	2420600	2571100	2762900	2968900
Max. Mem. #	3630900	3856600	4144300	4453400
V....	136100	139700	146600	156800
P. feet..	8.89	9.20	9.42	9.47
R....	50400	52100	56000	62100
W....	69300	70900	74000	78800
Q. feet..	17.46	18.13	18.67	18.84
w. lbs..	35	35	35	35
Rivet dia....	1"	1"	1"	1"

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
	fixed	free	fixed	free	fixed	free	fixed	free	
10	242	242	257	257	276	276	297	297	.072
12	202	201	214	213	230	229	247	246	.103
14	173	166	184	177	197	189	212	204	.140
16	151	139	161	148	173	160	186	172	.183
18	135	119	143	126	153	135	165	146	.232
20	121	102	129	109	138	116	148	125	.287
21	115	94	122	100	132	109	141	116	.316
22	110	88	117	94	126	101	135	108	.347
23	105	82	112	87	120	94	129	101	.379
24	101	77	107	81	115	88	124	95	.413
25	97	72	103	76	110	82	119	88	.448
26	93	67	99	71	106	77	114	83	.484
27	90	63	95	67	102	72	110	77	.522
28	87	59	92	63	99	68	106	73	.562
29	84	56	89	59	95	63	102	68	.602
30	81	52	86	55	92	59	99	64	.645
31	78	49	83	52	89	56	96	61	.688
32	76	...	80	...	86	...	93733
33	73	...	78	...	84	...	90780
34	71	...	76	...	81	...	87832
35	69	...	74	...	79	...	85877
36	67	...	72	...	77	...	82928
38	64	...	68	...	73	...	78	...	1.03
40	61	...	64	...	69	...	74	...	1.15
42	58	...	61	...	66	...	71	...	1.26
44	55	...	58	...	63	...	67	...	1.39
46	53	...	56	...	60	...	65	...	1.52
48	50	...	54	...	58	...	62	...	1.65
50	48	...	51	...	55	...	59	...	1.79

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

28" B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

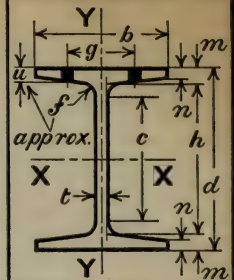
R is Allowable End Reaction for 3 1/2" bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

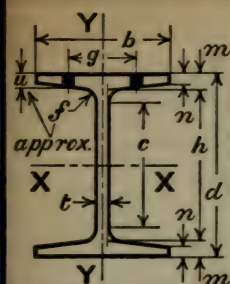
w is Weight of one Standard Connection including Angles and Web Rivets.

Rivet given is Maximum diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.



Depth = d". Wt. per foot. Area, Sq. In.	27.69	27.88	28.00	28.12	28.25	28.38	28.59		
	85.0	91.0	97.0	104.0	112.0	119.0	133.0		
	24.96	26.86	28.61	30.66	32.95	35.11	39.09		
	b.....	9.980	9.980	10.000	10.030	10.065	10.095	10.160	
	t.....	.450	.450	.470	.500	.535	.565	.630	
	h.....	26.008	26.008	26.008	26.008	26.008	26.008	26.008	
	m.....	.841	.936	.996	1.056	1.121	1.186	1.291	
	n.....	.444	.539	.599	.659	.724	.789	.894	
	f.....	.60	.60	.60	.60	.60	.60	.60	
	c.....	24.875	24.875	24.875	24.875	24.875	24.875	24.875	
g.....	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2		
u.....	9/8	23/32	25/32	27/32	29/32	31/32	1 1/2		
A X E S	I.....	3075.2	3441.1	3711.5	4003.3	4328.0	4647.4	5204.0	
	S.....	222.12	246.85	265.11	284.73	306.41	327.51	364.04	
	r.....	11.10	11.32	11.39	11.43	11.46	11.50	11.54	
	I.....	91.0	106.7	117.4	128.7	141.2	153.7	175.3	
Y - Y	S.....	18.2	21.4	23.5	25.7	28.1	30.5	34.5	
	r.....	1.91	1.99	2.03	2.05	2.07	2.09	2.12	
	Coef. Str.....	2665400	2962200	3181300	3416700	3676900	3930100	4368500	
	Max. Mom. * #	3998100	4443300	4771900	5125100	5515300	5895200	6552800	
V.....	P. feet.....	8.91	9.83	10.07	10.13	10.13	10.21	10.11	
	S.....	51800	51700	55900	62100	69500	75900	89900	
	W.....	81000	81000	84600	90000	95400	95400	95400	
	Q. feet.....	16.45	18.29	18.80	18.98	19.27	20.60	22.90	
w. lbs.	w. lbs.....	40	40	40	40	40	40	40	
	Rivet dia....	1"	1"	1"	1"	1"	1"	1"	
	Live Load deflection must not exceed 1/360 of the Span.								
Live Load Def. = Total Def. X Live Load Tabular Load									
Total Deflection in inches for Maximum Load; laterally fixed beam.									

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
	10	267	267	296	296	316	316	337	337	363	363	385	385	.066
	12	222	222	247	247	265	265	285	285	306	306	328	328	.096
	14	190	185	212	206	227	221	244	238	263	256	281	274	.123
	16	167	157	185	174	199	187	214	201	230	216	246	232	.170
	18	148	133	165	149	177	159	190	171	204	184	218	197	.215
	20	133	115	148	128	159	137	171	148	184	159	197	171	.266
	21	127	107	141	119	151	127	163	138	175	148	187	158	.293
	22	121	99	135	111	145	119	155	128	167	138	179	148	.322
	23	116	93	129	104	138	111	149	120	160	129	171	138	.352
	24	111	87	123	96	133	104	142	112	153	121	164	130	.383
	25	107	82	118	90	127	97	137	105	147	113	157	121	.416
	26	103	77	114	85	122	91	131	98	141	106	151	114	.450
	27	99	72	110	80	118	86	127	93	136	100	146	107	.485
	28	95	67	106	75	114	81	122	87	131	93	140	100	.521
	29	92	64	102	70	110	76	118	82	127	88	136	95	.559
	30	89	60	99	67	106	71	114	77	123	83	131	89	.599
	31	86	56	96	63	103	68	110	72	119	78	127	84	.639
	32	83	53	93	59	99	63	107	69	115	74	123	79	.681
	33	81	50	90	56	96	60	104	65	111	70	119	75	.724
	34	78	...	87	...	94	...	100	...	108	...	116769
	35	76	...	85	...	91	...	98	...	105	...	112815
	36	74	...	82	...	88	...	95	...	102	...	109862
	38	70	...	78	...	84	...	90	...	97	...	103960
	40	67	...	74	...	80	...	85	...	92	...	98	...	1.06
	42	64	...	71	...	76	...	81	...	88	...	94	...	1.17
	44	61	...	67	...	72	...	78	...	84	...	89	...	1.29
	46	58	...	64	...	69	...	74	...	80	...	85	...	1.40
	48	56	...	62	...	66	...	71	...	77	...	82	...	1.53
	50	53	...	59	...	64	...	68	...	74	...	79	...	1.66



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.

30"
B

Depth = d".	29.78	29.88	30.00	30.12	30.25	30.44	30.65
Wt. per foot.	110.0	115.0	121.0	129.0	137.0	149.0	163.0
Area Sq. In..	32.45	33.80	35.65	37.82	40.40	43.93	48.00
b.....	10.470	10.480	10.500	10.530	10.570	10.620	10.680
t.....	.520	.530	.550	.580	.620	.670	.730
m.....	27.690	27.690	27.690	27.690	27.690	27.690	27.690
n.....	1.045	1.095	1.155	1.215	1.280	1.375	1.480
f.....	.630	.680	.740	.800	.865	.960	1.065
g.....	.65	.65	.65	.65	.65	.65	.65
e.....	26.50	26.50	26.50	26.50	26.50	26.50	26.50
d.....	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2	5 1/2
c.....	27 3/32	7 1/8	15 1/16	1"	1 1/16	1 3/16	1 9/32
A X E S							
I.....	4687.7	4942.9	5269.7	5622.7	6026.7	6606.6	7270.7
S.....	314.82	330.85	351.31	373.35	398.46	434.07	474.43
r.....	12.02	12.09	12.16	12.19	12.21	12.26	12.31
I.....	141.8	151.8	164.3	177.6	192.6	214.5	239.8
S.....	27.1	29.0	31.3	33.7	36.4	40.4	44.9
r.....	2.09	2.12	2.15	2.17	2.18	2.21	2.24
Coef. Str.....	3777900	3970200	4215800	4480200	4781500	5208900	5693200
Max. Mor. "S"	5666800	5955300	6323600	6720400	7172300	7813300	8539800
V.....	185800	190000	198000	209700	225100	244700	268500
P, feet..	10.17	10.45	10.65	10.68	10.62	10.64	10.60
R.....	66600	68400	72800	79400	84800	99700	113400
W.....	105300	107400	107400	107400	107400	107400	107400
Q, feet..	17.94	18.48	19.63	20.86	22.26	24.25	26.50
w, lbs....	45	45	45	45	45	45	45
Rivet dia....	1"	1"	1"	1"	1"	1"	1"
Live Load deflection must not exceed 1/360 of the Span.							
Live Load Def. = Total Def. x Live Load Tabular Load							
Total Deflection in inches for Maximum Load; Laterally fixed beam.							

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free		
12	315	315	331	331	351	351	373	373	398	398	434	434	474	474	.089			
14	270	266	284	280	301	296	320	315	342	337	372	367	407	403	.122			
16	236	225	248	236	263	250	280	267	299	285	326	311	356	340	.159			
18	210	192	221	203	234	214	249	229	266	245	289	266	316	292	.201			
20	189	166	198	174	211	186	224	198	239	211	261	231	285	253	.248			
21	180	155	189	163	201	173	213	184	228	197	248	215	271	236	.274			
22	172	145	180	152	192	162	204	172	217	184	237	201	259	221	.300			
23	164	135	173	143	183	151	195	161	208	172	227	189	248	207	.329			
24	157	127	165	133	176	142	187	151	199	161	217	176	237	193	.358			
25	151	119	159	125	169	133	179	141	191	151	208	165	228	182	.388			
26	145	112	153	118	162	125	172	133	184	142	200	155	219	171	.420			
27	140	105	147	111	156	117	166	125	177	134	193	146	211	161	.452			
28	135	99	142	104	151	111	160	118	171	126	186	138	203	151	.487			
29	130	93	137	98	145	104	154	111	165	119	180	130	196	142	.522			
30	126	88	132	92	141	99	149	104	159	112	174	123	190	135	.559			
31	122	83	128	87	136	93	144	99	154	106	168	116	184	127	.596			
32	118	78	124	83	132	88	140	93	149	100	163	110	178	120	.636			
33	115	75	120	78	128	83	136	89	145	95	158	104	173	114	.676			
34	111	70	117	74	124	78	132	84	141	90	153	98	167	107	.718			
35	108	...	113	...	120	74	128	79	137	85	149	93	163	102	.760			
36	105	...	110	...	117	...	124	...	133	...	145	...	158804			
38	99	...	104	...	111	...	118	...	126	...	137	...	150896			
40	95	...	99	...	105	...	112	...	120	...	130	...	142993			
42	90	...	95	...	100	...	107	...	114	...	124	...	136	...	1.10			
44	86	...	90	...	96	...	102	...	109	...	118	...	129	...	1.20			
46	82	...	86	...	92	...	97	...	104	...	113	...	124	...	1.31			
48	79	...	83	...	88	...	93	...	100	...	109	...	119	...	1.43			
50	76	...	79	...	84	...	90	...	96	...	104	...	114	...	1.55			
52	73	...	76	...	81	...	86	...	92	...	100	...	109	...	1.68			
54	70	...	74	...	78	...	83	...	89	...	96	...	105	...	1.81			

Live Load deflection must not exceed 1/360 of the Span.

Live Load Def. = Total Def. \times Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

33" B

BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

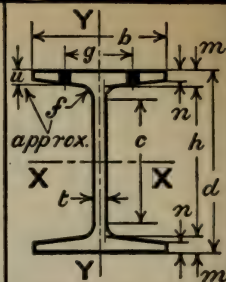
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".	32.89	33.00	33.12	33.27	33.50
Wt. per foot.	125.0	135.0	143.0	152.0	165.0
Area, Sq. In..	36.83	39.55	42.05	44.65	48.52
b".....	11.205	11.250	11.285	11.312	11.350
t".....	.535	.580	.615	.642	.680
h".....	30.676	30.676	30.676	30.676	30.676
m".....	1.107	1.162	1.222	1.297	1.412
n".....	.663	.718	.778	.853	.968
c".....	.70	.70	.70	.70	.70
e".....	29.375	29.375	29.375	29.375	29.375
g".....	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$
u".....	$13\frac{1}{16}$	$7\frac{1}{8}$	$15\frac{1}{16}$	1"	$1\frac{1}{8}$
AXES					
X-X	I.....	6498.2	6967.4	7442.2	7991.4
X-X	S.....	395.15	422.27	449.41	480.40
X-X	r.....	13.28	13.27	13.30	13.38
Y-Y	I.....	183.2	198.7	215.1	234.9
Y-Y	S.....	32.7	35.3	38.1	41.5
Y-Y	r.....	2.23	2.24	2.26	2.29
Coef. Str.....	4741800	5067200	5392900	5764800	6329800
Max. Mom. #/ft	7112700	7600800	8089300	8647100	9494800
V.....	211200	229700	244400	256300	273400
P, feet.....	11.23	11.03	11.03	11.25	11.58
R.....	69300	79700	87900	94300	103500
W.....	107370	107370	107370	107370	107370
Q, feet.....	22.08	23.60	25.11	26.85	29.48
w, lbs.....	45	45	45	45	45
Rivet dia.....	1"	1"	1"	1"	1"

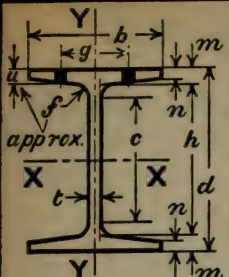
Live Load deflection must not exceed 1/360 of the Span.

Live Load Def. = Total Def. x Live Load Tabular Load

Total Deflection in inches for Maximum Load; laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
12	395	395	422	422	449	449	480	480	527	527	.081
14	339	338	362	362	385	385	412	411	452	451	.111
16	296	287	317	307	337	327	360	349	396	384	.144
18	263	246	282	265	300	282	320	301	352	331	.183
20	237	214	253	229	270	245	288	261	317	288	.226
21	226	200	241	214	257	229	275	245	301	268	.249
22	216	188	230	200	245	214	262	229	288	252	.273
23	206	174	220	188	235	201	251	215	275	236	.298
24	198	164	211	177	225	189	240	201	264	222	.325
25	190	154	203	166	216	177	231	188	253	208	.353
26	182	145	195	157	207	166	222	177	244	197	.381
27	176	138	188	148	200	157	214	167	234	185	.411
28	169	129	181	139	193	149	206	158	226	175	.442
29	164	123	175	132	186	140	199	149	218	165	.475
30	158	116	169	124	180	133	192	141	211	155	.508
31	153	110	164	118	174	125	186	134	204	146	.542
32	148	104	158	111	169	119	180	127	198	139	.578
33	144	99	154	106	163	112	175	121	192	132	.614
34	140	94	149	100	159	107	170	115	186	125	.652
35	136	89	145	95	154	101	165	109	181	119	.691
36	132	84	141	90	150	96	160	103	176	113	.731
38	125	..	133	..	142	..	152	..	167	..	.815
40	119	..	127	..	135	..	144	..	158	..	.903
42	113	..	121	..	128	..	137	..	151	..	.995
44	108	..	115	..	123	..	131	..	144	..	1.09
46	103	..	110	..	117	..	125	..	138	..	1.19
48	99	..	106	..	112	..	120	..	132	..	1.30
50	95	..	101	..	108	..	115	..	127	..	1.41
52	91	..	97	..	104	..	111	..	122	..	1.53
54	88	..	94	..	100	..	107	..	117	..	1.65

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.



BETHLEHEM BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds.
 P is Minimum Span in feet, uniformly loaded to cause V.
 R is Allowable End Reaction for 3/4" bearing. For details see page of Allowable End Reactions.
 W is Maximum Load on one Standard Connection.
 Q is Minimum Span in feet, uniformly loaded to cause W.
 w is Weight of one Standard Connection including Angles and Web Rivets.
 Rivet given is Maximum Diameter in flange.
 Allowable concentrated center loads are 50% and their deflections 80% of those shown.

36" B

Depth = d".		35.9	36.00	36.12	36.25	36.52
Wt. per foot.		147.0	155.0	164.0	173.0	190.0
Area, Sq.In.		43.23	45.58	48.10	50.94	55.87
b".		11.968	12.000	12.030	12.065	12.111
t".		.583	.615	.645	.680	.726
h".		33.502	33.502	33.502	33.502	33.502
m".		1.199	1.249	1.309	1.374	1.509
n".		.725	.775	.835	.900	1.035
f".		.75	.75	.75	.75	.75
c".		32.125	32.125	32.125	32.125	32.125
g".		7 1/2	7 1/2	7 1/2	7 1/2	7 1/2
u".		29 3/32	31 3/32	11 3/32	15 3/32	17 3/32
AXES						
X-X	I....	9036.3	9547.4	10133.	10784.	12049.
	S....	503.42	530.41	561.07	594.98	659.86
	r....	14.46	14.47	14.51	14.55	14.68
Y-Y	I....	243.3	259.9	279.4	301.1	344.9
	S....	40.7	43.	46.	49.	57.0
	r....	2.37	2.39	2.41	2.43	2.48
Coef. Str....		6041000	6364900	6732900	7139800	7918300
Max.Mom." #		9061500	9547400	10099300	10709600	11877400
V....		251200	265700	279600	295800	318200
P. feet....		12.02	11.98	12.04	12.07	12.44
R....		80200	88100	95500	104300	116100
W....		107370	107370	107370	107370	107370
Q. feet....		28.13	29.64	31.35	33.25	36.87
w. lbs....		45	45	45	45	45
Rivet dia....		1"	1"	1"	1"	1"
Total Deflection in inches for Maximum Load; Laterally fixed beam.						
Live Load Def. = Total Def. x Live Load						
Live Load deflection must not exceed 1/360 of the Span.						

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
	feet	fixed	free	fixed	free	fixed	free	fixed	free	
12	502	502	530	530	559	559	592	592	636	.074
14	432	432	455	455	481	481	510	510	566	.101
16	378	372	398	392	421	415	446	440	495	.132
18	336	321	354	333	374	358	397	380	440	.167
20	302	279	318	294	337	312	357	331	396	.207
21	288	262	303	276	321	293	340	310	377	.228
22	275	246	289	258	306	274	325	291	360	.250
23	263	231	277	243	293	258	310	273	344	.273
24	252	217	265	229	281	243	297	257	330	.298
25	242	204	255	216	269	228	286	243	317	.323
26	232	192	245	203	259	216	275	229	305	.350
27	224	182	236	192	249	203	264	215	293	.377
28	216	172	227	181	240	192	255	204	283	.406
29	208	162	219	171	232	182	246	193	273	.435
30	201	154	212	162	224	172	238	183	264	.466
31	195	146	205	154	217	163	230	173	255	.497
32	189	139	199	146	210	155	223	164	247	.530
33	183	131	193	139	204	147	216	156	240	.563
34	178	125	187	132	198	140	210	148	233	.598
35	173	119	182	125	192	133	204	141	226	.634
36	168	113	177	119	187	126	198	134	220	.670
38	159	102	167	108	177	115	188	122	208	.747
40	151	...	159	...	168	104	178	110	198	.828
42	144	...	152	...	160	...	170	...	189	.912
44	137	...	145	...	153	...	162	...	180	1.001
46	131	...	138	...	146	...	155	...	172	1.094
48	126	...	133	...	140	...	149	...	165	1.191
50	121	...	127	...	135	...	143	...	158	1.293
52	116	...	122	...	129	...	137	...	152	1.399
54	112	...	118	...	125	...	132	...	147	1.508

Live Load deflection must not exceed 1/360 of the Span.	Live Load Def. = Total Def. x Live Load Tabular Load
Live Load Def. = Total Def. x Live Load Tabular Load	
Total Deflection in inches for Maximum Load; Laterally fixed beam.	
.074	
.101	
.132	
.167	
.207	
.228	
.250	
.273	
.298	
.323	
.350	
.377	
.406	
.435	
.466	
.497	
.530	
.563	
.598	
.634	
.670	
.747	
.828	
.912	
1.001	
1.094	
1.191	
1.293	
1.399	
1.508	

ALLOWABLE END REACTIONS FOR BETHLEHEM BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per foot	Web t	Unit Stress in Buckling	Reaction R for $\frac{3}{4}$ " Bearing	Min. Span for $\frac{3}{4}$ " Bearing	Reaction R for $\frac{5}{8}$ " Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V	Length of Bearing to develop V
8	17.5	.250"	15000	20600	4.19'	24000	3750	24000	4.40"
	19.0	.270	15000	22300	4.25	26100	4050	26100	4.44
9	20.5	.250	14800	21300	5.41	27000	3700	27000	5.05
	22.0	.260	15000	22400	5.54	28300	3900	28300	5.01
10	21.0	.240	14030	20200	6.49	27000	3370	28500	5.96
	23.5	.250	14210	21300	6.93	28400	3550	30000	5.94
	26.0	.270	14660	23700	6.91	31700	3960	32700	5.76
	28.5	.285	14840	25400	7.15	33800	4230	34800	5.73
12	25.0	.240	12780	19900	9.39	26000	3070	34200	8.17
	28.0	.245	12860	20500	10.42	26800	3150	35300	8.21
	31.5	.270	13470	23800	10.22	31000	3640	39300	7.77
	36.0	.300	14090	27800	9.93	36200	4230	44100	7.36
	40.0	.330	14750	31700	9.50	41400	4870	47500	6.75
	44.0	.360	15000	35300	9.40	46100	5400	52400	6.67
14	48.5	.395	15000	38900	9.40	50800	5930	58100	6.74
	30.0	.265	12350	22900	11.13	29400	3270	44100	9.99
	33.0	.265	12290	22800	12.57	29300	3260	44500	10.15
	37.5	.305	13260	28300	11.52	36400	4040	51700	9.30
15	42.0	.340	13920	33100	11.10	42600	4730	58100	8.78
	36.0	.280	12220	24800	13.34	31600	3420	50100	10.90
	38.5	.290	12460	26200	13.67	33400	3610	52200	10.70
	40.0	.305	12830	28400	13.01	36200	3910	55000	10.30
16	42.5	.325	13290	31300	12.50	40000	4320	58900	9.89
	46.0	.365	14150	37400	11.06	47700	5160	64600	8.77
	50.5	.385	14360	40100	11.33	51200	5530	68700	8.67
	54.5	.410	14720	43800	11.27	55800	6040	73800	8.48
	59.5	.450	15000	48900	10.97	62400	6750	81700	8.35
	71.5	.520	15000	56600	11.30	72200	7800	93600	8.25
18	35.0	.285	11900	25400	13.02	32200	3390	54100	11.96
	40.0	.295	12080	26700	14.78	33800	3560	56600	11.90
	45.0	.330	12880	31900	13.87	40400	4250	63800	11.01
	50.0	.365	13530	37100	13.32	46900	4940	71200	10.41
	56.5	.375	13860	39000	14.38	49400	5200	71500	9.75
	60.5	.390	14060	41100	14.82	52100	5480	74900	9.67
20	66.0	.420	14450	45500	14.53	57700	6070	81200	9.38
	71.5	.455	14840	50600	14.21	64100	6750	88700	9.14
	47.0	.325	11940	31000	16.49	38800	3880	70000	13.54
	49.0	.330	12030	31800	16.83	39700	3970	71300	13.46
	52.0	.355	12600	35800	15.80	44700	4470	76900	12.69
	54.5	.370	12910	38200	15.53	47800	4780	80500	12.35
22	59.0	.380	13200	40200	16.15	50200	5020	80900	11.62
	64.5	.400	13460	43100	16.50	53900	5390	85800	11.43
	69.0	.420	13780	46300	16.61	57900	5790	90700	11.19
	74.0	.440	14080	49500	16.63	61900	6190	95700	10.95

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

ALLOWABLE END REACTIONS FOR BETHLEHEM BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per foot	Web t	Unit Stress in Buckling	Reaction R for $3\frac{1}{2}''$ Bearing	Min. Span for $3\frac{1}{2}''$ Bearing	Reaction R for $5\frac{1}{2}''$ Bearing	Increase in R for $1''$ Additional Bearing	Max. Web Shear V	Length of Bearing to develop V
20	56.0	.375"	12260	39100	16.77	48300	4600	89500	14.46"
	59.5	.375	12210	38900	18.23	48100	4580	90000	14.66
	62.0	.390	12520	41500	17.87	51300	4880	93900	14.23
	64.5	.400	12710	43200	17.88	53400	5080	96600	14.00
	68.5	.410	12930	45100	18.28	55700	5300	97800	13.45
	73.0	.430	13230	48400	18.41	59700	5690	103200	13.14
	78.0	.460	13690	53500	17.70	66100	6300	110900	12.61
22	54.5	.360	11190	36000	18.88	44100	4030	94000	17.89
	58.0	.360	11140	36000	20.78	44000	4010	94500	18.10
	62.5	.370	11330	37700	21.64	46100	4190	97700	17.82
	67.5	.390	11720	41300	21.51	50400	4570	103500	17.12
	73.0	.415	12170	45800	21.16	55900	5050	110800	16.38
	77.0	.425	12480	47700	21.46	58300	5300	111600	15.56
	83.0	.455	12950	53000	20.86	64800	5890	120100	14.89
24	89.0	.485	13370	58400	20.33	71300	6480	128700	14.36
	96.5	.525	13850	65400	19.58	80000	7270	140200	13.78
	70.0	.395	11190	42000	23.38	50800	4420	113200	19.61
	73.5	.395	11150	41800	25.22	50600	4400	113800	19.85
	79.5	.430	11850	48400	23.33	58600	5090	124300	18.40
	84.5	.460	12380	54100	22.24	65500	5700	132500	17.26
	90.5	.475	12590	56800	22.67	68800	5980	137500	16.99
26	95.5	.505	13080	62700	21.55	73000	6600	144900	15.94
	99.5	.525	13350	66600	21.33	80600	7010	151200	15.57
	104.5	.550	13660	71400	20.91	86400	7510	159000	15.16
	81.0	.440	11450	50400	24.01	60500	5040	136100	20.50
	85.5	.450	11570	52100	24.68	62500	5210	139700	20.33
	91.0	.470	11920	56000	24.66	67200	5600	146600	19.66
	98.0	.500	12410	62100	23.90	74500	6210	156800	18.77
28	85.0	.450	11040	51800	25.75	61700	4970	149500	23.18
	91.0	.450	10980	51700	28.65	61600	4940	150600	23.52
	97.0	.470	11310	55900	28.46	66500	5320	157900	22.68
	104.0	.500	11790	62100	27.51	73900	5900	168700	21.56
	112.0	.535	12290	69500	26.45	82700	6580	181400	20.51
	119.0	.565	12670	75900	25.91	90200	7160	192400	19.78
	133.0	.630	13400	89900	24.30	106800	8440	216100	18.45
30	110.0	.520	11640	66600	28.36	78700	6050	185800	23.21
	115.0	.530	11740	68400	29.02	80900	6220	190000	23.05
	121.0	.550	12040	72800	28.95	86000	6620	198000	22.41
	129.0	.580	12450	79400	28.21	93900	7220	209700	21.54
	137.0	.620	12890	88400	27.05	104400	7990	225100	20.61
	149.0	.670	13390	99700	26.13	117600	8970	244700	19.66
	163.0	.730	13910	113400	25.11	133700	10160	268500	18.78
33	125.0	.535	11040	69300	34.23	81100	5910	211200	27.51
	135.0	.580	11690	79700	31.79	93200	6780	229700	25.63
	143.0	.615	12130	87900	30.68	102800	7460	244400	24.48
	152.0	.642	12430	94300	30.55	110300	7980	256300	23.80
	165.0	.680	12820	103500	30.59	120900	8710	273400	23.01
	147.0	.583	11030	80200	37.66	93100	6430	251200	30.09
	155.0	.615	11460	88100	36.12	102200	7050	265700	28.69
36	164.0	.645	11820	95500	35.25	110700	7620	279600	27.66
	173.0	.680	12210	104300	34.23	120900	8300	295800	26.58
	190.0	.726	12660	116100	34.11	134500	9190	318200	25.49

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

CONNECTION ANGLES FOR BETHLEHEM BEAMS

DIMENSIONS, WEIGHTS, AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles				Connection Details.			
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length	Weight inc. Web Rivets				
			Single Shear										
			Power Driven Rivets	Unfinished Bolts									
8"	17.5	22500	23860	17670	3/16	IC.13.10	2 5/8	6" x 4" x 3/8" 0' — 5 1/2" Long	13 lbs.				
	19.0	24300	23860	17670	3/16	IC.13.10	2 5/8						
9"	20.5	22500	23860	17670	3/16	IC.13.10	2 5/8						
	22.0	23400	23860	17670	3/16	IC.13.10	2 5/8						
10"	21.0	21600	23860	17670	3/16	IC.13.10	2 5/8						
	23.5	22500	23860	17670	3/16	IC.13.10	2 5/8						
	26.0	24300	23860	17670	3/16	IC.13.10	2 5/8						
	28.5	24460	23860	17670	3/16	IC.13.10	2 5/8						
12"	25.0	21600	23860	17670	3/16	IC.13.10	2 5/8						
	28.0	22050	23860	17670	2/16	IC.13.10	2 5/8						
	31.5	24300	23860	17670	3/16	IC.13.10	2 5/8						
	36.0	27000	23860	17670	3/16	IC.13.10	2 5/8						
	40.0	29700	23860	17670	1/4	IC.13. 9	2 9/16						
	44.0	32400	23860	17670	1/4	IC.13. 9	2 9/16						
	48.5	35570	23860	17670	1/4	IC.13. 9	2 9/16						
14"	30.0	23850	47720	35340	3/16	IC.19.10	2 5/8	4" x 3 1/2" x 3/8" 0' — 11 1/2" Long	19 lbs.				
	33.0	23850	47720	35340	3/16	IC.19.10	2 5/8						
	37.5	27450	47720	35340	3/16	IC.19.10	2 5/8						
	42.0	30600	47720	35340	1/4	IC.19. 9	2 9/16						
15"	36.0	25200	47720	35340	3/16	IC.19.10	2 5/8						
	38.5	26100	47720	35340	3/16	IC.19.10	2 5/8						
	40.0	27450	47720	35340	1/4	IC.19.10	2 5/8						
	42.5	29250	47720	35340	1/4	IC.19. 9	2 9/16						
	46.0	32850	47720	35340	1/4	IC.19. 9	2 9/16						
	50.5	34650	47720	35340	1/4	IC.19. 9	2 9/16						
	54.5	36900	47720	35340	1/4	IC.19. 9	2 9/16						
	59.5	40500	47720	35340	5/16	IC.19. 8	2 1/2						
	71.5	46800	47720	35340	5/16	IC.19. 8	2 1/2						
16"	35.0	25650	47720	35340	3/16	IC.19.10	2 5/8				4" x 3 1/2" x 3/8" 1' — 2 1/2" Long	25 lbs.	
	40.0	25650	47720	35340	3/16	IC.19.10	2 5/8						
	45.0	28800	47720	35340	1/4	IC.19. 9	2 9/16						
	50.0	32400	47720	35340	1/4	IC.19. 9	2 9/16						
	56.5	33750	47720	35340	1/4	IC.19. 9	2 9/16						
	60.5	35100	47720	35340	1/4	IC.19. 9	2 9/16						
	66.0	37800	47720	35340	1/4	IC.19. 9	2 9/16						
	71.5	40960	47720	35340	5/16	IC.19. 8	2 1/2						
18"	47.0	36580	59650	44180	1/4	IC.25. 9	2 9/16	4" x 3 1/2" x 3/8" 1' — 2 1/2" Long	30 lbs.				
	49.0	37130	59650	44180	1/4	IC.25. 9	2 9/16						
	52.0	39940	59650	44180	1/4	IC.25. 9	2 9/16						
	54.5	41630	59650	44180	1/4	IC.25. 9	2 9/16						
	59.0	42750	59650	44180	1/4	IC.25. 9	2 9/16						
	64.5	45000	59650	44180	1/4	IC.25. 9	2 9/16						
	69.0	47250	59650	44180	1/4	IC.25. 9	2 9/16						
	74.0	49500	59650	44180	5/16	IC.25. 8	2 1/2						
20"	56.0	42200	59650	44180	1/4	IC.25. 9	2 9/16						
	59.5	42200	59650	44180	1/4	IC.25. 9	2 9/16						
	62.0	43880	59650	44180	1/4	IC.25. 9	2 9/16						
	64.5	45000	59650	44180	1/4	IC.25. 9	2 9/16						
	68.5	46150	59650	44180	1/4	IC.25. 9	2 9/16						
	73.0	48380	59650	44180	1/4	IC.25. 9	2 9/16						
	78.0	51750	59650	44180	5/16	IC.25. 8	2 1/2						
22"	54.5	48600	71580	53020	1/4	IC.30. 9	2 9/16	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.				
	58.0	48600	71580	53020	1/4	IC.30. 9	2 9/16						
	62.5	49980	71580	53020	1/4	IC.30. 9	2 9/16						
	67.5	52680	71580	53020	1/4	IC.30. 9	2 9/16						
	73.0	56060	71580	53020	1/4	IC.30. 9	2 9/16						
	77.0	57390	71580	53020	1/4	IC.30. 9	2 9/16						
	83.0	61440	71580	53020	5/16	IC.30. 8	2 1/2						
	89.0	65490	71580	53020	5/16	IC.30. 8	2 1/2						
	96.5	70890	71580	53020	5/16	IC.30. 8	2 1/2						
24"	70.0	53330	71580	53020	1/4	IC.30. 9	2 9/16						
	73.5	53330	71580	53020	1/4	IC.30. 9	2 9/16						
	79.5	58050	71580	52020	5/16	IC.30. 9	2 9/16						
	84.5	62100	71580	53020	5/16	IC.30. 8	2 1/2						
	90.5	64140	71580	53020	5/16	IC.30. 8	2 1/2						
	95.5	68180	71580	53020	5/16	IC.30. 8	2 1/2						
	99.5	70880	71580	53020	5/16	IC.30. 8	2 1/2						
	104.5	71580	71580	53020	5/16	IC.30. 8	2 1/2						

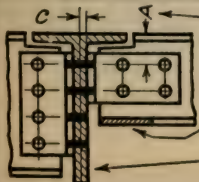
LOADS BY A. I. S. C. SPECIFICATION

CONNECTION ANGLES FOR BETHLEHEM BEAMS

DIMENSIONS, WEIGHTS AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles				Weight inc. Web Rivets	Connection Details.			
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage	Size and Length						
			Power Driven Rivets	Unfinished Bolts					Single Shear					
26"	81.0	69300	83510	61850	5/16	IC.35. 8	2 1/2	4" x 3 1/2" x 3/8" Long 1' — 8 1/2" Long	35 lbs.					
	85.5	70875	83510	61850	5/16	IC.35. 8	2 1/2							
	91.0	74030	83510	61850	5/16	IC.35. 8	2 1/2							
	98.0	78750	83510	61850	5/16	IC.35. 8	2 1/2							
28"	85.0	81040	95440	70690	5/16	IC.40. 8	2 1/2	4" x 3 1/2" x 3/8" Long 1' — 11 1/4" Long	40 lbs.					
	91.0	81040	95440	70690	5/16	IC.40. 8	2 1/2							
	97.0	84640	95440	70690	5/16	IC.40. 8	2 1/2							
	104.0	90000	95440	70690	5/16	IC.40. 8	2 1/2							
	112.0	95440	95440	70690	5/16	IC.40. 8	2 1/2							
	119.0	95440	95440	70690	3/8	IC.40. 7	2 7/16							
	133.0	95440	95440	70690	3/8	IC.40. 7	2 7/16							
	30"	110.0	105300	107370	79530	5/16	IC.45. 8				2 1/2	4" x 3 1/2" x 3/8" Long 2' — 2 1/2" Long	45 lbs.	
		115.0	107370	107370	79530	5/16	IC.45. 8				2 1/2			
		121.0	107370	107370	79530	5/16	IC.45. 8				2 1/2			
129.0		107370	107370	79530	3/8	IC.45. 7	2 7/16							
137.0		107370	107370	79530	3/8	IC.45. 7	2 7/16							
149.0		107370	107370	79530	3/8	IC.45. 7	2 7/16							
33"	152.0	107370	107370	79530	3/8	IC.45. 6	2 3/8	4" x 3 1/2" x 3/8" Long 2' — 2 1/2" Long	45 lbs.					
	125.0	107370	107370	79530	5/16	IC.45. 8	2 1/2							
	135.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	143.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	152.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	165.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
36"	147.0	107370	107370	79530	3/8	IC.45. 7	2 7/16	4" x 3 1/2" x 3/8" Long 2' — 2 1/2" Long	45 lbs.					
	155.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	164.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	173.0	107370	107370	79530	3/8	IC.45. 7	2 7/16							
	190.0	107370	107370	79530	7/16	IC.45. 6	2 3/8							



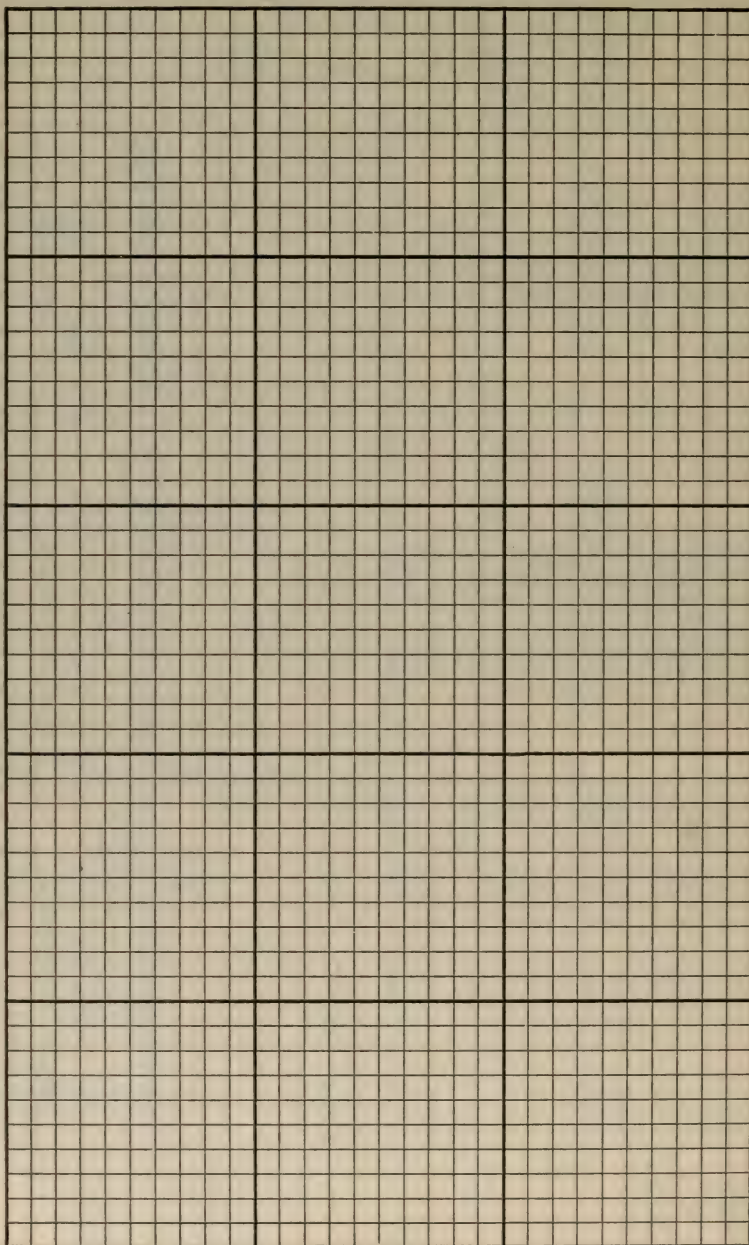
When $A = 2\frac{3}{4}"$ all beams up to and including 26" can be framed opposite with tops flush.

When $A = 3"$ all beams except 14" can be framed opposite with tops flush.

Flange must be cut away as shown for field riveting on all beams framing opposite a larger beam, if flange interferes with outstanding rivets.

Minimum Web required to develop Single Shearing Value is .33"
Minimum Web required to develop Double Shearing Value is .53"

NOTES and DIAGRAMS



Part IV

Section 6

BETHLEHEM GIRDER BEAM SECTIONS

Dimensions—Technical Functions

Allowable Total Loads by A. I. S. C. Specification

Allowable End Reactions—Standard Connection Angles

Usual Stock Sizes

Depth	Weight	Depth	Weight	Depth	Weight
8"	33.0 *	16"	81.0 *	26"	151.0 *
9"	38.5 *	18"	86.0 *	28"	165.0 *
10"	44.5 *	20"	113.0 *	30"	180.0 *
12"	55.5 *	22"	108.0 *	33"	210.0 *
15"	74.0 *	24"	120.0 *	36"	240.0 *

Manufacturers Section Index

Sec. Index	Depth	Weight				Sec. Index	Depth	Weight					
G 8	8"	29.5	33.0	36.5		G 20	20"	99.0	107.0	113.0	120.0		
G 9	9"	36.0	38.5	43.5		G 20a	20"	127.0	135.0	142.0	149.0		
G 10	10"	41.5	44.5	50.0		G 22	22"	101.0	108.0	116.0	124.0	132.0	
G 12	12"	51.5	55.5	61.0		G 24	24"	107.0	113.0	120.0	128.0		
G 12a	12"	66.0	70.5	76.5		G 24a	24"	132.0	140.0	148.0			
G 15	15"	64.5	69.0	74.0	80.5	G 26	26"	138.0	144.0	151.0	160.0		
G 15a	15"	94.0	99.0	105.0	111.0	G 28	28"	145.0	156.0	165.0	175.0	186.0	
G 15b	15"	127.0	135.0	141.0	147.0	G 30	30"	173.0	180.0	190.0	200.0	220.0	240.0
G 16	16"	74.5	81.0	87.0	94.0	G 33	33"	200.0	210.0	220.0	230.0	245.0	260.0
G 18	18"	80.0	86.0	92.0	99.0	G 36	36"	230.0	240.0	250.0	260.0	280.0	300.0

G

[illegible]

Depth = d".		7.88	8.00	8.12	deflection must not exceed 1/360 of the Span.
Wt. per foot.		29.5	33.0	36.5	
Area. Sq. In.		8.69	9.69	10.81	
b.....		7.995	8.000	8.020	
t.....		.285	.290	.310	
h.....		6.738	6.738	6.738	
m.....		.571	.631	.691	
n.....		.250	.310	.370	
f.....		.40	.40	.40	
c.....		5.938	5.938	5.938	
g.....		51/32	51/32	51/32	
u.....		11/32	13/32	15/32	
AXES	X-X	100.7	116.1	132.6	
	S.....	25.56	29.03	32.66	
	r.....	3.41	3.46	3.50	
	Y-Y	28.4	33.6	39.0	
	I.....	7.10	8.39	9.72	Total Deflection in inches for Maximum load; Laterally fixed end; 1 in.
	r.....	1.81	1.86	1.90	
Coef. Str.....		306700	348300	391900	
Max.Mom.%		460000	522500	587900	
V.....		26900	27800	30200	Live Load Def. = Total Def. \times Live Load Tabular load
P. feet.....		5.70	6.27	6.49	
R.....		23400	23900	25700	
W.....		25650	26100	27920	
Q. feet.....		5.98	6.67	7.02	
w. lbs.....		16	16	16	
Rivet dia.....		7/8	7/8	7/8	

Span feet	Laterally		Laterally		Laterally		T in L
	fixed	free	fixed	free	fixed	free	
5	54	54	56	56	60	60	
6	51	51	56	56	60	60	.084
7	44	44	50	50	56	56	.114
8	38	38	44	44	49	49	.149
9	34	34	39	39	44	44	.189
10	31	31	35	35	39	39	.233
11	28	27	32	31	36	35	.281
12	26	25	29	28	33	32	.335
13	24	22	27	25	30	28	.394
14	22	20	25	23	28	26	.456
15	20	18	23	20	26	23	.524
16	19	16	22	19	24	21	.596
17	18	15	20	17	23	19	.674
18	17	14	19	15	22	18	.754
19	16	13	18	14	21	16	.840
20	15	11	17	13	20	15	.931

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

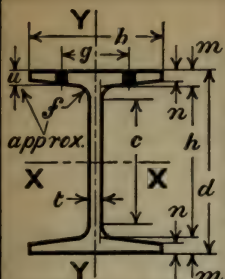
Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

9"

G



Depth = d"	8.94	9.00	9.12
Wt. per foot.	36.0	38.5	43.5
Area, Sq. In.	10.66	11.35	12.73
b"	8.480	8.500	8.540
t	.290	.310	.350
h	7.628	7.628	7.628
m	.656	.686	.746
n	.315	.345	.405
f	.40	.40	.40
c	6.875	6.875	6.875
e	5½	5½	5½
u	15½	15½	15½
AXES			
X-X	I.... 160.5	171.9	195.4
S	35.91	38.20	42.85
r	3.88	3.89	3.92
Y-Y	I.... 41.0	44.4	51.3
S	9.67	10.4	12.0
r	1.96	1.98	2.01
Coef. Str....	430900	458400	514200
Max. M. m. %	646300	687600	771300
V	31100	33500	38300
P, feet..	6.93	6.84	6.71
R	25000	26700	30200
W	26100	27900	31500
Q, feet..	8.26	8.22	8.16
w, lbs...	16	16	16
Rivet dia....	7/8	7/8	7/8

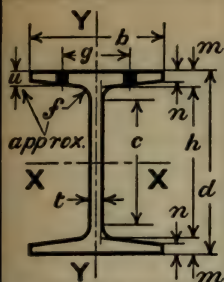
Live Load deflection must not exceed 1/360 of the Span.

Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		
	fixed	free	fixed	free	fixed	free	
5	62	62	67	67	77	77	
6	62	62	67	67	77	77	
7	62	62	66	66	74	74	.101
8	54	54	57	57	64	64	.132
9	48	48	51	51	57	57	.168
10	43	43	46	46	51	51	.207
11	39	39	42	42	47	47	.250
12	36	35	38	37	43	42	.298
13	33	31	35	33	40	38	.350
14	31	29	33	31	37	34	.406
15	29	26	31	28	34	31	.466
16	27	24	29	26	32	28	.530
17	25	22	27	23	30	26	.599
18	24	20	25	21	29	24	.670
19	23	19	24	20	27	22	.747
20	22	17	23	18	26	21	.828

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.



BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

12"

G

Depth = d".	11.91	12.00	12.12	11.88	12.00	12.12
Wt. per foot.	51.5	55.5	61.0	66.0	70.5	76.5
Area, Sq. In.	15.21	16.35	17.92	19.32	20.79	22.50
b".	9.980	10.000	10.030	10.230	10.250	10.290
t.	.360	.380	.410	.450	.470	.510
h.	10.388	10.388	10.388	10.066	10.066	10.066
m.	.761	.806	.866	.907	.967	1.027
n.	.360	.405	.465	.500	.560	.620
f.	.45	.45	.45	.55	.55	.55
c.	9.5	9.5	9.5	9.0	9.0	9.0
g.	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$
u.	$9\frac{1}{16}$	$5\frac{1}{8}$	$11\frac{1}{16}$	$23\frac{1}{32}$	$25\frac{1}{32}$	$13\frac{1}{16}$
AXES	I.....	400.6	435.6	483.6	496.9	543.6
	S.....	67.27	72.60	79.80	83.65	90.60
	r.....	5.13	5.16	5.20	5.07	5.11
Y-Y	I.....	76.9	84.9	95.9	108.3	119.7
	S.....	15.4	17.0	19.1	21.2	23.4
	r.....	2.25	2.28	2.31	2.37	2.40
Coef. Str.	807300	871200	957600	1003800	1087200	1176600
Max. Mo. n. %	1210900	1306800	1436400	1505800	1630800	1764900
V.....	51500	54700	59700	64100	67700	74200
P, feet..	7.84	7.96	8.02	7.83	8.03	7.93
R.....	35100	37100	40000	43900	45800	49700
W.....	48600	51300	55350	60750	63450	68850
Q, feet..	8.31	8.49	8.65	8.26	8.57	8.54
w, lbs...	24	24	24	24	24	24
Rivet dia.	1"	1"	1"	1"	1"	1"

Live Load deflection must not exceed $\frac{1}{360}$ of the Span.

Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
6	103	103	109	109	119	119	128	128	135	135	148	148	
7	103	103	109	109	119	119	128	128	135	135	148	148	
8	101	101	109	109	119	119	126	126	135	135	147	147	
9	90	90	97	97	106	106	112	112	121	121	131	131	.126
10	81	81	87	87	96	96	100	100	109	109	118	118	.155
11	73	73	79	79	87	87	91	91	99	99	107	107	.188
12	67	67	73	73	80	80	84	84	91	91	98	98	.223
13	62	61	67	66	74	73	77	77	84	84	91	91	.263
14	58	56	62	60	68	66	72	71	78	76	84	82	.304
15	54	52	58	55	64	61	67	64	72	69	78	75	.341
16	50	47	54	51	60	56	63	59	68	64	74	70	.398
17	48	44	51	47	56	52	59	55	64	59	69	64	.449
18	45	41	48	43	53	48	56	51	60	55	65	59	.503
19	43	38	46	41	50	44	53	47	57	51	62	55	.560
20	40	35	44	38	48	41	50	44	54	47	59	52	.621
21	38	32	41	35	46	39	48	41	52	44	56	48	.684
22	37	30	40	33	44	36	46	38	49	41	54	45	.751
23	35	28	38	31	42	34	44	36	47	38	51	42	.822
24	34	27	36	28	40	31	42	33	45	36	49	39	.894
25	32	24	35	27	38	29	40	31	43	33	47	37	.970

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

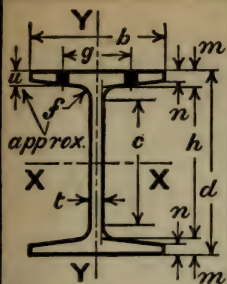
BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.

15"
G

Depth = d".	14.75	14.88	15.00	15.12					
Wt. per foot.	127.0	135.0	141.0	147.0					
Area. Sq. In..	37.47	39.58	41.44	43.30					
b.....	11.680	11.720	11.750	11.780					
t.....	.730	.770	.800	.830					
h.....	11.908	11.908	11.908	11.908					
m.....	1.421	1.486	1.546	1.606					
n.....	.965	1.030	1.090	1.150					
f.....	.90	.90	.90	.90					
c.....	10.250	10.250	10.250	10.250					
g.....	7½	7½	7½	7½					
u.....	1⅛	1⅛	1⅛	1⅛					
A X E S									
X-X	I.... 1415.6	1509.9	1596.8	1685.4					
	S.... 191.95	202.94	212.91	222.94					
	r.... 6.15	6.18	6.21	6.24					
Y-Y	I.... 289.1	309.7	328.5	347.5					
	S.... 49.5	52.9	55.9	59.0					
	r.... 2.78	2.80	2.82	2.83					
Coef. Str....	2303300	2435300	2554900	2675200					
Max. Mom. %	3455000	3653000	3832300	4012800					
V.....	129200	137400	144000	150600					
P. feet..	8.91	8.86	8.87	8.88					
R.....	79400	83700	87000	90300					
W.....	95440	95440	95440	95440					
Q. feet..	12.07	12.76	13.38	14.02					
w. lbs....	33	33	33	33					
Rivet dia....	1"	1"	1"	1"					
Span	Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
	feet	fixed	free	fixed	free	fixed	free	fixed	
6	258	258	275	275	288	288	301	301	.101 .124
7	258	258	275	275	288	288	301	301	
8	258	258	275	275	288	288	301	301	
9	256	256	271	271	284	284	297	297	
10	230	230	243	243	255	255	267	267	
11	209	209	221	221	232	232	243	243	.150
12	192	192	203	203	213	213	223	223	.179
13	177	177	187	187	197	197	206	206	.210
14	165	165	174	174	182	182	191	191	.243
15	154	153	162	161	170	169	178	177	.279
16	144	141	152	149	160	157	167	164	.318
17	136	131	143	138	150	145	157	152	.359
18	128	121	135	128	142	135	149	142	.402
19	121	113	128	120	134	125	141	132	.448
20	115	106	122	112	128	118	134	123	.497
21	110	99	116	105	122	110	127	115	.547
22	105	93	111	98	116	103	122	108	.601
23	100	87	106	92	111	97	116	101	.651
24	96	82	101	86	106	90	111	95	.715
25	92	77	97	81	102	86	107	90	.776
26	89	73	94	77	98	80	103	85	.839
27	85	68	90	72	95	76	99	80	.905
28	82	64	87	68	91	72	96	76	.973
29	79	61	84	65	88	68	92	71	1.040
30	77	58	81	61	85	64	89	67	1.120
32	72	52	76	55	80	58	84	61	1.270
34	68	47	72	50	75	52	79	55	1.440
36	68	45	71	47	74	49	1.610

allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. × Live Load Tabular Load

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

16" G

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

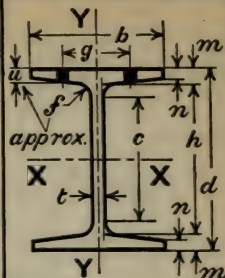
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d". Wt. per foot. Area, Sq. In.	b	11.470	11.500	11.530	11.565	Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. × Live Load Tabular Load				
	t	.390	.420	.450	.485					
	h	14.018	14.018	14.018	14.018					
	m	.931	.991	1.051	1.116					
	n	.469	.529	.589	.654					
	f	.60	.60	.60	.60					
	c	12.875	12.875	12.875	12.875					
	g	7 1/2	7 1/2	7 1/2	7 1/2					
	u	5/8	1 1/16	3/4	13/16					
	AXES	X-X	I	1033.6	1131.3		1230.8	1341.4		
Y-Y		S	130.18	141.41	152.70	165.10				
		r	6.86	6.89	6.92	6.95				
		I	148.1	164.6	181.3	199.9				
Coef. Str. Max. Mom. *# V..... P, feet..... R..... W..... Q, feet..... w, lbs..... Rivet dia.	S	25.8	28.6	31.5	34.6	Total Deflection in inches for Maximum Load; Laterally fixed beam.				
	r	2.60	2.63	2.66	2.68					
	1562100	1696900	1832400	1981100						
	2343200	2545400	2748700	2971700						
	74300	80600	87000	94600						
	10.51	10.53	10.53	10.47						
	41300	45700	50000	54600						
	70200	75600	81000	87300						
	11.13	11.22	11.31	11.35						
	33	33	33	33						
1"	1"	1"	1"							
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		
		fixed	free	fixed	free	fixed	free	fixed	free	
10	149	149	161	161	174	174	189	189		
11	142	142	154	154	167	167	180	180		
12	130	130	141	141	153	153	165	165		
13	120	120	131	131	141	141	152	152		
14	112	112	121	121	131	131	142	142		
15	104	103	113	112	122	121	132	131	.262	
16	98	96	106	104	115	112	124	121	.298	
17	92	88	100	96	108	104	117	113	.336	
18	87	82	94	89	102	96	110	104	.377	
19	82	76	89	83	96	89	104	97	.420	
20	78	71	85	78	92	84	99	91	.466	
21	74	66	81	73	87	78	94	85	.513	
22	71	62	77	68	83	73	90	79	.563	
23	68	59	74	64	80	69	86	74	.616	
24	65	55	71	60	76	64	83	70	.670	
25	63	52	68	56	73	61	79	66	.727	
26	60	49	65	53	71	58	76	62	.787	
27	58	46	63	50	68	54	73	58	.848	
28	56	43	61	48	65	51	71	55	.912	
29	54	41	59	45	63	48	68	52	.979	
30	52	39	57	43	61	46	66	49	1.047	
32	49	35	53	38	57	41	62	44	1.192	
34	46	31	50	34	54	37	58	40	1.346	
36	43	28	47	31	51	33	55	36	1.508	

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
 r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V .

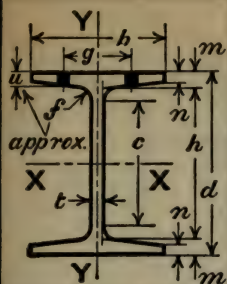
R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W .

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
 Allowable concentrated center loads are 50%
 and their deflections 80% of those shown.

18"
G

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.
		fixed	free	fixed	free	fixed	free	fixed	free	
	8	180	180	190	190	200	200	212	212	
	9	180	180	190	190	200	200	212	212	
	10	180	180	190	190	200	200	212	212	
	11	168	168	182	182	196	196	211	211	
	12	154	154	167	167	180	180	194	194	
	13	143	143	154	154	166	166	179	179	
	14	132	132	143	143	154	154	166	166	
	15	124	123	134	133	144	143	155	154	
16	116	114	125	123	135	132	145	142		
17	109	105	118	114	127	123	137	132		
18	103	98	111	105	120	114	129	123		
19	98	92	106	99	114	107	122	114		
20	93	85	100	92	108	99	116	107		
21	88	79	95	86	103	93	111	100		
22	84	74	91	81	98	87	106	94		
23	81	71	87	76	94	82	101	88		
24	77	66	84	72	90	77	97	83		
25	74	62	80	67	86	72	93	78		
26	71	58	77	63	83	68	89	73		
27	69	56	74	60	80	64	86	69		
28	66	52	72	57	77	61	83	66		
29	64	49	69	53	74	57	80	62		
30	62	47	67	51	72	54	77	58		
32	58	42	63	46	67	49	73	53		
34	55	38	59	41	63	44	68	47		
36	51	34	56	37	60	40	65	43		
38	49	31	53	34	57	36	61	39		
40	46	...	50	...	54	...	58	...		

AXES	Y-Y	I.....	1380.7	1503.6	1628.5	1767.7	Live Load deflection must not exceed 1/360 of the Span.
	X-X	S.....	154.44	167.07	179.75	193.72	
	X-X	r.....	7.65	7.70	7.75	7.79	
	Y-Y	I.....	157.8	174.9	192.2	211.3	
AXES	Y-Y	S.....	26.9	29.8	32.7	35.8	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$
	Y-Y	r.....	2.59	2.63	2.66	2.69	
	Coef. Str.		1853300	2004800	2157000	2324600	
	Max. Mom. %		2779900	3007200	3235400	3487000	
AXES	V.....		90100	95000	100000	106200	Total Deflection in inches for Maximum Load; Laterally fixed beam.
	P. feet...		10.28	10.55	10.79	10.94	
	R.....		46200	49500	52800	56900	
	W.....		94500	99000	103500	109100	
AXES	Q. feet...		9.81	10.13	10.42	10.65	Total Deflection in inches for Maximum Load; Laterally fixed beam.
	w. lbs...		41	41	41	41	
	Rivet dia....		1"	1"	1"	1"	

20" G

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

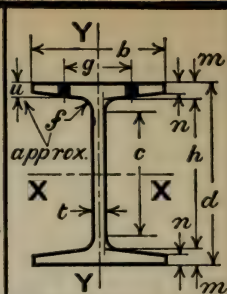
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

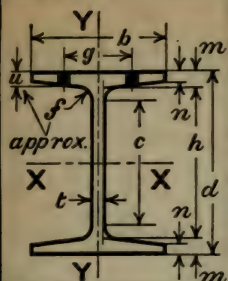
Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d".	19.75	19.88	20.00	20.12	19.75	19.88	20.00	20.12	Live Load deflection must not exceed 1/360 of the Span.	Total Def. x Live Load Tabular Load
Wt. per foot.	99.0	107.0	113.0	120.0	127.0	135.0	142.0	149.0		
Area, Sq. In.	29.21	31.36	33.20	35.24	37.33	39.58	41.71	43.84		
b".	11.950	11.980	12.000	12.030	12.690	12.720	12.750	12.780		
t.....	.510	.540	.560	.590	.600	.630	.660	.690		
h.....	17.626	17.626	17.626	17.626	17.170	17.170	17.170	17.170		
m.....	1.062	1.127	1.187	1.247	1.289	1.354	1.414	1.474		
n.....	.585	.650	.710	.770	.785	.851	.911	.971		
f.....	.65	.65	.65	.65	.75	.75	.75	.75		
c.....	16.375	16.375	16.375	16.375	15.750	15.750	15.750	15.750		
g.....	7 1/2	7 1/2	7 1/2	7 1/2	7 1/2	7 1/2	7 1/2	7 1/2		
u.....	25/32	13/16	7/8	15/16	1"	1 1/16	1 1/8	1 1/4		
A X E S	I....	2034.4	2206.5	2362.8	2528.0	2607.3	2788.9	2960.6	3134.9	Live Load deflection must not exceed 1/360 of the Span.
	S....	206.02	221.98	236.28	251.29	264.03	280.57	296.06	311.62	
	r....	8.35	8.39	8.44	8.47	8.36	8.39	8.43	8.46	
Y - Y	I....	202.1	222.4	240.8	260.2	313.0	337.7	361.0	384.6	Live Load deflection must not exceed 1/360 of the Span.
	S....	33.8	37.1	40.1	43.3	49.3	53.1	56.6	60.2	
	r....	2.63	2.66	2.69	2.72	2.90	2.92	2.94	2.96	
Coef. Str. ...	Max. Mom. %	2472200	2663800	2835400	3015500	3168400	3366900	3552700	3739400	Total Deflection in inches for Maximum Load; Laterally fixed beam.
	V.....	3708300	3995700	4253000	4523300	4752500	5050300	5329100	5609200	
	P. feet...	12.02	10.34	10.55	10.58	11.14	11.20	11.21	11.22	
Q.....	R.....	62400	67200	70700	75200	76500	80300	84200	88000	
	W.....	114800	119300	119300	119300	119300	119300	119300	119300	
	Q. feet...	10.77	11.16	11.88	12.64	13.28	14.11	14.89	15.67	
Rivet dia.	w. lbs.	41	41	41	41	41	41	41	41	
	1"	1"	1"	1"	1"	1"	1"	1"		
	1"	1"	1"	1"	1"	1"	1"	1"		
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Total Deflection in inches for Maximum Load; Laterally fixed beam.
	8	242	242	258	258	269	269	285	285	
	9	242	242	258	258	269	269	285	285	
10	242	242	258	258	269	269	285	285	285	.134
	11	225	225	242	242	258	258	274	274	
	12	206	206	222	222	236	236	251	251	
13	190	190	205	205	218	218	232	232	244	.158
	14	177	177	190	190	203	203	215	215	
	15	165	165	178	178	189	189	201	201	
16	155	153	167	164	177	174	188	185	198	.183
	17	145	141	157	152	167	162	177	172	
	18	137	131	148	142	158	151	168	161	
19	130	122	140	132	149	140	159	150	167	.210
	20	124	115	133	123	142	131	151	140	
	21	118	107	127	116	135	123	144	131	
22	112	100	121	108	129	115	137	123	144	.239
	23	108	95	116	102	123	108	131	115	
	24	103	89	111	96	118	102	126	109	
25	99	84	107	91	113	96	121	103	127	.270
	26	95	79	102	85	109	91	116	97	
	27	92	75	99	81	105	86	112	91	
28	88	70	95	76	101	81	108	86	113	.302
	29	85	66	92	72	98	77	104	82	
	30	82	63	89	68	95	73	100	77	
32	77	56	83	61	89	65	94	69	99	.336
	34	73	51	78	55	83	58	63	93	
	36	69	46	74	50	79	53	57	88	
38	65	42	70	45	75	48	51	48	79	.373
	40	62	..	67	..	71	44	44	75	
	42	58	..	63	..	67	40	40	71	
44	54	32	60	37	63	37	40	37	60	.411
	46	50	28	33	59	33	33	56	56	
	48	46	24	29	29	55	29	29	52	
46	42	32	48	27	49	25	32	25	46	.451
	48	38	24	21	45	21	21	42	42	
	50	34	20	17	17	41	17	17	38	
48	38	26	36	19	39	18	36	18	36	.493
	50	34	22	15	35	15	15	32	32	
	52	30	18	11	31	11	11	28	28	
50	34	22	32	15	35	15	35	15	32	.537
	52	30	18	11	31	11	11	28	28	
	54	26	14	7	27	7	7	24	24	
52	30	18	28	11	31	11	31	11	28	.582
	54	26	14	7	27	7	7	24	24	
	56	22	10	3	23	3	3	20	20	
54	26	14	24	7	27	7	27	7	24	.630
	56	12	8	5	19	5	5	16	16	
	58	10	6	3	15	3	3	12	12	
56	22	10	20	3	23	3	23	3	20	.679
	58	18	12	7	21	7	21	7	18	
	60	14	8	4	17	4	4	14	14	
58	18	12	18	5	19	5	19	5	18	.736
	60	14	8	4	17	4	17	4	14	
	62	10	6	3	13	3	3	10	10	
60	14	8	14	3	15	3	15	3	14	.783
	62	10	6	3	13	3	13	3	10	
	64	8	4	2	11	2	2	8	8	
62	10	6	10	2	11	2	11	2	10	.838
	64	8	4	2	11	2	11	2	8	
	66	6	3	1	9	1	1	6	6	
64	8	4	8	1	9	1	9	1	8	.954
	66	6	3	1	7	1	7	1	6	
	68	4	2	1	5	1	1	4	4	
66	6	3	6	1	7	1	7	1	6	1.08
	68	4	2	1	5	1	5	1	4	
	70	3	1	1	3	1	1	3	3	
68	4	2	4	1	5	1	5	1	4	1.21
	70	3	1	1	3	1	3	1	3	
	72	2	1	1	2	1	1	2	2	
70	3	1	3	1	4	1	4	1	3	1.34
	72	2	1	1	3	1	3	1	2	
	74	1	1	1	1	1	1	1	1	
72	2	1	2	1	3	1	3	1	2	1.49
	74	1	1	1	2	1	2	1	1	
	76	1	1	1	1	1	1	1	1	



BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

22"
G

Depth = d".	21.88	22.00	22.12	22.25	22.38
Wt. per foot.	101.0	108.0	116.0	124.0	132.0
Area, Sq. In.	29.68	31.89	34.12	36.59	38.96
b".	12.970	13.000	13.030	13.065	13.095
t.	.450	.480	.510	.545	.575
h.	19.798	19.798	19.798	19.798	19.798
m.	1.041	1.101	1.161	1.226	1.291
n.	.519	.579	.639	.704	.769
f.	.65	.65	.65	.65	.65
c.	18.625	18.625	18.625	18.625	18.625
g.	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$
u.	$\frac{3}{4}$	$\frac{13}{16}$	$\frac{7}{8}$	$\frac{15}{16}$	1"

A X E S	I....	2590.4	2804.3	3021.2	3261.7	3501.2
	X-X	236.78	254.94	273.16	293.19	312.89
	r....	9.34	9.38	9.41	9.44	9.48
	I....	238.1	261.9	286.0	312.6	339.3
Y-Y	S....	36.7	40.3	43.9	47.9	51.8
	r....	2.83	2.87	2.90	2.92	2.95

Live Load deflection must not exceed $1/360$ of the Span.

Live Load Def. = Total Def. \times Live Load

Coef. Str.	2841400	3059200	3278000	3518200	3754600
Max. Mom. %	4262100	4588800	4917000	5277300	5632000
V.	118200	126700	135400	145500	154400
P. feet....	12.02	12.07	12.10	12.09	12.16
W.	52300	57600	62900	69100	75200
R.	121600	129600	137800	143160	143160
Q. feet....	11.68	11.80	11.89	12.29	13.11
w. lbs....	49	49	49	49	49
Rivet dia.	1"	1"	1"	1"	1"

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Laterally	
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
12	236	236	253	253	271	271	291	291	309	309
13	219	219	235	235	252	252	271	271	289	289
14	203	203	219	219	234	234	251	251	268	268
15	189	189	204	204	219	219	235	235	250	250
16	178	178	191	191	205	205	220	220	235	235
17	167	167	180	178	193	191	207	205	221	219
18	158	154	170	166	182	178	195	191	209	204
19	150	144	161	155	173	167	185	179	198	191
20	142	135	153	145	164	156	176	167	188	179
21	135	126	146	137	156	146	168	157	179	168
22	129	119	139	128	149	137	160	148	171	158
23	124	112	133	121	143	130	153	139	163	148
24	118	105	128	114	137	122	147	131	157	140
25	114	100	122	107	131	115	141	124	150	132
26	109	94	118	102	126	109	135	117	144	125
27	105	89	113	96	121	103	130	111	139	118
28	102	85	109	91	117	98	126	105	134	112
29	98	80	106	87	113	93	121	99	130	107
30	95	76	102	82	109	88	117	94	125	101
32	89	69	96	74	102	79	110	85	117	91
34	84	63	90	67	96	72	104	78	110	82
36	79	56	85	61	91	65	98	70	104	75
38	75	52	81	56	86	59	93	64	99	68
40	71	47	77	51	82	54	88	58	94	62
42	68	43	73	46	78	50	84	53	89	57
44	65	...	70	...	75	...	80	...	86	...
46	62	...	67	...	71	...	76	...	82	...

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.

For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

24" C

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

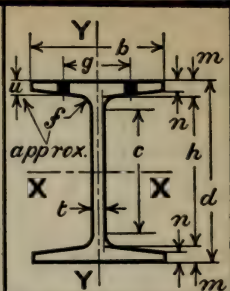
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d".	23.78	23.88	24.00	24.12	23.88	24.00	24.12	Live Load deflection must not exceed 1/360 of the Span.
Wt. per foot.	107.0	113.0	120.0	128.0	132.0	140.0	148.0	
Area, Sq. In..	31.60	33.18	35.36	37.79	38.82	41.13	43.68	
b".....	12.195	12.210	12.240	12.280	13.210	13.240	13.280	
t".....	.485	.500	.530	.570	.570	.600	.640	
h".....	21.604	21.604	21.604	21.604	21.386	21.386	21.386	
m".....	1.088	1.138	1.198	1.258	1.247	1.307	1.367	
n".....	.600	.650	.710	.770	.720	.780	.840	
f".....	.65	.65	.65	.65	.70	.70	.70	
c".....	20.373	20.375	20.375	20.375	20.125	20.125	20.125	
g".....	7½	7½	7½	7½	7½	7½	7½	
s".....	25/32	13/16	7/8	15/16	15/16	1"	1 1/16	
AXES	I.....	3173.1	3363.3	3607.8	3867.1	3939.6	4201.3	4478.0
	S.....	266.87	281.68	300.65	320.66	329.95	350.11	371.31
	r.....	10.02	10.07	10.10	10.12	10.07	10.11	10.13
	I.....	220.0	236.1	256.3	277.5	329.9	355.6	382.5
Y-Y	I.....	36.1	38.7	41.9	45.2	50.0	53.7	57.6
	r.....	2.64	2.67	2.69	2.71	2.92	2.94	2.96
Coef. Str....	3202500	3380200	3607800	3847900	3959300	4201300	4455700	Total Deflection in inches for Maximum Load; Laterally fixed end.
Max.Mom.*#	4803700	5070300	5411700	5771800	5939000	6301900	6683600	
V.....	138400	143300	152600	165000	163300	172800	185200	
P, feet..	11.57	11.79	11.82	11.66	12.12	12.16	12.03	
R.....	58800	61700	67500	75300	75200	81000	88800	
W.....	130980	135000	143160	143160	143160	143160	143160	
Q, feet..	12.22	12.52	12.60	13.44	13.83	14.67	15.56	
w, lbs....	49	49	49	49	49	49	49	
Rivet dia....	1"	1"	1"	1"	1"	1"	1"	

Live Load deflection must not exceed 1/360 of the Span.

Live Load Def. = Total Def. \times Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
	10	11	12	13	14	15	16	17	18	19	20	21	22	23	
10	277	277	287	287	305	305	330	330	327	327	346	346	370	370	
11	277	277	287	287	305	305	330	330	327	327	346	346	370	370	.112
12	267	267	282	282	301	301	321	321	327	327	346	346	370	370	.131
13	246	246	260	260	278	278	296	296	305	305	323	323	343	343	.152
14	229	229	241	241	258	258	275	275	283	283	300	300	318	318	.175
15	214	214	225	225	241	241	257	257	264	264	280	280	297	297	
16	200	198	211	209	225	223	240	238	247	247	263	263	278	278	.199
17	188	183	199	194	212	207	226	221	233	231	247	245	262	260	.225
18	178	170	188	181	200	192	214	206	220	215	233	229	248	243	.251
19	169	160	178	168	190	180	203	192	208	201	221	214	235	227	.280
20	160	149	169	157	180	168	192	179	198	189	210	200	223	213	.310
21	153	140	161	148	172	158	183	168	189	178	200	188	212	200	.342
22	146	132	154	139	164	148	175	158	180	167	191	177	203	188	.375
23	139	123	147	130	157	139	167	148	172	157	183	167	194	177	.411
24	133	116	141	123	150	131	160	139	165	148	175	157	186	167	.447
25	128	109	135	115	144	123	154	132	158	140	168	148	178	158	.485
26	123	103	130	109	139	117	148	124	152	132	162	141	171	149	.525
27	119	98	125	103	134	110	143	118	147	126	156	133	165	141	.566
28	114	92	121	98	129	104	137	111	141	118	150	126	159	134	.608
29	110	87	117	92	124	98	133	106	137	113	145	120	154	127	.653
30	107	83	113	87	120	93	128	100	132	107	140	114	149	121	.698
32	100	74	106	79	113	84	120	89	124	97	131	102	139	109	.795
34	94	67	99	71	106	76	113	81	116	87	124	93	131	99	.897
36	89	61	94	64	100	68	107	73	110	80	117	85	124	90	1.01
38	84	55	89	58	95	62	101	66	104	72	111	77	117	82	1.12
40	80	50	85	53	90	57	96	60	99	66	105	70	111	75	1.24
42	76	...	80	...	86	...	92	...	94	60	100	64	106	68	1.37
44	73	...	77	...	82	...	87	...	90	56	95	59	101	63	1.50
46	70	...	73	...	78	...	84	...	86	...	91	...	97	...	1.64
48	67	...	70	...	75	...	80	...	82	...	88	...	93	...	1.79

LOADS BY A. I. S. C. SPECIFICATION

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

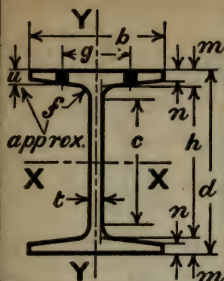
Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

26"

G



Depth = d".	25.81	25.88	26.00	26.12	Live Load deflection must not exceed 1/360 of the Span.	Total Deflection in inches for Maximum Load; Laterally fixed beam.		
	138.0	144.0	151.0	160.0				
Wt. per foot.	40.65	42.38	44.55	47.25				
Area, Sq. In..	13.700	13.730	13.750	13.790				
b.....	.580	.610	.630	.670				
t.....	23.336	23.336	23.336	23.336				
h.....	1.237	1.272	1.332	1.392				
n.....	.690	.725	.785	.845				
f.....	.75	.75	.75	.75				
c.....	22.0	22.0	22.0	22.0				
g.....	10"	10"	10"	10"				
u.....	27/32	7/8	31/32	1 1/32				
A X E S	I....	4779.9	4983.4	5289.8				
	S....	370.39	385.12	406.91				
	r....	10.84	10.84	10.90				
Y - Y	I....	357.4	375.0	402.8				
	S....	52.2	54.6	58.6				
	r....	2.97	2.97	3.01				
Coef. Str.	4444700	4621400	4882900	5172500				
Max. Mom. %	6667000	6932100	7324300	7758700				
V.....	179600	189400	196600	210000				
P. feet..	12.37	12.20	12.42	12.32				
R.....	78500	84300	88300	96400				
W.....	167000	167000	167000	167000				
Q. feet..	13.31	13.84	14.62	15.49				
w. lbs....	58	58	58	58				
Rivet dia.	1"	1"	1"	1"				
Span	Laterally		Laterally		Laterally			
	feet	fixed free	fixed free	fixed free	fixed free	fixed free		
11	359	359	379	379	393	393	420	420
12	359	359	379	379	393	393	420	420
13	342	342	355	355	376	376	398	398
14	317	317	330	330	349	349	369	369
15	296	296	308	308	326	326	345	345
16	278	278	289	289	305	305	323	323
17	261	261	272	272	287	287	304	304
18	247	244	257	254	271	268	287	284
19	234	229	243	237	257	251	272	266
20	222	214	231	223	244	235	259	250
21	212	201	220	209	233	222	246	234
22	202	189	210	197	222	208	235	221
23	193	178	201	186	212	196	225	208
24	185	168	193	176	203	185	215	196
25	178	160	185	166	195	175	207	186
26	171	151	178	157	188	166	199	176
27	165	143	171	149	181	157	192	167
28	159	136	165	141	174	149	185	158
29	153	129	159	134	168	141	178	150
30	148	122	154	127	163	135	172	143
32	139	111	144	115	153	122	162	130
34	131	101	136	105	144	111	152	117
36	124	92	128	95	136	101	144	107
38	117	84	122	87	128	92	136	98
40	111	76	116	80	122	84	129	89
42	106	...	110	73	116	77	123	82
44	101	...	105	67	111	71	118	76
46	97	...	100	...	106	...	112	...
48	93	...	96	...	102	...	108	...
50	89	...	92	...	98	...	103	...

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

28"

G

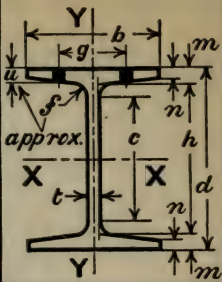
BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".	27.75	27.88	28.00	28.12	28.31	Live Load deflection must not exceed 1/360 of the Span. Total Def. x Live Load Tabular Load					
Wt. per foot.	145.0	156.0	165.0	175.0	186.0						
Area, Sq. In.	42.69	45.93	48.75	51.45	54.73						
b".	14.160	14.210	14.250	14.285	14.305						
t".	.585	.635	.675	.710	.730						
h".	25.268	25.268	25.268	25.268	25.268						
m".	1.241	1.306	1.366	1.426	1.521						
n".	.675	.740	.800	.860	.955						
f".	.80	.80	.80	.80	.80						
c".	23.750	23.750	23.750	23.750	23.750						
g".	10"	10"	10"	10"	10"						
u".	27/32	29/32	31/32	1 1/32	1 1/8						
A X E S	I.....	5772.3	6218.6	6624.6	7026.0	7604.0					
	S.....	416.02	446.10	473.19	499.72	537.20					
	r.....	11.63	11.64	11.66	11.69	11.79					
Y - Y	I.....	389.8	425.4	458.3	491.1	539.7					
	S.....	55.1	59.9	64.3	68.8	75.5					
	r.....	3.02	3.04	3.07	3.09	3.14					
Coef. Str.	4992300	5353200	5678200	5996600	6446300	Total Deflection in inches for Maximum Load; Laterally fixed beam.					
Max. Mom. %	7488400	8029700	8517300	8994900	9669500						
V.....	194800	212400	226800	239600	248000						
P. feet..	12.81	12.60	12.52	12.51	13.00						
R.....	80000	90600	99100	106700	111100						
W.....	167000	167000	167000	167000	167000						
Q. feet..	14.95	16.03	17.00	17.95	19.30						
w. lbs..	58	58	58	58	58						
Rivet dia.	1"	1"	1"	1"	1"						
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally			
	feet	fixed	free	fixed	free	fixed	free	fixed	free		
12	390	390	425	425	454	454	479	479	496	496	.113 .123 .150
13	384	384	412	412	437	437	461	461	496	496	
14	357	357	382	382	406	406	428	428	460	460	
15	333	333	357	357	379	379	400	400	430	430	
16	312	312	335	335	355	355	375	375	403	403	
17	294	294	315	315	334	334	353	353	379	379	.193
18	277	276	297	296	315	314	333	332	358	357	.215
19	263	259	282	278	299	295	316	311	339	334	.240
20	250	243	268	261	284	277	300	292	322	314	.266
21	238	228	255	245	270	259	286	275	307	295	.293
22	227	215	243	230	258	245	273	259	293	278	.322
23	217	203	233	218	247	231	261	244	280	262	.352
24	208	192	223	205	237	219	250	231	269	249	.383
25	200	181	214	194	227	206	240	218	258	235	.416
26	192	172	206	184	218	195	231	207	248	223	.450
27	185	163	198	175	210	186	222	196	239	212	.485
28	178	154	191	166	203	176	214	186	230	200	.521
29	172	147	185	158	196	168	207	177	222	190	.559
30	166	139	178	150	189	159	200	169	215	181	.599
32	156	127	167	136	177	144	187	153	201	164	.681
34	147	115	157	124	167	132	176	139	190	150	.769
36	139	105	149	113	158	120	167	127	179	137	.862
38	131	96	141	103	149	109	158	116	170	125	.960
40	125	88	134	95	142	101	150	107	161	114	1.06
42	119	81	127	87	135	92	143	98	154	106	1.17
44	113	74	122	80	129	85	136	90	147	97	1.29
46	109	69	116	74	123	78	130	83	140	89	1.40
48	104	...	112	...	118	...	125	...	134	...	1.53
50	100	...	107	...	114	...	120	...	129	...	1.66
52	96	...	103	...	109	...	115	...	124	...	1.80

BETHLEHEM GIRDER BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

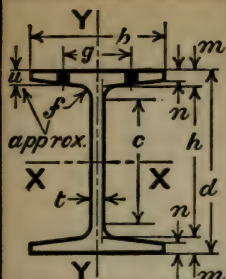
Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

30"

C



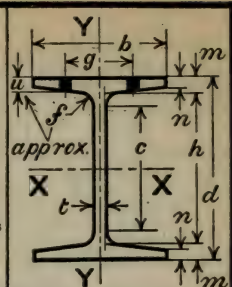
Depth = d".	29.88	30.00	30.12	30.25	30.50	30.75
Wt. per foot.	173.0	180.0	190.0	200.0	220.0	240.0
Area, Sq. In..	50.80	53.20	55.90	58.92	64.82	70.60
b.....	14.980	15.000	15.030	15.065	15.135	15.200
t.....	.660	.680	.710	.745	.815	.880
h.....	27.148	27.148	27.148	27.148	27.148	27.148
m.....	1.366	1.426	1.486	1.551	1.676	1.801
n.....	.769	.829	.889	.954	1.079	1.204
f.....	.85	.85	.85	.85	.85	.85
c.....	25.50	25.50	25.50	25.50	25.50	25.50
g.....	10"	10"	10"	10"	10"	10"
u.....	3 1/32	1 1/32	1 3/32	1 5/32	1 9/32	1 13/32
AXES	X.....	7895.2	8343.1	8818.0	9343.8	10378.0
	I.....	528.46	556.21	585.52	617.77	680.52
	r.....	12.47	12.52	12.56	12.59	12.65
	Y.....	519.1	555.1	592.7	634.2	716.1
	S.....	69.3	74.0	78.9	84.2	94.6
	r.....	3.20	3.23	3.26	3.28	3.32
Coef. Str....	6341500	6674500	7026300	7413300	8166300	8915500
Max. Mom. *"	9512300	10011700	10539400	11119900	12249400	13373300
V.....	236600	244800	256600	270400	298300	324700
P, feet....	13.40	13.63	13.69	13.71	13.69	13.73
R.....	97200	101600	108400	116400	132300	147200
W.....	190880	190880	190880	190880	190880	190880
Q, feet....	16.61	17.48	18.40	19.42	21.39	23.35
w, lbs....	66	66	66	66	66	66
Rivet dia....	1"	1"	1"	1"	1"	1"

Deflection must not exceed $\frac{1}{360}$ of the Span.
Live Load Def. = Total Def. \times Live Load
Tabular Load

Total Deflection in inches for Maximum Load: Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load: Laterally fixed beam.
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
13	473	473	490	490	513	513	541	597	597	649	649		
14	453	453	477	477	502	502	530	530	583	583	636	636	.122
15	423	423	445	445	468	468	494	494	544	544	594	594	.140
16	396	396	417	417	439	439	463	463	510	510	557	557	.159
17	373	373	393	393	413	413	436	436	480	480	524	524	.180
18	352	352	371	371	390	390	412	412	454	454	495	495	.201
19	334	333	351	350	370	369	390	389	430	429	469	468	.224
20	317	312	334	329	351	346	371	366	408	402	446	441	.248
21	302	294	318	310	335	326	353	344	389	379	425	415	.274
22	288	277	303	292	319	307	337	325	371	358	405	391	.300
23	276	262	290	276	305	290	322	306	355	338	388	370	.329
24	264	248	278	261	293	275	309	290	340	320	372	351	.358
25	254	235	267	247	281	260	297	275	327	304	357	332	.388
26	244	223	257	235	270	247	285	261	314	288	343	315	.420
27	235	212	247	223	260	234	275	248	302	273	330	299	.452
28	226	201	238	211	251	223	265	236	292	260	318	284	.487
29	219	192	230	201	242	212	256	225	282	248	307	270	.522
30	211	182	222	192	234	202	247	213	272	236	297	258	.559
32	198	166	209	175	220	184	232	195	255	214	279	235	.636
34	187	152	196	159	207	168	218	177	240	195	262	214	.718
36	176	138	185	145	195	153	206	162	227	179	248	196	.804
38	167	127	176	134	185	141	195	148	215	164	235	186	.896
40	159	117	167	123	176	130	185	136	204	151	223	165	.993
42	151	107	159	113	167	119	177	126	194	139	212	152	1.10
44	144	99	152	104	160	110	168	116	186	128	203	141	1.20
46	138	91	145	96	153	102	161	107	178	119	194	130	1.31
48	132	84	139	89	146	94	154	99	170	110	186	120	1.43
50	127	...	133	78	141	87	148	92	163	102	178	111	1.55
52	122	...	128	...	135	...	143	...	157	...	171	...	1.68
54	117	...	124	...	130	...	137	...	151	...	165	...	1.81

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.



AXES			Depth = d".	32.88	33.00	33.12	33.25	33.44	33.63	Live Load deflection must not exceed 1/360 of the Span.	Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$
			Wt. per foot..	200.0	210.0	220.0	230.0	245.0	260.0		
			Area, Sq. In.	58.87	61.91	64.80	67.85	72.19	76.54		
b	t	15.715	15.750	15.780	15.810	15.850	15.890	15.890		
t	t700	.735	.765	.795	.835	.875			
h	t	29.904	29.904	29.904	29.904	29.904	29.904	29.904		
m	t	1.488	1.548	1.608	1.673	1.768	1.863			
n	t862	.922	.982	1.047	1.142	1.237			
f	t90	.90	.90	.90	.90	.90			
c	t	28.250	28.250	28.250	28.250	28.250	28.250	28.250		
g	t	10 ³ / ₃₂	10 ³ / ₃₂	10 ³ / ₃₂	10 ³ / ₃₂	10 ³ / ₃₂	10 ³ / ₃₂	10 ³ / ₃₂		
u	t	13 ³ / ₃₂	15 ³ / ₃₂	17 ³ / ₃₂	19 ³ / ₃₂	13 ³ / ₁₆	115 ³ / ₃₂			
X	X	I.....	11055	11671	12278	12935	13895	14868			
		S.....	672.45	707.33	741.43	778.05	831.04	884.21			
		r.....	13.70	13.73	13.77	13.81	13.87	13.94			
Y	Y	I.....	664.6	708.5	752.2	799.6	869.2	939.8			
		S.....	84.6	90.0	95.3	101.2	109.7	118.3			
		r.....	3.36	3.38	3.41	3.43	3.47	3.50			
Coef. Str.....			8069300	8488000	8897100	9336500	9972500	10610500			
Max.Mom. "W			12104000	12732000	13345700	14004800	14958700	15915800			
V.....			276200	291100	304000	317200	335100	353100			
P. feet.....			14.61	14.58	14.63	14.72	14.87	15.02			
R.....			108000	116300	123600	130900	140700	150500			
W.....			190880	190880	190880	190880	190880	190880			
Q. feet.....			21.14	22.23	23.31	24.46	26.12	27.79			
w. lbs.....			66	66	66	66	66	66			
Rivet dia.			1"	1"	1"	1"	1"	1"			
Total Deflection in inches for Maximum load; Laterally fixed beam.											

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Tensile Load
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
	14	552	552	582	582	608	608	634	634	670	670	706	706	
16	504	504	531	531	556	556	584	584	623	623	663	663	144	
18	448	448	472	472	494	494	519	519	554	554	589	589	183	
20	403	401	424	422	445	443	467	465	499	498	531	530	226	
21	384	378	404	398	424	418	445	439	475	469	505	497	249	
22	367	357	386	376	404	394	424	413	453	442	482	468	273	
23	351	338	369	355	387	373	406	391	434	419	451	445	298	
24	336	320	354	337	371	353	389	371	416	397	442	422	325	
25	323	304	340	320	356	335	373	351	399	376	424	398	353	
26	310	288	326	303	342	318	359	334	384	357	408	380	381	
27	299	274	314	288	330	303	346	318	369	339	393	361	411	
28	288	260	303	274	318	288	333	302	356	323	379	344	442	
29	278	248	293	262	307	275	322	288	344	307	366	328	475	
30	269	237	283	249	297	262	311	274	332	293	354	313	508	
31	260	226	274	238	287	250	301	262	322	280	342	298	542	
32	252	216	265	227	278	238	292	250	312	268	332	285	578	
33	245	207	257	217	270	228	283	239	302	255	322	273	614	
34	237	196	250	208	262	218	275	229	293	243	312	261	652	
35	231	189	243	199	254	208	267	219	285	234	303	250	691	
36	224	181	236	191	247	200	259	209	277	224	295	239	731	
38	212	166	223	175	234	184	246	193	262	206	279	220	815	
40	202	153	212	161	222	169	233	177	249	190	265	202	903	
42	192	141	202	149	212	156	222	163	237	175	253	186	995	
44	183	130	193	137	202	144	212	151	227	162	241	173	1.09	
46	175	120	185	127	193	133	203	140	217	150	231	160	1.19	
48	168	112	177	118	185	123	195	130	208	139	221	148	1.30	
50	161	103	170	109	178	115	187	121	199	128	212	137	1.41	
52	155	96	163	101	171	107	180	112	192	120	204	128	1.53	
54	149	..	157	..	165	..	173	..	185	..	197	..	1.65	
56	144	..	152	..	159	..	167	..	178	..	189	..	1.77	

For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Live Load deflection must not exceed $1/360$ of the Span.

$$\text{Live Load Def.} = \frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$$

**Total Deflection in
inches for Maximum
Load; Laterally fixed
beam.**

BETHLEHEM GIRDER BEAMS.

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

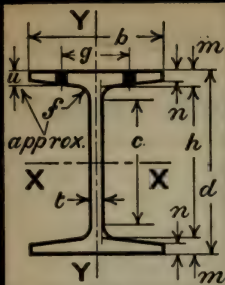
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

36"
G



Depth = d".	35.88	36.00	36.12	36.24	36.50	36.72
Wt. per foot.	230.0	240.0	250.0	260.0	280.0	300.0
Area, Sq. In. . .	67.67	70.55	73.61	76.50	82.45	88.12
t.	16.475	16.500	16.530	16.555	16.600	16.655
b.765	.790	.820	.845	.890	.945
h.	32.706	32.706	32.706	32.706	32.706	32.706
m.	1.587	1.647	1.707	1.767	1.897	2.007
n.933	.993	1.053	1.113	1.243	1.353
f.95	.95	.95	.95	.95	.95
c.	31.000	31.000	31.000	31.000	31.000	31.000
g.	10"	10"	10"	10"	10"	10"
r.	13 ¹ / ₁₆	11 ¹ / ₄	15 ¹ / ₁₆	13 ¹ / ₈	11 ¹ / ₂	15 ¹ / ₈
AXES						
I.	14960	15696	16457	17205	18811	20262
S.	833.89	872.00	911.24	949.50	1030.74	1103.59
r.	14.87	14.92	14.95	15.00	15.10	15.16
I.	824.5	873.5	923.8	973.7	1081.4	1177.7
S.	100.1	105.9	111.8	117.6	130.3	141.4
r.	3.49	3.52	3.54	3.57	3.62	3.66
Coef. Str. . . .	10006700	10464000	10934900	11394000	12368900	13243100
Max. Mom. *"	15010000	15696000	16402300	17091100	18553300	19864700
V.	329400	341300	355400	367500	389800	416400
P. feet. . . .	15.19	15.33	15.38	15.50	15.87	15.90
R.	125600	132000	139700	146000	158000	172300
Q.	190880	190880	190880	190880	190880	190880
W. lbs. . . .	26.21	27.41	28.64	29.85	32.40	34.69
w. lbs. . . .	66	66	66	66	66	66
Rivet dia. . .	1"	1"	1"	1"	1"	1"

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. x Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
16	625	625	654	654	683	683	712	712	773	773	828	828	.132
18	556	556	581	581	607	607	633	633	687	687	736	736	.167
20	500	500	523	523	547	547	570	570	618	618	662	662	.207
21	477	474	498	496	521	519	542	540	589	587	631	629	.228
22	455	448	476	469	497	490	518	511	562	554	602	594	.250
23	435	424	455	444	475	463	495	483	538	525	576	562	.273
24	417	402	436	420	455	439	475	458	515	498	552	534	.298
25	400	381	418	399	437	417	456	435	495	473	530	507	.323
26	385	363	402	379	420	396	438	413	476	449	509	481	.350
27	371	345	387	360	405	377	422	394	458	428	490	457	.377
28	358	329	374	344	390	359	407	375	442	408	473	436	.406
29	345	314	361	328	377	343	393	358	427	389	457	417	.435
30	334	299	349	313	364	327	380	342	412	371	441	397	.466
31	323	286	337	299	353	313	367	326	399	354	427	380	.497
32	313	274	327	286	342	299	356	312	387	339	414	363	.530
33	303	261	317	273	331	286	345	298	375	323	401	347	.563
34	294	250	308	262	322	274	335	285	364	310	389	332	.598
35	286	240	299	251	312	262	325	273	353	297	378	319	.634
36	278	230	291	241	304	252	316	262	344	286	368	306	.670
38	263	211	275	221	288	232	300	242	326	263	348	281	.747
40	250	195	262	205	273	213	285	223	309	242	331	260	.828
42	238	180	249	189	260	197	271	206	295	224	315	240	.912
44	228	168	238	175	248	182	259	191	281	206	301	223	1.001
46	218	155	227	162	238	170	248	177	269	192	288	208	1.094
48	209	144	218	150	228	158	237	164	258	179	276	192	1.191
50	200	134	209	140	219	147	228	153	247	166	265	179	1.293
52	193	125	201	130	210	136	219	142	238	155	255	167	1.399
54	185	116	194	122	202	127	211	133	229	144	245	155	1.508
56	179	107	187	113	195	119	203	125	221	137	236	144	1.622
58	173	100	180	106	189	113	196	119	213	128	228	137	1.740

ALLOWABLE END REACTIONS FOR BETHLEHEM GIRDER BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per foot	Web t	Unit Stress in Buckling	Reaction R for $3\frac{1}{2}$ " Bearing	Min. Span for $3\frac{1}{2}$ " Bearing	Reaction R for $5\frac{1}{2}$ " Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V	Length of Bearing to develop V
8	29.5	.285"	15000	23400	6.55'	32000	4280	26900	4.32"
	33.0	.290	15000	23900	7.29	32600	4350	27800	4.39
	36.5	.310	15000	25700	7.62	35000	4650	30200	4.46
9	36.0	.290	15000	25000	8.62	31100	4350	31100	4.90
	38.5	.310	15000	26700	8.58	33500	4650	33500	4.96
	43.5	.350	15000	30200	8.50	38300	5260	38300	5.05
10	41.5	.310	15000	27900	9.81	36900	4650	36900	5.44
	44.5	.320	15000	28800	10.27	38400	4800	38400	5.50
	50.0	.360	15000	32400	10.15	43200	5400	43700	5.60
12	51.5	.360	15000	35100	11.50	45900	5400	51500	6.54
	55.5	.380	15000	37100	11.74	48500	5700	54700	6.60
	61.0	.410	15000	40000	11.97	52300	6150	59700	6.70
	66.0	.450	15000	43900	11.44	57400	6750	64100	6.49
	70.5	.470	15000	45800	11.87	59900	7050	67700	6.60
	76.5	.510	15000	49700	11.84	65000	7650	74200	6.70
15	64.5	.390	14510	41000	15.24	52400	5660	69400	8.51
	69.0	.420	14850	45200	14.55	57700	6240	75000	8.27
	74.0	.440	15000	47900	14.91	61100	6600	79200	8.25
	80.5	.480	15000	52200	14.86	66600	7200	87100	8.35
	94.0	.540	15000	58700	15.06	74900	8100	95900	8.09
	99.0	.570	15000	62000	14.93	79100	8550	101700	8.15
	105.0	.600	15000	65300	15.09	83300	9000	108000	8.25
	111.0	.640	15000	69600	15.04	88800	9600	116200	8.35
	127.0	.730	15000	79400	14.51	101300	10950	129200	8.05
	135.0	.770	15000	83700	14.54	106800	11550	137400	8.15
	141.0	.800	15000	87000	14.68	111000	12000	144000	8.25
	147.0	.830	15000	90300	14.81	115200	12450	150600	8.34
16	74.5	.390	14100	41300	18.91	52300	5500	74300	9.49
	81.0	.420	14490	45700	18.57	57800	6090	80600	9.23
	87.0	.450	14830	50000	18.32	63400	6670	87000	9.04
	94.0	.485	15000	54600	18.14	69100	7280	94600	8.99
18	80.0	.420	13820	46200	20.06	57800	5800	90100	11.06
	86.0	.440	14070	49500	20.25	61900	6190	95000	10.85
	92.0	.460	14300	52800	20.43	66000	6580	100000	10.67
	99.0	.485	14560	56900	20.43	71000	7060	106200	10.48

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

ALLOWABLE END REACTIONS FOR BETHLEHEM GIRDER BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per foot	Web t	Unit Stress in Buckling	Reaction R for 3 1/2" Bearing	Min. Span for 3 1/2" Bearing	Reaction R for 5 1/2" Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V	Length of Bearing to develop V
20	99.0	.510	14400	62400	19.81'	77100	7340	120900	11.47"
	107.0	.540	14650	67200	19.82	83000	7910	128800	11.28
	113.0	.560	14850	70700	20.05	87300	8320	134400	11.16
	120.0	.590	15000	75200	20.05	92900	8850	142500	11.10
	127.0	.600	15000	76500	20.71	94500	9000	142200	10.80
	135.0	.630	15000	80300	20.97	99200	9450	150300	10.90
	142.0	.660	15000	84200	21.10	104000	9900	158400	11.00
	149.0	.690	15000	88000	21.25	108700	10350	166600	11.10
22	101.0	.450	12910	52300	27.16	63900	5810	118200	14.84
	108.0	.480	13380	57600	26.56	70400	6400	126700	14.30
	116.0	.510	13700	62900	26.06	76900	6990	135400	13.87
	124.0	.545	14090	69100	25.46	84500	7680	145500	13.45
	132.0	.575	14370	75200	24.98	91700	8260	154400	13.09
24	107.0	.485	12850	58800	27.23	71300	6230	138400	16.27
	113.0	.500	13040	61700	27.39	74800	6520	143300	16.01
	120.0	.530	13420	67500	26.72	81800	7110	152600	15.46
	128.0	.570	13860	75300	25.55	91100	7900	165000	14.86
	132.0	.570	13930	75200	26.33	91100	7940	163300	14.60
	140.0	.600	14210	81000	25.93	98100	8530	172800	14.26
26	148.0	.640	14560	88800	25.09	107300	9320	185200	13.84
	138.0	.580	13530	78500	28.31	94200	7850	179600	16.38
	144.0	.610	13820	84300	27.41	101100	8430	189400	16.00
	151.0	.630	14020	88300	27.65	106000	8830	196500	15.76
28	160.0	.670	14390	96400	26.83	115700	9640	210000	15.30
	145.0	.585	13090	80060	31.20	95300	7660	194800	18.49
	156.0	.635	13620	90900	29.54	107900	8650	212400	17.58
	165.0	.675	13990	99100	28.65	118000	9440	226900	17.03
	175.0	.710	14270	106700	28.10	126900	10130	239600	16.62
30	186.0	.730	14390	111100	29.00	132100	10510	248000	16.53
	173.0	.660	13420	97200	32.62	114900	8860	236600	19.23
	180.0	.680	13590	101600	32.85	120100	9240	244800	18.99
	190.0	.710	13850	108400	32.41	128100	9830	256600	18.57
	200.0	.745	14120	116400	31.84	137400	10520	270400	18.14
	220.0	.815	14590	132300	30.86	156100	11890	298300	17.46
33	240.0	.880	14960	147200	30.27	173600	13160	324700	16.98
	200.0	.700	13160	108000	37.37	126400	9210	276200	21.77
	210.0	.735	13470	116300	36.49	136100	9900	291100	21.15
	220.0	.765	13710	123600	35.99	144600	10490	304000	20.70
	230.0	.795	13940	130900	35.66	153000	11080	317200	20.32
	245.0	.835	14200	140700	35.45	164400	11860	335100	19.89
	260.0	.875	14440	150500	35.25	175800	12640	353100	19.53
36	230.0	.765	13170	125600	39.82	145800	10080	329400	23.71
	240.0	.790	13370	132000	39.64	153100	10560	341300	23.32
	250.0	.820	13600	139700	39.14	162000	11150	355400	22.84
	260.0	.845	13780	146000	39.02	169500	11640	367500	22.51
	280.0	.890	14060	158000	39.15	183000	12510	389800	22.03
	300.0	.945	14380	172300	38.43	199500	13590	416400	21.46

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

CONNECTION ANGLES FOR BETHLEHEM GIRDER BEAMS

DIMENSIONS, WEIGHTS AND WORKING LOADS

 $\frac{3}{4}$ " POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles				Connection Details.						
Depth	Weight per foot	Web	Outstanding Single Shear			A.I.S.C. Mark	Gage g	Size and Length	Weight inc. Web Rivets							
			Power Driven Rivets	Unfin-ished Bolts												
8"	31.0	25650	47720	35340	$\frac{3}{16}$	IC.16.10	2 $\frac{5}{8}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $\frac{5}{16}''$	16 lbs.							
	33.0	26100	47720	35340	$\frac{3}{16}$	IC.16.10	2 $\frac{5}{8}$									
	37.0	27920	47720	35340	$\frac{3}{16}$	IC.16.10	2 $\frac{5}{8}$									
9"	36.0	26100	47720	35340	$\frac{3}{16}$	IC.16.10	2 $\frac{5}{8}$				$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $\frac{5}{16}''$	16 lbs.				
	38.5	27900	47720	35340	$\frac{1}{4}$	IC.16.10	2 $\frac{5}{8}$									
	43.5	31500	47720	35340	$\frac{3}{16}$	IC.16.10	2 $\frac{5}{8}$									
10"	41.5	27900	47720	35340	$\frac{1}{4}$	IC.16.10	2 $\frac{5}{8}$							$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $\frac{5}{16}''$	16 lbs.	
	44.5	28800	47720	35340	$\frac{1}{4}$	IC.16. 9	2 $\frac{9}{16}$									
	50.0	32400	47720	35340	$\frac{1}{4}$	IC.16. 9	2 $\frac{9}{16}$									
12"	51.5	48600	71580	53020	$\frac{1}{4}$	IC.24. 9	2 $\frac{9}{16}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $8\frac{1}{2}''$	24 lbs.							
	55.5	51300	71580	53020	$\frac{1}{4}$	IC.24. 9	2 $\frac{9}{16}$									
	61.0	55350	71580	53020	$\frac{1}{4}$	IC.24. 9	2 $\frac{9}{16}$									
	66.0	60750	71580	53020	$\frac{5}{16}$	IC.24. 8	2 $\frac{1}{2}$									
	70.5	63450	71580	53020	$\frac{5}{16}$	IC.24. 8	2 $\frac{1}{2}$									
	76.5	68850	71580	53020	$\frac{5}{16}$	IC.24. 8	2 $\frac{1}{2}$									
15"	64.5	70200	95440	70690	$\frac{1}{4}$	IC.33. 9	2 $\frac{9}{16}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $11\frac{1}{2}''$	33 lbs.							
	69.0	75600	95440	70690	$\frac{1}{4}$	IC.33. 9	2 $\frac{9}{16}$									
	74.0	79200	95440	70690	$\frac{5}{16}$	IC.33. 8	2 $\frac{1}{2}$									
	80.5	86400	95440	70690	$\frac{5}{16}$	IC.33. 8	2 $\frac{1}{2}$									
	94.0	95440	95440	70690	$\frac{5}{16}$	IC.33. 8	2 $\frac{1}{2}$									
	99.0	95440	95440	70690	$\frac{3}{8}$	IC.33. 7	2 $\frac{7}{16}$									
	105.0	95440	95440	70690	$\frac{3}{8}$	IC.33. 7	2 $\frac{7}{16}$									
	111.0	95440	95440	70690	$\frac{3}{8}$	IC.33. 7	2 $\frac{7}{16}$									
	127.0	95440	95440	70690	$\frac{7}{16}$	*	*									
	135.0	95440	95440	70690	$\frac{7}{16}$	*	*									
16"	141.0	95440	95440	70690	$\frac{7}{16}$	*	*	$6'' \times 6'' \times \frac{3}{8}''$ Long 0' — $11\frac{1}{2}''$	33 lbs.							
	147.0	95440	95440	70690	$\frac{1}{2}$	*	*									
	74.5	70200	95440	70690	$\frac{1}{4}$	IC.33. 9	2 $\frac{9}{16}$									
	81.0	75600	95440	70690	$\frac{1}{4}$	IC.33. 9	2 $\frac{9}{16}$									
18"	87.0	81000	95440	70690	$\frac{5}{16}$	IC.33. 8	2 $\frac{1}{2}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 1' — $2\frac{1}{2}''$	41 lbs.							
	94.0	87300	95440	70690	$\frac{5}{16}$	IC.33. 8	2 $\frac{1}{2}$									
	80.0	94500	119300	88360	$\frac{1}{4}$	IC.41. 9	2 $\frac{9}{16}$									
	86.0	99000	119300	88360	$\frac{5}{16}$	IC.41. 8	2 $\frac{1}{2}$									
20"	92.0	103500	119300	88360	$\frac{5}{16}$	IC.41. 8	2 $\frac{1}{2}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 1' — $2\frac{1}{2}''$	41 lbs.							
	99.0	109100	119300	88360	$\frac{5}{16}$	IC.41. 8	2 $\frac{1}{2}$									
	99.0	114800	119300	88360	$\frac{5}{16}$	IC.41. 8	2 $\frac{1}{2}$									
	107.0	113900	119300	88360	$\frac{5}{16}$	IC.41. 8	2 $\frac{1}{2}$									
	113.0	119300	119300	88360	$\frac{3}{8}$	IC.41. 8	2 $\frac{1}{2}$									
	120.0	119300	119300	88360	$\frac{3}{8}$	IC.41. 7	2 $\frac{7}{16}$									
	127.0	119300	119300	88360	$\frac{3}{8}$	IC.41. 7	2 $\frac{7}{16}$									
	135.0	119300	119300	88360	$\frac{3}{8}$	IC.41. 7	2 $\frac{7}{16}$									
20"	142.0	119300	119300	88360	$\frac{3}{8}$	IC.41. 7	2 $\frac{7}{16}$	$6'' \times 6'' \times \frac{3}{8}''$ Long 1' — $2\frac{1}{2}''$	41 lbs.							
	149.0	119300	119300	88360	$\frac{7}{16}$	IC.41. 7	2 $\frac{7}{16}$									

*Special Connections must be used for 15", 127, 135, 141, and 147 lb., Girder Beams. The values given are for 8 web and 16 field rivets.

Following Beams can be framed opposite with tops flush when:—

A = $2\frac{3}{4}$ " all 8", 9", 10", 12", 15", to 80.5 lb., and 16".

A = 3" all 9", 10", 12", 15", 16", 18", 20", 22", and 24", to 129 lb.

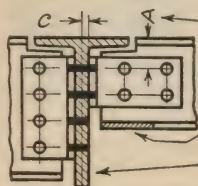
A = $3\frac{1}{4}$ " all 9", 10", 12", 15", to 80.5 lb., 16", 18", 93 and 100 lb., 20", 22", 24" and 26"

A = $3\frac{1}{2}$ " all 10", 12", 20", 22", 24", 26", 28" and 30".

Flange must be cut away as shown for field riveting on all beams framing opposite a larger beam, if flange interferences with outstanding rivets.

Minimum Web required to develop Single Shearing Value is .33"

Minimum Web required to develop Double Shearing Value is .53"



CONNECTION ANGLES FOR BETHLEHEM GIRDER BEAMS

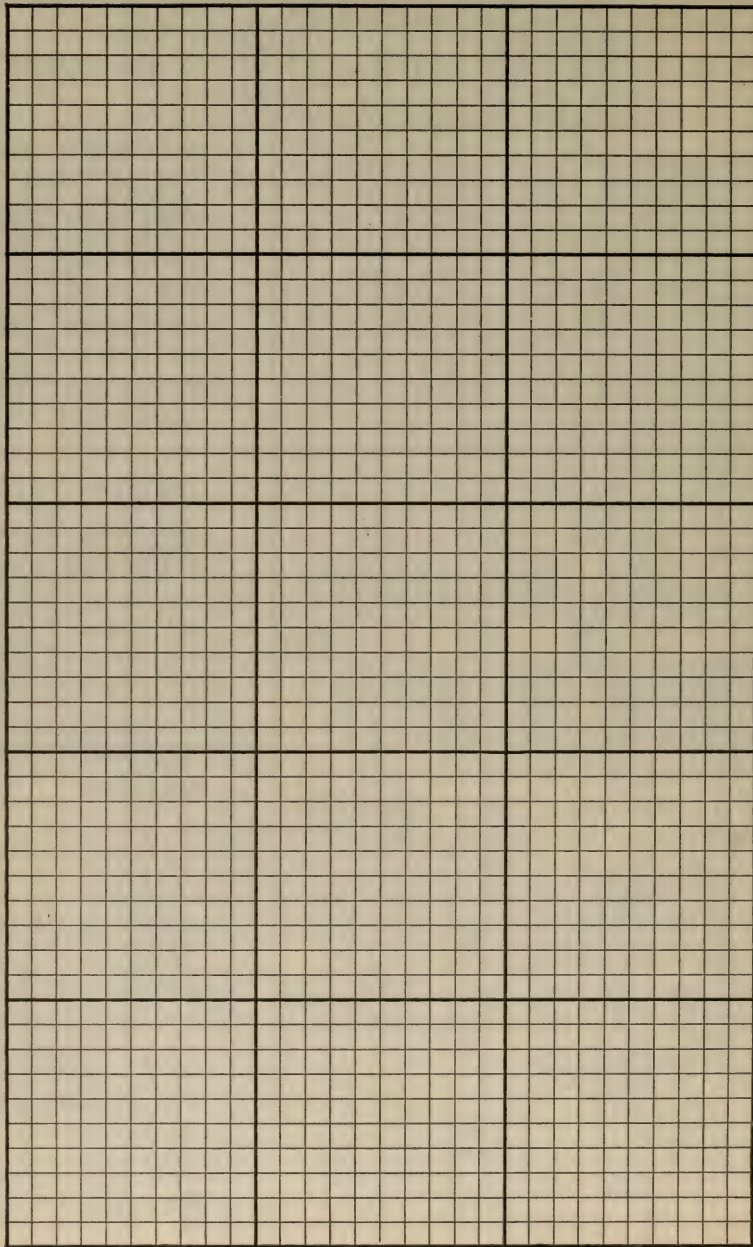
DIMENSIONS, WEIGHTS, AND WORKING LOADS

¾" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles			Connection Details	
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length		Weight inc. Web Rivets
			Single Shear							
			Power Driven Rivets	Unfinished Bolts						
22"	101.0	121600	143160	106030	5/16	IC.49. 8	2 1/2	6" x 6" x 3/8" 1' — 5 1/2" Long		
	108.0	129600	143160	106030	5/16	IC.49. 8	2 1/2			
	116.0	137800	143160	106030	5/16	IC.49. 8	2 1/2			
	124.0	143160	143160	106030	5/16	IC.49. 8	2 1/2			
	132.0	143160	143160	106030	3/8	IC.49. 7	2 7/16			
24"	107.0	130980	143160	106030	5/16	IC.49. 8	2 1/2		49 lbs.	
	113.0	135000	143160	106030	5/16	IC.49. 8	2 1/2			
	120.0	143160	143160	106030	5/16	IC.49. 8	2 1/2			
	128.0	143160	143160	106030	3/8	IC.49. 7	2 7/16			
	132.0	143160	143160	106030	3/8	IC.49. 7	2 7/16			
	140.0	143160	143160	106030	3/8	IC.49. 7	2 7/16			
	148.0	143160	143160	106030	3/8	IC.49. 7	2 7/16			
	138.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	144.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	151.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
28"	160.0	167020	167020	123700	3/8	IC.58. 7	2 7/16		58 lbs.	
	145.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	156.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	165.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	175.0	167020	167020	123700	7/16	IC.58. 6	2 3/8			
	186.0	167020	167020	123700	7/16	IC.58. 6	2 3/8		6" x 6" x 3/8" 1' — 8 1/2" Long	
	145.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	156.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	165.0	167020	167020	123700	3/8	IC.58. 7	2 7/16			
	175.0	167020	167020	123700	7/16	IC.58. 6	2 3/8			
30"	186.0	167020	167020	123700	7/16	IC.58. 6	2 3/8		6" x 6" x 3/8" 1' — 11 1/2" Long	
	173.0	190880	190880	141380	3/8	IC.66. 7	2 7/16			
	180.0	190880	190880	141380	3/8	IC.66. 7	2 7/16			
	190.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
	200.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
33"	220.0	190880	190880	141380	1/2	IC.66. 5	2 5/16		66 lbs.	
	240.0	190880	190880	141380	1/2	IC.66. 5	2 5/16			
	200.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
	210.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
	220.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
36"	230.0	190880	190880	141380	1/2	IC.66. 5	2 5/16		66 lbs.	
	245.0	190880	190880	141380	1/2	IC.66. 5	2 5/16			
	260.0	190880	190880	141380	1/2	IC.66. 5	2 5/16			
	230.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
	240.0	190880	190880	141380	7/16	IC.66. 6	2 3/8			
	250.0	190880	190880	141380	1/2	IC.66. 5	2 5/16	66 lbs.		
	260.0	190880	190880	141380	1/2	IC.66. 5	2 5/16			
	280.0	190880	190880	141380	1/2	IC.66. 5	2 5/16			
	300.0	190880	190880	141380	9/16	IC.66. 4	2 1/4			

*Layer-out starts with this dimension at left end of beam. With beams ordered one inch short, as usual in standard shop practice, this leaves sufficient end distance or clearance at right end, in case of full allowable 1/2" underrun or 1/2" overrun in beam lengths.

NOTES and DIAGRAMS



Part IV

Section 7

CARNEGIE BEAM SECTIONS

Dimensions—Technical Functions

Allowable Total Loads by A. I. S. C. Specification

Allowable End Reactions—Standard Connection Angles

Usual Stock Sizes

Usual Stock Sizes					
Depth	Weight	Depth	Weight	Depth	Weight
8"	24.0 *	16"	35.0 *	30"	115.0 *
9"	29.0 *	18"	47.0 *	33"	125.0 *
10"	21.0 *	21"	55.0 *	36"	147.0 *
12"	25.0 *	24"	70.0 *		
14"	30.0 *	27"	85.0 *		

Manufacturers Section Index

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8"

C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

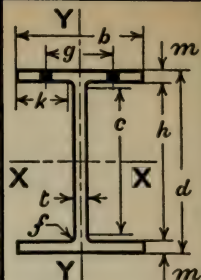
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d".	8.000	8.098	8.196	8.060	8.198	8.360
Wt. per foot.	24.0	27.0	30.0	31.0	36.0	42.0
Area.	7.06	7.93	8.81	9.10	10.58	12.34
b".	6.500	6.529	6.559	8.000	8.046	8.100
t.	.239	.268	.298	.290	.336	.390
h.	$7\frac{3}{16}$	$7\frac{3}{16}$	$7\frac{3}{16}$	$7\frac{3}{16}$	$7\frac{3}{16}$	$7\frac{3}{16}$
m.	.400	.449	.498	.430	.499	.580
k.	$21\frac{1}{16}$	$21\frac{1}{16}$	$21\frac{1}{16}$	$3\frac{3}{8}$	$3\frac{3}{8}$	$3\frac{3}{8}$
c.	.45	.45	.45	.45	.45	.45
f.	$6\frac{1}{4}$	$6\frac{1}{4}$	$6\frac{1}{4}$	$6\frac{1}{4}$	$6\frac{1}{4}$	$6\frac{1}{4}$
g.	$3\frac{1}{2}$	$3\frac{1}{2}$	$3\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$
A X E S	I....	84.3	95.9	107.8	110.9	131.3
	S....	21.08	23.68	26.31	27.52	32.03
	r....	3.46	3.48	3.50	3.49	3.52
Y - V	I....	18.3	20.8	23.4	36.7	43.4
	S....	5.6	6.4	7.1	9.2	10.8
	r....	1.61	1.62	1.63	2.01	2.02
Coef. Str....	252900	284200	315700	330200	384400	448400
Max. Mom. %	379400	426300	473500	495300	576600	672600
V....	22900	26000	29300	28100	33100	39100
P. feet....	5.52	5.46	5.38	5.88	5.81	5.74
R....	19720	22210	24800	23990	27970	32700
W....	21510	23860	23860	26100	30240	35100
Q. feet....	5.88	5.95	6.62	6.32	6.35	6.38
w lbs....	13	13	13	16	16	16
Rivet dia....	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$

Live Load deflection must not exceed $\frac{1}{360}$ of the Span.

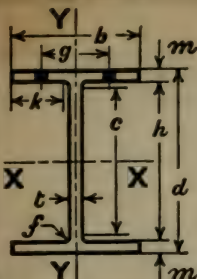
Total Def. \times Live Load

Live Load Def. = Tabular Load

Total Deflection in inches for Maximum Load: Laterally fixed beam.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		Total Deflection in inches for Maximum Load: Laterally fixed beam.
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
3	45.9	45.9	52.1	52.1	58.6	58.6	56.1	56.1	66.1	66.1	78.2	78.2	
4	45.9	45.9	52.1	52.1	58.6	58.6	56.1	56.1	66.1	66.1	78.2	78.2	
5	45.9	45.9	52.1	52.1	58.6	58.6	56.1	56.1	66.1	66.1	78.2	78.2	
6	42.1	42.1	47.3	47.3	52.6	52.6	55.0	55.0	64.1	64.1	74.8	74.8	.084
7	36.1	36.1	40.6	40.6	45.1	45.1	47.2	47.2	54.9	54.9	64.1	64.1	.114
8	31.6	31.6	35.5	35.5	39.5	39.5	41.3	41.3	48.0	48.0	56.1	56.1	.149
9	28.1	27.5	31.6	30.9	35.1	34.3	36.7	36.7	42.7	42.7	49.8	49.8	.189
10	25.3	24.0	28.4	27.0	31.6	30.1	33.0	33.0	38.4	38.4	44.9	44.9	.233
11	23.0	21.2	25.8	23.8	28.7	26.5	30.0	29.4	34.9	34.2	40.8	40.0	.281
12	21.1	18.8	23.7	21.2	26.3	23.5	27.5	26.3	32.0	30.6	37.4	36.6	.335
13	19.4	16.8	21.9	18.9	24.3	21.1	25.4	23.7	29.6	27.6	34.5	32.3	.394
14	18.1	15.1	20.3	16.9	22.6	18.9	23.6	21.5	27.5	25.0	32.0	29.3	.456
15	16.9	18.9	21.1	22.0	25.6	29.9	26.6	.524
16	15.8	17.8	19.7	20.6	24.0	28.0596
17	14.9	16.7	18.6	19.4	22.6	26.4674
18	14.1	15.8	17.5	18.3	21.4	24.9754
19	13.3	15.0	16.6	17.4	20.2	23.6840
20	12.6	14.2	15.8	16.5	19.2	22.4931
21	12.0	13.5	15.0	15.7	18.3	21.5	1.03
22	11.5	12.9	14.4	15.0	17.5	20.4	1.13
23	11.0	12.4	13.7	14.4	16.7	19.5	1.23
24	10.5	11.8	13.2	13.8	16.0	18.7	1.34
25	10.1	11.4	12.6	13.2	15.4	17.9	1.46

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.



CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

9"

C

Depth = d"	9.000	9.096	9.192	9.000	9.122	9.242
Wt. per foot.	29.0	32.0	35.0	38.0	43.0	48.0
Area.....	8.53	9.40	10.29	11.17	12.65	14.11
b"	6.500	6.528	6.556	6.584	6.612	6.640
t.....	.279	.307	.335	.363	.391	.419
h.....	8"	8"	8"	8"	8"	8"
m.....	.470	.518	.566	.614	.662	.710
k.....	2 $\frac{1}{2}$ "	2 $\frac{1}{2}$ "	2 $\frac{1}{2}$ "	3 $\frac{1}{2}$ "	3 $\frac{1}{2}$ "	3 $\frac{1}{2}$ "
f.....	.50	.50	.50	.50	.50	.50
c.....	7"	7"	7"	7"	7"	7"
g.....	3"	3"	3"	5 $\frac{1}{2}$ "	5 $\frac{1}{2}$ "	5 $\frac{1}{2}$ "
A X E S						
I.....	126.0	140.5	155.4	170.4	195.5	221.1
S.....	28.00	30.89	33.81	37.87	42.86	47.85
r.....	3.84	3.87	3.89	3.91	3.93	3.96
I.....	21.5	24.0	26.6	29.1	31.6	34.1
S.....	6.6	7.4	8.1	8.9	9.7	10.5
r.....	1.59	1.60	1.61	1.62	1.63	1.64
Coef. Str....	336000	370700	405700	440700	475700	510700
Max.Mom.*#	504000	556100	608200	660300	712400	764500
V.....	30100	33500	37000	40400	43800	47200
P, feet....	5.58	5.53	5.49	5.44	5.39	5.34
R.....	24060	26590	29130	31670	34210	36750
W.....	23860	23860	23860	23860	23860	23860
Q, feet....	7.04	7.77	8.50	9.23	9.96	10.69
w lbs.....	13	13	13	16	16	16
Rivet dia....	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$

Live Load Deflection must not exceed 1/360 of the Span.

Total Def. \times Live Load
Tabular Load

Total Deflection in inches for Maximum Load: Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Span	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally
feet	fixed	free	fixed	free	fixed	free
3	60.3	60.3	67.0	67.0	73.9	73.9
4	60.3	60.3	67.0	67.0	73.9	73.9
5	60.3	60.3	67.0	67.0	73.9	73.9
6	56.0	56.0	61.8	61.8	67.6	67.6
7	48.0	48.0	53.0	53.0	58.0	58.0
8	42.0	42.0	46.4	46.4	50.7	50.7
9	37.3	36.5	41.2	40.3	45.1	44.1
10	33.6	31.9	37.1	35.2	40.6	38.7
11	30.5	28.2	33.7	31.1	36.9	34.0
12	28.0	24.9	30.9	27.6	33.8	30.3
13	25.8	22.3	28.5	24.6	31.2	27.1
14	24.0	20.0	26.5	22.1	29.0	24.2
15	22.4	18.0	24.7	19.9	27.1	21.8
16	21.0	16.3	23.2	17.9	25.4	19.7
17	19.8	15.0	21.8	16.5	23.9	18.4
18	18.7	14.0	20.6	15.5	22.5	17.2
19	17.7	13.1	19.5	14.5	21.4	16.1
20	16.8	12.3	18.5	13.6	20.3	15.0
21	16.0	11.6	17.7	12.8	19.3	14.1
22	15.3	11.0	16.9	12.1	18.4	13.3
23	14.6	10.4	16.1	11.5	17.6	12.5
24	14.0	9.9	15.4	10.9	16.9	11.8
25	13.4	9.4	14.8	10.3	16.2	11.2

Total Deflection in inches for Maximum Load: Laterally fixed beam.

10" C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

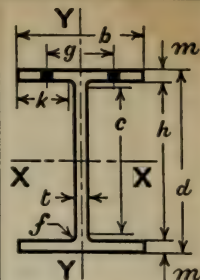
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d"	9.902	10.000	10.098	10.228
Wt. per foot.	21.0	23.0	26.0	30.0
Area, in ²	6.17	6.76	7.64	8.82
t, in.	6.000	6.000	6.029	6.068
c, in.	.230	.230	.259	.298
h, in.	$9\frac{3}{16}$	$9\frac{3}{16}$	$9\frac{3}{16}$	$9\frac{3}{16}$
m, in.	.332	.381	.430	.495
k, in.	$2\frac{9}{16}$	$2\frac{9}{16}$	$2\frac{9}{16}$	$2\frac{9}{16}$
f, in.	.30	.30	.30	.30
c, in.	$8\frac{5}{8}$	$8\frac{5}{8}$	$8\frac{5}{8}$	$8\frac{5}{8}$
g, in.	3"	3"	3"	3"
AXES				
I, X-X	107.6	122.2	139.5	163.2
S, X-X	21.73	24.44	27.63	31.91
r, X-X	4.18	4.25	4.27	4.30
I, Y-Y	12.0	13.7	15.7	18.5
S, Y-Y	4.0	4.6	5.2	6.1
r, Y-Y	1.39	1.43	1.43	1.45
Coef. Str.	260800	293300	331500	382900
Max. Mom. #	391200	439900	497300	574400
V, lbs.	27300	27600	31400	36600
P, feet	4.76	5.30	5.28	5.23
R, lbs.	18900	18890	22410	27070
W, lbs.	20700	20700	23310	23860
Q, feet	6.29	7.08	7.11	8.02
w, lbs.	13	13	13	13
Rivet dia.	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{3}{4}$

Live Load deflection must not exceed $\frac{1}{360}$ of the Span.

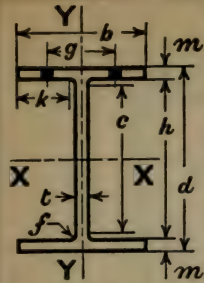
Live Load Def. = Total Def. \times Live Load / Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Span feet	Laterally		Laterally		Laterally		Laterally	
	fixed	free	fixed	free	fixed	free	fixed	free
3	55	55	55	55	63	63	73	73
4	55	55	55	55	63	63	73	73
5	52	52	55	55	63	63	73	73
6	44	44	49	49	55	55	64	64
7	37	37	42	42	47	47	55	55
8	33	32	37	36	41	41	48	47
9	29	28	33	31	37	35	43	41
10	26	24	29	27	33	31	38	36
11	24	21	27	24	30	27	35	31
12	22	19	24	21	28	24	32	29
13	20	17	23	19	26	21	30	25
14	19	15	21	17	24	19	27	22
15	17	13	20	15	22	17	26	20
16	16	12	18	14	21	15	24	18
17	15	11	17	12	20	14	23	16
18	15	...	16	...	18	13	21	15
19	14	...	15	...	18	...	20	...
20	13	...	15	...	17	...	19	...
21	12	...	14	...	16	...	18	...
22	12	...	13	...	15	...	17	...
23	11	...	13	...	14	...	17	...
24	11	...	12	...	14	...	16	...
25	10	...	12	...	13	...	15	...

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CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

10"
C

Depth = d"	10.000	10.000	10.000	10.000	10.000	10.000	10.000
Wt. per foot.	31.0	36.0	42.0	49.0	54.0	59.0	64.0
Area	9.11	10.58	12.35	14.40	15.87	17.34	18.81
b"	8.000	8.147	8.324	10.000	10.147	10.294	10.441
t	.320	.467	.644	.350	.497	.644	.791
h	9 $\frac{1}{16}$	9 $\frac{3}{8}$	9 $\frac{1}{2}$	8 $\frac{7}{8}$	8 $\frac{7}{8}$	8 $\frac{7}{8}$	8 $\frac{7}{8}$
m	.381	.381	.381	.558	.558	.558	.558
k	3 $\frac{9}{16}$	3 $\frac{9}{16}$	3 $\frac{9}{16}$	4 $\frac{3}{8}$	4 $\frac{3}{8}$	4 $\frac{3}{8}$	4 $\frac{3}{8}$
c	.30	.30	.30	.45	.45	.45	.45
f	8 $\frac{5}{8}$	8 $\frac{5}{8}$	8 $\frac{5}{8}$	7 $\frac{1}{2}$	7 $\frac{1}{2}$	7 $\frac{1}{2}$	7 $\frac{1}{2}$
g	4 $\frac{1}{2}$	4 $\frac{1}{2}$	4 $\frac{1}{2}$	5 $\frac{1}{2}$	5 $\frac{1}{2}$	5 $\frac{1}{2}$	5 $\frac{1}{2}$
AXES							
I	163.4	175.6	190.4	272.0	284.3	296.5	308.8
S	32.68	35.12	38.08	54.40	56.86	59.30	61.76
r	4.23	4.07	3.93	4.35	4.23	4.13	4.05
I	32.5	34.4	36.8	93.0	97.3	101.7	106.3
S	8.1	8.5	8.9	18.6	19.2	19.8	20.4
r	1.89	1.80	1.73	2.54	2.48	2.42	2.38
Coef. Str.	392200	421400	457000	652800	682300	711600	741120
Max. Mom. %	588200	632200	685400	979200	1023500	1067400	1111700
V	38400	56000	77300	42000	59600	77300	94900
P, feet	5.11	3.76	2.96	7.77	5.72	4.60	3.90
R	28800	42030	57960	31500	44730	57960	71190
Q	28800	42030	47720	31520	44730	47720	47720
W, lbs.	6.81	5.01	4.79	10.36	7.63	7.46	7.77
w	16	16	16	16	16	16	16
Rivet dia.	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$

Live Load deflection must not exceed 1/360 of the span.

Live Load Def. = Total Def. \times Live Load Tabular Load

Total Deflection in inches for Maximum Load: Laterally fixed beam.

Span feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally	
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
3	77	77	112	112	152	152	84	84	119	119	155	155	190	190
4	77	77	105	105	114	114	84	84	119	119	155	155	185	185
5	77	77	84	84	91	91	84	84	119	119	142	142	148	148
6	65	65	70	70	76	76	84	84	114	114	119	119	124	124
7	56	56	60	60	65	65	84	84	97	97	102	102	106	106
8	49	49	53	53	57	57	82	82	85	85	89	89	93	93
9	44	44	47	47	51	51	73	73	76	76	79	79	82	82
10	39	39	42	42	46	46	65	65	68	68	71	71	74	74
11	36	35	38	38	42	41	59	59	62	62	65	65	67	67
12	33	31	35	34	38	37	54	54	57	57	59	59	62	62
13	30	28	32	30	35	33	50	50	52	52	55	55	57	57
14	28	26	30	28	33	30	47	45	49	48	51	50	53	52
15	26	23	28	25	31	28	44	42	45	44	47	46	49	48
16	25	21	26	23	29	25	41	38	43	40	44	42	46	44
17	23	19	25	21	27	23	38	35	40	37	42	39	44	41
18	22	...	23	...	25	...	36	...	38	...	40	...	41	...
19	21	...	22	...	24	...	34	...	36	...	37	...	39	...
20	20	...	21	...	23	...	33	...	34	...	36	...	37	...
21	19	...	20	...	22	...	31	...	32	...	34	...	35	...
22	18	...	19	...	21	...	30	...	31	...	32	...	34	...
23	17	...	18	...	20	...	28	...	30	...	31	...	32	...
24	16	...	18	...	19	...	27	...	28	...	30	...	31	...
25	16	...	17	...	18	...	26	...	27	...	28	...	30	...

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12" C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

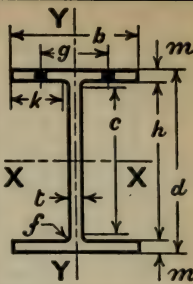
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d". Wt. per foot. Area. b". t". h". m". k". f". c". g".	11.924 25.0 7.34 6.000 .240 11 ¹ / ₈ .382 2 ¹ / ₂ .35 10 ³ / ₈ 3"	12.000 28.0 8.22 6.500 .240 11 ¹ / ₈ .420 2 ³ / ₄ .35 10 ³ / ₈ 3 ¹ / ₂ "	12.118 32.0 9.40 6.534 .274 11 ¹ / ₈ .479 2 ³ / ₄ .35 10 ³ / ₈ 3 ¹ / ₂ "	*12.022 34.0 9.99 6.635 .375 11 ¹ / ₈ .431 2 ³ / ₄ .35 10 ³ / ₈ 3 ¹ / ₂ "	12.236 36.0 10.59 6.568 .308 11 ¹ / ₈ .538 2 ³ / ₄ .35 10 ³ / ₈ 3 ¹ / ₂ "	12.000 40.0 11.76 8.000 .290 10 ¹⁵ / ₁₆ .526 3 ³ / ₈ .50 9 ⁷ / ₈ 4"	12.130 45.0 13.23 8.036 .326 10 ¹⁵ / ₁₆ .591 3 ³ / ₈ .50 9 ⁷ / ₈ 4"	12.258 50.0 14.69 8.071 .361 10 ¹⁵ / ₁₆ .655 3 ³ / ₈ .50 9 ⁷ / ₈ 4"											
	AXES	I.... S.... r....	183.0 30.69 4.99	213.4 35.57 5.10	246.3 40.65 5.12	238.1 39.61 4.88	280.1 45.78 5.14	313.7 52.28 5.17	356.9 58.85 5.19	400.5 65.35 5.22									
	Y-Y	I.... S.... r....	13.8 4.6 1.37	19.2 5.9 1.53	22.3 6.8 1.54	21.0 6.3 1.45	25.4 7.7 1.55	44.9 11.2 1.95	51.2 12.7 1.97	57.5 14.2 1.98									
	Coef. Str.	368300	426800	487800	475300	549400	627400	706100	784100										
	Max.Mom. #	552500	640200	731700	713000	824100	941100	1059200	1176200										
	V.	34300	34600	39800	45100	45200	41800	47500	53100										
	P. feet.	5.36	6.18	6.13	4.39	6.08	7.51	7.43	7.39										
	R.	19840	19820	24290	36590	28790	26400	31140	35550										
	W.	21600	21600	23860	23860	23860	23860	23860	23860										
	Q feet.	8.53	9.88	10.22	9.96	11.51	13.14	14.79	16.43										
w lbs..	13	13	13	13	13	13	13	13											
Rivet dia.	7/8	7/8	7/8	7/8	7/8	7/8	7/8	7/8											
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.	Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. x Live Load Tabular Load
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free		
	3	69	69	69	69	80	80	108	108	90	90	84	84	95	95	106	106	.099 .126 .155	
	4	69	69	69	69	80	80	108	108	90	90	84	84	95	95	106	106		
	5	69	69	69	69	80	80	95	95	90	90	84	84	95	95	106	106		
	6	61	61	69	69	80	80	79	79	90	90	84	84	95	95	106	106		
	7	53	53	61	61	70	70	68	68	79	79	84	84	95	95	106	106		
	8	46	45	53	53	61	61	59	59	69	69	78	78	88	88	98	98		
	9	41	39	47	46	54	53	53	52	61	60	70	70	79	79	87	87		
	10	37	34	43	41	49	47	48	46	55	52	63	63	71	71	78	78		
	11	34	30	39	36	44	41	43	40	50	46	57	56	64	63	71	70		
	12	31	27	36	32	41	36	40	36	46	41	52	50	59	56	65	63		
	13	28	24	33	28	38	32	37	32	42	37	48	45	54	51	60	57		
	14	26	21	31	25	35	29	34	29	39	33	45	41	50	46	56	51		
	15	25	19	29	23	33	26	32	26	37	30	42	37	47	42	52	47		
	16	23	17	27	21	31	24	30	23	34	27	39	34	44	38	49	43		
	17	22	15	25	19	29	21	28	21	32	24	37	31	42	35	46	39		
	18	21	14	24	17	27	20	26	19	31	22	35	28	39	32	44	36		
	19	19	13	23	16	26	18	25	18	29	20	33	26	37	30	41	33		
	20	18	11	21	14	24	16	24	16	28	18	31	24	35	27	39	30		
21	18	...	20	13	23	15	23	15	26	17	30	22	34	25	37	28			
22	17	...	19	...	22	...	22	...	25	...	29	...	32	...	36	...			
23	16	...	19	...	21	...	21	...	24	...	27	...	31	...	34	...			
24	15	...	18	...	20	...	20	...	23	...	26	...	29	...	33	...			
25	15	...	17	...	19	...	19	...	22	...	25	...	28	...	31	...			
* Special Sections. Web Thickness 3/8".																			

* Special Sections. Web Thickness $\frac{3}{8}$ ".

LOADS BY A. I. S. C. SPECIFICATION

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

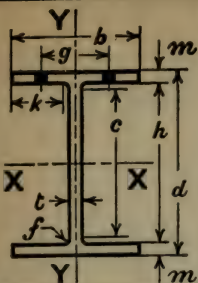
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

12"
C

Depth = d"	12.000	12.118	12.260	12.000	12.000	12.000
Wt. per foot.	55.0	60.0	66.0	65.0	70.0	76.0
Area sq. in.	16.17	17.65	19.41	19.11	20.58	22.35
b"	9.000	9.034	9.073	12.000	12.123	12.270
t	.375	.409	.448	.400	.523	.670
h	$10\frac{5}{8}$	$10\frac{5}{8}$	$10\frac{5}{8}$	$10\frac{3}{4}$	$10\frac{3}{4}$	$10\frac{3}{4}$
m	.665	.724	.795	.608	.608	.608
k	$3\frac{3}{4}$	$3\frac{3}{4}$	$3\frac{3}{4}$	$5\frac{1}{4}$	$5\frac{1}{4}$	$5\frac{1}{4}$
f	.55	.55	.55	.55	.55	.55
c	$9\frac{1}{2}$	$9\frac{1}{2}$	$9\frac{1}{2}$	$9\frac{5}{8}$	$9\frac{5}{8}$	$9\frac{5}{8}$
g	$5\frac{1}{2}$	$5\frac{1}{2}$	$5\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$	$7\frac{1}{2}$
AXES						
X-X	I. 428.4	I. 472.0	I. 525.7	I. 521.3	I. 539.0	I. 560.2
S	71.40	77.90	85.76	86.88	89.83	93.36
r	5.15	5.17	5.20	5.22	5.12	5.01
Y-Y	I. 80.9	I. 89.0	I. 99.1	I. 175.2	I. 180.7	I. 187.5
S	18.0	19.7	21.8	29.2	29.8	30.6
r	2.24	2.25	2.26	3.03	2.96	2.90
Coef. Str.	856800	934800	1029100	1042600	1078000	1120400
Max. Mom. *	1285200	1402200	1543700	1563900	1617000	1680600
V	54000	59500	65900	57600	75300	96500
P, feet.	7.93	7.86	7.81	9.05	7.16	5.80
R	36560	40060	44120	39000	50990	65300
W	50640	55220	60480	54000	70610	71580
Q, feet.	8.46	8.46	8.51	9.65	7.63	7.83
w, lbs.	24	24	24	24	24	24
Rivet dia.	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$
ALLOWABLE TOTAL LOADS						
Span	Laterally		Laterally		Laterally	
	fixed	free	fixed	free	fixed	free
3	108	108	119	119	132	132
4	108	108	119	119	132	132
5	108	108	119	119	132	132
6	108	108	119	119	132	132
7	108	108	119	119	132	132
8	107	107	117	117	129	129
9	95	95	104	104	114	114
10	86	86	93	93	103	103
11	78	78	85	85	94	94
12	71	70	78	77	86	85
13	66	64	72	70	79	77
14	61	58	67	63	74	70
15	57	53	62	58	69	64
16	54	49	58	53	64	58
17	50	45	55	49	61	54
18	48	41	52	45	57	50
19	45	38	49	41	54	46
20	43	35	47	38	51	42
21	41	33	45	36	49	39
22	39	..	43	..	47	..
23	37	..	41	..	45	..
24	36	..	39	..	43	..
25	34	..	37	..	41	..
DEFLECTION						
Total Deflection in inches for Maximum Load; Laterally fixed beam.						
3	193	193	193	193	193	193
4	193	193	193	193	193	193
5	193	193	193	193	193	193
6	187	187	187	187	187	187
7	160	160	160	160	160	160
8	140	140	140	140	140	140
9	124	124	124	124	124	124
10	112	112	112	112	112	112
11	102	102	102	102	102	102
12	93	93	93	93	93	93
13	86	86	86	86	86	86
14	80	80	80	80	80	80
15	75	75	75	75	75	75
16	69	69	69	69	69	69
17	66	66	66	66	66	66
18	62	62	62	62	62	62
19	59	59	59	59	59	59
20	56	56	56	56	56	56
21	53	53	53	53	53	53
22	51	51	51	51	51	51
23	49	49	49	49	49	49
24	47	47	47	47	47	47
25	45	45	45	45	45	45

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Live Load Deflection must not exceed $\frac{1}{360}$ of the Span.
Live Load Def. = Total Def. \times Live Load
Tabular Load

14" C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

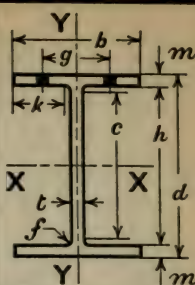
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".	13.964	14.000	14.080	*14.000	14.160	14.240							
Wt. per foot.	30.0	33.0	36.0	38.0	39.0	42.0							
Area.	8.82	9.71	10.58	11.18	11.47	12.35							
b".	6.000	6.750	6.774	6.855	6.798	6.822							
t".	.270	.270	.294	.375	.318	.342							
m.	13 ¹ / ₁₆	13 ¹ / ₁₆	13 ¹ / ₁₆	13 ¹ / ₁₆	13 ¹ / ₁₆	13 ¹ / ₁₆							
h.	.431	.449	.489	.449	.529	.569							
k.	27 ¹ / ₁₆	21 ³ / ₁₆	21 ³ / ₁₆	21 ³ / ₁₆	21 ³ / ₁₆	21 ³ / ₁₆							
f.	.40	.40	.40	.40	.40	.40							
c.	12 ¹ / ₄	12 ¹ / ₄	12 ¹ / ₄	12 ¹ / ₄	12 ¹ / ₄	12 ¹ / ₄							
g.	3"	3 ¹ / ₂ "	3 ¹ / ₂ "	3 ¹ / ₂ "	3 ¹ / ₂ "	3 ¹ / ₂ "							
A X E S	I.....	292.0	333.4	365.6	357.5	398.3							
	S.....	41.82	47.63	51.93	51.07	56.26							
	r.....	5.75	5.86	5.88	5.66	5.89							
Y - Y	I.....	15.5	23.0	25.4	24.2	27.7							
	S.....	5.2	6.8	7.5	7.1	8.2							
	r.....	1.33	1.54	1.55	1.47	1.56							
Coef. Str.	501900	571500	623200	612900	675100	727200							
Max.Mom. %	752800	857300	934800	919300	1012600	1090900							
V.....	45200	45400	49700	63000	54000	58400							
P. feet..	5.54	6.30	6.27	4.87	6.25	6.22							
R.....	23500	23490	26880	38340	30290	33720							
W.....	24300	24300	26460	33750	28620	30780							
Q. feet..	10.32	11.75	11.78	9.08	11.79	11.81							
w lbs....	19	19	19	19	19	19							
Rivet dia..	7/8	7/8	7/8	7/8	7/8	7/8							
Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Total Deflection in inches for Maximum Load: Laterally fixed beam.
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	
4	91	91	91	91	99	99	126	126	108	108	117	117	
5	91	91	91	91	99	99	123	123	108	108	117	117	
6	84	84	91	91	99	99	102	102	108	108	117	117	.065
7	72	72	82	82	89	89	88	88	96	96	104	104	.085
8	63	62	72	72	78	78	77	77	84	84	91	91	.108
9	56	53	64	63	69	68	68	67	75	74	81	80	.133
10	50	47	57	55	62	60	61	59	68	65	73	70	.161
11	46	41	52	49	57	53	56	52	61	57	66	62	.192
12	42	36	48	43	52	47	51	47	56	51	61	55	.225
13	39	32	44	39	48	42	47	42	52	46	56	49	.261
14	36	29	41	35	45	38	44	37	48	41	52	44	.299
15	34	26	38	31	42	34	41	34	45	37	49	40	.341
16	31	23	36	28	39	31	38	31	42	34	46	36	.384
17	32	21	34	26	37	28	36	28	40	30	43	33	.431
18	28	19	32	23	35	25	34	25	38	28	40	30	.480
19	26	17	30	21	33	23	32	23	36	25	38	27	.532
20	25	16	29	20	31	21	31	21	34	23	36	25	.587
21	24	...	27	18	30	20	29	19	32	21	35	23	.644
22	23	...	26	16	28	18	28	18	31	20	33	21	.704
23	22	...	25	...	27	...	27	...	29	...	32766
24	21	...	24	...	26	...	26	...	28	...	30831
25	20	...	23	...	25	...	25	...	27	...	29899
26	19	...	22	...	24	...	24	...	26	...	28970
27	19	...	21	...	23	...	23	...	25	...	27	...	1.043
28	18	...	20	...	22	...	22	...	24	...	26	...	1.119
29	17	...	20	...	21	...	21	...	23	...	25	...	1.197
30	17	...	19	...	21	...	20	...	23	...	24	...	

Live Load Deflection must not exceed 1/360 of the Span.

Live Load Def. = Total Def. × Live Load Tabular Load

* Special Section. Web Thickness $\frac{3}{8}$ ".

LOADS BY A. I. S. C. SPECIFICATION

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

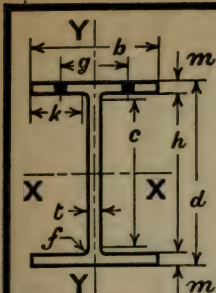
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.

14"
C

Depth = d". Wt. per foot. Area.	14.000 48.0 14.12	14.122 53.0 15.59	14.242 58.0 17.05	14.094 61.0 17.94	14.238 68.0 19.99	14.382 75.0 22.05	14.000 85.0 24.99	14.186 95.0 27.93	14.370 105.0 30.88								
	b". t. h. m. k. f. c. e.	8.000 .343 12 ³ / ₄ .395 3 ¹ / ₄ .55 11 ⁵ / ₈ 4	8.035 .378 12 ³ / ₄ .656 3 ¹ / ₄ .55 11 ⁵ / ₈ 4	8.070 .413 12 ³ / ₄ .716 3 ¹ / ₄ .55 11 ⁵ / ₈ 4	10.000 .382 12 ³ / ₄ .642 4 ¹ / ₄ .55 11 ⁵ / ₈ 5 ¹ / ₂	10.043 .425 12 ³ / ₄ .714 4 ¹ / ₄ .55 11 ⁵ / ₈ 5 ¹ / ₂	10.086 .468 12 ³ / ₄ .786 4 ¹ / ₄ .55 11 ⁵ / ₈ 5 ¹ / ₂	12.000 .435 12 ³ / ₄ .805 5 ¹ / ₈ .65 11" 7 ¹ / ₂	12.050 .485 12 ³ / ₄ .898 5 ¹ / ₈ .65 11" 7 ¹ / ₂	12.101 .536 12 ³ / ₄ .990 5 ¹ / ₈ .65 11" 7 ¹ / ₂							
A X E S	I. S. r.	496.0 70.86 5.93	552.5 78.25 5.95	609.4 85.58 5.98	656.2 93.12 6.05	738.8 103.78 6.08	823.5 114.52 6.11	921.3 131.61 6.07	1044.0 147.19 6.11	1169.6 162.78 6.15							
	V. S. r.	50.8 12.7 1.90	56.8 14.1 1.91	62.8 15.6 1.92	107.1 21.4 2.44	120.6 24.0 2.46	134.5 26.7 2.47	232.0 38.7 3.05	262.0 43.5 3.06	292.6 48.4 3.08							
Coef. Str. . . . Max. Mom. % V. P. feet . . . R. W. Q. feet . . . w. lbs. Rivet dia. . . .	850300 1275400 57600 7.38 33820 46300 9.18 24 7 ¹ / ₈	939000 1408400 64100 7.32 38810 51030 9.20 24 7 ¹ / ₈	1026900 1540400 70600 7.28 43740 55760 9.21 24 7 ¹ / ₈	1117400 1676100 64600 8.65 39360 51570 10.83 24 1"	1245300 1868000 72600 8.58 45000 57370 10.85 24 1"	1374200 2061300 80800 8.51 49810 63180 10.88 24 1"	1579400 2369100 73100 10.80 45670 58730 13.45 24 1"	1766200 2694900 82600 10.70 51260 65470 13.49 24 1"	1953400 2930100 92400 10.57 57020 71580 13.64 24 1"								
	Total Deflection in inches for Maximum Load; Laterally fixed beam.	Total Deflection must not exceed 1/360 of the Span. Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$															
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.	Span feet	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free	Laterally fixed	Laterally free						
	4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30	115 115 115 115 106 95 85 77 71 65 61 57 53 50 47 45 43 41 39 37 36 35 34 33 32 31	115 115 115 115 106 95 85 76 68 61 57 50 46 42 39 35 33 31 28 26 24 22 20 19 18 17	128 128 128 128 128 104 94 84 75 72 66 59 55 52 49 46 43 41 39 37 35 34 32 31	128 128 128 128 128 114 104 84 75 74 68 61 56 51 47 43 40 37 34 31 29 27 25 24 22	141 141 141 141 141 114 104 93 84 86 78 73 66 60 55 51 47 44 41 39 37 35 34 32 31	141 141 141 141 129 129 129 129 129 124 125 113 104 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	129 129 129 129 129 138 125 113 104 95 88 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	145 145 145 145 145 138 125 113 104 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	162 162 162 162 162 153 137 125 113 104 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	162 162 162 162 162 153 137 125 113 104 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34		146 146 146 146 146 146 146 144 144 132 122 113 105 98 92 88 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	146 146 146 146 146 146 146 144 144 132 122 113 105 98 92 88 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	165 165 165 165 165 165 165 161 161 153 142 136 126 118 110 103 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	165 165 165 165 165 165 165 161 161 153 142 136 126 118 110 103 96 89 83 78 73 68 63 59 54 50 47 44 41 39 37 35 34	185 185 185 185 185 185 185 178 178 163 150 140 130 121 112 104 97 90 83 77 72 68 63 59 54 50 47 44 41 39 37 35 34

16"

C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

V is Maximum Web Shear in Pounds.

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $31\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

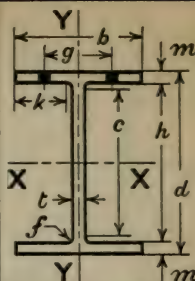
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".	15.930	16.012	16.000	*15.934	16.128	16.254	16.000	16.114	16.226											
Wt. per foot.	35.0	38.0	40.0	43.0	45.0	50.0	58.0	63.0	68.0											
Area.	10.29	11.17	11.75	12.65	13.23	14.70	17.06	18.52	20.00											
b"	6.000	6.024	7.000	7.085	7.036	7.072	8.500	8.531	8.563											
t.	.290	.314	.290	.375	.326	.362	.375	.406	.438											
h.	14 1/16	14 1/16	14 1/16	14 1/16	14 1/16	14 1/16	14 1/16	14 1/16	14 1/16											
m.	.485	.526	.520	.487	.584	.647	.663	.720	.776											
k.	2 3/8	2 3/8	2 7/8	2 7/8	2 7/8	2 7/8	3 7/16	3 7/16	3 7/16											
f.	.45	.45	.45	.45	.45	.45	.65	.65	.65											
c.	14"	14"	14"	14"	14"	14"	13 3/4"	13 3/4"	13 3/4"											
g.	3"	3"	4"	4"	4"	4"	5 1/2"	5 1/2"	5 1/2"											
A X E S																				
I . . .	435.5	475.1	524.6	523.8	595.0	666.0	776.6	849.9	923.7											
S . . .	54.68	59.34	65.58	65.75	73.78	81.95	97.08	105.49	113.85											
r . . .	6.50	6.52	6.68	6.44	6.71	6.73	6.75	6.77	6.80											
Y . Y .																				
I . . .	17.5	19.2	29.8	28.9	34.0	38.2	68.0	74.6	81.3											
S . . .	5.8	6.4	8.5	8.2	9.7	10.8	16.0	17.5	19.0											
r . . .	1.30	1.31	1.59	1.51	1.60	1.61	2.00	2.01	2.02											
Coef. Str.	656100	712100	786900	789000	885400	983400	1164900	1265800	1366200											
Max. Mom. %	984200	1068200	1180400	1183400	1328100	1475100	1747400	1898700	2049400											
V . . .	55400	60300	55700	71700	63100	70600	72000	78500	85300											
P. feet .	5.92	5.90	7.07	5.50	7.02	6.96	8.09	8.06	8.01											
R . . .	25990	29590	25970	38830	31390	36890	38840	43580	48480											
W . . .	26100	28260	26100	33750	29340	32580	67500	73080	78840											
Q. feet .	12.56	12.59	15.06	11.69	15.09	15.09	8.63	8.66	8.66											
w lbs. .	19	19	19	19	19	19	33	33	33											
Rivet dia.	7/8	7/8	7/8	7/8	7/8	7/8	7/8	7/8	7/8											
Span																				
feet																				
5	111	111	121	121	111	111	143	143	126	126	141	141	144	144	157	157	171	171		
6	109	109	118	118	111	111	132	132	126	126	141	141	144	144	157	157	171	171		
7	94	94	102	102	111	111	113	113	126	126	140	140	144	144	157	157	171	171		
8	82	81	89	88	98	98	99	99	111	111	123	123	144	144	157	157	171	171		
9	73	70	79	76	87	87	88	87	98	98	109	109	129	129	141	141	152	152		
10	66	61	71	66	79	77	79	77	89	86	98	95	117	117	127	127	137	137		
11	60	53	65	58	72	68	72	68	80	76	89	84	106	105	115	114	124	123		
12	55	47	59	51	66	61	66	61	74	68	82	76	97	94	106	102	114	111		
13	51	42	55	45	61	54	61	54	68	61	76	68	90	85	97	93	105	100		
14	47	37	51	41	56	48	56	49	63	54	70	61	83	77	90	84	98	91		
15	44	34	47	36	52	43	53	42	59	49	66	55	78	70	84	77	91	83		
16	41	30	44	33	49	40	49	40	55	45	61	50	73	65	79	70	85	76		
17	39	27	42	30	46	36	47	37	52	41	58	46	69	59	75	64	80	70		
18	37	25	40	27	44	33	44	33	49	37	55	42	65	54	70	59	76	64		
19	35	22	37	24	41	30	42	30	47	34	52	38	61	50	67	55	72	59		
20	33	20	36	22	39	27	40	28	44	31	49	35	58	46	63	50	68	55		
21	31	...	34	...	37	25	38	26	42	28	47	32	56	43	60	47	65	50		
22	30	...	32	...	36	23	36	24	40	26	45	29	53	40	58	43	62	47		
23	29	...	31	...	34	21	34	22	38	24	43	27	51	37	55	40	59	43		
24	27	...	30	...	33	...	33	...	37	...	41	...	49	34	53	37	57	40		
25	26	...	28	...	31	...	32	...	35	...	39	...	47	32	51	35	55	38		
26	25	...	27	...	30	...	30	...	34	...	38	...	45	30	49	33	53	35		
27	24	...	26	...	29	...	29	...	33	...	36	...	43	28	47	30	51	33		
28	24	...	25	...	28	...	28	...	32	...	35	...	42	26	45	28	49	31		
29	23	...	25	...	27	...	27	...	31	...	34	...	40	...	44	...	47	...		
30	22	...	24	...	26	...	26	...	30	...	33	...	39	...	42	...	46	...		
31	21	...	23	...	25	...	26	...	29	...	32	...	38	...	41	...	44	...		
32	21	...	22	...	25	...	25	...	28	...	31	...	36	...	40	...	43	...		
33	20	...	22	...	24	...	24	...	27	...	30	...	35	...	38	...	41	...		
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.																				

* Special Section, Web Thickness $\frac{3}{8}$ "

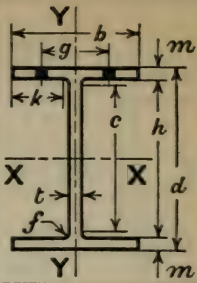
LOADS BY A. I. S. C. SPECIFICATION

18"
C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets
Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d"	18.000	*18.024	18.114	18.252
Wt. per foot.	47.0	51.0	52.0	58.0
Area.....	13.82	15.00	15.30	17.05
b".....	7.500	7.555	7.534	7.573
t.....	.320	.375	.354	.393
h.....	167/8	167/8	167/8	167/8
m.....	.550	.562	.607	.676
k.....	31/16	31/16	31/16	31/16
c.....	.50	.50	.50	.50
f.....	157/8	157/8	157/8	157/8
g.....	3/4	3/4	3/4	3/4
A X E S				
X · X	I..... 768.6	810.0	855.1	960.8
S.....	85.4	89.88	94.41	105.28
r.....	7.46	7.35	7.48	7.51
Y · Y	I..... 38.7	40.5	43.3	49.0
S.....	10.3	10.7	11.5	13.0
r.....	1.67	1.64	1.68	1.70
Coef. Str.....	1024800	1078600	1133000	1263400
Max Mom. * ..	1537200	1617800	1699400	1895100
V.....	69100	81100	77000	86100
P, feet.....	7.41	6.65	7.36	7.34
R.....	30170	39020	35610	41950
W.....	36000	42190	39830	44220
Q, feet.....	14.23	12.78	14.22	14.28
w lbs.....	25	25	25	25
Rivet dia.....	7/8	7/8	7/8	7/8

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. × Live Load / Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free	
	fixed	free	fixed	free	fixed	free	fixed	free
6	138	138	162	162	154	154	172	172
7	138	138	154	154	154	154	172	172
8	128	128	135	135	142	142	158	158
9	114	114	120	120	126	126	140	140
10	102	101	108	106	113	112	126	125
11	93	90	98	94	103	99	115	111
12	85	80	90	85	94	89	105	99
13	79	72	83	76	87	80	97	89
14	73	65	77	69	81	72	90	80
15	68	59	72	62	76	65	84	73
16	64	54	67	57	71	59	79	67
17	60	49	63	52	67	54	74	61
18	57	45	60	47	63	49	70	55
19	54	41	57	43	60	45	66	51
20	51	38	54	40	57	42	63	47
21	49	35	51	37	54	38	60	43
22	47	32	49	34	52	35	57	40
23	45	30	47	31	49	33	55	37
24	43	27	45	29	47	30	53	34
25	41	25	43	27	45	28	51	32
26	39	...	41	...	44	...	49	...
27	38	...	40	...	42	...	47	...
28	37	...	39	...	40	...	45	...
29	35	...	37	...	39	...	44	...
30	34	...	36	...	38	...	42	...
31	33	...	35	...	37	...	41	...
32	32	...	34	...	35	...	39	...
33	31	...	33	...	34	...	38	...
34	30	...	32	...	33	...	37	...
35	29	...	31	...	32	...	36	...

* Special Section. Web Thickness 3/8"

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

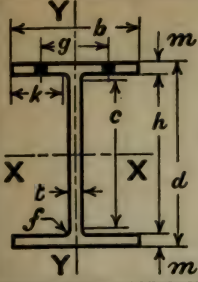
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.

18"
C



Depth = d".	18.000	18.110	18.242	18.000	18.120	18.238
Wt. per foot.	67.0	72.0	78.0	86.0	93.0	100.0
Area.....	19.69	21.17	22.94	25.29	27.35	29.40
b".	8.500	8.530	8.565	12.000	12.034	12.069
t.....	.406	.436	.471	.429	.463	.498
h.....	16½	16½	16½	16½	16½	16½
m.....	.745	.800	.866	.745	.805	.864
c.....	3¾	3¾	3¾	5½	5½	5½
f.....	.70	.70	.70	.70	.70	.70
d.....	15½	15½	15½	15½	15½	15½
g.....	5½	5½	5½	7½	7½	7½
A X E S	I.....	1117.1	1208.1	1318.8	1514.1	1783.4
	X-X.....	124.12	133.42	144.59	168.23	195.57
	r.....	7.53	7.55	7.58	7.74	7.79
Y Y	I.....	76.4	82.9	90.9	214.7	234.0
	S.....	18.0	19.4	21.2	35.8	38.9
	r.....	1.97	1.98	1.99	2.91	2.93
Coef. Str.....	1489500	1601000	1735100	2018800	2183300	2346800
Max. M. m. %	2234200	2401500	2602600	3028200	3275000	3520200
V.....	87700	94800	103100	92700	100700	109000
P. feet.....	8.49	8.45	8.41	10.89	10.84	10.77
R.....	44040	48930	54670	47760	53310	59040
Q.....	91350	98100	105980	96530	104180	112050
W. feet.....	8.15	8.16	8.18	10.46	10.48	10.47
w lbs.....	41	41	41	41	41	41
Rivet dia....	7/8	7/8	7/8	1"	1"	1"

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. x Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free	
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
6	175	175	190	190	206	206	185	185	201	201	218	218	218	218	218	218
7	175	175	190	190	206	206	185	185	201	201	218	218	218	218	218	218
8	175	175	190	190	206	206	185	185	201	201	218	218	218	218	218	218
9	165	165	178	178	193	193	185	185	201	201	218	218	218	218	218	218
10	149	149	160	160	174	174	185	185	201	201	218	218	218	218	218	218
11	135	134	146	144	158	156	184	184	198	198	213	213	213	213	213	213
12	124	120	133	130	145	141	168	168	182	182	196	196	196	196	196	196
13	115	109	123	117	133	127	155	155	168	168	181	181	181	181	181	181
14	106	99	114	106	124	116	144	144	156	156	168	168	168	168	168	168
15	99	90	107	97	116	105	135	135	146	146	156	156	156	156	156	156
16	93	83	100	89	108	96	126	124	136	134	144	144	144	144	144	144
17	88	76	94	81	102	88	119	115	128	125	138	138	138	138	138	138
18	83	69	89	75	96	81	112	107	121	116	130	125	135	135	135	135
19	78	64	84	69	91	75	106	100	115	108	124	116	132	132	132	132
20	74	59	80	64	87	69	101	93	109	101	117	109	125	125	125	125
21	71	55	76	59	83	64	96	88	104	95	112	102	122	122	122	122
22	68	51	73	55	79	60	92	82	99	89	107	96	119	119	119	119
23	65	47	70	51	75	55	88	77	95	83	102	90	116	116	116	116
24	62	44	67	47	72	51	84	73	91	78	98	85	113	113	113	113
25	60	41	64	44	69	48	81	68	87	74	94	80	110	110	110	110
26	57	38	62	41	67	45	78	64	84	70	90	75	107	107	107	107
27	55	36	59	38	64	42	75	61	81	66	87	71	104	104	104	104
28	53	33	57	36	62	39	72	58	78	62	84	67	101	101	101	101
29	51	...	55	...	60	...	70	54	75	59	81	64	98	98	98	98
30	50	...	53	...	58	...	67	52	73	56	78	60	96	96	96	96
31	48	...	52	...	56	...	65	49	70	53	76	57	94	94	94	94
32	47	...	50	...	54	...	63	46	68	50	73	54	92	92	92	92
33	45	...	49	...	53	...	61	...	66	...	71	...	90	90	90	90
34	44	...	47	...	51	...	59	...	64	...	69	...	88	88	88	88
35	43	...	46	...	50	...	58	...	62	...	67	...	86	86	86	86
36	41	...	44	...	48	...	56	...	61	...	65	...	84	84	84	84

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

21" C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details,

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

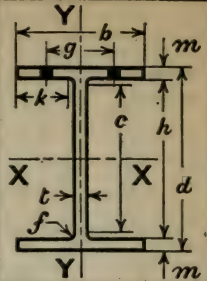
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d"	20.890	21.000	21.126	21.248	21.370					
Wt. per foot.	55.0	58.0	64.0	70.0	76.0					
Area	16.17	17.05	18.82	20.59	22.34					
b	8.000	8.000	8.036	8.073	8.109					
t	.360	.360	.396	.433	.469					
h	19 $\frac{3}{4}$	19 $\frac{3}{4}$	19 $\frac{3}{4}$	19 $\frac{3}{4}$	19 $\frac{3}{4}$					
m	.553	.608	.671	.732	.793					
k	3 $\frac{1}{4}$	3 $\frac{1}{4}$	3 $\frac{1}{4}$	3 $\frac{1}{4}$	3 $\frac{1}{4}$					
f	.55	.55	.55	.55	.55					
c	18 $\frac{5}{8}$	18 $\frac{5}{8}$	18 $\frac{5}{8}$	18 $\frac{5}{8}$	18 $\frac{5}{8}$					
g	4"	4"	4"	4"	4"					
AXES	I	1166.7	1263.2	1403.3	1542.9	1684.0				
	S	111.70	120.30	132.85	145.23	157.60				
	r	8.49	8.61	8.64	8.66	8.68				
Y-Y	I	47.29	52.0	58.2	64.3	70.67				
	S	11.8	13.0	14.5	15.9	17.4				
	r	1.71	1.75	1.76	1.77	1.78				
Coef. Str.	1340400	1443600	1594200	1742700	1891200					
Max. Mom. *#	2010600	2165500	2391300	2614100	2836900					
V	90240	90700	100400	110400	120300					
P, feet	7.43	7.96	7.94	7.89	7.86					
R	36210	36180	42460	49010	55460					
W	48600	48600	53460	58460	63320					
Q, feet	13.79	14.85	14.91	14.91	14.93					
w, lbs.	30	30	30	30	30					
Rivet dia.	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$					
Span	Laterally		Laterally		Laterally		Laterally		Laterally	
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed
7	180	180	181	181	201	201	221	221	241	241
8	168	168	180	180	199	199	218	218	236	236
9	149	149	160	160	177	177	194	194	210	210
10	134	134	144	144	159	159	174	174	189	189
11	122	119	131	128	145	142	158	156	172	169
12	112	107	120	115	133	127	145	139	158	151
13	103	96	111	104	123	115	134	126	145	136
14	96	87	103	94	114	104	124	114	135	124
15	89	79	96	85	106	94	116	103	126	112
16	84	72	90	78	100	86	109	94	118	102
17	79	66	85	71	94	79	103	86	111	94
18	74	61	80	65	89	72	97	79	105	86
19	71	56	76	60	84	67	92	73	100	79
20	67	51	72	55	80	61	87	67	95	73
21	64	47	69	51	76	57	83	62	90	68
22	61	44	66	47	72	52	79	57	86	63
23	58	41	63	44	69	49	76	53	82	58
24	56	38	60	41	66	45	73	49	79	54
25	54	35	58	38	64	42	70	46	76	50
26	52	33	56	35	61	39	67	43	73	46
27	50	31	53	33	59	37	65	41	70	44
28	48	29	50	31	57	35	62	39	68	42
29	46	27	48	29	55	33	60	37	65	40
30	45	26	47	28	53	32	58	36	63	39
32	42	24	44	26	50	30	54	34	60	37
34	39	22	41	24	47	28	51	32	56	35
36	37	21	40	23	44	27	48	31	53	34
38	35	20	38	22	42	26	46	30	50	33
40	33	19	36	21	40	25	44	29	47	32
42	32	18	34	20	38	24	41	28	45	31
Total Deflection must not exceed 1/360 of the Span.										
Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$										
Total Deflection in inches for Maximum Load; Laterally fixed beam.										

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

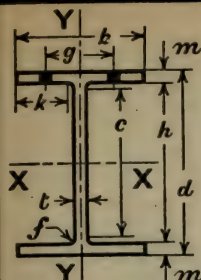
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

21"
C

Depth = d". Wt. per foot. Area. b". t. h. m. k. f. c. g.	21.000	21.120	21.240	21.358	21.000	21.126	21.248	21.372	21.492	Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. x Live Load Tabular Load		
	80.0	86.0	92.0	98.0	104.0	112.0	120.0	128.0	136.0			
	23.53	25.28	27.05	28.82	30.57	32.93	35.28	37.65	40.00			
	9.000	9.032	9.064	9.097	13.000	13.034	13.070	13.105	13.141			
	.438	.470	.502	.535	.465	.499	.535	.570	.606			
	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆	195 ¹ / ₁₆			
	.815	.875	.935	.994	.815	.878	.939	1.001	1.061			
	3 ¹ / ₂	3 ¹ / ₂	3 ¹ / ₂	3 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂			
	.75	.75	.75	.75	.75	.75	.75	.75	.75			
	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈	17 ⁷ / ₈			
5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	7 ¹ / ₂	7 ¹ / ₂	7 ¹ / ₂	7 ¹ / ₂	7 ¹ / ₂				
AXES	X-X	I.....	1794.4	1939.3	2086.4	2234.5	2475.3	2683.7	2890.9	3103.4	3313.7	
	S.....	r.....	170.90	183.65	196.46	209.24	235.74	254.07	272.11	290.42	308.37	
			8.73	8.76	8.78	8.80	9.00	9.03	9.05	9.08	9.10	
	Y-Y	I.....	99.2	107.7	116.3	125.0	298.7	324.3	349.7	375.9	401.7	
	S.....	r.....	22.0	23.8	25.7	27.5	45.9	49.8	53.5	57.4	61.1	
			2.05	2.06	2.07	2.08	3.13	3.14	3.15	3.16	3.17	
Coef. Str.			2050700	2203700	2357500	2510900	2828900	3048800	3265300	3485000	3700400	
Max. Mom. #s			3076100	3305600	3536300	3766400	4243400	4573200	4898000	5227500	5550600	
V.			110400	119100	128000	137100	117200	126500	136400	146200	156300	
P. feet.			9.29	9.25	9.21	9.16	12.07	12.05	11.97	11.92	11.84	
R.			49880	55580	61320	67260	54660	60730	67190	73500	80020	
W.			59130	63450	67770	71580	104630	112280	119300	126300	133000	
Q. feet.			17.34	17.37	17.39	17.54	13.52	13.58	13.69	14.61	15.51	
w. lbs.			30	30	30	30	41	41	41	41	41	
Rivet dia.			⁷ / ₈	⁷ / ₈	⁷ / ₈	⁷ / ₈	1"	1"	1"	1"	1"	
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.	Span	feet	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Total Deflection in inches for Maximum Load; Laterally fixed beam.	
			fixed	free	fixed	free	fixed	free	fixed	free		
	7	221	221	238	238	256	256	274	274	234		234
	8	221	221	238	238	256	256	274	274	234		234
	9	221	221	238	238	256	256	274	274	234		234
	10	205	205	220	220	236	236	251	251	234		234
	11	186	186	200	200	214	214	228	228	234		234
	12	171	168	184	181	196	194	209	207	234		234
	13	158	153	170	164	181	175	193	187	218		218
	14	146	138	157	149	168	160	179	170	202		202
15	137	127	147	136	157	146	167	156	189	189		
16	128	116	138	125	147	134	157	143	177	177		
17	121	106	130	115	139	123	148	131	166	164		
18	114	98	122	106	131	114	139	121	157	154		
19	108	91	116	98	124	105	132	112	149	143		
20	103	84	110	91	118	97	126	103	141	134		
21	98	78	105	84	112	90	120	96	135	126		
22	93	73	100	78	107	83	114	89	129	119		
23	89	67	96	73	103	78	109	83	123	111		
24	85	63	92	67	98	73	105	77	118	105		
25	82	59	88	63	94	68	100	72	113	99		
26	79	55	85	59	91	63	97	68	109	94		
27	76	51	82	55	87	59	93	63	105	89		
28	73	48	79	52	84	56	90	59	101	84		
29	71	45	76	48	81	52	87	56	98	80		
30	68	42	73	46	79	49	84	52	94	76		
32	64	..	69	..	74	..	78	..	88	68		
34	60	..	65	..	69	..	74	..	83	62		
36	57	..	61	..	65	..	70	..	79	56		
38	54	..	58	..	62	..	66	..	74	..		
40	51	..	55	..	59	..	63	..	71	..		
42	49	..	52	..	56	..	60	..	67	..		
44	47	..	50	..	54	..	58	..	65	..		
46	45	..	48	..	52	..	56	..	63	..		
48	43	..	46	..	50	..	54	..	61	..		
50	41	..	44	..	48	..	52	..	59	..		
52	39	..	42	..	46	..	50	..	57	..		
54	37	..	40	..	44	..	48	..	55	..		
56	35	..	38	..	42	..	46	..	53	..		
58	33	..	36	..	40	..	44	..	51	..		
60	31	..	34	..	38	..	42	..	49	..		
62	29	..	32	..	36	..	40	..	47	..		
64	27	..	30	..	34	..	38	..	45	..		
66	25	..	28	..	32	..	36	..	43	..		
68	23	..	26	..	30	..	34	..	41	..		
70	21	..	24	..	28	..	32	..	39	..		
72	19	..	22	..	26	..	30	..	37	..		
74	17	..	20	..	24	..	28	..	35	..		
76	15	..	18	..	22	..	26	..	33	..		
78	13	..	16	..	20	..	24	..	31	..		
80	11	..	14	..	18	..	22	..	29	..		
82	9	..	12	..	16	..	20	..	27	..		
84	7	..	10	..	14	..	18	..	25	..		
86	5	..	8	..	12	..	16	..	23	..		
88	3	..	6	..	10	..	14	..	21	..		
90	1	..	4	..	8	..	12	..	19	..		
92	0	..	2	..	6	..	10	..	17	..		
94	0	..	0	..	4	..	8	..	15	..		
96	0	..	0	..	2	..	6	..	13	..		
98	0	..	0	..	0	..	4	..	11	..		
100	0	..	0	..	0	..	2	..	9	..		
102	0	..	0	..	0	..	0	..	7	..		
104	0	..	0	..	0	..	0	..	5	..		
106	0	..	0	..	0	..	0	..	3	..		
108	0	..	0	..	0	..	0	..	1	..		
110	0	..	0	..	0	..	0	..	0	..		
112	0	..	0	..	0	..	0	..	0	..		
114	0	..	0	..	0	..	0	..	0	..		
116	0	..	0	..	0	..	0	..	0	..		
118	0	..	0	..	0	..	0	..	0	..		
120	0	..	0	..	0	..	0	..	0	..		
122	0	..	0	..	0	..	0	..	0	..		
124	0	..	0	..	0	..	0	..	0	..		
126	0	..	0	..	0	..	0	..	0	..		
128	0	..	0	..	0	..	0	..	0	..		
130	0	..	0	..	0	..	0	..	0	..		
132	0	..	0	..	0	..	0	..	0	..		
134	0	..	0	..	0	..	0	..	0	..		
136	0	..	0	..	0	..	0	..	0	..		
138	0	..	0	..	0	..	0	..	0	..		
140	0	..	0	..	0	..	0	..	0	..		
142	0	..	0	..	0	..	0	..	0	..		
144	0	..	0	..	0	..	0	..	0	..		
146	0	..	0	..	0	..	0	..	0	..		
148	0	..	0	..	0	..	0	..	0	..		
150	0	..	0	..	0	..	0	..	0	..		
152	0	..	0	..	0	..	0	..	0	..		
154	0	..	0	..	0	..	0	..	0	..		
156	0	..	0	..	0	..	0	..	0	..		
158	0	..	0	..	0	..	0	..	0	..		
160	0	..	0	..	0	..	0	..	0	..		
162	0	..	0	..	0	..	0	..	0	..		
164	0	..	0	..	0	..	0	..	0	..		
166	0	..	0	..	0	..	0	..	0	..		
168	0	..	0	..	0	..	0	..	0	..		
170	0	..	0	..	0	..	0	..	0	..		
172	0	..	0	..	0	..	0	..	0	..		
174	0	..	0	..	0	..	0	..	0	..		
176	0	..	0	..	0	..	0	..	0	..		
178	0	..	0	..	0	..	0	..	0	..		
180	0	..	0	..	0	..	0	..	0	..		
182	0	..	0	..	0	..	0	..	0	..		
184	0	..	0	..	0	..	0	..	0	..		
186	0	..	0	..	0	..	0	..	0	..		
188	0	..	0	..	0	..	0	..	0	..		
190	0	..	0	..	0	..	0	..	0	..		
192	0	..	0	..	0	..	0	..	0	..		
194	0	..	0	..	0	..	0	..	0	..		
196	0	..	0	..	0	..	0	..	0	..		
198	0	..	0	..	0	..	0	..	0	..		
200	0	..	0	..	0	..	0	..	0	..		
202	0	..	0	..	0	..	0	..	0	..		
204	0	..	0	..	0	..	0	..	0	..		
206	0	..	0	..	0	..	0	..	0	..		
208	0	..	0	..	0	..	0	..	0	..		
210	0	..	0	..	0	..	0	..	0	..		
212	0	..	0	..	0	..	0	..	0	..		
214	0	..	0	..	0	..	0	..	0	..		
216	0	..	0	..	0	..	0	..	0	..		
218	0	..	0	..	0	..	0	..	0	..		
220	0	..	0	..	0	..	0	..	0	..		
222	0	..	0	..	0	..	0	..				

24" C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia **S** is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for 3½" bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

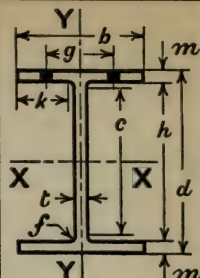
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Depth = d".		24.000		24.000		24.154		24.308		Live Load deflection must not exceed 1/360 of the Span.	Total Def. x Live Load	Tabular Load			
Wt. per foot.		70.0		76.0		85.0		94.0							
Area.....		20.58		22.35		24.99		27.64							
b.....		8.500		9.750		9.797		9.844							
t.....		.400		.405		.452		.499							
h.....		22 ⁵ / ₈		22 ⁵ / ₈		22 ⁵ / ₈		22 ⁵ / ₈							
m.....		.663		.663		.740		.817							
k.....		37 ¹ / ₁₆		41 ¹ / ₁₆		41 ¹ / ₁₆		41 ¹ / ₁₆							
f.....		.60		.60		.60		.60							
c.....		21 ³ / ₈		21 ³ / ₈		21 ³ / ₈		21 ³ / ₈							
g.....		4		5 ¹ / ₂		5 ¹ / ₂		5 ¹ / ₂							
A X E S	X - X	I....	1953.8		2184.4		2457.2		2734.9	Live Load deflection must not exceed 1/360 of the Span.	Total Def. x Live Load	Tabular Load			
	X - X	S....	162.82		182.03		203.46		225.02						
	X - X	r....	9.74		9.89		9.92		9.95						
A X E S	Y - Y	I....	68.0		102.6		116.2		130.2	Live Load deflection must not exceed 1/360 of the Span.	Total Def. x Live Load	Tabular Load			
	Y - Y	S....	16.0		21.0		23.7		26.4						
	Y - Y	r....	1.82		2.14		2.16		2.17						
Coef. Str....		1953800		2184400		2441500		2700200		Total Deflection in inches for Maximum Load; Laterally fixed beam.					
Max.Mom.#		2930700		3276600		3662300		4050400							
V.....		115200		116600		131000		145600							
P. feet..		8.48		9.36		9.32		9.27							
R.....		42750		43680		52580		61640							
W.....		54000		54680		61020		67370							
Q. feet..		18.09		19.97		20.00		20.04							
w lbs....		30		30		30		30							
Rivet dia....		7/8		7/8		7/8		7/8							
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally					Total Deflection in inches for Maximum Load; Laterally fixed beam.		
	feet	fixed	free	fixed	free	fixed	free	fixed	free						
	8	230	230	233	233	262	262	291	291	.078					
	10	195	195	218	218	244	244	270	270						
	12	163	158	182	182	203	203	225	225				.112		
	14	140	130	156	151	174	169	193	187						
	16	122	108	137	127	153	142	169	158				.199		
	18	109	91	121	108	136	121	150	134						
	20	98	78	109	93	122	104	135	115				.310		
	21	93	72	104	87	116	97	129	108						
	22	89	67	99	81	111	90	123	100				.375		
	23	85	62	95	75	106	84	117	94						
24	81	57	91	70	102	79	113	88	.447						
25	78	54	87	66	98	74	108	82							
	26	75	50	84	62	94	69	104	77	.525					
	27	72	47	81	58	90	65	100	72						
	28	70	44	78	54	87	61	96	68	.608					
	29	67	...	75	51	84	57	93	64						
	30	65	...	73	48	81	54	90	60	.698					
	31	63	...	70	45	79	51	87	57						
	32	61	...	68	43	76	48	84	53	.795					
	33	59	...	66	...	74	...	82	...						
	34	57	...	64	...	72	...	79897					
	35	56	...	62	...	70	...	77	...						
	36	54	...	61	...	68	...	75	...	1.01					
	38	51	...	57	...	64	...	71	...						
	40	49	...	55	...	61	...	68	...	1.24					
	42	47	...	52	...	58	...	64	...						
	44	44	...	50	...	55	...	61	...	1.50					
	46	42	...	47	...	53	...	59	...						
	48	41	...	46	...	51	...	56	...	1.79					
	50	39	...	44	...	49	...	54	...						

LOADS BY A. I. S. C. SPECIFICATION

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.

24"

C

Depth = d"	24 000	24 156	24 310	24 250	24 388	24 526	24 664
Wt. per foot.	100 0	110 0	120 0	130 0	140 0	150 0	160 0
Area	29 41	32 34	35 29	38 23	41 16	44 10	47 06
b	12 000	12 044	12 089	14 000	14 041	14 082	14 123
t	450	494	539	547	588	629	670
h	22½	22½	22½	22½	22½	22½	22½
m	.787	.865	.942	.912	.981	1 050	1 119
k	5°	5°	5°	5½/16	5½/16	5½/16	5½/16
c	80	80	80	80	80	80	80
f	20¾	20¾	20¾	20¾	20¾	20¾	20¾
g	7½	7½	7½	10"	10"	10"	10"
A X E S	I	3020 5	3343 5	3669 7	4045 1	4380 4	4720 5
	X	251 71	276 83	301 91	333 62	359 23	384 94
	r	10 14	10 17	10 20	10 29	10 32	10 35
Y	I	226 9	252 2	277 8	417 5	453 1	489 3
	X	37 8	41 9	46 0	59 6	64 5	69 5
	r	2 78	2 79	2 81	3 31	3 32	3 33
Coef. Str.	3020500	3321900	3622900	4003400	4310700	4619300	4929300
Max. Mom. %	4530700	4982900	5434300	6005100	6466100	6928900	7394000
V	129600	143200	157200	159200	172100	185100	198300
P. feet.	11 65	11 60	11 52	12 57	12 52	12 47	12 43
R.	52200	66650	69400	70920	78940	87000	95100
Q.	121500	133380	143160	143160	143160	143160	143160
W. feet.	12 43	12 45	12 65	13 98	15 06	16 13	17 22
w lbs.	49	49	49	49	49	49	49
Rivet dia.	1"	1"	1"	1"	1"	1"	1"

Live Load deflection must not exceed 1/360 of the Span.

Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Total Deflection in inches for Maximum Load: Laterally fixed beam.

Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally	
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed
8	259	259	286	286	314	314	318	318	344	344	370	370	397	397
10	259	259	286	286	314	314	318	318	344	344	370	370	397	397
12	252	252	277	277	302	302	318	318	344	344	370	370	397	397
14	216	216	237	237	259	259	286	286	308	308	330	330	352	352
16	189	186	208	205	226	223	250	250	269	269	289	289	308	308
18	168	160	185	176	201	193	222	221	239	238	257	255	274	273
20	151	140	166	154	181	168	200	194	216	209	231	224	246	239
21	144	131	158	144	173	158	191	182	205	196	220	210	235	225
22	137	123	151	135	165	148	182	172	196	185	210	198	224	212
23	131	115	144	127	158	139	174	162	187	174	201	188	214	200
24	126	109	138	119	151	131	167	153	180	165	192	177	205	189
25	121	102	133	112	145	123	160	145	172	156	185	167	197	179
26	116	96	128	106	139	116	154	137	166	148	178	158	190	170
27	112	91	123	100	134	110	148	130	160	140	171	150	183	160
28	108	86	119	95	129	104	143	123	154	133	165	143	176	153
29	104	81	115	90	125	98	138	117	149	126	159	135	170	145
30	101	77	111	85	121	93	133	111	144	121	154	129	164	138
31	97	73	107	80	117	88	129	106	139	114	149	123	159	131
32	94	69	104	75	113	84	125	101	135	109	144	117	154	125
33	92	66	101	71	110	79	121	96	131	104	140	112	149	119
34	89	63	98	68	107	75	118	92	127	99	136	106	145	113
35	86	59	95	64	104	72	114	88	123	94	132	102	141	108
36	84	57	92	61	101	68	111	84	120	90	128	97	137	104
38	79	51	87	55	95	62	105	77	113	82	122	88	130	95
40	76	47	83	...	91	56	100	70	108	75	115	80	123	87
42	72	...	79	...	86	...	95	64	103	69	110	75	117	80
44	69	...	75	...	82	...	91	...	98	...	105	...	112	73
46	66	...	72	...	79	...	87	...	94	...	100	...	107	...
48	63	...	69	...	75	...	83	...	90	...	96	...	103	...
50	60	...	66	...	72	...	80	...	86	...	92	...	99	...

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.

For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

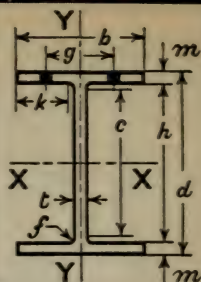
152
.199
.251
.310
.342
.375
.411
.447
.485
.525
.566
.608
.653
.698
.746
.795
.845
.897
.950
1.01
1.12
1.24
1.37
1.50
1.64
1.79
1.94

C

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.



Depth = d".		26.820	27.000	27.166	27.340	27.536	27.742			
Wt. per foot.		85.0	91.0	101.0	112.0	124.0	137.0			
Area.		25.00	26.76	29.70	32.94	36.47	40.29			
b".		9.750	9.750	9.799	9.855	9.913	9.977			
t.....		.461	.461	.510	.566	.624	.688			
h.....		257 ¹ / ₁₆	257 ¹ / ₁₆	257 ¹ / ₁₆	257 ¹ / ₁₆	257 ¹ / ₁₆	257 ¹ / ₁₆			
m.....		.665	.755	.838	.925	1.023	1.126			
k.....		4"	4"	4"	4"	4"	4"			
f.....		.65	.65	.65	.65	.65	.65			
c.....		24 ¹ / ₂	24 ¹ / ₂	24 ¹ / ₂	24 ¹ / ₂	24 ¹ / ₂	24 ¹ / ₂			
g.....		5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂	5 ¹ / ₂			
A X E S	I.....	2899.3	3217.0	3595.7	4007.6	4472.1	4975.9			
	S.....	216.20	238.30	264.72	293.17	324.82	358.73			
	r.....	10.77	10.97	11.00	11.03	11.07	11.11			
Y - Y	I.....	103.0	116.9	131.7	148.0	166.7	187.1			
	S.....	21.1	24.0	26.9	30.0	33.6	37.5			
	r.....	2.03	2.09	2.11	2.12	2.14	2.16			
Coef. Str.....		2594500	2859500	3176600	3518000	3897800	4304700			
Max.Mom. %		3891700	4289300	4765000	5277000	5846700	6457100			
V.....		148400	149400	166300	185700	206200	229000			
P. feet.....		8.74	9.57	9.55	9.47	9.45	9.40			
R.....		54140	54120	64140	75810	88050	101660			
W.....		82980	82980	91800	95440	95440	95440			
Q. feet.....		15.63	17.23	17.30	18.43	20.42	22.55			
w lbs.....		40	40	40	40	40	40			
Rivet dia.....		1"	1"	1"	1"	1"	1"			
Span	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Total Deflection in Inches for Maximum Load; Laterally fixed beam.		
	feet	fixed free	fixed free	fixed free	fixed free	fixed free	fixed free			
8	297	297	299	299	333	333	371	412	458	458
10	259	259	286	286	318	318	352	352	390	423
12	216	216	238	238	265	265	293	293	325	352
14	185	179	204	198	227	219	251	244	278	302
16	162	151	179	166	199	185	220	206	244	264
18	144	128	159	141	176	158	195	175	217	235
20	130	111	143	122	159	136	176	151	195	211
21	124	103	136	114	151	126	168	140	186	201
22	118	96	130	106	144	118	160	131	177	192
23	113	90	124	99	138	110	153	122	169	184
24	108	84	119	92	132	102	147	114	162	176
25	104	78	114	86	127	96	141	107	156	169
26	100	73	110	81	122	90	135	100	150	163
27	96	69	106	76	118	85	130	94	144	157
28	93	65	102	71	113	79	126	88	139	151
29	89	61	99	67	110	75	121	83	134	146
30	86	57	95	63	106	70	117	78	130	141
31	84	54	92	59	102	65	113	74	126	136
32	81	51	89	56	99	62	110	69	122	132
33	79	48	87	53	96	59	107	66	118	128
34	76	45	84	50	93	56	103	63	115	124
35	74	43	82	48	91	54	101	61	111	121
36	72	41	79	46	88	52	98	59	108	117
38	68	37	75	42	84	48	93	55	103	111
40	65	34	71	39	79	45	88	52	97	106
42	62	31	68	36	76	42	84	49	93	101
44	59	28	65	33	72	39	80	46	89	96
46	56	25	62	30	69	36	76	43	85	92
48	54	23	60	28	66	34	73	41	81	88
50	52	21	57	26	64	32	70	39	78	85
Live Load Def. = Total Def. x Live Load										
Tabular Load										
Live Load deflection must not exceed 1/360 of the Span.										

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

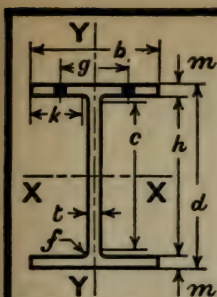
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

27"
C

Depth = d".		27.000	27.200	27.400	27.598
Wt. per foot.		145.0	160.0	175.0	190.0
Area.		42.64	47.04	51.47	55.87
b".		14.000	14.059	14.118	14.176
t".		.580	.639	.698	.756
h.		25"	25"	25"	25"
m.		.985	1.085	1.185	1.284
k.		5 13/16"	5 13/16"	5 13/16"	5 13/16"
f.		.90	.90	.90	.90
c.		23 1/4	23 1/4	23 1/4	23 1/4
g.		10	10	10	10
AXES					
I....		5508.7	6121.8	6746.8	7376.9
S....		408.05	450.13	492.47	534.60
r....		11.37	11.41	11.45	11.49
I....		451.0	503.2	556.6	610.7
S....		64.4	71.6	78.9	86.2
r....		3.25	3.27	3.29	3.31
Coef. Str.		4896600	5401600	5909600	6415200
Max.Mom.*'		7344900	8102400	8864400	9622700
V.		187900	208600	229500	250400
P. feet.		13.03	12.95	12.88	12.81
R.		78620	90990	103470	115800
W.		167020	167020	167020	167020
Q. feet.		14.66	16.17	17.69	19.20
w lbs.		58	58	58	58
Rivet dia.		1"	1"	1"	1"
Span					
feet					
Laterally					
fixed free					
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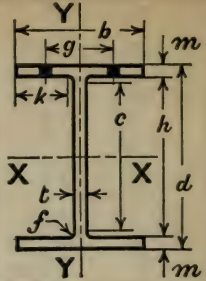
30"
C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds.
P is Minimum Span in feet, uniformly loaded to cause V.
R is Allowable End Reaction for 3½" bearing. For details see page of Allowable End Reactions.
W is Maximum Load on one Standard Connection.
Q is Minimum Span in feet, uniformly loaded to cause W.
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.



Depth = d"	30.000	30.162	30.344	30.538	30.742
Wt. per foot.	115.0	126.0	138.0	151.0	165.0
Area.....	33.81	37.05	40.58	44.41	48.52
b"	10.500	10.551	10.604	10.662	10.725
t.....	.530	.581	.634	.692	.755
h.....	283 ¹ / ₁₆	283 ¹ / ₁₆	283 ¹ / ₁₆	283 ¹ / ₁₆	283 ¹ / ₁₆
m.....	.882	.963	1.054	1.151	1.253
k.....	45 ¹ / ₁₆	45 ¹ / ₁₆	45 ¹ / ₁₆	45 ¹ / ₁₆	45 ¹ / ₁₆
c.....	.70	.70	.70	.70	.70
f.....	263 ¹ / ₄	263 ¹ / ₄	263 ¹ / ₄	263 ¹ / ₄	263 ¹ / ₄
g.....	5½	5½	5½	5½	5½
I.....	4985.3	5486.7	6049.5	6663.7	7326.7
X - X	332.35	363.82	398.73	436.42	476.66
S.....	12.14	12.17	12.21	12.25	12.29
Y - Y	170.6	189.0	210.1	233.4	258.7
S.....	32.5	35.8	39.6	43.8	48.2
r.....	2.25	2.26	2.28	2.29	2.31
Coef. Str....	3988200	4365800	4784700	5237000	5719900
Max. Mom. %	5982400	6548700	7177100	7855600	8579900
V.....	190800	210300	230900	253600	278500
P. feet.....	10.45	10.38	10.36	10.33	10.27
R.....	68410	79670	91550	104700	119090
Q.....	107330	107370	107370	107370	107370
W. feet.....	18.58	20.33	22.28	24.38	26.64
w lbs.....	45	45	45	45	45
Rivet dia....	1"	1"	1"	1"	1"

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. × Live Load Tabular Load

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Span feet	Laterally fixed		Laterally free		Laterally fixed		Laterally free		Laterally fixed		Laterally free		Total Deflection in inches for Maximum Load; Laterally fixed beam.
	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	
10	382	382	421	421	462	462	507	507	557	557			
12	332	332	364	364	399	399	436	436	477	477			
14	285	281	312	307	342	338	374	370	409	404			.122
16	249	237	273	260	299	286	327	313	358	342			.159
18	222	203	243	223	266	245	291	268	318	293			.201
20	199	176	218	193	239	211	262	232	286	254			.248
21	190	164	208	179	228	197	249	216	272	237			.274
22	181	153	198	168	217	184	238	202	260	222			.300
23	173	143	190	157	208	173	228	189	249	208			.329
24	166	134	182	147	199	162	218	178	238	195			.358
25	160	126	175	138	191	152	209	166	229	183			.388
26	153	118	168	130	184	142	201	157	220	172			.420
27	148	111	162	122	177	134	194	147	212	162			.452
28	142	105	156	115	171	126	187	139	204	153			.487
29	138	98	151	108	165	119	181	131	197	143			.522
30	133	93	145	102	159	112	175	124	191	136			.559
31	129	88	141	97	154	106	169	116	185	128			.596
32	125	83	136	91	150	100	164	110	179	121			.636
33	121	78	132	86	145	95	159	104	173	114			.676
34	117	74	128	81	141	90	154	99	168	109			.718
35	114	70	125	77	137	85	150	93	163	103			.760
36	111	...	121	...	133	...	145	...	159804
38	105	...	115	...	126	...	138	...	151896
40	100	...	109	...	120	...	131	...	143993
42	95	...	104	...	114	...	125	...	136	...			1.10
44	91	...	99	...	109	...	119	...	130	...			1.20
46	87	...	95	...	104	...	114	...	124	...			1.31
48	83	...	91	...	100	...	109	...	119	...			1.43
50	80	...	87	...	96	...	105	...	114	...			1.55
52	77	...	84	...	92	...	101	...	110	...			1.68

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

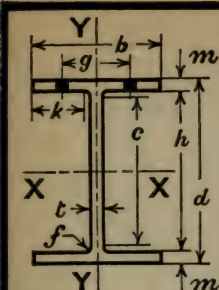
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.

30"
C



Depth = d".		30.000	30.263	30.522	30.781				
Wt. per foot.		180.0	200.0	220.0	240.0				
Area		52.93	58.82	64.70	70.58				
b"		14.000	14.073	14.146	14.218				
t		.670	.743	.816	.888				
h		27 ⁹ / ₁₆	27 ⁹ / ₁₆	27 ⁹ / ₁₆	27 ⁹ / ₁₆				
m		1.207	1.338	1.468	1.597				
k		5 ¹¹ / ₁₆	5 ¹¹ / ₁₆	5 ¹¹ / ₁₆	5 ¹¹ / ₁₆				
f		1.00	1.00	1.00	1.00				
c		25 ¹ / ₂	25 ¹ / ₂	25 ¹ / ₂	25 ¹ / ₂				
g		10 ⁷ / ₈	10 ⁷ / ₈	10 ⁷ / ₈	10 ⁷ / ₈				
A X E S	I	8301.4	9305.7	10320.4	11356.0				
	S	553.43	614.99	676.26	737.86				
	r	12.52	12.58	12.63	12.69				
Y - Y	I	552.7	622.7	693.9	766.9				
	S	79.0	88.5	98.1	107.9				
	r	3.23	3.25	3.28	3.30				
Coef. Str.		6641100	7379900	8115100	8854300				
Max. Mom. %		9961700	11069800	12172700	13281400				
V		241200	269800	298900	328000				
P, feet		13.77	13.68	13.58	13.50				
R		99440	115940	132570	149090				
W		190880	190880	190880	190880				
Q, feet		17.40	19.33	21.26	23.19				
w lbs.		66	66	66	66				
Rivet dia.		1"	1"	1"	1"				
Span	feet	Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.			
		fixed	free	fixed	free				
10	482	482	540	540	598	598	656	656	
12	482	482	540	540	598	598	656	656	
14	474	474	527	527	580	580	632	632	.122
16	415	415	461	461	507	507	553	553	.159
18	369	366	410	408	451	449	492	490	.201
20	332	321	369	358	406	394	443	430	.248
21	316	302	351	336	386	371	422	405	.274
22	302	285	335	317	369	349	402	382	.300
23	289	268	321	300	353	329	385	359	.329
24	277	254	307	282	338	312	369	340	.358
25	266	240	295	268	325	294	354	322	.388
26	255	227	284	253	312	279	341	305	.420
27	246	215	273	240	301	264	328	289	.452
28	237	205	264	227	290	251	316	274	.487
29	229	195	254	216	280	239	305	261	.522
30	221	185	246	206	271	227	295	249	.559
31	214	176	238	196	262	216	286	236	.596
32	208	167	231	187	254	205	277	225	.636
33	201	160	224	178	246	196	268	215	.676
34	195	152	217	170	239	188	260	205	.718
35	190	145	211	162	232	179	253	196	.760
36	184	139	205	155	225	171	246	187	.804
38	175	127	194	141	214	156	233	171	.896
40	166	116	184	130	203	143	221	157	.993
42	158	107	176	119	193	131	211	144	1.10
44	151	98	168	109	184	121	201	132	1.20
46	144	90	160	101	176	111	192	122	1.31
48	138	...	154	...	169	...	184	...	1.43
50	133	...	148	...	162	...	177	...	1.55
52	128	...	142	...	156	...	170	...	1.68

LOADS BY A. I. S. C. SPECIFICATION

33"

C

CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

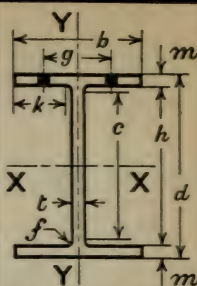
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets.

Rivet given is Maximum diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



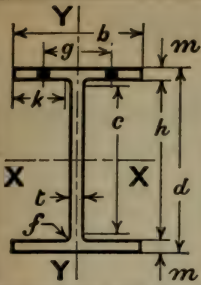
Depth = d" . . .	33.000	33.164	33.342	33.530	33.000	33.272	33.546	33.786
Wt. per foot . . .	125.0	138.0	152.0	167.0	200.0	220.0	240.0	260.0
Area	36.75	40.58	44.69	49.12	58.82	64.70	70.58	76.47
b"	12.000	12.056	12.115	12.179	16.000	16.046	16.090	16.150
t"540	.596	.655	.719	.720	.766	.810	.870
h"	31 $\frac{3}{8}$	31 $\frac{3}{8}$	31 $\frac{3}{8}$	31 $\frac{3}{8}$	30 $\frac{3}{4}$	30 $\frac{3}{4}$	30 $\frac{3}{4}$	30 $\frac{3}{4}$
m"797	.879	.968	1.062	1.1255	1.2615	1.3985	1.5185
k"	4 $\frac{3}{4}$	4 $\frac{3}{4}$	4 $\frac{3}{4}$	4 $\frac{3}{4}$	6 $\frac{3}{8}$	6 $\frac{3}{8}$	6 $\frac{3}{8}$	6 $\frac{3}{8}$
c"	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$	1 $\frac{1}{2}$
f"	29 $\frac{1}{2}$	29 $\frac{1}{2}$	29 $\frac{1}{2}$	29 $\frac{1}{2}$	28 $\frac{3}{4}$	28 $\frac{3}{4}$	28 $\frac{3}{4}$	28 $\frac{3}{4}$
g"	7 $\frac{1}{2}$	7 $\frac{1}{2}$	7 $\frac{1}{2}$	7 $\frac{1}{2}$	10 $\frac{1}{2}$	10 $\frac{1}{2}$	10 $\frac{1}{2}$	10 $\frac{1}{2}$
I	6514.3	7223.0	7998.5	8836.1	11049.6	12385.5	13750.6	15037.7
S	394.81	435.59	479.79	527.06	669.67	744.50	819.81	890.17
r	13.31	13.34	13.38	13.41	13.71	13.84	13.96	14.02
V	230.1	257.5	287.8	321.0	769.5	870.0	972.5	1068.0
P	38.4	42.7	47.5	52.7	96.2	108.4	120.9	132.3
Q	2.50	2.52	2.54	2.56	3.62	3.67	3.71	3.74
W	4737700	5227100	5757400	6324700	8036100	8934000	9837700	10682100
Max. Mom. # . . .	7106500	7840700	8636100	9487000	12054100	13401000	14756500	16023100
V	218890	237200	262100	289300	285100	305800	326100	352700
P	11.08	11.02	10.99	10.93	14.09	14.61	15.09	15.14
R	70370	83420	97450	112860	112770	123930	134790	149460
Q	107370	107370	107370	107370	190880	190880	190880	190880
W	22.06	24.34	26.81	29.45	21.05	23.40	25.77	27.98
w . lbs.	45	45	45	45	66	66	66	66
Rivet dia	1"	1"	1"	1"	1"	1"	1"	1"

Live Load deflection must not exceed 1/360 of the Span.
Live Load Def. = Total Def. \times Live Load Tabular Load

Total Deflection in inches for Maximum Load; laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.

Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally	
feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
12	395	395	436	436	480	480	527	527	570	570	612	612	652	652	705	705
14	338	338	373	373	411	411	452	452	500	500	548	548	596	596	652	652
16	296	292	327	322	360	356	395	391	432	428	468	464	508	504	556	552
18	263	252	290	278	320	307	351	337	384	369	424	409	468	453	516	501
20	237	219	261	242	288	268	316	294	342	320	368	346	404	382	448	426
21	226	205	249	227	274	251	301	275	328	303	364	338	396	370	436	410
22	215	193	238	213	262	235	288	258	316	286	344	314	372	342	408	378
23	206	181	227	200	250	221	275	243	300	268	328	296	356	324	392	360
24	197	170	218	188	240	208	264	228	300	264	328	292	356	324	392	360
25	190	160	209	177	230	196	253	215	321	304	357	338	394	372	427	405
26	182	151	201	167	221	185	243	204	309	289	344	321	378	353	411	385
27	175	143	194	158	213	174	234	193	298	274	331	305	364	336	396	366
28	169	135	187	150	206	165	226	182	287	261	319	299	351	320	382	349
29	163	128	180	142	199	156	218	172	277	249	308	277	339	305	368	332
30	155	121	174	134	192	148	211	163	268	238	298	264	328	292	356	317
31	153	115	169	127	186	140	204	155	259	227	288	252	317	279	345	303
32	148	109	163	121	180	133	198	147	251	217	279	241	307	266	334	299
33	144	103	158	115	174	126	192	139	244	207	271	230	298	255	324	277
34	139	98	154	109	169	120	186	132	236	200	263	229	294	251	314	272
35	135	93	149	103	165	114	181	126	230	194	255	223	281	245	305	261
36	132	89	145	98	160	108	176	120	223	188	248	217	273	237	297	257
38	125	80	138	89	152	98	166	109	211	175	235	205	259	225	281	241
40	118		131	81	144	90	158	99	201	165	223	195	246	217	267	231
42	113		124		137		151		191		213		234		254	
44	108		119		131		144		183		203		224		243	
46	103		114		125		138		175		194		214		232	
48	99		109		120		132		167		186		205		223	
50	95		105		115		127		161		179		197		214	
52	91		101		111		122		155		172		189		205	
54	88		97		107		117		149		165		182		198	
56	85		93		103		113		144		160		176		191	
58	82		90		99		109		139		154		170		184	



CARNEGIE BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page 1 of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets.

Rivet given is Maximum diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.

36"

C

Depth = d". Wt. per foot. Area.	36.000		36.183		36.395		36.645		36.000		36.243		36.550		36.851	
	147.0		160.0		175.0		192.0		230.0		250.0		275.0		300.0	
	43.23		47.06		51.47		56.47		67.65		73.53		80.87		88.23	
b".	12.000		12.045		12.096		12.150		16.000		16.055		16.121		16.189	
t.	.590		.635		.686		.740		.769		.824		.890		.958	
h.	34 $\frac{1}{8}$		34 $\frac{1}{8}$		34 $\frac{1}{8}$		34 $\frac{1}{8}$		33 $\frac{3}{8}$		33 $\frac{3}{8}$		33 $\frac{3}{8}$		33 $\frac{3}{8}$	
m.	.9345		1.026		1.132		1.257		1.290		1.4115		1.565		1.7155	
k.	41 $\frac{1}{16}$		41 $\frac{1}{16}$		41 $\frac{1}{16}$		41 $\frac{1}{16}$		6 $\frac{5}{8}$		6 $\frac{5}{8}$		6 $\frac{5}{8}$		6 $\frac{5}{8}$	
f.	1"		1"		1"		1"		1"		1"		1"		1"	
e.	32 $\frac{1}{4}$		32 $\frac{1}{4}$		32 $\frac{1}{4}$		32 $\frac{1}{4}$		31 $\frac{1}{2}$		31 $\frac{1}{2}$		31 $\frac{1}{2}$		31 $\frac{1}{2}$	
g.	7 $\frac{1}{2}$		7 $\frac{1}{2}$		7 $\frac{1}{2}$		7 $\frac{1}{2}$		10"		10"		10"		10"	
AXES	I....	9040.4	9933.2	10978.8	12208.5	15012.9	16499.3	18400.2	20317.7							
	S....	502.24	549.05	603.31	666.31	834.05	910.48	1006.85	1102.69							
	r....	14.46	14.53	14.61	14.70	14.90	14.98	15.08	15.18							
V-Y-X-X	I....	269.9	299.8	335.0	377.2	882.2	975.4	1095.1	1215.9							
	S....	45.0	49.8	55.4	62.1	110.3	121.5	135.9	150.2							
	r....	2.50	2.52	2.55	2.58	3.61	3.64	3.68	3.71							
Coef. Str.	6026900	6588600	7239800	7995700	10008600	10925800	12082200	13232300								
	Max.Mom."s	9040400	9883000	10859600	11993600	15012900	16388700	18123300	19848500							
	V....	254900	275700	299600	325400	332200	358400	390400	423600							
P. feet....	11.82	11.95	12.08	12.29	15.06	15.24	15.48	15.62								
R....	81940	93050	105870	119740	126690	140860	158030	175860								
W....	107370	107370	107370	107370	190880	190880	190880	190880								
Q. feet....	28.07	30.68	33.71	37.23	26.22	28.62	31.65	34.66								
w. lbs....	45	45	45	45	66	66	66	66								
Rivet dia.	1"	1"	1"	1"	1"	1"	1"	1"								
Span	feet	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally
		fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed
12	502	502	549	549	599	599	651	651	664	664	717	717	781	781	847	847
14	430	430	471	471	517	517	571	571	664	664	717	717	781	781	847	847
16	377	377	412	406	452	447	500	494	626	626	683	683	755	755	827	827
18	335	320	366	350	402	386	444	426	556	607	607	671	671	735	735	735
20	301	279	329	306	362	337	400	372	500	500	546	546	604	604	662	662
21	287	261	314	286	345	315	381	348	477	471	520	514	575	569	630	625
22	274	245	300	268	329	296	363	327	455	445	497	486	549	537	601	590
23	262	230	286	252	315	278	348	307	435	421	475	459	525	508	575	559
24	251	217	275	237	302	261	333	289	417	399	455	435	503	483	551	529
25	241	204	264	223	290	246	320	272	400	378	437	413	483	459	529	502
26	232	192	253	210	278	232	308	257	385	359	420	392	465	436	509	477
27	223	182	244	199	268	219	296	242	371	342	405	373	447	414	490	454
28	215	172	235	188	259	207	286	229	357	325	390	355	431	395	473	432
29	208	163	227	178	250	196	276	217	345	310	377	339	417	376	456	412
30	201	154	220	168	241	186	267	205	334	296	364	323	403	359	441	393
31	194	146	213	160	234	176	258	196	323	282	352	308	390	342	427	375
32	188	138	206	151	226	167	250	186	313	270	341	295	378	327	414	358
33	183	131	200	144	219	159	242	176	303	258	331	282	366	313	401	343
34	177	125	194	137	213	151	235	167	294	247	321	269	355	299	389	328
35	172	119	188	130	207	143	228	159	286	236	312	258	345	287	378	314
36	167	113	183	124	201	136	222	151	278	226	304	247	336	275	368	301
38	159	102	173	113	191	124	210	137	263	208	288	227	318	253	348	277
40	151		165	102	181	112	200	125	250	192	273	209	302	233	331	255
42	143		157		172		190		238	177	260	193	288	215	315	235
44	137		150		165		182		227	164	248	179	275	199	301	219
46	131		143		157		174		218	152	238	165	263	184	288	203
48	126		137		151		167		209	141	228	153	252	171	276	188
50	121		132		145		160		200	131	219	143	242	159	265	175
52	116		127		139		154		192	121	210	133	232	147	254	162
54	112		122		134		148		185		202		224		245	
56	108		118		129		143		179		195		216		236	
58	104		114		125		138		173		188		208		228	
60	100		110		121		133		167		182		201		221	
Allowable Uniform Load in Kips, For laterally fixed beam loads not tabulated, divided by Coefficient of Strength by Span in feet.																

ALLOWABLE END REACTIONS FOR CARNEGIE BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for $3\frac{1}{2}"$ Bearing	Min. Span for $3\frac{1}{2}"$ Bearing	Reaction R for $5\frac{1}{2}"$ Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V .	Length of Bearing to develop V .
8	24.0	.239"	15000	19720	6.41'	26890	3590	22900	4.40
	27.0	.268	15000	22210	6.40	30250	4020	26000	4.45
	30.0	.298	15000	24800	6.37	33740	4470	29300	4.51
	31.0	.290	15000	23990	6.88	32690	4350	28100	4.43
	36.0	.336	15000	27970	6.87	38050	5040	33100	4.51
	42.0	.390	15000	32700	6.86	44400	5850	39100	4.60
9	29.0	.279	15000	24060	6.98	32430	4190	30100	4.95
	32.0	.307	15000	26590	6.97	35800	4610	33500	5.00
	35.0	.335	15000	29130	6.96	39180	5030	37000	5.06
	38.0	.316	15000	27250	8.34	36730	4740	34100	4.95
	43.0	.357	15000	30950	8.31	41660	5360	39100	5.02
	48.0	.398	15000	34690	8.28	46630	5970	44100	5.08
10	21.0	.230	13750	18900	6.90	25220	3160	27300	6.17
	23.0	.230	13690	18890	7.76	25190	3150	27600	6.27
	26.0	.259	14360	22410	7.40	29850	3720	31400	5.91
	30.0	.298	15000	27070	7.07	36010	4470	36600	5.63
	31.0	.320	15000	28800	6.81	38400	4800	38400	5.50
	36.0	.467	15000	42030	5.01	56040	7010	56000	5.50
	42.0	.644	15000	57960	3.94	77280	9660	77300	5.50
	49.0	.350	15000	31500	10.36	42000	5250	42000	5.50
	54.0	.497	15000	44730	7.63	59640	7460	59600	5.50
	59.0	.644	15000	57960	6.14	77280	9660	77300	5.50
12	25.0	.240	12750	19840	9.28	25960	3060	34300	8.24
	28.0	.240	12710	19820	10.77	25920	3050	34600	8.33
	32.0	.274	13580	24290	10.04	31730	3720	39800	7.68
	*34.0	.375	15000	36590	6.50	47840	5630	54100	6.61
	36.0	.308	14250	28790	9.54	37570	4390	45200	7.24
	40.0	.290	14000	26400	11.88	34520	4060	41800	7.28
	45.0	.326	14630	31140	11.34	40680	4770	47500	6.92
	50.0	.361	15000	35550	11.03	46380	5420	53100	6.74
	55.0	.375	15000	36560	11.72	47810	5630	54000	6.60
	60.0	.409	15000	40060	11.67	52330	6140	59500	6.67
	66.0	.448	15000	44120	11.66	57560	6720	65900	6.74
	65.0	.400	15000	39000	13.37	51000	6000	57600	6.60
	70.0	.523	15000	50990	10.57	66680	7850	75300	6.60
	76.0	.670	15000	65330	8.57	85430	10050	96500	6.60

The beam web is treated as a column with fixed ends, having an effective length l of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

*Special Section. Web Thickness $\frac{3}{8}"$

ALLOWABLE END REACTIONS FOR CARNEGIE BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for $3\frac{1}{2}$ " Bearing	Min. Span for $3\frac{1}{2}$ " Bearing	Reaction R for $5\frac{1}{2}$ " Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
14	30.0	.270	12450	23500	10.68'	30220	3360	45200	9.97
	33.0	.270	12430	23490	12.17	30200	3360	45400	10.02
	36.0	.294	13020	26880	11.59	34540	3830	49700	9.46
	*38.0	.375	14610	38340	7.99	49300	5480	63000	8.00
	39.0	.318	13530	30290	11.14	38890	4300	54000	9.02
	42.0	.342	13970	33720	10.78	43280	4780	58400	8.68
	48.0	.343	14090	33820	11.57	43480	4830	57600	8.43
	53.0	.378	14600	38810	12.10	49850	5520	64100	8.07
	58.0	.413	15000	43740	11.74	56130	6200	70600	7.83
	61.0	.382	14670	39360	14.20	50560	5600	64600	8.01
	68.0	.425	15000	45000	13.84	57750	6380	72600	7.83
	75.0	.468	15000	49810	13.79	63850	7020	80800	7.91
	85.0	.435	15000	45670	17.29	58720	6530	73100	7.70
	95.0	.485	15000	51260	17.23	65810	7280	82600	7.80
	105.0	.536	15000	57020	17.13	73100	8040	92400	7.90
16	35.0	.290	11980	25990	12.62	32930	3470	55400	11.98
	38.0	.314	12560	29590	12.03	37470	3940	60300	11.30
	40.0	.290	11940	25970	15.15	32890	3460	55700	12.08
	*43.0	.375	13840	38830	10.16	49210	5190	71700	9.84
	45.0	.326	12790	31390	14.10	39730	4170	63100	11.11
	50.0	.362	13470	36890	13.33	46650	4880	70600	10.41
	58.0	.375	13810	38840	15.00	49200	5180	72000	9.90
	63.0	.406	14260	43580	14.52	55160	5790	78500	9.54
	68.0	.438	14650	48480	14.09	61320	6420	85300	9.24
	76.0	.419	14480	45510	17.49	57650	6070	80500	9.26
	83.0	.458	14920	51450	16.90	65110	6830	88600	8.94
	90.0	.495	15000	56130	16.79	70990	7430	96500	8.93
	100.0	.464	15000	52200	20.50	66120	6960	89100	8.80
	107.0	.496	15000	56000	20.45	70880	7440	95900	8.86
	115.0	.532	15000	60320	20.41	76280	7980	103700	8.93

The beam web is treated as a column with fixed ends, having an effective length l of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests.

When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

*Special Section. Web Thickness $\frac{3}{8}$ ".

ALLOWABLE END REACTIONS FOR CARNEGIE BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for $\frac{3}{4}$ " Bearing	Min. Span for $\frac{3}{4}$ " Bearing	Reaction R for $\frac{5}{8}$ " Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
18	47.0	.320	11790	30170	16.98'	37710	.3770	69100	13.83
	*51.0	.375	13000	39020	13.82	48780	4880	81100	12.14
	52.0	.354	12530	35610	15.91	44490	4440	77000	12.82
	58.0	.393	13240	41950	15.06	52350	5200	86100	11.98
	67.0	.406	13560	44040	16.91	55060	5510	87700	11.43
	72.0	.436	13980	48930	16.36	61130	6100	94800	11.02
	78.0	.471	14400	54670	15.87	68230	6780	103100	10.64
	86.0	.429	13920	47760	21.13	59700	5970	92700	11.02
	93.0	.463	14340	53310	20.48	66590	6640	100700	10.63
	100.0	.498	14710	59040	19.88	73700	7330	109000	10.32
	55.0	.360	11530	36210	18.51	44510	4150	90200	16.52
	58.0	.360	11490	36180	19.95	44460	4140	90700	16.69
21	64.0	.396	12210	42460	18.77	52140	4840	100400	15.48
	70.0	.433	12850	49010	17.78	60130	5560	110400	14.54
	76.0	.469	13370	55460	17.05	68000	6270	120300	13.83
	80.0	.438	13010	49880	18.45	61280	5700	110400	14.11
	86.0	.470	13470	55580	19.83	68240	6330	119100	13.54
	92.0	.502	13860	61320	19.22	75240	6960	128000	13.07
	98.0	.535	14220	67260	18.67	82480	7610	137100	12.68
	104.0	.465	13430	54660	25.88	67140	6240	117200	13.51
	112.0	.499	13860	60730	25.10	74570	6920	126500	13.01
	120.0	.535	14250	67190	24.30	82430	7620	136400	12.58
	128.0	.570	14580	73500	23.71	90120	8310	146200	12.24
	136.0	.606	14880	80020	23.12	98060	9020	156300	11.96
24	70.0	.400	11250	42750	22.85	51750	4500	115200	19.60
	76.0	.405	11350	43680	25.00	52880	4600	116600	19.37
	85.0	.452	12200	52580	23.22	63600	5510	131000	17.73
	94.0	.499	12900	61640	21.90	74520	6440	145600	16.54
	100.0	.450	12210	52200	28.93	63180	5490	129600	17.59
	110.0	.494	12870	60650	27.39	73370	6360	143200	16.48
	120.0	.539	13440	69400	26.10	83880	7240	157200	15.62
	130.0	.547	13560	70920	28.23	85760	7420	159200	15.40
	140.0	.588	13990	78940	27.30	95400	8230	172100	14.82
	150.0	.629	14360	87000	26.55	105600	9030	185100	14.36
	160.0	.670	14680	95100	25.92	114780	9840	198300	13.99

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When the reaction from the load exceeds the allowable reaction R, the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V.

*Special Section. Web Thickness $\frac{3}{8}$ ".

ALLOWABLE END REACTIONS FOR CARNEGIE BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for 3½" Bearing	Min. Span for 3½" Bearing	Reaction R for 5½" Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
27	85.0	.461	11510	54140	23.96	64750	5305	148400	21.26
	91.0	.461	11450	54120	26.42	64680	5280	149400	21.54
	101.0	.510	12220	64140	24.76	76600	6230	166300	19.88
	112.0	.566	12960	75810	23.20	90490	7340	185700	18.48
	124.0	.624	13590	88050	22.14	105000	8480	206200	17.43
	137.0	.688	14160	101660	21.17	121150	9740	229000	16.57
	145.0	.580	13220	78620	31.14	93960	7670	187900	17.75
	160.0	.639	13830	90990	29.68	108670	8840	208600	16.81
	175.0	.698	14320	103470	28.56	123470	10000	229500	16.11
	190.0	.756	14730	115800	27.70	138080	11140	250400	15.59
30	115.0	.530	11730	68410	29.15	80850	6220	190800	23.18
	126.0	.581	12420	79670	27.40	94100	7220	210300	21.60
	138.0	.634	13030	91550	26.13	108060	8260	230900	20.37
	151.0	.692	13590	104700	25.01	123500	9400	253600	19.34
	165.0	.755	14100	119090	24.01	140390	10650	278500	18.47
	180.0	.670	13490	99440	33.39	117520	9040	241200	19.18
	200.0	.743	14100	115940	31.83	136900	10480	269800	18.19
	220.0	.816	14600	132570	30.61	156390	11910	298900	17.46
	240.0	.888	15000	149090	29.69	175730	13320	328000	16.93
33	125.0	.540	11090	70370	33.66	82340	5990	213800	27.45
	138.0	.596	11870	83420	31.33	97560	7070	237200	25.24
	152.0	.655	12570	97450	29.54	113910	8230	262100	23.50
	167.0	.719	13210	112860	28.02	131860	9500	289300	22.08
	200.0	.720	13330	112770	35.63	131970	9600	285100	21.46
	220.0	.766	13690	123930	36.04	144900	10490	305800	20.84
	240.0	.810	14000	134790	36.49	157470	11340	326100	20.37
	260.0	.870	14380	149460	35.74	174480	12510	352700	19.75
36	147.0	.590	11110	81940	36.78	95050	6550	254900	29.89
	160.0	.635	11680	93050	35.41	107880	7420	275700	28.13
	175.0	.686	12250	105870	34.19	122680	8400	299600	26.56
	192.0	.740	12780	119740	33.39	138650	9460	325400	25.25
	230.0	.769	13180	126690	39.50	146960	10140	332200	23.78
	250.0	.824	13610	140860	38.78	163290	11210	358400	22.90
	275.0	.890	14050	158030	38.23	183030	12500	390400	22.08
	300.0	.958	14440	175860	37.62	203530	13830	423600	21.41

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When the reaction from the load exceeds the allowable reaction R, the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V.

CONNECTION ANGLES FOR CARNEGIE BEAMS													
DIMENSIONS, WEIGHTS AND WORKING LOADS								¾" POWER DRIVEN RIVETS					
Beam		Connection Value			Framing Distance C	Connection Angles			Connection Details.				
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length		Weight inc. Web Rivets			
			Power Driven Rivets	Unfin-ished Bolts									
8"	24.0	21510	23860	17670	3/16	IC.13.10	2 5/8	6" x 4" x 3/8" 0' — 5 1/2" Long	13 lbs.				
	27.0	24120	23860	17670	3/16	IC.13.10	2 5/8						
	30.0	26820	23860	17670	3/16	IC.13.10	2 5/8						
9"	29.0	25110	23860	17670	3/16	IC.13.10	2 5/8						
	32.0	27630	23860	17670	3/16	IC.13.10	2 5/8						
	35.0	30150	23860	17670	1/4	IC.13. 9	2 9/16						
10"	21.0	20700	23860	17670	3/16	IC.13.10	2 5/8						
	23.0	20700	23860	17670	3/16	IC.13.10	2 5/8						
	26.0	23310	23860	17670	3/16	IC.13.10	2 5/8						
	30.0	26820	23860	17670	3/16	IC.13.10	2 5/8						
12"	25.0	21600	23860	17670	3/16	IC.13.10	2 5/8						
	28.0	21600	23860	17670	3/16	IC.13.10	2 5/8						
	32.0	24660	23860	17670	3/16	IC.13.10	2 5/8						
	34.0	33750	23860	17670	1/4	IC.13. 9	2 9/16						
	36.0	27720	23860	17670	3/16	IC.13.10	2 5/8						
	40.0	26120	23860	17670	3/16	IC.13.10	2 5/8						
	45.0	29340	23860	17670	1/4	IC.13. 9	2 9/16						
14"	50.0	32490	23860	17670	1/4	IC.13. 9	2 9/16						
	30.0	24300	47720	35340	3/16	IC.19.10	2 5/8	4" x 3 1/2" x 3/8" 0' — 11 1/2" Long	19 lbs.				
	33.0	24300	47720	35340	3/16	IC.19.10	2 5/8						
	36.0	26460	47720	35340	3/16	IC.19.10	2 5/8						
	38.0	33750	47720	35340	1/4	IC.19. 9	2 9/16						
	39.0	28620	47720	35340	1/4	IC.19. 9	2 9/16						
	42.0	30780	47720	35340	1/4	IC.19. 9	2 9/16						
16"	35.0	26100	47720	35340	3/16	IC.19.10	2 5/8						
	38.0	28260	47720	35340	3/16	IC.19.10	2 5/8						
	40.0	26100	47720	35340	3/16	IC.19.10	2 5/8						
	43.0	33750	47720	35340	1/4	IC.19. 9	2 9/16						
	45.0	29340	47720	35340	1/4	IC.19. 9	2 9/16						
	50.0	32580	47720	35340	1/4	IC.19. 9	2 9/16						
18"	47.0	36000	59650	44180	1/4	IC.25. 9	2 9/16	4" x 3 1/2" x 3/8" 1' — 2 1/2" Long	25 lbs.				
	51.0	42190	59650	44180	1/4	IC.25. 9	2 9/16						
	52.0	39830	59650	44180	1/4	IC.25. 9	2 9/16						
	58.0	44220	59650	44180	1/4	IC.25. 9	2 9/16						

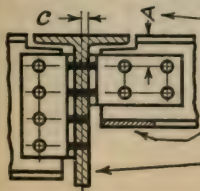
*Layer-out starts with this dimension at left end of beam. With beams ordered one inch short, as usual in standard shop practice, this leaves sufficient end distance or clearance at right end, in case of full allowable 3/8" underrun or 3/8" overrun in beam lengths.

CONNECTION ANGLES FOR CARNEGIE BEAMS

DIMENSIONS, WEIGHTS AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles				Connection Details.			
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length	Weight inc. Web Rivets				
			Single Shear	Unfin-ished Bolts									
			Power Driven Rivets										
21"	55.0	48600	71580	53020	1/4	IC. 30. 9	2 9/16	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.				
	58.0	48600	71580	53020	1/4	IC. 30. 9	2 9/16						
	64.0	53460	71580	53020	1/4	IC. 30. 9	2 9/16						
	70.0	58460	71580	53020	1/4	IC. 30. 9	2 9/16						
	76.0	63320	71580	53020	5/16	IC. 30. 8	2 1/2						
	80.0	59130	71580	53020	5/16	IC. 30. 8	2 1/2						
24"	86.0	63450	71580	53020	5/16	IC. 30. 8	2 1/2	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.				
	92.0	67770	71580	53020	5/16	IC. 30. 8	2 1/2						
	98.0	71580	71580	53020	5/16	IC. 30. 8	2 1/2						
	70.0	54000	71580	53020	1/4	IC. 30. 9	2 9/16						
	76.0	54680	71580	53020	1/4	IC. 30. 9	2 9/16						
	85.0	61020	71580	53020	5/16	IC. 30. 8	2 1/2						
24"	94.0	67370	71580	53020	5/16	IC. 30. 8	2 1/2	4" x 3 1/2" x 3/8" 1' — 5 1/2" Long	30 lbs.				
	85.0	82980	95440	70690	5/16	IC. 40. 8	2 1/2				4" x 3 1/2" x 3/8" 1' — 11 1/2" Long	40 lbs.	
	91.0	82980	95440	70690	5/16	IC. 40. 8	2 1/2						
	97.0	91800	95440	70690	5/16	IC. 40. 8	2 1/2						
	112.0	95440	95440	70690	3/8	IC. 40. 8	2 1/2						
	124.0	95440	95440	70690	3/8	IC. 40. 7	2 7/16						
137.0	95440	95440	70690	7/16	IC. 40. 6	2 3/8							
30"	115.0	107330	107370	79530	5/16	IC. 45. 8	2 1/2	4" x 3 1/2" x 3/8" 2' — 3 1/2" Long	45 lbs.				
	126.0	107370	107370	79530	5/16	IC. 45. 7	2 7/16						
	138.0	107370	107370	79530	5/16	IC. 45. 7	2 7/16						
	151.0	107370	107370	79530	3/8	IC. 45. 6	2 3/8						
	165.0	107370	107370	79530	7/8	IC. 45. 6	2 3/8						
33"	125.0	107370	107370	79530	5/16	IC. 45. 8	2 1/2	4" x 3 1/2" x 3/8" 2' — 3 1/2" Long	45 lbs.				
	138.0	107370	107370	79530	3/8	IC. 45. 7	2 7/16						
	152.0	107370	107370	79530	3/8	IC. 45. 7	2 7/16						
	167.0	107370	107370	79530	7/16	IC. 45. 6	2 3/8						
36"	147.0	107370	107370	79530	3/8	IC. 45. 7	2 7/16	4" x 3 1/2" x 3/8" 2' — 3 1/2" Long	45 lbs.				
	160.0	107370	107370	79530	3/8	IC. 45. 7	2 7/16						
	175.0	107370	107370	79530	3/8	IC. 45. 7	2 7/16						
	192.0	107370	107370	79530	7/16	IC. 45. 6	2 3/8						



-When $A = 3''$ all beams can be framed opposite with tops flush.

Flange must be cut away as shown for field riveting on all beams framing opposite a larger beam, if flange interferes with outstanding rivets.

Minimum Web required to develop Single Shearing Value is .33"
Minimum Web required to develop Double Shearing Value is .53"

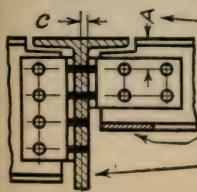
LOADS BY A. I. S. C. SPECIFICATION

CONNECTION ANGLES FOR CARNEGIE BEAMS

DIMENSIONS, WEIGHTS AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles			Connection Details.		
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length			Weight inc. Web Rivets
			Power Driven Rivets	Unfinished Bolts							
24"	100.0	121500	143160	106030	5/16	IC.49. 8	2 1/2	6" x 6" x 3/8" 1' — 5 1/2" Long	49 lbs.		
	110.0	133380	143160	106030	5/16	IC.49. 8	2 1/2				
	120.0	143160	143160	106030	5/16	IC.49. 8	2 1/2				
	130.0	143160	143160	106030	5/16	IC.49. 8	2 1/2				
	140.0	143160	143160	106030	3/8	IC.49. 7	2 7/16				
	150.0	143160	143160	106030	3/8	IC.49. 7	2 7/16				
	160.0	143160	143160	106030	3/8	IC.49. 7	2 7/16				
27"	145.0	167020	167020	123700	3/8	IC.58. 7	2 7/16	6" x 6" x 3/8" 1' — 8 1/2" Long	58 lbs.		
	150.0	167020	167020	123700	3/8	IC.58. 7	2 7/16				
	175.0	167020	167020	123700	7/16	IC.58. 6	2 3/8				
	190.0	167020	167020	123700	7/16	IC.58. 6	2 3/8				
30"	180.0	190880	190880	141380	3/8	IC.66. 7	2 7/16	6" x 6" x 3/8" 1' — 11 1/2" Long	66 lbs.		
	200.0	190880	190880	141380	7/16	IC.66. 6	2 3/8				
	220.0	190880	190880	141380	1/2	IC.66. 5	2 5/16				
	240.0	190880	190880	141380	1/2	IC.66. 5	2 5/16				
33"	200.0	190880	190880	141380	7/16	IC.66. 6	2 3/8				
	220.0	190880	190880	141380	7/16	IC.66. 6	2 3/8				
	240.0	190880	190880	141380	7/16	IC.66. 6	2 3/8				
	260.0	190880	190880	141380	1/2	IC.66. 5	2 5/16				
36"	230.0	190880	190880	141380	7/16	IC.66. 6	2 3/8				
	250.0	190880	190880	141380	1/2	IC.66. 5	2 5/16				
	275.0	190880	190880	141380	1/2	IC.66. 5	2 5/16				
	300.0	190880	190880	141380	9/16	IC.66. 4	2 1/4				



—Following Beams can be framed opposite with tops flush when:—

A = 3" all 8", 9", 10", 12", 14", 16", 18", 21", and 24" (100 to 130#)

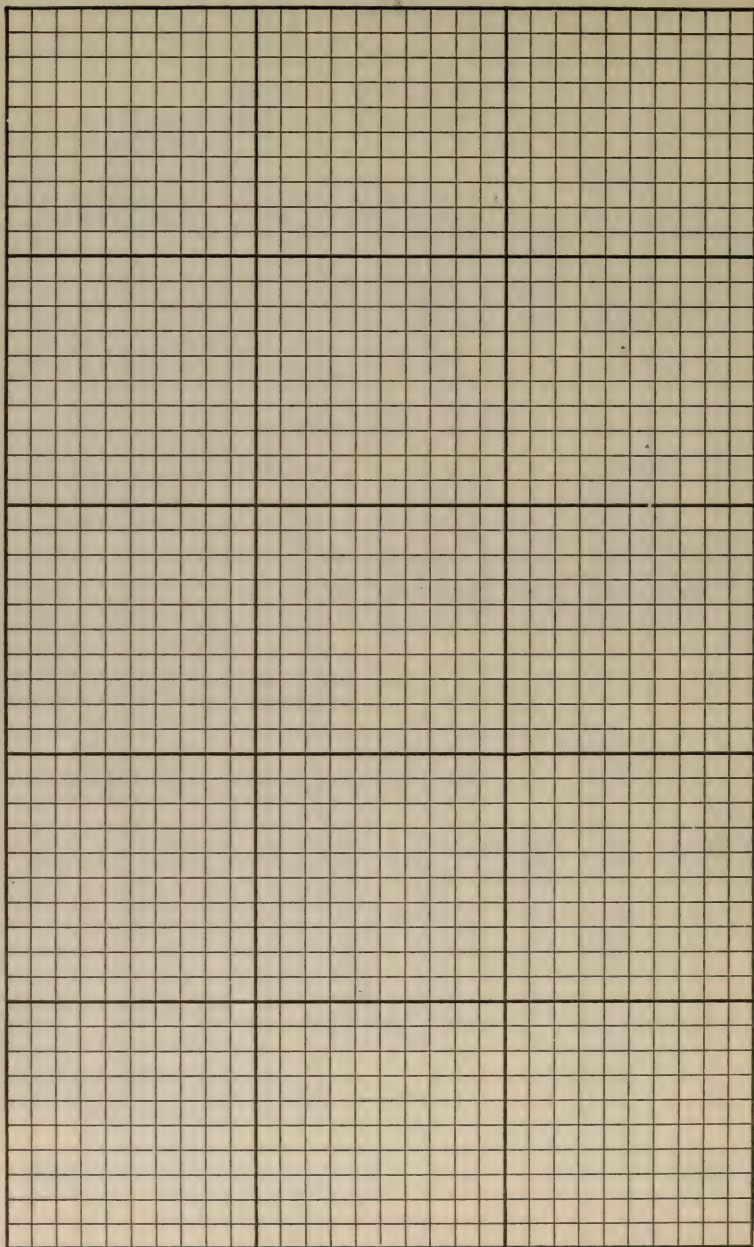
A = 31 $\frac{1}{4}$ " all 9", 10", 12", 14", 16", 18", 21", 24", and 27" (145 and 160#)

A = $33\frac{3}{4}^\circ$ all $9^\circ, 10^\circ, 14^\circ, 16^\circ, 21^\circ, 24^\circ, 27^\circ$, and 30° .

Flange must be cut away as shown for field riveting on all beams framing opposite a larger beam, if flange interferes with outstanding rivets.

Minimum Web required to develop Single Shearing Value is .33'
Minimum Web required to develop Double Shearing Value is .53'

NOTES and DIAGRAMS



Part IV

Section 8

Miscellaneous Beam Sections

Dimensions

Technical Functions

Allowable Total Loads

by

A. I. S. C. Specification

Allowable End Reactions

Standard Connection Angles

for

Carnegie Mill Sections

Carnegie H Sections

J. and L. Junior Beams

Bethlehem Steel Joists

Phoenix Special I Beams

8"

C
M

CARNEGIE MILL SECTIONS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus
 r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V .

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

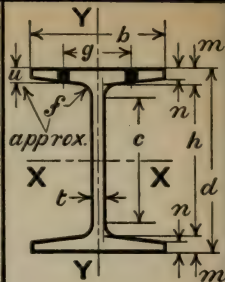
Q is Minimum Span in feet, uniformly loaded to cause W .

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by Span in feet.	Span feet	Laterally		Laterally		Total Deflection in inches for Maximum Load; Laterally fixed beam.	Live Load deflection must not exceed 1/360 of the Span.	Live Load Def. = Total Def. \times Live Load Tabular Load
		fixed	free	fixed	free			
	3	44.4	44.4	63.4	63.4	.037 .058		
	4	42.9	42.9	47.6	47.6			
	5	34.3	34.3	38.1	38.1			
	6	28.6	28.6	31.7	31.7	.084		
	7	24.5	23.9	27.2	26.6	.114		
	8	21.5	20.1	23.8	22.5	.149		
	9	19.1	17.1	21.1	19.2	.189		
	10	17.2	14.8	19.0	16.6	.233		
	11	15.6	12.8	17.3	14.4	.281		
	12	14.3	11.2	15.9	12.6	.335		
	13	13.2	9.9	14.6	11.1	.394		
	14	12.3	8.7	13.6	9.8	.456		
	15	11.4		12.7524		
	16	10.7		11.9596		
	17	10.1		11.2674		
	18	9.6		10.6754		
	19	9.1		10.0840		
	20	8.6		9.5931		

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
 For laterally fixed beam loads not tabulated, divide the
 Coefficient of Strength by the Span in feet.

CARNEGIE MILL SECTIONS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

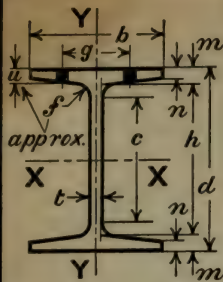
w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.

9"

C
M

Depth = d"	9.00	9.00
Wt. per foot.	20.5	25.0
Area Sq. In..	6.02	7.34
b"	5.234	5.380
t.....	.234	.380
h.....	8.008	8.008
m.....	.496	.496
n.....	.277	.277
f.....	.275	.275
c.....	$7\frac{1}{2}$	$7\frac{1}{2}$
g.....	$2\frac{1}{2}$	$2\frac{1}{2}$
u.....	$13\frac{3}{32}$	$13\frac{3}{32}$
A X E S		
X - X	I.... 86.6	95.5
S....	19.24	21.22
r....	3.79	3.61
Y - Y	I.... 8.0	8.8
S....	3.1	3.3
r....	1.15	1.09
Coef. Str....	230930	254670
Max. Mom. %	346400	382000
V.....	25270	41040
P. feet..	4.57	3.10
R.....	19430	32770
Q.....	21060	23860
W. feet..	5.48	5.34
w. lbs....	13	13
Rivet dia....	$\frac{3}{4}$	$\frac{3}{4}$

Live Load deflection must not exceed $\frac{1}{360}$ of the Span.Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Total Deflection in inches for Maximum Load; Laterally fixed beam.

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

Span feet	Laterally		Laterally		
	fixed	free	fixed	free	
3	50.5	50.5	82.1	82.1	
4	50.5	50.5	63.7	63.7	
5	46.1	46.1	50.9	50.9	.052
6	38.4	38.4	42.4	42.4	.074
7	32.9	32.4	36.4	36.1	.101
8	28.8	27.4	31.8	30.6	.132
9	25.6	23.4	28.3	26.2	.168
10	23.1	20.2	25.5	22.7	.207
11	20.9	17.6	23.1	19.8	.250
12	19.2	15.5	21.2	17.4	.298
13	17.7	13.7	19.6	15.3	.350
14	16.5	12.1	18.2	13.6	.406
15	15.4	10.7	17.0	12.1	.466
16	14.4	9.6	15.9	10.8	.530
17	13.6		15.0		.599
18	12.8		14.1		.670
19	12.1		13.4		.747
20	11.5		12.7		.828

4" TO 8"**CARNEGIE H BEAMS**

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia

S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $\frac{3}{4}$ " bearing. For details see page of Allowable End Reactions.

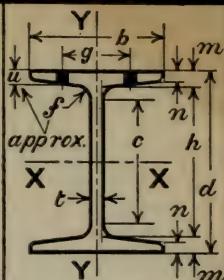
W is Maximum Load on one Standard Connection.

Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50% and their deflections 80% of those shown.



Depth = d".....		4"	5"	6"	6"	6"	6"	8"	8"	8"									
Weight per foot.....		13.8	18.9	20.0	22.5	25.0	27.5	32.6	34.3	37.7									
Area Sq In.....		3.99	5.47	5.86	6.61	7.33	8.08	9.50	10.00	11.00									
b.....		4.000	5.000	5.938	6.063	5.938	6.063	7.938	8.000	8.125									
t.....		.313	.313	.250	.375	.313	.438	.313	.375	.500									
h.....		3.094	3.994	5.042	5.042	4.840	4.840	6.880	6.880	6.880									
m.....		.453	.503	.479	.479	.580	.580	.560	.560	.560									
n.....		.290	.330	.280	.280	.381	.381	.358	.358	.358									
f.....		.313	.313	.313	.313	.313	.313	.313	.313	.313									
c.....		2.522	3.413	4.458	4.458	4.256	4.256	6.287	6.287	6.287									
g.....		2 1/4	2 3/4	3 1/2	3 1/2	3 1/2	3 1/2	4 1/2	4 1/2	4 1/2									
u.....		3/8	7/16	3/8	3/8	1/2	1/2	1/2	1/2	1/2									
A X E S	I.....	10.7	23.8	38.8	41.0	47.0	49.3	112.8	115.5	120.8									
	S.....	5.35	9.52	12.93	13.67	15.67	16.43	28.20	28.88	30.20									
	r.....	1.64	2.08	2.57	2.49	2.53	2.47	3.45	3.40	3.31									
	I.....	3.6	7.8	11.4	12.2	14.9	16.0	34.2	35.1	36.9									
	S.....	1.8	3.1	3.8	4.0	5.0	5.3	8.6	8.8	9.1									
	r.....	0.95	1.20	1.39	1.36	1.43	1.41	1.90	1.87	1.83									
Coef Str.....		64200	114240	155160	164040	188040	197160	338400	346560	362400									
Max Mom. #.....		96300	173160	232740	246060	282060	295740	507600	519840	543600									
V.....		15020	18780	18000	27000	22540	31540	30050	36000	48000									
P. feet.....		2.14	3.04	4.31	3.04	4.17	3.13	5.63	4.81	3.78									
R.....		21130	22300	18750	28130	23480	32850	25820	30940	41250									
W.....		11930	11930	11250	11930	11930	11930	23860	23860	23860									
Q. feet.....		2.69	4.79	6.90	6.88	7.88	8.26	7.09	7.26	7.59									
w lbs.....		6	6	6	6	6	6	13	13	13									
Rivet dia.....		5/8	5/8	3/4	3/4	3/4	3/4	3/4	3/4	3/4									
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally	Laterally
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
	3	21.2	21.2	37.6	37.6	36.0	36.0	54.0	54.0	45.1	45.1	63.1	63.1	60.1	60.1	72.0	72.0	96.0	96.0
	4	15.9	15.9	28.5	28.5	36.0	36.0	41.0	41.0	45.1	45.1	49.3	49.3	60.1	60.1	72.0	72.0	90.6	90.6
	5	12.7	12.7	22.8	22.8	31.0	31.0	32.8	32.8	37.6	37.6	39.4	39.4	60.1	60.1	69.4	69.4	72.5	72.5
	6	10.6	10.1	19.0	19.0	25.9	25.9	27.4	27.4	31.4	31.4	32.9	32.9	56.4	56.4	57.8	57.8	60.4	60.4
	7	9	8.3	16.3	15.9	22.2	22.2	23.4	23.4	26.9	26.9	28.2	28.2	48.3	48.3	49.5	49.5	51.8	51.8
	8	8	8.0	14.3	13.4	19.4	19.0	20.5	20.3	23.5	23.1	24.6	24.4	42.3	42.3	43.4	43.4	45.3	45.3
	9	7	7.1	12.7	12.7	17.2	16.4	18.2	17.5	20.9	20.9	21.9	21.0	37.6	37.6	38.5	38.5	40.3	40.3
	10	6	6.4	11.4	11.4	15.5	14.3	16.4	15.3	18.8	17.3	19.7	18.3	33.8	33.8	34.7	34.7	36.2	36.2
	11	5	5.8	10.4	10.4	14.1	14.1	14.9	14.9	17.1	17.1	17.9	17.9	30.8	30.8	31.5	31.5	32.9	32.9
	12	5	5.4	9.5	9.5	12.9	12.9	13.7	13.7	15.7	15.7	16.4	16.4	28.2	28.2	29.7	29.7	30.2	30.2
	13	4	4.9	8.9	8.9	11.9	11.9	12.6	12.6	14.5	14.5	15.2	15.2	26.0	26.0	27.4	27.4	29.7	29.7
	14	4	4.6	8.2	8.2	11.1	11.1	11.7	11.7	13.4	13.4	14.1	14.1	24.2	24.2	25.8	25.8	27.4	27.4
	15	4	4.3	7.7	7.7	10.3	10.3	10.9	10.9	12.5	12.5	13.1	13.1	22.6	22.6	23.1	23.1	24.2	24.2
	16	4	4.0	7.2	7.2	9.8	9.8	10.3	10.3	11.9	11.9	12.5	12.5	21.2	21.2	21.7	21.7	22.7	22.7
	17	4	3.8	6.8	6.8	9.3	9.3	9.8	9.8	11.4	11.4	12.0	12.0	19.9	19.9	20.4	20.4	21.3	21.3
Total Deflection in inches for Maximum Load; Laterally fixed beam. Live Load deflection must not exceed 1/360 of the Span.	Live Load Def. = $\frac{\text{Total Def} \times \text{Live Load}}{\text{Tabular Load}}$	3	.042050050037
	4	.074	.059078078058058
	5	.116	.093	.078
	6	.168	.134	.112112112084084084
	7	.228	.182	.152152152114114114
	8	.298	.238	.198198198149149149
	9	.378	.302	.252252252189189189
	10	.465	.372	.310310310233233233
	11	.562	.450	.375375375281281281
	12	.670	.537	.447447447335335335
	13630	.525525525394394394
	14730	.608608608456456456
	15698698698524524524
	16596596596
	17674674674

6" to 12"

J AND L JUNIOR BEAMS

ROLLED FROM COPPER BEARING STEEL

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus r is Radius of Gyration
V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $2\frac{1}{2}$ " bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

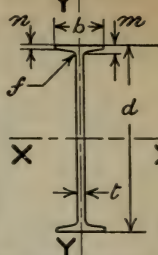
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



		6"	7"	8"	9"	10"	11"	12"									
Depth = d"		6.028	7.028	8.028	9.018	10.026	11.024	12.028									
Weight per foot.		4.41	5.48	6.54	7.48	8.96	10.23	11.74									
Area Sq. In.		1.30	1.61	1.92	2.20	2.64	3.01	3.45									
b		1.84	2.08	2.28	2.38	2.69	2.84	3.06									
t		.114	.126	.135	.145	.155	.165	.175									
f		.200	.212	.224	.231	.247	.258	.272									
p		.142	.148	.154	.155	.165	.170	.178									
r		.150	.165	.180	.195	.210	.225	.240									
A X E S	I	7.30	12.13	18.67	26.20	39.01	53.08	72.21									
	X-X	2.42	3.45	4.65	5.81	7.78	9.63	12.01									
	S	2.372	2.744	3.116	3.450	3.847	4.200	4.573									
	I	.1654	.2482	.3434	.3939	.6078	.7459	.9776									
	X-X	.1794	.2389	.3011	.3317	.4523	.5246	.6385									
	S	.3569	.3925	.4226	.4230	.4802	.4979	.5320									
Coef. Str.		29074	41425	55817	69727	93369	115555	144088									
Max. Mom. #s		43610	62137	83726	104591	140054	173332	216131									
V		8210	10580	12960	15660	18330	20930	23700									
P. feet.		1.77	1.96	2.15	2.23	2.55	2.76	3.04									
R.		5620	6370	6900	7550	8240	8960	9710									
W.		5130	5670	6075	6525	6975	7425	7875									
Q. feet		2.83	3.65	4.59	5.34	6.69	7.78	9.15									
w. lbs.		4	5	5	5	5	5	5									
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally		Laterally	
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
	6	4.85	3.05	6.90	4.80	9.30	6.90	11.62	8.86	15.56	12.73	19.26	16.20	24.02	20.90	28.02	24.90
	7	4.15	...	5.92	...	7.97	5.28	9.96	6.82	13.34	9.96	16.51	12.76	20.58	16.61	24.02	20.90
	8	3.63	...	5.18	...	6.98	...	8.72	5.34	11.67	7.92	14.44	10.21	18.01	13.41	24.02	20.90
	9	3.23	...	4.60	...	6.20	...	7.75	...	10.37	...	12.84	8.28	16.01	10.96	24.02	20.90
	10	2.91	...	4.14	...	5.58	...	6.97	...	9.34	...	11.56	...	14.41	...	24.02	20.90
	11	2.64	...	3.77	...	5.07	...	6.34	...	8.49	...	10.51	...	13.10	...	24.02	20.90
	12	2.42	...	3.45	...	4.65	...	5.81	...	7.78	...	9.63	...	12.01	...	24.02	20.90
	13	2.24	...	3.19	...	4.29	...	5.36	...	7.18	...	8.89	...	11.08	...	24.02	20.90
	14	2.08	...	2.96	...	3.99	...	4.98	...	6.67	...	8.25	...	10.29	...	24.02	20.90
	15	1.94	...	2.76	...	3.72	...	4.65	...	6.23	...	7.70	...	9.61	...	24.02	20.90
	16	1.82	...	2.59	...	3.49	...	4.36	...	5.84	...	7.22	...	9.01	...	24.02	20.90
	17	1.71	...	2.44	...	3.28	...	4.10	...	5.49	...	6.80	...	8.48	...	24.02	20.90
	18	1.62	...	2.30	...	3.10	...	3.87	...	5.19	...	6.42	...	8.01	...	24.02	20.90
	19	1.53	...	2.18	...	2.94	...	3.67	...	4.91	...	6.08	...	7.58	...	24.02	20.90
	20	1.45	...	2.07	...	2.79	...	3.49	...	4.67	...	5.78	...	7.20	...	24.02	20.90
	21	1.38	...	1.97	...	2.66	...	3.32	...	4.45	...	5.50	...	6.86	...	24.02	20.90
	22	1.32	...	1.88	...	2.54	...	3.17	...	4.24	...	5.25	...	6.55	...	24.02	20.90
	23	1.26	...	1.80	...	2.43	...	3.03	...	4.06	...	5.02	...	6.27	...	24.02	20.90
	24	1.21	...	1.73	...	2.33	...	2.91	...	3.89	...	4.82	...	6.00	...	24.02	20.90
	25	1.16	...	1.66	...	2.23	...	2.79	...	3.74	...	4.62	...	5.76	...	24.02	20.90
	26	1.12	...	1.59	...	2.15	...	2.68	...	3.59	...	4.44	...	5.54	...	24.02	20.90
Total Deflection in inches for Maximum Load; Laterally fixed beam. Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. x Live Load Tabular Load	9	.252		.216		.189		.168		.151		.137		.126		.115	
	10	.310		.266		.233		.207		.186		.169		.155		.141	
	11	.375		.321		.281		.250		.225		.205		.188		.171	
	12	.447		.383		.335		.298		.268		.244		.223		.204	
	13	.525		.450		.394		.350		.315		.286		.263		.241	
	14	.608		.521		.456		.406		.365		.332		.304		.279	
	15	.698		.599		.524		.466		.419		.381		.341		.313	
	16	.795		.681		.596		.530		.477		.434		.398		.367	
	17	.898		.770		.674		.599		.539		.490		.449		.415	
	18	1.01		.861		.754		.670		.603		.548		.503		.467	
	19	1.12		.960		.840		.747		.672		.611		.560		.522	
	20	1.24		1.06		.931		.828		.745		.677		.621		.581	
	21	1.37		1.17		1.03		.912		.821		.746		.684		.642	
	22	1.51		1.29		1.13		1.00		.901		.819		.751		.707	
	24	1.79		1.53		1.34		1.19		1.07		.975		.894		.848	
	26	2.10		1.80		1.57		1.40		1.26		1.14		1.05		.994	

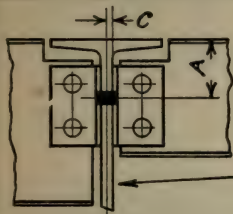
LOADS BY A. I. S. C. SPECIFICATION

CONNECTION ANGLES FOR J AND L JUNIOR BEAMS

DIMENSIONS, WEIGHTS, AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles			Weight inc. Web Rivets	Connection Details
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage	Size and Length		
			Single Shear							
			Power Driven Rivets	Unfin-ished Bolts						
6"	4.41	5130	9000	6000	3/8	IC. 4.15	1 15/16	3 x 3 x 1/4 4 1/4" Long	4 lbs.	<p>For IC. 4.15: - a = 2" For IC. 5.15: - a = 2 5/8"</p>
7"	5.48	5670	9000	6000	3/8	IC. 5.15	1 15/16	3 x 3 x 1/4 4 7/8" Long	5 lbs.	
8"	6.54	6075	9000	6000	3/8	IC. 5.15	1 15/16			
9"	7.48	6525	9000	6000	3/8	IC. 5.15	1 15/16			
10"	8.96	6975	9000	6000	3/8	IC. 5.15	1 15/16			
11"	10.23	7425	9000	6000	3/8	IC. 5.15	1 15/16			
12"	11.74	7875	9000	6000	3/8	IC. 5.15	1 15/16			



*Layer-out starts with this dimension at left end of beam. With beams ordered one half inch short, as recommended for J & L Junior beams, this leaves sufficient end distance at right end, in case of full allowable $\frac{3}{8}$ " underrun in beam lengths.

When A = 3½' all Junior beams can be framed opposite with tops flush.

Minimum Web required to develop Single Shearing Value is .33"
Minimum Web required to develop Double Shearing Value is .53"

ALLOWABLE END REACTIONS FOR J AND L JUNIOR BEAMS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for 2½" Bearing	Min. Span for 2½" Bearing	Reaction R for 3½" Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
6"	4.41	.114	12310	5620	2.59	7020	1400	8210	4.35
7"	5.48	.126	11890	6370	3.25	7860	1500	10580	5.32
8"	6.54	.135	11360	6900	4.05	8430	1530	12960	6.45
9"	7.48	.145	10960	7550	4.62	9140	1590	15660	7.60
10"	8.96	.155	10630	8240	5.67	9880	1650	18330	8.63
11'	10.23	.165	10340	8960	6.45	10660	1710	20930	9.52
12'	11.74	.175	10090	9710	7.42	11480	1770	23700	10.42

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests. When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

LOADS BY A. I. S. C. SPECIFICATION

6" TO 12"

BJ

BETHLEHEM STEEL JOISTS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia **S** is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for 2½" bearing. For details see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

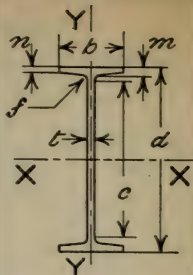
Q is Minimum Span in feet, uniformly loaded to cause W.

is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



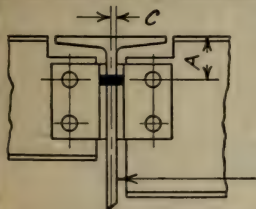
		6'		8'		10'		12'					
Depth—d".....		6.00	8.00	8.12	10.00	10.16	12.00	12.16					
Weight per foot.....		11.0	14.5	16.0	16.5	19.0	18.5	21.0					
Area, Sq. In.....		3.25	4.28	4.74	4.86	5.60	5.44	6.22					
b".....		3.33	3.875	3.875	4.000	4.010	4.125	4.135					
t".....		.230	.240	.240	.240	.250	.240	.250					
m.....		.359	.391	.451	.397	.477	.402	.482					
n.....		.230	.240	.300	.240	.320	.240	.320					
c.....		.25	.30	.30	.30	.30	.30	.30					
e.....		4.82	6.67	6.67	8.65	8.65	10.64	10.64					
AXES	X - X	I.....	19.3	44.9	52.4	77.4	94.5	121.5	147.0				
	S.....	6.43	11.23	12.91	15.48	18.60	20.25	24.18					
	r.....	2.44	3.24	3.32	3.99	4.11	4.73	4.86					
	Y - Y	I.....	1.64	2.73	3.31	3.02	3.90	3.33	4.30				
S.....	.98	1.41	1.71	1.51	1.95	1.61	2.08						
r.....	.71	.80	.84	.79	.83	.78	.83						
Coef. Str.....		77200	134700	154880	185760	223230	243000	290130					
Max. Mom. #.....		115800	202050	232320	278640	334840	364500	435200					
V.....		16560	23040	23390	28800	30480	34560	36480					
P. feet.....		2.33	2.92	3.31	3.23	3.66	3.52	3.98					
R.....		13800	16200	16300	16750	17790	16770	17890					
W.....		10360	10800	10800	10800	11260	10800	11260					
Q. feet.....		3.72	6.24	7.17	8.6	9.91	11.25	12.88					
w. lbs.....		6	9	9	9	9	9	9					
Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.	Span in feet	Laterally		Laterally		Laterally		Laterally		Laterally		Laterally	
	feet	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free	fixed	free
	6	12.86	11.58	22.45	20.92	25.81	24.45	30.96	29.60	37.21	35.60	40.50	39.05
	7	11.02	9.29	19.24	17.31	22.13	19.91	26.54	24.16	31.89	29.05	34.71	31.94
	8	9.65	7.58	16.84	14.31	19.36	16.46	23.22	20.03	27.90	24.09	30.38	26.56
	9	8.57	6.24	14.97	11.98	17.21	13.77	20.64	16.81	24.80	20.22	27.00	22.34
	10	7.72	5.20	13.47	10.12	15.49	11.63	18.58	14.24	22.32	17.13	24.30	18.97
	11	7.01	4.36	12.25	8.61	14.08	9.90	16.89	12.15	20.49	14.62	22.09	16.23
	12	6.43		11.22	7.37	12.91	8.49	15.48	10.44	18.29	12.57	20.25	13.98
	13	5.94		10.36		11.91		14.29	9.02	17.17	10.86	18.69	12.11
	14	5.51		9.62		11.06		13.27		15.95		17.36	
	15	5.14		8.98		10.33		12.38		14.88		16.20	
	16	4.83		8.42		9.68		11.61		13.95		15.19	
	17	4.54		7.92		9.11		10.93		13.13		14.29	
	18	4.29		7.48		8.60		10.32		12.40		13.50	
	19	4.06		7.09		8.15		9.78		11.75		12.79	
	20	3.86		6.74		7.74		9.29		11.16		12.15	
	22	3.51		6.12		7.04		8.44		10.15		11.05	
	24	3.22		5.61		6.45		7.74		9.30		10.13	
	26	2.97		5.18		5.96		7.14		8.59		9.35	
Total Deflection in inches for Maximum Load; Laterally fixed beam. Live Load deflection must not exceed 1/360 of the Span. Live Load Def. = Total Def. × Live Load Tabular Load	6	.112	.084	.084	.067	.067	.056	.056					
	7	.152	.114	.114	.091	.091	.076	.076					
	8	.198	.149	.149	.119	.119	.099	.099					
	9	.252	.189	.188	.151	.151	.126	.126					
	10	.310	.233	.233	.186	.186	.155	.155					
	11	.375	.281	.281	.225	.225	.188	.188					
	12	.447	.335	.335	.268	.268	.223	.223					
	13	.525	.394	.394	.315	.315	.263	.263					
	14	.608	.456	.456	.365	.365	.304	.304					
	15	.698	.524	.524	.419	.419	.341	.341					
	16	.795	.596	.596	.477	.477	.398	.398					
	17	.898	.674	.674	.539	.539	.449	.449					
	18	1.01	.754	.754	.603	.603	.503	.503					
	19	1.12	.840	.840	.672	.672	.560	.560					
20	1.24	.931	.931	.745	.745	.621	.621						
22	1.51	1.13	1.13	.901	.901	.751	.751						
24	1.79	1.34	1.34	1.07	1.07	.894	.894						
26	2.10	1.57	1.57	1.26	1.26	1.05	1.05						

CONNECTION ANGLES FOR BETHLEHEM STEEL JOISTS

DIMENSIONS, WEIGHTS, AND WORKING LOADS

3/4" POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles			Connection Details
Depth	Weight per foot	Web	Outstanding Single Shear			A.I.S.C. Mark	Gage g	Size and Length	
				Power Driven Rivets	Unfinished Bolts				
6"	11.0	10360	11930	8840	3/16	IC. 6.10	2 3/8	6" x 4" x 3/8" 0'-2 1/2' Long	6 lbs.
8"	14.5 16.0	10800 10800	11930 11930	8840 8840	3/16 3/16	IC. 9.10 IC. 9.10	2 5/8 2 5/8		
10"	16.5 19.0	10800 11260	11930 11930	8840 8840	3/16 3/16	IC. 9.10 IC. 9.10	2 5/8 2 5/8	4" x 3 1/2" x 3/8" 0'-3 1/2' Long	9 lbs.
12"	18.5 21.0	10800 11260	11930 11930	8840 8840	3/16 3/16	IC. 9.10 IC. 9.10	2 5/8 2 5/8		



*Layer-out starts with this dimension at left end of beam. With beams ordered one half inch short, as recommended for Bethlehem Steel Joists, this leaves sufficient end distance at right end, in case of full allowable $\frac{3}{8}$ " underrun in beam lengths.

When A = 3" all Bethlehem Steel Joists can be framed opposite with tops flush.

Minimum Web required to develop Single Shearing Value is .33"
Minimum Web required to develop Double Shearing Value is .53"

ALLOWABLE END REACTIONS FOR BETHLEHEM STEEL JOISTS

DETERMINED BY

BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for 2½" Bearing	Min. Span for 2½" Bearing	Reaction R for 3½" Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
6"	11.0	.230	15000	13800	2.80	17250	3450	16560	3.30
8"	14.5	.240	15000	16200	4.16	19800	3600	23040	4.40
	16.0	.240	15000	16300	4.75	19900	3600	23390	4.47
10"	16.5	.240	13960	16750	5.55	20100	3350	28800	6.10
	19.0	.250	14110	17790	6.27	21320	3530	30480	6.09
12"	18.5	.240	12710	16770	7.25	19820	3050	34560	8.33
	21.0	.250	12910	17890	8.11	21120	3230	36480	8.25

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests. When the reaction from the load exceeds the allowable reaction R , the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V .

12"
AND
15"
P

SPECIAL PHOENIX I BEAMS

DIMENSIONS—FUNCTIONS—ALLOWABLE TOTAL LOADS

I is Moment of Inertia S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

R is Allowable End Reaction for $3\frac{1}{2}$ " bearing. For details

see page of Allowable End Reactions.

W is Maximum Load on one Standard Connection.

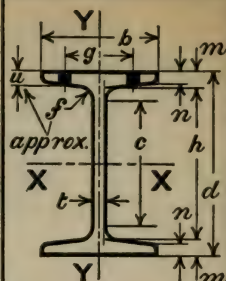
Q is Minimum Span in feet, uniformly loaded to cause W.

w is Weight of one Standard Connection including Angles and Web Rivets

Rivet given is Maximum Diameter in flange.

Allowable concentrated center loads are 50%

and their deflections 80% of those shown.



DIMENSIONS AND FUNCTIONS

Depth = d"	12"	15"
Wt. per foot.	27.5	36.0
Area.	8.09	10.59
b"	5.00	5.50
t"	.255	.289
h"	10.580	13.390
m"	.710	.805
n"	.315	.371
f"	.40	.45
c"	$9\frac{3}{4}$	$12\frac{5}{8}$
g"	3	$3\frac{1}{2}$
u"	$\frac{1}{2}$	$9\frac{1}{8}$
AXES	I....	405.1
	S....	54.01
	r....	6.17
Y-Y	I....	8.70
	S....	4.91
	r....	1.13
Coef. Str....	399200	648160
Max. Mom. %	598800	972240
V....	36700	52000
P. feet....	5.44	6.23
R....	21800	26000
W....	22950	26010
Q. feet....	8.70	12.46
w lbs....	13	19
Rivet dia....	$\frac{3}{4}$	$\frac{3}{4}$

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least. For laterally fixed beam loads not tabulated, divide the Coefficient of Strength by the Span in feet.

ALLOWABLE LOADS AND DEFLECTIONS

Span feet	12"			15"			Deflection
	Laterally		Total Deflect.	Laterally		Total Deflect.	
	fixed	free		fixed	free		
4	73.4	73.4	.025	104	104	.020	Live Load deflection must not exceed 1-360 of the Span. Total Def. x Live Load ----- Tabular Load
5	73.4	73.4	.039	104	104	.031	
6	66.5	66.5	.056	104	104	.045	
7	57.0	55.5	.076	92.6	92.1	.061	
8	49.9	46.8	.099	81.0	78.1	.079	
9	44.4	40.0	.126	72.0	67.1	.101	
10	39.9	34.4	.155	64.8	58.2	.124	
11	36.3	29.9	.188	58.9	50.8	.150	
12	33.3	26.2	.223	54.0	44.7	.179	
13	30.7	22.9	.263	49.9	39.5	.210	
14	28.5	20.2	.304	46.3	35.1	.243	
15	26.6	17.9	.341	43.2	31.3	.279	
16	25.0	16.0	.398	40.5	28.0	.318	
17	23.5449	38.1	25.1	.359	
18	22.2503	36.0	22.6	.402	
19	21.0560	34.1448	
20	20.0621	32.4497	
21	19.0684	30.9547	
22	18.1751	29.5601	
23	17.4822	28.2651	
Total Deflection in inches for Max. Load: Laterally fixed beam.							

CONNECTION ANGLES FOR SPECIAL PHOENIX I BEAMS

DIMENSIONS, WEIGHTS, AND WORKING LOADS

$\frac{3}{4}$ " POWER DRIVEN RIVETS

Beam		Connection Value			Framing Distance C	Connection Angles			Connection Details.
Depth	Weight per foot	Web	Outstanding			A.I.S.C. Mark	Gage g	Size and Length and Weight inc. Web Rivets	
			Single Shear						
			Power Driven Rivets	Unfin-ished Bolts					
12"	27.5	22950	23860	17670	3/16	IC.13.10	2 5/8	13	For complete details see drawing of Connection Angles of same weight as used for American Std. Beams.
15"	36.0	26010	47720	35340	3/16	IC.19.10	2 5/8	19	

ALLOWABLE END REACTIONS FOR SPECIAL PHOENIX I BEAMS DETERMINED BY BUCKLING OF UNSTIFFENED WEBS OVER VARIOUS LENGTHS OF BEARING

Depth in Inches	Weight per Foot	Web t	Unit Stress in Buckling	Reaction R for $3\frac{1}{2}$ " Bearing	Min. Span for $3\frac{1}{2}$ " Bearing	Reaction R for $5\frac{1}{2}$ " Bearing	Increase in R for 1" Additional Bearing	Max. Web Shear V.	Length of Bearing to develop V.
12	27.5	.255	13150	21800	9.16	28500	3350	36700	7.96
15	36.0	.289	12420	26000	12.46	33200	3590	52000	10.74

The beam web is treated as a column with fixed ends, having an effective length L of one-half the beam depth. The unit stress is determined by the A. I. S. C. column formula. The length of web resisting buckling is assumed as the actual bearing on the bracket or wall plate plus one-fourth the beam depth. This agrees with the results of numerous tests. When the reaction from the load exceeds the allowable reaction R, the beam web must be stiffened or additional length of bearing provided; but in no case shall the reaction exceed the allowable shearing value V.

LOADS BY A. I. S. C. SPECIFICATION

Part IV

Section 9

Beam Summary

giving
Size and Weight
of
Beams
to be used for
Spans
from 4—50 feet
and for
Loads
from 1—650 Kips.

Continuous Load, Uniformly Distributed

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET—BEAMS LATERALLY FIXED																					
			4	5	6	7	8	9	10	11	12	13	14	15	16	18	20	22	24					
3" I	5.7	1.67	5.0	4.0	3.3	2.9	2.5	2.2	2.0	1.8	1.7	1.5	1.4	1.3										
3" I	6.5	1.80	5.4	4.3	3.6	3.1	2.7	2.4	2.2	2.0	1.8	1.7	1.5	1.4										
3" I	7.5	1.93	5.8	4.6	3.9	3.3	2.9	2.6	2.3	2.1	1.9	1.8	1.7	1.5										
6" J	4.41	2.42	7.3	5.8	4.9	4.2	3.6	3.2	2.9	2.6	2.4	2.2	2.1	1.9										
4" I	7.7	3.0	9.0	7.2	6.0	5.1	4.5	4.0	3.6	3.3	3.0	2.8	2.6	2.4										
4" I	8.5	3.15	10	8	6	5	5	4	4	3	3	3	3	3										
5" I	9.5	3.35	10	8	7	6	5	5	4	4	3	3	3	3										
7" J	5.48	3.45	10	8	7	6	5	5	4	4	3	3	3	3										
4" I	10.5	3.55	11	9	7	6	5	5	4	4	3	3	3	3										
8" J	6.54	4.65	14	11	9	8	7	6	6	5	5	4	4	4	3	3		3	3					
5" I	10.0	4.84	15	12	10	8	7	7	6	5	5	5	4	4	4	3	3		3	3				
5" I	12.25	5.40	16	13	11	9	8	7	7	6	5	5	5	4	4	4	3	3		3	3			
9" J	7.48	5.81	17	14	12	10	9	8	7	6	6	5	5	5	4	4	4	3	3					
5" I	14.75	6.00	18	14	12	10	9	8	7	6	6	5	5	5	4	4	4	3	3					
6" BJ	11.0	6.43	19	15	13	11	10	9	8	7	6	6	5	5	4	4	4	3	3					
6" I	12.5	7.27	22	17	15	13	11	10	9	8	7	7	6	6	5	4	4	4	3	3				
10" J	8.96	7.78	23	19	16	13	12	10	9	8	7	7	6	6	5	4	4	4	3	3				
6" I	14.75	7.93	24	19	16	14	12	11	10	9	8	7	7	6	5	4	4	4	3	3				
6" I	17.25	8.67	26	21	17	15	13	12	10	10	9	8	7	7	6	5	4	4	3	3				
11" J	10.23	9.63	29	23	19	17	14	13	12	11	10	9	8	8	7	6	5	4	3	3				
7" I	15.3	10.34	31	25	21	18	16	14	12	11	10	10	9	8	7	6	5	4	3	3				
7" I	17.5	11.11	33	27	22	19	17	15	13	12	11	10	10	9	8	7	6	5	4	3				
8" BJ	14.5	11.23	34	27	22	19	17	15	13	12	11	10	10	9	8	7	6	5	4	3				
7" I	20.0	11.97	36	29	24	21	18	16	14	13	12	11	10	10	9	8	7	6	5	4				
12" J	11.74	12.01	36	29	24	21	18	16	14	13	12	11	10	10	9	8	7	6	5	4				
8" BJ	16.0	12.91	39	31	26	22	19	17	15	14	13	12	11	10	10	9	8	7	6	5				
8" I	18.4	14.22	43	34	29	24	21	19	17	16	14	13	12	11	11	9	8	7	6	5				
8" Cm	17.5	14.35	43	34	29	25	22	19	17	16	14	13	12	11	11	10	9	8	7	6				
8" B	17.5	14.43	43	35	29	25	22	19	17	16	14	13	12	12	11	10	9	8	7	6				
8" I	20.5	15.05	45	36	30	26	23	20	18	16	15	14	13	12	11	10	9	8	7	6				
10" BJ	16.5	15.48	46	37	31	27	23	21	19	17	15	14	13	12	12	10	9	8	7	6				
8" B	19.0	15.81	47	38	32	27	24	21	19	17	16	15	14	13	12	11	9	8	7	6				
8" Cm	21.0	15.85	48	38	32	27	24	21	19	17	16	15	14	13	12	11	10	9	8	7				
8" I	23.0	16.05	48	39	32	28	24	21	19	18	16	15	14	13	12	11	10	9	8	7				
8" I	25.5	17.02	51	41	34	29	26	23	20	19	17	16	15	14	13	11	10	9	8	7				
10" BJ	19.0	18.60	56	45	37	32	28	25	22	20	19	17	16	15	14	12	11	10	9	8				
9" I	21.8	18.67	57	45	38	32	28	25	23	21	19	17	16	15	14	13	11	10	9	8				
9" B	20.5	19.22	54	46	39	33	29	26	23	21	19	18	17	15	14	13	12	11	10	9				
9" Cm	20.5	19.24	51	46	39	33	29	26	23	21	19	18	17	15	14	13	12	11	10	9				
12" BJ	18.5	20.25	61	49	41	35	30	27	24	22	20	19	17	16	15	14	12	11	10	9				
9" I	25.0	20.31	61	49	41	35	31	27	24	22	20	19	17	16	15	14	12	11	10	9				
9" B	22.0	20.73	57	50	42	36	31	28	25	23	21	19	18	17	16	14	12	11	10	9				
8" C	24.0	21.08	46	46	42	36	32	28	25	23	21	19	18	17	16	14	13	12	11	10				
9" Cm	25.0	21.22	64	51	42	36	32	28	26	23	21	20	18	17	16	14	13	12	11	10				
10" C	21.0	21.73	55	52	44	37	33	29	26	24	22	20	19	17	16	15	13	12	11	10				
10" B	21.0	21.84	57	52	44	38	33	29	26	24	22	20	19	18	16	15	13	12	11	10				
9" I	30.0	22.53	68	54	45	39	34	30	27	25	23	21	19	18	17	15	14	12	11	10				
8" C	27.0	23.68	52	52	47	41	36	32	28	26	24	22	20	19	18	16	14	13	12	11				
12" BJ	21.0	24.18	73	58	48	41	36	32	29	26	24	22	21	19	18	16	15	13	12	11				
10" I	25.4	24.42	73	59	49	42	37	33	29	26	24	23	21	20	18	16	15	13	12	11				
10" C	23.0	24.44	55	55	49	42	37	33	29	27	24	23	21	20	18	16	15	13	12	11				
10" B	23.5	24.64	60	59	49	42	37	33	30	27	25	23	21	20	19	17	15	14	12	11				
9" I	35.0	24.73	74	59	50	42	37	33	30	27	25	23	21	20	19	17	15	14	12	11				
8" G	29.5	25.56	54	54	51	44	38	34	31	28	26	24	22	20	19	17	15	14	12	11				
8" C	30.0	26.31	59	59	53	45	40	35	32	29	26	24	23	21	20	18	16	14	13	12				
10" I	30.0	26.70	80	64	53	46	40	36	32	29	27	25	23	21	20	18	16	15	13	12				
10" B	26.0	27.33	65	65	55	47	41	36	33	30	27	25	23	22	21	18	16	15	14	12				
8" C	31.0	27.52	56	56	55	47	41	37	33	30	28	25	24	22	21	18	17	15	14	12				
10" C	26.0	27.63	63	63	55	47	41	37	33	30	28	26	24	22	21	18	17	15	14	12				
9" C	29.0	28.00	60	60	56	48	42	37	34	31	28	26	24	22	21	19	17	15	14	12				
8" G	33.0	29.03	56	56	56	50	44	39	35	32	29	27	25	23	22	19	17	16	15	13				
10" I	35.0	29.16	88	70	58	50	44	39	35	32	29	27	25	23	22	21	18	16	15	13				
10" B	28.5	30.25	70	70	61	52	45	40	36	33	30	28	26	24	23	20	18	16	15	13				
12" C	25.0	30.69	69	69	61	53	46	41	37	34	31	28	26	25	23	21	18	17	15	13				
9" C	32.0	30.89	67	67	62	53	46	41	37	34	31	29	27	25	23	21	19	17	15	13				
12" B	25.0	31.16	68	68	62	53	47	42	37	34	31	29	27	25	23	21	19	17	15	13				
10" I	40.0	31.60	95	76	63	54	47	42	38	35	32	29	27	25	24	21	19	17	15	13				
10" C	30.0	31.91	73	73	64	55	48	43	38	35	32	30	27	26	24	21	19	17	15					

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET — BEAMS Laterally Fixed																	
			4	6	8	10	11	12	13	14	15	16	18	20	22	24	26	28	30	
8" C	36.0	32.03	66	64	48	38	35	32	30	28	26	24	21	19	18	16				
8" G	36.5	32.66	60	60	49	39	36	33	30	28	26	24	22	20	18	16				
10" C	31.0	32.68	77	65	49	39	36	33	30	28	26	25	22	20	18	16				
12" P	27.5	33.27	73	67	50	40	36	33	31	29	27	25	22	20	18	16				
9" C	35.0	33.81	74	68	51	41	37	34	31	29	27	25	23	20	18	17				
10" C	36.0	35.12	105	70	53	42	38	35	32	30	28	26	23	21	19	18				
12" C	28.0	35.57	69	69	53	43	39	36	33	31	28	27	24	21	19	18				
12" B	28.0	35.60	71	71	53	43	39	36	33	31	28	27	24	21	19	18				
9" G	36.0	35.91	62	62	54	43	39	36	33	31	29	27	24	22	20	18				
12" I	31.8	35.97	101	72	54	43	39	36	33	31	29	27	24	22	20	18				
8" C	42.0	37.37	78	75	56	45	41	37	35	32	30	28	25	22	20	19				
12" I	35.0	37.83	114	76	57	45	41	38	35	32	30	28	25	23	21	19				
9" C	38.0	37.87	68	68	57	45	41	38	35	33	30	28	25	23	21	19				
10" C	42.0	38.08	114	76	57	46	42	38	35	33	31	29	25	23	21	19				
9" G	38.5	38.20	67	67	57	46	42	38	35	33	31	29	25	23	21	19				
12" C	34.0	39.61	108	79	59	48	43	40	37	34	32	30	26	24	22	20				
12" B	31.5	40.54	79	79	61	49	44	41	37	35	32	30	27	24	22	20				
12" C	32.0	40.65	80	80	61	49	44	41	38	35	33	31	27	24	22	20				
14" C	30.0	41.82	91	84	63	50	46	42	39	36	34	31	28	25	23	21	19	18	17	
14" B	30.0	42.49	88	85	64	51	46	43	39	36	34	32	28	26	23	21	20	18	17	
9" G	43.5	42.85	77	77	64	51	47	43	40	37	34	32	29	26	23	21				
9" C	43.0	42.86	78	78	64	51	47	43	40	37	34	32	29	26	23	21				
12" I	40.8	44.82	132	90	67	54	49	45	41	38	36	34	30	27	24	22				
10" G	41.5	45.57	74	74	68	55	50	46	42	39	36	34	30	27	25	23				
12" C	36.0	45.78	90	90	69	55	50	46	42	39	37	34	31	28	25	23				
12" B	36.0	46.01	88	88	69	55	50	46	42	39	37	35	31	28	25	23				
12" I	45.0	47.35	142	95	71	57	52	47	44	41	38	36	32	28	26	24				
14" C	33.0	47.63	91	91	72	57	52	48	44	41	38	36	32	29	26	24	22	20	19	
14" B	33.0	47.76	89	89	72	57	52	48	44	41	38	36	32	29	26	24	22	21	19	
9" C	48.0	47.85	88	88	72	57	52	48	44	41	38	36	32	29	26	24				
10" G	44.5	49.34	77	77	74	59	54	49	46	42	39	37	33	30	27	25				
12" B	40.0	50.20	95	95	75	60	55	50	46	43	40	38	33	30	27	25				
12" I	50.0	50.27	151	101	75	60	55	50	46	43	40	38	34	30	27	25				
14" C	38.0	51.07	126	102	77	61	56	51	47	44	41	38	34	31	28	26	24	22	20	
14" C	36.0	51.93	99	99	78	62	57	52	48	45	42	39	35	31	28	26	24	22	21	
12" C	40.0	52.28	84	84	78	63	57	52	48	45	42	39	35	31	29	26				
12" I	55.0	53.22	160	106	80	64	58	53	49	46	43	40	36	32	29	27				
15" P	36.0	54.01	104	104	81	65	59	54	50	46	43	41	36	32	30	27				
14" B	37.5	54.35	103	103	82	65	59	54	50	47	44	41	36	33	30	27	25	23	22	
10" C	49.0	54.40	84	84	82	65	59	54	50	47	44	41	36	33	30	27				
16" C	35.0	54.68	111	109	82	66	60	55	51	47	44	41	37	33	30	27	25	24	22	
10" G	50.0	54.84	87	87	82	66	60	55	51	47	44	41	37	33	30	27				
15" B	36.0	55.12	100	100	83	66	60	55	51	47	44	41	37	33	30	28	25	24	22	
16" B	35.0	55.13	108	108	83	66	60	55	51	47	44	41	37	33	30	28	25	24	22	
12" B	44.0	55.30	105	105	83	66	60	55	51	47	44	41	37	33	30	28				
14" C	39.0	56.26	108	108	84	68	61	56	52	48	45	42	38	34	31	28	26	24	23	
10" C	54.0	56.86	119	114	85	68	62	57	52	49	45	43	38	34	31	28				
12" C	45.0	58.85	95	95	88	71	64	59	54	50	47	44	39	35	32	29				
15" I	42.9	58.91	148	118	88	71	64	59	54	50	47	44	39	35	32	29	27	25	24	
10" C	59.0	59.30	155	119	89	71	65	59	55	51	47	44	40	36	32	30				
16" C	38.0	59.34	121	118	89	71	65	59	55	51	47	44	40	36	32	30	27	25	24	
15" B	38.5	59.68	104	104	90	72	65	60	55	51	48	45	40	36	33	30	28	26	24	
15" I	45.0	60.48	163	121	91	73	66	60	56	52	48	45	40	36	33	30	28	26	24	
14" C	42.0	60.60	117	117	91	73	66	61	56	52	49	46	40	36	33	30	28	26	24	
12" B	48.5	60.93	116	116	91	73	66	61	56	52	49	46	41	37	33	30				
14" B	42.0	61.26	116	116	92	74	67	61	57	53	49	46	41	37	33	31	28	26	25	
15" B	40.0	61.65	110	110	92	74	67	62	57	53	49	46	41	37	34	31	28	26	25	
10" C	64.0	61.76	185	124	93	74	67	62	57	53	49	46	41	37	34	31				
15" I	50.0	64.15	192	128	96	77	70	64	59	55	51	48	43	38	35	32	30	27	26	
15" B	42.5	65.21	118	118	98	78	71	65	60	56	52	49	43	39	36	33	30	28	26	
12" C	50.0	65.35	106	106	98	78	71	65	60	56	52	49	44	39	36	33				
15" B	40.0	65.58	111	111	98	79	72	66	61	56	52	49	44	39	36	33	30	28	26	
16" C	43.0	65.75	143	132	99	79	72	66	61	56	53	49	44	40	36	33	30	28	26	
16" B	40.0	65.78	113	113	99	79	72	66	61	56	53	49	44	40	36	33	30	28	26	
12" G	51.5	67.27	103	103	101	81	73	67	62	58	54	50	45	40	37	34				

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET—BEAMS Laterally Fixed																32	34	36	38
			6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36				
15" I	55.0	67.83	136	102	81	68	58	51	45	41	37	34	31	29	27							
15" B	46.0	68.91	129	103	83	69	59	52	46	41	38	35	32	30	28							
14" C	48.0	70.86	115	106	85	71	61	53	47	43	39	35	33	30	28							
12" C	55.0	71.40	108	107	86	71	61	54	48	43	39	36	33									
12" G	55.5	72.60	109	109	87	73	62	54	48	44	40	36	33									
16" B	45.0	73.76	128	111	89	74	63	55	49	44	40	37	34	32	30							
16" C	45.0	73.78	126	111	89	74	63	55	49	44	40	37	34	32	30							
15" B	50.5	75.71	137	114	91	76	65	57	50	45	41	38	35	32	30							
12" C	60.0	77.90	119	117	93	78	67	58	52	47	43	39	36									
14" C	53.0	78.25	128	117	94	78	67	59	52	47	43	39	36	34	31							
12" G	61.0	79.80	119	119	96	80	68	60	53	48	44	40	37									
15" I	60.8	81.20	162	122	97	81	70	61	54	49	44	41	37	35	32							
16" C	50.0	81.95	141	123	98	82	70	61	55	49	45	41	38	35	33							
15" B	54.5	82.27	148	123	99	82	71	62	55	49	45	41	38	35	33							
16" B	50.0	82.34	142	124	99	82	71	62	55	49	45	41	38	35	33	31						
12" G	66.0	83.65	128	126	100	84	72	63	56	50	46	42	39									
15" I	65.0	84.28	169	126	101	84	72	63	56	51	46	42	39	36	34							
18" B	47.0	85.18	140	128	102	85	73	64	57	51	47	43	39	37	34	32	30	28				
18" C	47.0	85.40	138	128	102	85	73	64	57	51	47	43	39	37	34	32	30	28				
14" C	58.0	85.58	141	128	103	86	73	64	57	51	47	43	40									
12" C	66.0	85.76	132	129	103	86	74	64	57	51	47	43	40									
12" C	65.0	86.88	115	115	104	87	75	65	58	52	47	43	40									
15" I	70.0	87.95	176	132	106	88	75	66	59	53	48	44	41	38	35							
18" I	54.7	88.39	177	133	106	88	76	66	59	53	48	44	41	38	35	33	31	29				
18" B	49.0	89.20	143	134	107	89	76	67	59	54	49	45	41	38	36	33	31	30				
15" B	59.5	89.44	163	134	107	89	77	67	60	54	49	45	41	38	36							
12" C	70.0	89.83	151	135	108	90	77	67	60	54	49	45	41									
18" C	51.0	89.88	162	135	108	90	77	67	60	54	49	45	41	39	36	34	32	30				
12" G	70.5	90.60	135	135	109	91	78	68	60	54	49	45	42									
15" I	75.0	91.63	183	137	110	92	79	69	61	55	50	46	42	39	37							
18" I	60.0	93.09	186	140	112	93	80	70	62	56	51	47	43	40	37	35	33	31				
14" C	61.0	93.12	129	129	112	93	80	70	62	56	51	47	43	40	37							
12" C	76.0	93.36	187	140	112	93	80	70	62	56	51	47	43									
16" B	56.5	93.49	143	140	112	94	80	70	62	56	51	47	43	40	37	35	33	31				
18" B	52.0	94.32	154	141	113	94	81	71	63	57	51	47	44	40	38	35	33	31				
18" C	52.0	94.41	154	142	113	94	81	71	63	57	52	47	44	40	38	35	33	31				
16" C	58.0	97.08	144	144	117	97	83	73	65	58	53	49	45	42	39	36	34	32				
18" I	65.0	97.53	195	146	117	98	84	73	65	59	53	49	45	42	39	37	34	32				
12" G	76.5	98.05	148	147	118	98	84	74	65	59	54	49	45									
18" B	54.5	98.91	161	148	119	99	85	74	66	59	54	49	46	42	40	37	35	33				
16" B	60.5	101.51	150	150	122	102	87	76	68	61	55	51	47	44	41	38	36	34				
18" I	70.0	101.94	204	153	122	102	87	76	68	61	56	51	47	44	41	38	36	34				
14" C	68.0	103.78	145	145	125	104	89	78	69	62	57	52	48	45	42							
15" G	64.5	104.13	139	139	125	104	89	78	69	63	57	52	48	45	42	39	37	35				
18" C	58.0	105.28	172	158	126	105	90	79	70	63	57	53	49	45	42	39	37	35				
16" C	63.0	105.49	157	157	127	106	90	79	70	63	58	53	49	45	42	40	37					
15" B	71.5	106.60	187	160	128	107	91	80	71	64	58	53	49	46	43	41	38	36	34			
18" B	59.0	108.20	162	162	130	108	93	81	72	65	59	54	50	46	43	41	39	37	35			
20" B	56.0	109.27	179	164	131	109	94	82	73	66	60	55	50	47	44	41	39	37	35			
15" G	69.0	109.58	150	150	132	110	94	82	73	66	60	55	51	47	44	41	39	37				
16" B	66.0	110.22	162	162	132	110	95	83	74	66	60	55	51	47	44	41						
21" C	55.0	111.70	180	168	134	112	96	84	74	67	61	56	52	48	45	42	39	37	35			
22" B	54.5	113.34	188	170	136	113	97	85	76	68	62	57	52	49	45	43	40					
16" C	68.0	113.85	171	171	137	114	98	85	76	68	62	57	53	49	46	43	40					
14" C	75.0	114.52	162	162	137	115	98	86	76	69	63	57	53	49	46							
20" I	65.4	116.95	234	175	140	117	100	88	78	70	64	58	54	50	47	44	41	39	37			
20" B	59.5	118.15	180	177	142	118	101	89	79	71	64	59	55	51	47	44	42	39	37			
18" B	64.5	118.53	172	172	142	119	102	89	79	71	65	59	55	51	47	44	42	40				
15" G	74.0	119.03	158	158	143	119	102	89	79	71	65	60	55	51	48	45	42	40				
16" B	71.5	119.82	177	177	144	120	103	90	80	72	65	60	55	51	48	45						
21" C	58.0	120.30	181	180	144	120	103	90	80	72	66	60	56	52	48	45	42	40	38			
20" I	70.0	121.42	243	182	146	121	104	91	81	73	66	61	56	52	49	46	43	40	38			
20" B	62.0	123.61	188	185	148	124	106	93	82	74	67	62	57	53	49	46	44	41	39			
18" C	67.0	124.12	175	175	149	124	106	93	83	74	68	62	57	53	50	47	44	41				
22" B	58.0	124.67	189	187	150	125	107	94	83	75	68	62	58	53	50	47	44	42	39			
20" I	75.0	126.35	253	190	152	126	108	95	84	76	69	63	58	54	51	47	45	42	40			
18" I	75.6	126.87	242	190	152	127	109	95	85	76	69	63	59	54	51	48	45	42				

LOADS BY A. I. S. C. SPECIFICATION

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET—BEAMS Laterally Fixed																	
			8	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	
18" B	69.0	128.19	181	154	128	110	96	85	77	70	64	59	55	51	48	45	43			
20" B	64.5	128.74	193	154	129	111	97	86	77	70	64	59	55	51	48	45	43	41		
15" G	80.5	129.29	174	155	129	111	97	86	78	71	65	60	55	52	48	46	43			
16" G	74.5	130.18	149	149	130	112	98	87	78	71	65	60	56	52	49	46	43			
18" I	80.0	130.76	196	157	131	112	98	87	78	71	65	60	56	52	49	46	44			
14" C	85.0	131.61	146	146	132	113	99	88	79	72	66	61	56	53						
16" C	76.0	132.66	161	159	133	114	100	88	80	72	66	61	57	53	50	47				
21" C	64.0	132.85	199	159	133	114	100	89	80	72	66	61	57	53	50	47	44	42		
18" C	72.0	133.42	190	160	133	114	100	89	80	73	67	62	57	53	50	47	44			
18" I	85.0	135.18	203	162	135	116	101	90	81	74	68	62	58	54	51	48	45			
22" B	62.5	135.95	195	163	136	117	102	91	82	74	68	63	58	54	51	48	45	43		
20" B	68.5	137.42	196	165	137	118	103	92	83	75	69	63	59	55	52	49	46	43		
18" B	74.0	137.88	191	165	138	118	103	92	83	75	69	64	59	55	52	49	46			
18" I	90.0	139.61	209	168	140	120	105	93	84	76	70	64	60	56	52	49	47			
16" G	81.0	141.41	161	171	141	121	106	94	85	77	71	65	61	57	53	50	47			
18" C	78.0	144.59	206	174	145	124	108	96	87	79	72	67	62	58	54	51	48			
16" C	83.0	144.88	177	174	145	124	109	97	87	79	72	67	62	58	54	51				
21" C	70.0	145.23	218	174	145	124	109	97	87	79	73	67	62	58	54	51	48	46	44	
20" I	81.4	146.63	220	176	147	126	110	98	88	80	73	68	63	59	55	52	49	46	44	
14" C	95.0	147.19	165	165	147	126	110	98	88	80	74	68	63	59						
15" G	94.0	147.32	192	177	147	126	111	98	88	80	74	68	63	59	55	52				
22" B	67.5	148.06	207	178	148	127	111	99	89	81	74	68	63	59	56	52	49	46	44	
20" B	73.0	148.50	206	178	149	127	111	99	89	81	74	69	64	59	56	52	50	47	45	
20" I	85.0	150.17	225	180	150	129	113	100	90	82	75	69	64	60	56	53	50	47	45	
16" G	87.0	152.70	174	174	153	131	115	102	92	83	76	71	65	61	57	54	51			
15" G	99.0	154.26	203	185	154	132	116	103	93	84	77	71	66	62	58	54	51			
18" G	80.0	154.44	180	180	154	132	116	103	93	84	77	71	66	62	58	55	51	49	46	
20" I	90.0	155.03	233	186	155	133	116	103	93	85	78	72	66	62	58	55	52	49	47	
16" C	90.0	157.08	193	189	157	135	118	105	94	86	79	73	67	63	59	55				
21" C	76.0	157.60	236	189	158	135	118	105	95	86	79	73	68	63	59	56	53	50	47	
20" B	78.0	157.84	222	189	158	135	118	105	95	86	79	73	68	63	59	56	53	50	47	
20" I	95.0	159.97	240	192	160	137	120	107	96	87	80	74	69	64	60	56	53	50	48	
22" B	73.0	161.50	222	194	162	138	121	108	97	88	81	75	69	65	61	57	54	51	48	
14" C	105.0	162.78	185	185	163	140	122	109	98	89	81	75	70	65						
24" C	70.0	162.82	230	195	163	140	122	109	98	89	81	75	70	65	61	57	54	51	49	
24" B	70.0	163.66	226	196	164	140	123	109	98	89	82	76	70	66	61	58	55	52	49	
15" G	105.0	164.17	216	197	164	141	123	109	99	90	82	76	70	66	62	58	55			
20" I	100.0	164.83	247	198	165	141	124	110	99	90	82	76	71	66	62	58	55	52	49	
16" G	94.0	165.10	189	189	165	142	124	110	99	90	83	76	71	66	62	58	55			
18" G	86.0	167.07	190	190	167	143	125	111	100	91	84	77	72	67	63	59	56	53	50	
18" C	86.0	168.23	185	185	168	144	126	112	101	92	84	78	72	67	63	59	56			
22" B	77.0	170.63	223	205	171	146	128	114	102	93	85	79	73	68	64	60	57	54	51	
21" C	80.0	170.90	221	205	171	146	128	114	103	93	85	79	73	68	64	60	57	54	51	
24" I	79.9	173.93	261	209	174	149	130	116	104	95	87	80	74	70	65	61	58	55	52	
15" G	111.0	174.51	232	209	175	150	131	116	105	95	87	81	75	70	65	62	58			
24" B	73.5	175.73	228	211	176	151	132	117	105	96	88	81	75	70	66	62	59	55	53	
16" C	100.0	178.35	178	178	178	153	134	119	107	97	89	82	76	71	67	63				
18" G	92.0	179.75	200	200	180	154	135	120	108	98	90	83	77	72	67	63	60	57	54	
24" I	85.0	180.00	270	216	180	154	135	120	108	98	90	83	77	72	68	63	60	57	54	
18" C	93.0	181.94	201	201	182	156	136	121	109	99	91	84	78	73	68	64	61			
24" C	76.0	182.03	233	218	182	156	137	121	109	99	91	84	78	73	68	64	61	57	55	
21" C	86.0	183.65	238	220	184	157	138	122	110	100	92	85	79	73	69	65	61	58	55	
22" B	83.0	184.23	240	221	184	158	138	123	111	101	92	85	79	74	69	65	61	58	55	
24" I	90.0	185.84	279	223	186	159	139	124	111	101	93	86	80	74	70	66	62	59	56	
24" B	79.5	188.19	249	226	188	161	141	125	113	103	94	87	81	75	71	66	63	59	56	
16" C	107.0	190.84	192	192	191	164	143	127	114	104	95	88	82	76	72	67				
24" I	95.0	191.80	288	230	192	164	144	128	115	105	96	89	82	77	72	68	64	61	58	
15" G	127.0	191.95	258	230	192	165	144	128	115	105	96	89	82	77	72	68				
18" G	99.0	193.72	212	212	194	166	145	129	116	106	97	89	83	77	73	68	65	61	58	
18" C	100.0	195.57	218	218	196	168	147	130	117	107	98	90	84	78	73	69	65			
21" C	92.0	196.46	256	236	196	168	147	131	118	107	98	91	84	79	74	69	65	62	59	
24" I	100.0	197.65	296	237	198	169	148	132	119	108	99	91	85	79	74	70	66	62	59	
22" B	89.0	197.88	257	237	198	170	148	132	119	108	99	91	85	79	74	70	66	63	59	
24" B	84.5	200.48	265	241	201	172	150	134	120	109	100	93	86	80	75	71	67	63	60	
26" B	81.0	201.71	272	242	202	173	151	135	121	110	101	93	87	81	76	71	67	64	61	

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET—BEAMS Laterally FIXED																	
			12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	45	50	
15" G	135.0	202.94	203	174	152	135	122	111	101	94	87	81	76	72	68					
24" C	85.0	203.46	203	174	153	136	122	111	102	94	87	81	76	72	68	64	61			
16" C	115.0	205.17	205	176	154	137	123	112	103	95	88	82	77	72						
20" G	99.0	206.02	206	177	155	137	124	112	103	95	88	82	77	73	69	65	62			
21" C	98.0	209.24	209	179	157	139	126	114	105	97	90	84	78	74	70	66	63			
15" G	141.0	212.91	213	182	160	142	128	116	106	98	91	85	80	75	71					
22" B	96.5	213.37	213	183	160	142	128	116	107	99	91	85	80	75	71	67	64			
26" B	85.5	214.26	214	184	161	143	129	117	107	99	92	86	80	76	72	68	64	57		
24" B	90.5	214.61	215	184	161	143	129	117	107	99	92	86	81	76	72	68	64			
27" C	85.0	216.20	216	185	162	144	130	118	108	100	93	86	81	76	72	68	65	58	52	
20" G	107.0	221.98	222	190	167	148	133	121	111	102	95	89	83	78	74	70	67			
28" B	85.0	222.12	222	190	167	148	133	121	111	103	95	89	83	78	74	70	67	59	53	
15" G	147.0	222.94	223	191	167	149	134	122	111	103	96	89	84	79	74					
24" C	94.0	225.02	225	193	169	150	135	123	113	104	96	90	84	79	75	71	68			
24" B	95.5	225.24	225	193	169	150	135	123	113	104	97	90	84	79	75	71	68			
26" B	91.0	230.24	230	197	173	153	138	126	115	106	99	92	86	81	77	73	69	61		
24" I	105.9	234.30	234	201	176	156	141	128	117	108	100	94	88	83	78	74	70			
21" C	104.0	235.74	234	202	177	157	141	129	118	109	101	94	88	83	79	74	71			
20" G	113.0	236.28	236	203	177	158	142	129	118	109	101	95	89	83	79	75	71			
22" G	101.0	236.78	236	203	178	158	142	129	118	109	101	95	89	84	79	75	71			
24" B	99.5	236.78	237	203	178	158	142	129	118	109	101	95	89	84	79	75	71			
27" C	91.0	238.30	238	204	179	159	143	130	119	110	102	95	89	84	79	75	71	64	57	
24" I	110.0	239.10	239	205	179	159	143	130	120	110	102	96	90	84	80	76	72			
24" I	115.0	245.04	245	210	184	163	147	134	123	113	105	98	92	86	82	77	74			
28" B	91.0	246.85	247	212	185	165	148	135	123	114	106	99	93	87	82	78	74	66	59	
26" B	98.0	247.41	247	212	186	165	148	135	124	114	106	99	93	87	82	78	74	66		
24" B	104.5	248.84	249	213	187	166	149	136	124	115	107	100	93	88	83	79	75			
24" I	120.0	250.90	251	215	188	167	151	137	125	116	108	100	94	89	84	79	75			
20" G	120.0	251.29	251	215	188	168	151	137	126	116	108	100	94	89	84	79	75			
24" C	100.0	251.71	252	216	189	168	151	137	126	116	108	101	94	89	84	79	76	67	60	
21" C	112.0	254.07	253	218	191	169	152	139	127	117	109	102	95	90	85	80	76			
22" G	108.0	254.94	253	219	191	170	153	139	128	118	109	102	96	90	85	81	77			
20" G	127.0	264.03	264	226	198	176	158	144	132	122	113	106	99	93	88	83	79			
27" C	101.0	264.72	265	227	199	176	159	144	132	122	113	106	99	93	88	84	79	71	64	
28" B	97.0	265.11	265	227	199	177	159	145	133	122	114	106	99	94	88	84	80	71	64	
24" G	107.0	266.87	267	229	200	178	160	146	133	123	114	107	100	94	89	84	80	71	64	
21" C	120.0	272.11	272	233	204	181	163	148	136	126	117	109	102	96	91	86	82			
22" G	116.0	273.16	271	234	205	182	164	149	137	126	117	109	102	96	91	86	82			
24" C	110.0	276.83	277	237	208	185	166	151	138	128	119	111	104	98	92	87	83	74	66	
20" G	135.0	280.57	281	240	210	187	168	153	140	130	120	112	105	99	94	89	84			
24" G	113.0	281.68	282	241	211	188	169	154	141	130	121	113	106	99	94	89	85	75	68	
28" B	104.0	284.73	285	244	214	190	171	155	142	131	122	114	107	100	95	90	85	76	68	
21" C	128.0	290.42	290	249	218	194	174	158	145	134	124	116	109	102	97	92	87			
27" C	112.0	293.17	293	251	220	195	176	160	147	135	126	117	110	103	98	93	88	78	70	
22" G	124.0	293.19	291	251	220	195	176	160	147	135	126	117	110	104	98	93	88			
20" G	142.0	296.06	296	254	222	197	178	162	148	137	127	118	111	105	99	94	89			
24" G	120.0	300.65	301	258	225	200	180	164	150	139	129	120	113	106	100	95	90	80	72	
24" C	120.0	301.91	302	259	226	201	181	165	151	139	129	121	113	107	101	95	91	81	72	
28" B	112.0	306.41	306	263	230	204	184	167	153	141	131	123	115	108	102	97	92	82	74	
21" C	136.0	308.37	308	264	231	206	185	168	154	142	132	123	116	109	103	97	93			
20" G	149.0	311.62	312	267	234	208	187	170	156	144	134	125	117	110	104	98	93			
22" G	132.0	312.88	309	268	235	209	188	171	157	144	134	125	117	110	104	99	94			
30" B	110.0	314.82	315	270	236	210	189	172	157	145	135	126	118	111	105	99	95	84	76	
24" G	128.0	320.66	321	275	240	214	192	175	160	148	137	128	120	113	107	101	96	86	77	
27" C	124.0	324.82	325	278	244	217	195	177	162	150	139	130	122	115	108	103	97	87	78	
28" B	119.0	327.51	328	281	246	218	197	179	164	151	140	131	123	116	109	103	98	87	79	
24" G	132.0	329.95	327	283	247	220	198	180	165	152	141	132	124	116	110	104	99	88	79	
30" B	115.0	330.85	331	284	248	221	198	180	166	153	142	132	124	117	110	104	99	88	79	
30" C	115.0	332.35	332	285	249	222	199	181	166	153	142	133	125	117	111	105	100	89	80	
24" C	130.0	333.62	318	286	250	222	200	182	167	154	143	133	125	118	111	105	100	89	80	
24" G	140.0	350.11	346	300	263	233	210	191	175	162	150	140	131	124	117	111	105	93	84	
30" B	121.0	351.31	351	301	263	234	211	192	176	162	151	141	132	124	117	111	105	94	85	
27" C	137.0	358.73	352	302	264	235	211	192	176	163	151	141	132	124	117	111	106	96	85	
24" C	140.0	359.23	344	308	269	239	216	196	180	166	154	144	135	127	120	113	108	96	86	
30" C	126.0	363.82	364	312	273	243	218	198	182	168	156	145	136	128	121	115	109	97	87	
28" B	133.0	364.04	364	312	273	243	219	199	182	168	156	146	137	129	121	115	109	97	87	
26" G	138.0	370.39	359	317	278	247	222	202	185	171	159	148	139	131	124	117	111	99	89	
24" G	148.0	371.31	370	318	278	248	223	203	186	171	159	149	139	131	124	117	111	99	89	
30" B	129.0	373.35	373	320	280	249	224	204	187	172	160	149	140	132	124	118	112	100	90	

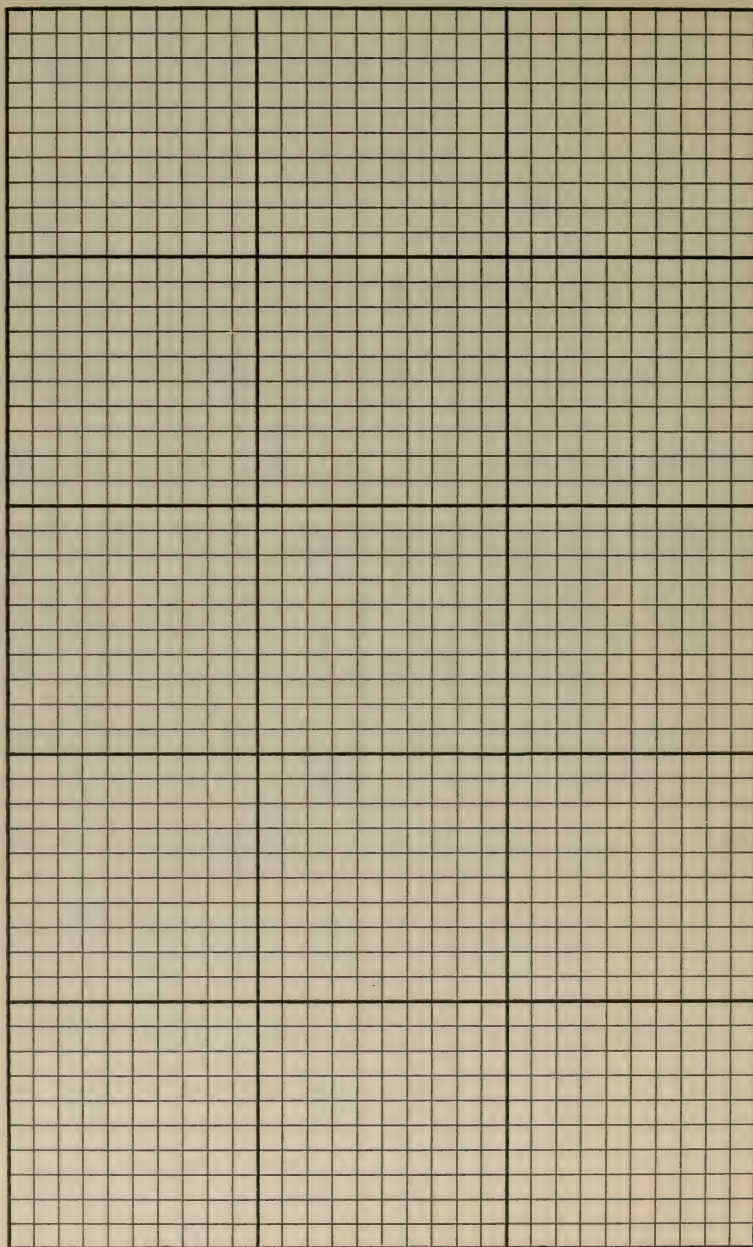
LOADS BY A. I. S. C. SPECIFICATION

SUMMARY OF BEAMS FOR VARIOUS UNIFORM LOADS AND SPANS

Size and Kind	Weight per Foot	Section Modulus	SPAN IN FEET—BEAMS Laterally Fixed																	
			12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	45	50	
24" C	150.0	384.94	370	330	289	257	231	210	192	178	165	154	144	136	128	122	115	103	92	
26" G	144.0	385.12	379	339	300	289	257	231	210	193	178	165	154	144	136	128	122	116	103	
33" C	125.0	394.81	395	338	296	263	237	215	197	182	169	158	148	139	132	125	118	105	95	
33" B	125.0	395.15	395	339	296	263	237	216	198	182	169	158	148	140	132	125	119	105	95	
30" B	137.0	398.46	398	342	299	266	239	217	199	184	171	159	149	141	133	126	120	106	96	
30" C	138.0	398.73	399	342	299	266	239	217	199	184	171	159	150	141	133	126	120	106	96	
26" G	151.0	406.91	393	349	305	271	244	222	203	188	174	163	153	144	136	128	122	109	98	
27" C	145.0	408.05	376	350	306	272	245	223	204	188	175	163	153	144	136	129	122	109	98	
24" C	160.0	410.78	397	352	308	274	246	224	205	190	176	164	154	145	137	130	123	110	99	
28" G	145.0	416.02	390	357	312	277	250	227	208	192	178	166	156	147	139	131	125	111	100	
33" B	135.0	422.27	422	362	317	282	253	230	211	195	181	169	158	149	141	133	127	113	101	
26" G	160.0	431.04	420	369	323	287	259	235	215	199	185	172	162	152	144	136	129	115	103	
30" B	149.0	434.07	434	372	326	289	261	237	217	200	186	174	163	153	145	137	130	116	104	
33" C	138.0	435.59	436	373	327	290	261	238	218	201	187	174	163	154	145	138	131	116	105	
30" C	151.0	436.42	436	374	327	291	262	238	218	201	187	175	164	154	145	138	131	116	105	
28" G	156.0	446.10	425	382	335	297	268	243	223	206	191	178	167	157	149	141	134	119	107	
33" B	143.0	449.41	449	385	337	300	279	245	225	207	193	180	169	159	150	142	135	120	108	
27" C	160.0	450.13	417	386	338	300	270	246	225	208	193	180	169	159	150	142	135	120	108	
28" G	165.0	473.19	454	406	355	315	284	258	237	218	203	189	177	167	158	149	142	126	114	
30" B	163.0	474.43	474	407	356	316	285	259	237	219	203	190	178	167	158	150	142	127	114	
30" C	165.0	476.66	477	409	358	318	286	260	238	220	204	191	179	168	159	151	143	127	114	
33" C	152.0	479.79	480	411	360	328	288	262	240	221	206	192	180	169	160	152	144	128	115	
33" B	152.0	480.40	480	412	360	320	288	262	240	222	206	192	180	170	160	152	144	128	115	
27" C	175.0	492.47	459	422	369	328	295	269	246	227	211	197	185	174	164	156	148	131	118	
28" G	175.0	499.72	479	428	375	333	300	273	250	231	214	200	187	176	167	158	150	133	120	
36" C	147.0	502.24	502	430	377	335	301	274	251	232	215	201	188	177	167	159	151	134	121	
36" B	147.0	503.42	502	432	378	336	302	275	252	232	216	201	189	178	168	159	151	134	121	
33" C	167.0	527.06	527	452	395	351	316	288	264	243	226	211	198	186	176	166	158	141	127	
33" B	165.0	527.49	527	452	396	352	317	288	264	244	226	211	198	186	176	167	158	141	127	
30" G	173.0	528.46	473	453	396	352	317	288	264	244	226	211	198	187	176	167	159	141	127	
36" B	155.0	530.41	530	455	398	354	318	289	265	245	227	212	199	187	177	167	159	141	127	
27" C	190.0	534.60	501	458	401	356	321	292	267	247	229	214	200	189	178	169	160	143	128	
28" G	186.0	537.19	496	460	402	358	322	293	269	248	230	215	201	190	179	170	161	143	128	
36" C	160.0	549.05	549	471	412	366	329	300	275	253	235	220	206	194	183	173	165	146	132	
30" C	180.0	553.43	482	474	415	369	332	302	277	255	237	221	208	195	184	175	166	148	133	
30" G	180.0	556.21	490	477	417	371	334	303	278	257	238	222	209	196	185	176	167	148	133	
36" B	164.0	561.07	559	481	421	374	337	306	281	259	240	224	210	198	187	177	168	150	135	
30" G	190.0	585.52	513	502	439	390	351	319	293	270	251	234	220	207	195	185	176	156	141	
36" B	173.0	594.98	592	510	446	397	357	325	297	275	255	238	223	210	198	188	178	159	143	
36" C	175.0	603.31	599	517	452	402	362	329	302	278	259	241	226	213	201	191	181	161	145	
30" C	200.0	614.99	540	527	461	410	369	335	307	284	264	246	231	217	205	194	184	164	148	
30" G	200.0	617.77	541	530	463	412	371	337	309	285	265	247	232	218	206	195	185	165	148	
36" B	190.0	659.86	636	566	495	440	396	360	330	305	283	264	247	233	220	208	198	176	158	
36" C	192.0	666.31	651	571	500	444	400	363	333	308	286	267	250	235	222	210	200	178	160	
33" C	200.0	669.67	570	570	502	446	402	365	335	309	287	268	251	236	223	211	201	179	161	
33" G	200.0	672.45	552	552	504	448	403	367	336	310	288	269	252	237	224	212	202	179	161	
30" C	220.0	676.26	598	580	507	451	406	369	338	312	290	271	254	239	225	214	203	180	162	
30" G	220.0	680.52	597	583	510	454	408	371	340	314	292	272	255	240	227	215	204	181	163	
33" G	210.0	707.33	582	582	531	472	424	386	354	326	303	283	265	250	236	223	212	189	170	
30" C	240.0	737.86	656	632	553	492	443	402	369	341	316	295	277	260	246	233	221	197	177	
33" G	220.0	741.43	608	608	556	494	445	404	371	342	318	297	278	262	247	234	222	198	178	
30" G	240.0	742.95	649	636	557	495	446	405	372	343	318	297	279	262	248	235	223	198	178	
33" C	220.0	744.50	612	612	558	496	447	406	372	344	319	298	279	263	248	235	223	199	179	
33" G	230.0	778.05	634	634	584	519	467	424	389	359	333	311	292	275	259	246	233	207	187	
33" C	240.0	819.81	652	652	615	547	492	447	410	378	351	328	307	289	273	259	246	219	197	
33" G	245.0	831.04	670	670	623	554	499	453	416	384	356	332	312	293	277	262	249	221	199	
36" G	230.0	833.89	659	659	625	556	500	455	417	385	358	334	313	294	278	263	250	222	200	
36" C	230.0	834.05	664	664	626	556	500	455	417	385	358	334	313	294	278	263	250	222	200	
36" G	240.0	872.00	683	683	654	581	523	476	436	402	374	349	327	308	291	275	262	233	209	
33" G	260.0	884.21	706	706	663	589	531	482	442	408	379	354	332	312	295	279	265	236	212	
33" C	260.0	890.17	705	705	668	593	534	486	445	411	382	356	334	314	297	281	267	237	214	
36" C	250.0	910.48	717	717	683	607	546	497	455	420	390	364	341	321	304	288	273	243	219	
36" C	250.0	911.24	711	711	683	607	547	497	455	420	390	364	342	322	304	288	273	243	219	
36" G	260.0	949.50	735	735	712	633	570	518	475	438	407	380	356	335	316	300	285	253	228	
36" C	275.0	1006.85	781	781	755	671	604	549	503	465	431	403	378	355	336	318	302	268	242	
36" G	280.0	1030.74	780	780	773	687	618	562	515	476	442	412	387	364	344	326	309	275	247	
36" C	300.0	1102.69	847	847	827															

LOADS BY A. I. S. C. SPECIFICATION

NOTES and DIAGRAMS



Part IV

Section 10

American Standard Beams as Columns

Dimensions

Technical Functions

Allowable Concentric Loads

by

A. I. S. C. Specification

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 3" TO 8" ROLLED COLUMNS

AMERICAN STANDARD BEAMS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET											
			3	4	5	6	7	8	9	10	11	12	13	14
3" AMERICAN STANDARD BEAMS														
5.7	1.64	0.53	23.5	20.3	17.2	14.6	12.3	10.5						
6.5	1.88	0.52	26.7	23.0	19.5	16.4	13.8	11.7						
7.5	2.17	0.52	30.9	26.5	22.5	18.9	15.9	13.5						
4" AMERICAN STANDARD BEAMS														
7.7	2.21	0.59	33.0	29.1	25.3	21.8	18.7	16.1	13.9					
8.5	2.46	0.58	36.5	32.1	27.8	23.9	20.4	17.6	15.1					
9.5	2.76	0.58	40.9	36.0	31.2	26.8	22.9	19.7	17.0					
10.5	3.05	0.57	44.9	39.4	34.0	29.1	24.9	21.3	18.3					
5" AMERICAN STANDARD BEAMS														
10.0	2.87	0.65	43.1	39.7	35.1	30.7	26.8	23.4	20.4	17.9				
12.25	3.56	0.63	53.4	48.5	42.6	37.1	32.2	28.0	24.4	21.3				
14.75	4.29	0.63	64.4	58.4	51.4	44.7	38.8	33.7	29.3	25.6				
6" AMERICAN STANDARD BEAMS														
12.5	3.61	0.72	54.2	52.1	46.9	41.8	37.0	32.7	28.9	25.6	22.7	20.1		
14.75	4.29	0.69	64.4	60.8	54.4	48.1	42.3	37.2	32.7	28.8	25.5			
17.25	5.02	0.68	75.3	70.8	63.1	55.7	48.9	42.9	37.7	33.1	29.2			
7" AMERICAN STANDARD BEAMS														
15.3	4.43	0.78	66.5	65.9	60.0	54.1	48.5	43.3	38.6	34.4	30.8	27.6	24.7	
17.5	5.09	0.76	76.4	75.0	68.1	61.1	54.6	48.6	43.2	38.4	34.3	30.6		
20.0	5.83	0.74	87.5	85.1	76.9	68.8	61.2	54.3	48.1	42.7	38.0	33.8		
8" AMERICAN STANDARD BEAMS														
18.4	5.34	0.84	80.1	80.1	74.9	68.2	61.8	55.7	50.1	45.0	40.5	36.5	32.9	29.6
20.5	5.97	0.82	89.6	89.6	82.8	75.2	67.9	61.0	54.7	49.1	44.1	39.6	35.7	
23.0	6.71	0.81	100.6	100.6	92.5	83.9	75.6	67.8	60.8	54.4	48.8	43.8	39.5	
25.5	7.43	0.80	111.5	111.2	101.9	92.2	82.9	74.3	66.4	59.4	53.2	47.8	42.9	

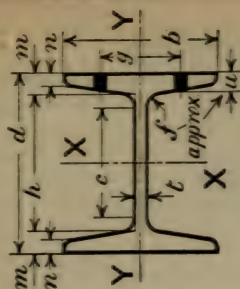
Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 3" TO 8" ROLLED COLUMNS

AMERICAN STANDARD BEAMS

Weight per foot	DIMENSIONS										AXIS X-X			AXIS Y-Y			
	d	b	t	h	m	n	f	e	g	u	Rev.	I	S	r	I	S	r
3" AMERICAN STANDARD BEAMS																	
5.7	3.000	2.33	170	3.300	350	170	27	1.843	1 1/2	5/16	3/8	2.5	1.67	1.23	0.46	0.40	0.53
6.5	3.000	2.41	175	3.300	350	170	27	1.843	1 1/2	5/16	3/8	2.7	1.80	1.19	0.51	0.43	0.52
7.5	3.000	2.51	180	3.300	350	170	27	1.843	1 1/2	5/16	3/8	2.9	1.93	1.15	0.59	0.47	0.52
4" AMERICAN STANDARD BEAMS																	
7.7	4.000	2.66	190	3.208	396	190	29	2.717	1 1/2	5/16	1/2	6.0	3.00	1.64	0.77	0.58	0.59
8.5	4.000	2.72	195	3.208	396	190	29	2.717	1 1/2	5/16	1/2	6.3	3.15	1.60	0.83	0.61	0.58
9.5	4.000	2.80	200	3.208	396	190	29	2.717	1 1/2	5/16	1/2	6.7	3.33	1.56	0.91	0.65	0.57
10.5	4.000	2.87	200	3.208	396	190	29	2.717	1 1/2	5/16	1/2	7.1	3.55	1.52	1.00	0.70	0.58
5" AMERICAN STANDARD BEAMS																	
10.0	5.000	3.00	210	4.114	443	210	31	3.589	1 3/4	3/8	1/2	12.1	4.84	2.05	1.2	0.82	0.65
12.25	5.000	3.14	217	4.114	443	210	31	3.589	1 3/4	3/8	1/2	13.5	5.40	1.95	1.4	0.91	0.63
14.75	5.000	3.28	224	4.114	443	210	31	3.589	1 3/4	3/8	1/2	15.0	6.00	1.87	1.7	1.00	0.63
6" AMERICAN STANDARD BEAMS																	
12.5	6.000	3.33	230	5.024	488	230	33	4.465	2"	3/8	5/8	21.8	7.27	2.46	1.8	1.1	0.72
14.75	6.000	3.44	243	5.024	488	230	33	4.465	2"	3/8	5/8	23.8	7.94	2.36	2.1	1.2	0.69
17.25	6.000	3.57	255	5.024	488	230	33	4.465	2"	3/8	5/8	26.0	8.67	2.28	2.3	1.3	0.68
7" AMERICAN STANDARD BEAMS																	
15.4	7.000	3.66	250	5.916	544	250	35	5.319	2 1/4	3/8	5/8	36.2	10.34	2.86	2.7	1.5	0.78
17.5	7.000	3.76	265	5.916	544	250	35	5.319	2 1/4	3/8	5/8	38.9	11.11	2.77	2.9	1.6	0.76
20.0	7.000	3.86	280	5.916	544	250	35	5.319	2 1/4	3/8	5/8	41.9	11.97	2.68	3.1	1.6	0.74
8" AMERICAN STANDARD BEAMS																	
18.4	8.000	4.00	270	6.838	581	270	37	6.211	2 1/2	7/16	3/4	56.9	14.22	3.26	3.8	1.9	0.84
20.5	8.000	4.08	280	6.838	581	270	37	6.211	2 1/2	7/16	3/4	60.2	15.05	3.18	4.0	2.0	0.82
23.0	8.000	4.17	290	6.838	581	270	37	6.211	2 1/2	7/16	3/4	64.2	16.05	3.09	4.4	2.1	0.81
25.5	8.000	4.26	300	6.838	581	270	37	6.211	2 1/2	7/16	3/4	68.1	17.02	3.03	4.7	2.2	0.80

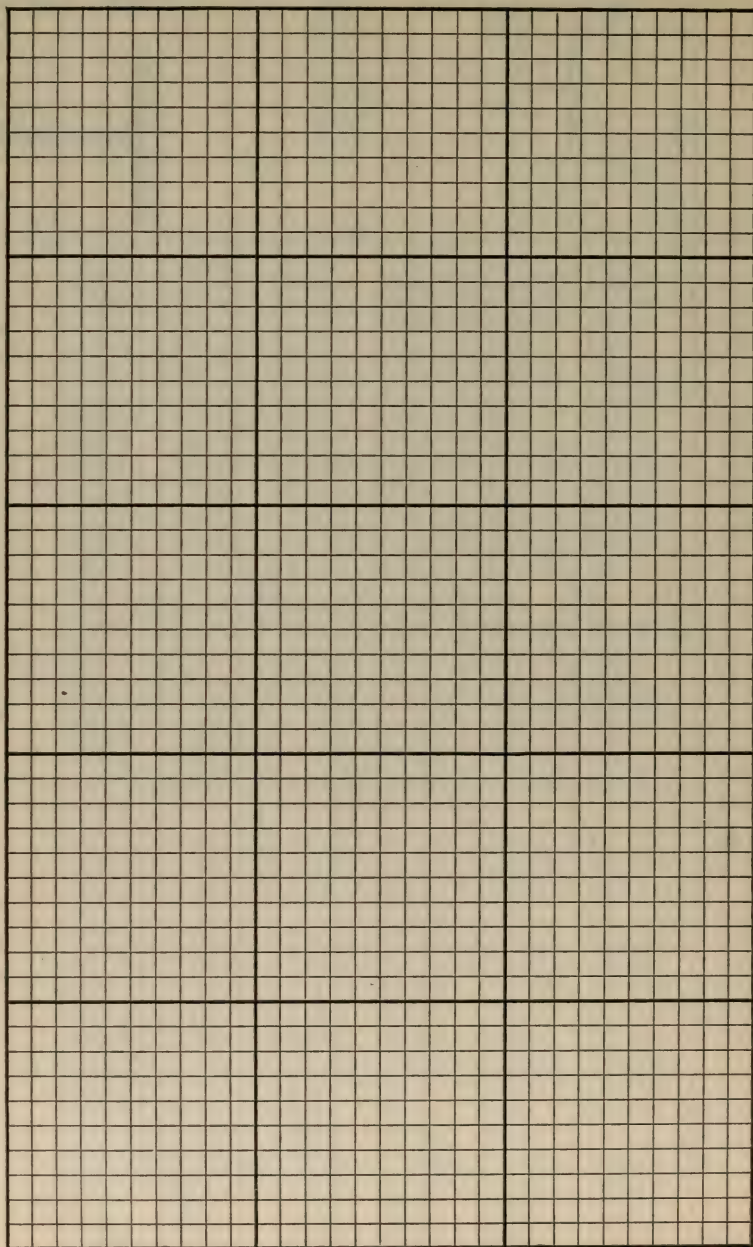


I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

3" to 8"



NOTES and DIAGRAMS



Part IV

Section 11

BETHLEHEM COLUMN SECTIONS

BETHLEHEM COLUMN SECTIONS WITH COVER PLATES

Dimensions—Technical Functions

Allowable Concentric Loads by A. I. S. C. Specification

Manufacturers Section Index

Sec. Index	Depth	Weight									
BS 6	6"	15.5	18.0								
H 6	6"	20.0	23.0	26.5	30.0	33.5	37.0	40.5			
H 6/10	6"	40.0	46.0	53.0	60.0	67.0	73.0	80.0	88.0		
H 8/6.5	8"	23.5	27.0	30.5	34.5						
H 8	8"	32.0	35.0	39.5	44.0	48.5	53.0	58.0	62.5	67.5	72.0
		77.0	81.5	86.0	91.0						
H 10/8	10"	33.5	38.0	42.5	47.5						
H 10	10"	49.5	55.0	60.5	66.0	72.0	77.5	83.5	89.0	95.0	100.5
		106.5	112.0	118.0	124.0	130.0	136.5				
H 10/12	10"	62.0	68.0	75.0	82.0	88.0	94.0	100.0	107.0	113.0	125.0
		133.0	140.0	148.0	155.0	162.0	170.0	177.0	185.0	192.0	200.0
		208.0	215.0	222.0	230.0	238.0	246.0				
H 12/8	12"	40.5	45.5	50.5	55.0						
H 12/10	12"	52.5	58.0	64.0	70.0						
H 12	12"	65.5	72.5	79.0	85.5	92.5	99.5	106.0	113.0	119.5	126.5
		133.5	140.5	147.5	154.5	162.0	169.0	176.0	183.0	190.0	
H 14/8	14"	43.0	48.0	53.5	58.5						
H 14/10	14"	55.0	61.5	67.5	73.5						
H 14/12	14"	69.0	76.0	83.0	90.0						
H 14	14"	84.0	92.0	100.0	107.5	115.5	123.5	131.5	139.0	147.0	155.0
		161.0	168.0	177.0	185.0	194.0	202.0	210.0	219.0	227.0	236.0
		245.0	254.0	262.0	271.0	280.0	289.0	298.0			
H 14b	14"	149.0									
H 16	16"	143.0	151.0	160.0	169.0	177.0	186.0	195.0	203.0	212.0	221.0
		230.0	238.0	247.0	256.0	265.0	274.0	288.0	301.0	314.0	328.0
		342.0	356.0	370.0	384.0	399.0	413.0	427.0			

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 6" ROLLED COLUMNS

BETHLEHEM SECTIONS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																			
			4	6	8	9	10	11	12	13	14	15	16	17	18	19	20	22	24	26	28	30
6" BETHLEHEM STANCHIONS.																						
15.5	4.61	1.41	69	69	66	63	59	56	53	49	46	44	41	38	36							
18.0	5.33	1.43	80	80	77	73	69	65	61	58	54	51	48	45	42							
6" BETHLEHEM H COLUMNS.																						
20.0	5.89	1.49	88	88	86	82	78	74	70	66	62	59	55	52	49	46	43	39	35			
23.0	6.76	1.51	101	101	99	95	90	85	81	76	72	68	64	60	57	54	51	45	40			
26.5	7.76	1.53	116	116	115	109	104	99	94	89	84	79	74	70	66	63	59	53	47			
30.0	8.77	1.54	132	132	130	124	118	112	106	101	95	90	85	80	75	71	67	60	54			
33.5	9.80	1.55	147	147	145	139	132	126	119	113	107	101	95	90	85	80	76	67	60			
37.0	10.83	1.57	162	162	161	154	147	140	133	126	119	113	106	101	95	90	85	76	68			
40.5	11.87	1.58	178	178	177	170	162	154	146	139	131	124	117	111	105	99	94	84	75			
6"/10 BETHLEHEM HEAVY WEIGHT STANCHIONS																						
40.0	11.71	2.46	176	176	176	176	176	176	176	172	167	162	157	152	148	143	138	129	120	111	104	96
46.0	13.54	2.49	203	203	203	203	203	203	203	200	195	189	183	177	172	168	161	150	140	130	121	113
53.0	15.59	2.52	234	234	234	234	234	234	234	231	225	219	212	206	199	193	187	174	163	152	141	131
60.0	17.65	2.55	265	265	265	265	265	265	265	263	256	249	243	234	227	220	213	199	186	173	162	151
67.0	19.70	2.58	296	296	296	296	296	296	296	295	287	279	271	263	255	247	240	224	210	196	183	170
73.0	21.47	2.60	322	322	322	322	322	322	322	322	314	305	297	288	279	271	262	246	230	215	201	187
80.0	23.53	2.62	353	353	353	353	353	353	353	345	336	326	317	308	298	289	271	253	237	221	207	193
88.0	25.89	2.65	388	388	388	388	388	388	388	388	381	371	361	351	340	330	320	300	281	263	246	230

Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 6" ROLLED COLUMNS

BETHLEHEM
SECTIONS

DIMENSIONS

AXIS X-X

AXIS Y-Y

6" BETHLEHEM STANCHIONS

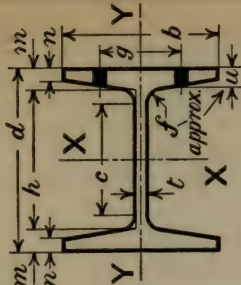
Weight per foot	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r
15.5	6.000	6.00	.240	5.404	.298	.240	.30	4.813	3 1/2	9/32	3/4	30.3	10.10	3.06
18.0	6.094	6.03	.270	5.404	.343	.285	.30	4.813	3 1/2	5/16	3/4	35.8	11.75	3.64

6" BETHLEHEM H COLUMNS

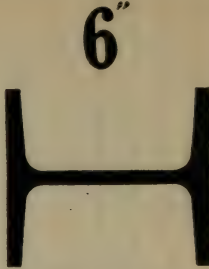
Weight per foot	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r
20.0	6.000	6.000	.250	5.193	.404	.346	.30	4.625	3 1/2	3/8	3/4	39.1	13.03	4.34
23.0	6.125	6.020	.270	5.193	.466	.409	.30	4.625	3 1/2	1/2	3/4	46.4	15.15	5.12
26.5	6.250	6.060	.310	5.193	.529	.471	.30	4.625	3 1/2	9/16	3/4	54.4	17.41	5.96
30.0	6.375	6.100	.350	5.193	.591	.534	.30	4.625	3 1/2	5/8	3/4	62.8	19.70	6.82
33.5	6.500	6.140	.390	5.193	.654	.596	.30	4.625	3 1/2	3/4	3/4	71.6	22.03	7.70
37.0	6.625	6.180	.430	5.193	.716	.659	.30	4.625	3 1/2	15/16	3/4	80.9	24.42	8.60
40.5	6.750	6.220	.470	5.193	.779	.721	.30	4.625	3 1/2	3/4	3/4	90.5	26.81	9.52

6" / 10 BETHLEHEM HEAVY WEIGHT STANCHIONS

Weight per foot	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r
40.0	6.216	9.875	.465	5.192	.512	.418	.30	4.625	5 1/2	1 1/2	3/4	82.3	26.48	2.65
46.0	6.356	9.944	.534	5.192	.582	.488	.30	4.625	5 1/2	1 7/8	3/4	97.4	30.65	2.68
53.0	6.512	10.022	.612	5.192	.660	.566	.30	4.625	5 1/2	2 1/8	3/4	115.2	35.38	2.72
60.0	6.666	10.099	.689	5.192	.737	.643	.30	4.625	5 1/2	1 1/2	3/4	133.9	40.17	2.75
67.0	6.818	10.175	.765	5.192	.813	.719	.30	4.625	5 1/2	3/4	3/4	153.3	44.97	2.79
73.0	6.946	10.241	.831	5.192	.877	.783	.30	4.625	5 1/2	2 1/2	3/4	170.6	49.12	2.82
80.0	7.096	10.315	.905	5.192	.952	.858	.30	4.625	5 1/2	2 7/8	3/4	191.7	54.03	2.85
88.0	7.265	10.400	.990	5.192	1.037	.942	.30	4.625	5 1/2	1	3/4	216.9	59.71	2.89



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 8" ROLLED COLUMNS

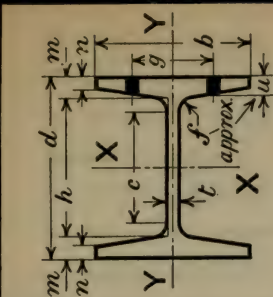
BETHLEHEM
SECTIONS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																			
			4	6	8	9	10	11	12	13	14	15	16	17	18	19	20	22	24	26	28	30
8" BETHLEHEM BEAMS																						
17.5	5.20	1.11	78	76	66	61	57	52	48	45	41	38	35	33	30							
19.0	5.68	1.13	85	83	73	68	63	58	54	50	46	42	39	36	34							
8" BETHLEHEM GIRDER BEAMS																						
29.5	8.69	1.81	130	130	130	130	126	121	116	111	106	101	96	92	87	83	79	71	65	59	53	
33.0	9.69	1.86	145	145	145	145	141	136	131	125	120	115	110	105	100	95	91	82	75	68	62	
36.5	10.81	1.90	162	162	162	162	159	154	148	142	136	130	124	119	113	108	103	94	86	78	71	
8" BETHLEHEM H COLUMNS.																						
23.5	6.85	1.57	103	103	102	98	93	89	84	80	75	71	67	64	60	57	54	48	43			
27.0	7.89	1.59	118	118	118	113	108	103	98	93	88	83	78	74	70	66	63	56	50			
30.5	8.95	1.61	134	134	134	129	123	117	112	106	100	95	90	85	81	76	72	65	58			
34.5	10.10	1.62	152	152	152	146	139	133	126	120	114	108	102	97	91	87	82	74	66	59		
32.0	9.30	1.96	140	140	140	140	139	134	129	124	119	114	109	105	100	96	91	83	76	70	64	58
35.0	10.30	2.00	155	155	155	155	155	149	144	139	133	128	123	117	113	108	103	94	86	79	72	66
39.5	11.63	2.01	174	174	174	174	174	169	163	157	151	145	139	133	128	122	117	107	98	89	82	75
44.0	12.96	2.03	194	194	194	194	194	189	182	176	169	162	156	149	143	137	131	120	110	101	93	85
48.5	14.31	2.04	215	215	215	215	215	209	202	194	187	180	173	166	159	152	146	133	122	112	103	94
53.0	15.66	2.06	235	235	235	235	235	230	222	214	206	198	190	182	175	168	161	147	135	124	114	105
58.0	17.03	2.07	255	255	255	255	255	250	242	233	224	216	207	199	191	183	175	161	148	134	124	114
62.5	18.40	2.09	276	276	276	276	276	271	262	253	244	235	225	217	208	199	191	176	161	148	136	125
67.5	19.79	2.10	297	297	297	297	297	292	282	273	263	253	243	234	224	215	206	190	174	160	147	135
72.0	21.18	2.11	318	318	318	318	318	313	303	292	282	271	261	251	241	231	222	204	187	172	158	146
77.0	22.59	2.12	339	339	339	339	339	335	324	313	301	290	279	269	258	248	238	218	201	185	170	156
81.5	23.91	2.14	359	359	359	359	359	355	344	332	321	309	297	286	275	264	253	233	215	197	181	167
86.0	25.33	2.15	380	380	380	380	380	377	365	353	340	328	316	304	292	281	269	248	228	210	194	178
91.0	26.77	2.16	402	402	402	402	402	399	386	374	361	348	335	322	310	298	286	263	242	223	206	190

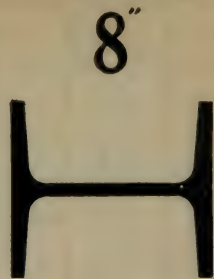
Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 8" ROLLED COLUMNS

BETHLEHEM
SECTIONS



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



8"

Weight per foot	DIMENSIONS										AXIS X-X					AXIS Y-Y				
	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r	I	S	r	I	S	r
8" BETHLEHEM GIRDER BEAMS																				
17.5	8 000	5 250	.250	7 164	.418	.210	.30	6.625	2 1/4	1 1/2	3/4	57.7	14.43	3.33	57.7	14.43	3.33	6.39	2.44	1.11
19.0	8 060	5 270	.270	7 164	.448	.240	.30	6.625	2 1/4	5/8	3/4	62.9	15.60	3.35	62.9	15.60	3.35	7.20	2.73	1.13
8" BETHLEHEM H COLUMNS																				
29.5	7 880	7 995	.285	6 738	.571	.250	.40	6.000	5 1/2	1 1/2	7/8	100.7	25.56	3.41	100.7	25.56	3.41	28.4	7.10	1.81
33.0	8 000	8 000	.290	6 738	.631	.310	.40	6.000	5 1/2	1 1/2	7/8	116.1	29.03	3.46	116.1	29.03	3.46	33.6	8.39	1.86
36.5	8 120	8 020	.310	6 738	.691	.370	.40	6.000	5 1/2	1 1/2	7/8	132.6	32.66	3.50	132.6	32.66	3.50	39.0	9.72	1.90
8" BETHLEHEM H COLUMNS																				
23.5	7 750	6 500	.250	6 923	.413	.351	.40	6.125	3 1/2	3/4	7/8	76.1	19.6	3.33	76.1	19.6	3.33	16.8	5.18	1.57
27.0	7 875	6 530	.280	6 923	.476	.413	.40	6.125	3 1/2	7/8	7/8	89.7	22.8	3.37	89.7	22.8	3.37	20.0	6.11	1.59
30.5	8 000	6 560	.310	6 923	.538	.476	.40	6.125	3 1/2	1 1/2	7/8	103.8	26.0	3.41	103.8	26.0	3.41	23.2	7.07	1.61
34.5	8 125	6 600	.350	6 923	.601	.538	.40	6.125	3 1/2	1 1/2	7/8	118.9	29.3	3.43	118.9	29.3	3.43	26.6	8.07	1.62
32.0	7 875	8 000	.310	6 923	.476	.399	.40	6.125	5 1/2	7/8	7/8	107.2	27.2	3.40	107.2	27.2	3.40	35.8	8.95	1.96
35.0	8 000	8 000	.310	6 923	.538	.462	.40	6.125	5 1/2	1 1/2	7/8	123.0	30.7	3.46	123.0	30.7	3.46	41.1	10.28	2.00
39.5	8 125	8 040	.350	6 923	.601	.524	.40	6.125	5 1/2	1 1/2	7/8	141.0	34.7	3.48	141.0	34.7	3.48	47.2	11.74	2.01
44.0	8 250	8 080	.390	6 923	.663	.587	.40	6.125	5 1/2	1 1/2	7/8	159.7	38.7	3.51	159.7	38.7	3.51	53.4	13.22	2.03
48.5	8 375	8 120	.430	6 923	.726	.649	.40	6.125	5 1/2	1 1/2	7/8	179.2	42.8	3.54	179.2	42.8	3.54	59.8	14.73	2.04
53.0	8 500	8 160	.470	6 923	.788	.712	.40	6.125	5 1/2	3/4	7/8	199.3	46.9	3.57	199.3	46.9	3.57	66.4	16.27	2.06
58.0	8 625	8 200	.510	6 923	.851	.774	.40	6.125	5 1/2	1 1/2	7/8	220.1	51.0	3.60	220.1	51.0	3.60	73.1	17.83	2.07
62.5	8 750	8 240	.550	6 923	.913	.837	.40	6.125	5 1/2	1 1/2	7/8	241.7	55.2	3.62	241.7	55.2	3.62	80.0	19.42	2.09
67.5	8 875	8 280	.590	6 923	.976	.899	.40	6.125	5 1/2	1 1/2	7/8	264.0	59.5	3.65	264.0	59.5	3.65	87.2	21.06	2.10
72.0	9 000	8 320	.630	6 923	1.038	.962	.40	6.125	5 1/2	1	7/8	287.1	63.8	3.68	287.1	63.8	3.68	94.5	22.72	2.11
77.0	9 125	8 360	.670	6 923	1.101	1.024	.40	6.125	5 1/2	1 1/2	7/8	311.0	68.2	3.71	311.0	68.2	3.71	102.0	24.40	2.12
81.5	9 250	8 390	.700	6 923	1.163	1.087	.40	6.125	5 1/2	1 1/2	7/8	335.0	72.4	3.74	335.0	72.4	3.74	109.2	26.03	2.13
86.0	9 375	8 430	.730	6 923	1.226	1.149	.40	6.125	5 1/2	1 1/2	7/8	360.5	76.9	3.77	360.5	76.9	3.77	117.1	27.78	2.14
91.0	9 500	8 470	.780	6 923	1.288	1.212	.40	6.125	5 1/2	1 1/2	7/8	386.8	81.4	3.80	386.8	81.4	3.80	125.1	29.54	2.16

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 10" ROLLED COLUMNS

BETHLEHEM SECTIONS

UNSUPPORTED LENGTH IN FEET

Weight per Foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET													
			6	7	8	9	10	12	14	16	18	20	22	24	26	28

10" BETHLEHEM Bs.

21.0	6.28	1.22	94	89	84	79	73	64	55	48	41	36					
23.5	6.96	1.25	104	100	94	89	83	72	63	54	47	41					
26.0	7.68	1.28	115	112	105	99	93	81	71	61	54	47					
28.5	8.41	1.30	126	123	116	109	103	90	78	68	60	52					

10" BETHLEHEM Cs.

41.5	12.23	2.07	183	183	183	183	183	174	161	149	137	126	116	106	97	89	82
44.5	13.14	2.10	197	197	197	197	197	188	174	161	149	137	126	116	106	98	90
50.0	14.62	2.13	219	219	219	219	219	210	196	181	168	154	142	131	120	110	102

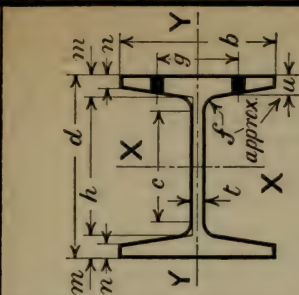
10" BETHLEHEM H COLUMNS.

33.5	9.80	1.93	147	147	147	147	145	135	124	114	104	95	86	79	71	66	
38.0	11.09	1.96	166	166	166	166	165	154	142	130	119	109	99	91	83	76	79
42.5	12.49	1.97	187	187	187	187	186	173	160	147	135	123	113	103	94	86	89
47.5	13.90	1.99	209	209	209	209	208	194	179	165	151	138	126	116	106	97	
49.5	14.57	2.47	219	219	219	219	219	219	209	196	184	172	160	149	139	129	120
55.0	16.12	2.50	242	242	242	242	242	242	232	219	205	192	179	165	156	145	135
60.5	17.77	2.51	267	267	267	267	267	267	256	241	227	212	198	185	172	160	149
66.0	19.44	2.53	292	292	292	292	292	292	281	265	249	233	218	203	190	177	165
72.0	21.11	2.54	317	317	317	317	317	317	306	288	271	254	237	222	207	193	180
77.5	22.80	2.56	342	342	342	342	342	342	331	313	294	276	258	241	225	210	196
83.0	24.49	2.57	367	367	367	367	367	367	356	336	317	297	278	260	242	226	211
89.0	26.30	2.59	393	393	393	393	393	393	382	361	340	319	299	280	261	244	225
95.0	27.91	2.60	419	419	419	419	419	419	408	386	363	341	319	299	279	261	243
100.5	29.53	2.61	443	443	443	443	443	443	432	409	385	362	339	317	296	277	258
106.5	31.26	2.63	469	469	469	469	469	469	459	434	409	385	361	338	316	295	276
112.0	33.00	2.64	495	495	495	495	495	495	485	459	427	407	382	358	335	313	292
118.0	34.76	2.65	521	521	521	521	521	521	511	484	457	430	403	378	354	331	309
124.0	36.52	2.66	548	548	548	548	548	548	538	510	481	453	425	398	373	348	326
130.0	38.30	2.68	575	575	575	575	575	575	566	536	507	477	448	420	393	368	344
136.5	40.08	2.69	601	601	601	601	601	601	593	562	531	500	470	441	413	386	362

Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 10" ROLLED COLUMNS

BETHLEHEM
SECTIONS



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

10"



Weight per Foot	DIMENSIONS										AXIS X-X					AXIS Y-Y				
	d	b	t	h	m	n	f	c	g	u	Rivet	I	S	r	I	S	r	I	S	r
10" BETHLEHEM Bs.																				
21.0	9.90	5.740	.240	8.972	.464	.235	.30	8.375	2 3/4	11/32	7/8	108.1	21.84	4.15	9.3	3.24	1.22			
23.5	10.00	5.750	.250	8.972	.514	.285	.30	8.375	2 3/4	1 1/8	7/8	133.2	24.64	4.21	10.9	3.80	1.25			
26.0	10.09	5.770	.270	8.972	.559	.330	.30	8.375	2 3/4	1 5/16	7/8	137.9	27.33	4.24	12.5	4.33	1.28			
28.5	10.19	5.785	.285	8.972	.609	.380	.30	8.375	2 3/4	1 1/2	7/8	154.1	30.25	4.28	14.2	4.92	1.30			
10" BETHLEHEM Gs.																				
41.5	9.91	8.990	.310	8.506	.702	.340	.40	7.750	5 1/2	1 1/2	7/8	225.8	45.57	4.30	52.6	11.7	2.07			
44.5	10.00	9.000	.320	8.506	.747	.385	.40	7.750	5 1/2	9/16	7/8	246.7	49.34	4.33	58.2	12.9	2.10			
50.0	10.12	9.040	.360	8.506	.807	.445	.40	7.750	5 1/2	5/8	7/8	277.5	54.84	4.36	66.4	14.7	2.13			
10" BETHLEHEM H COLUMNS																				
33.5	9.635	8.00	.28	8.653	.486	.408		7.688	5 1/2	7/16	7/8	169.9	35.30	4.16	36.6	9.15				
38.0	9.750	8.03	.31	8.653	.548	.471		7.688	5 1/2	1/2	7/8	195.6	40.12	4.20	42.4	10.56				
42.5	9.875	8.07	.35	8.653	.611	.533		7.688	5 1/2	9/16	7/8	223.0	45.16	4.23	48.5	12.02				
47.5	10.000	8.11	.39	8.653	.673	.596		7.688	5 1/2	5/8	7/8	251.3	50.26	4.25	54.8	13.51				
49.5	9.875	9.97	.36	8.653	.611	.514		7.688	5 1/2	9/16	7/8	267.2	54.1	4.28	89.1	17.9				
55.0	10.000	10.00	.39	8.653	.673	.577		7.688	5 1/2	5/8	7/8	300.4	60.1	4.32	100.4	20.1				
60.5	10.125	10.04	.43	8.653	.736	.639		7.688	5 1/2	1 1/8	7/8	335.5	66.3	4.34	112.2	22.3				
66.0	10.250	10.08	.47	8.653	.798	.702		7.688	5 1/2	3/4	7/8	371.7	72.5	4.37	124.2	24.6				
72.0	10.375	10.12	.51	8.653	.861	.764		7.688	5 1/2	1 1/2	7/8	408.9	78.8	4.40	136.3	27.0				
77.5	10.500	10.16	.55	8.653	.923	.827		7.688	5 1/2	7/8	7/8	447.2	85.2	4.43	149.1	29.4				
83.5	10.625	10.20	.59	8.653	.986	.889		7.688	5 1/2	1 5/16	7/8	486.6	91.6	4.46	162.0	31.8				
89.0	10.750	10.24	.63	8.653	1.048	.952		7.688	5 1/2	1 1/2	7/8	527.2	98.1	4.49	175.2	34.2				
95.0	10.875	10.28	.67	8.653	1.111	1.014		7.688	5 1/2	1 1/8	7/8	568.9	104.6	4.51	188.6	36.7				
100.5	11.000	10.31	.70	8.653	1.173	1.077		7.688	5 1/2	1 1/8	7/8	610.6	111.0	4.55	201.7	39.1				
106.5	11.125	10.35	.74	8.653	1.236	1.139		7.688	5 1/2	1 3/16	7/8	654.7	117.7	4.58	215.7	41.7				
112.0	11.250	10.39	.78	8.653	1.298	1.202		7.688	5 1/2	1 1/4	7/8	699.9	124.4	4.60	229.9	44.3				
118.0	11.375	10.43	.82	8.653	1.361	1.264		7.688	5 1/2	1 5/16	7/8	746.3	131.2	4.63	244.5	46.9				
124.0	11.500	10.47	.86	8.653	1.423	1.327		7.688	5 1/2	1 3/8	7/8	794.0	138.1	4.66	259.4	49.5				
130.0	11.625	10.51	.90	8.653	1.486	1.389		7.688	5 1/2	1 7/16	7/8	843.0	145.0	4.69	274.5	52.2				
136.5	11.750	10.55	.94	8.653	1.548	1.452		7.688	5 1/2	1 1/2	7/8	893.3	152.1	4.72	290.0	55.0				

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 10" ROLLED COLUMNS

BETHLEHEM
SECTIONS

UNSUPPORTED LENGTH IN FEET

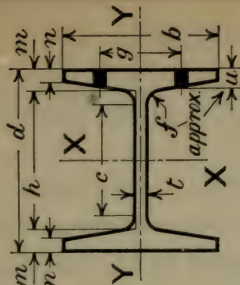
Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET															
			12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	
10" BETHLEHEM H COLUMNS																		
62.0	18.29	3.04	274	274	270	258	245	232	220	208	196	185	174	164	155	146	138	
68.0	20.13	3.05	302	302	297	283	270	256	242	229	216	204	193	182	171	162	152	
75.0	22.00	3.08	330	330	326	311	296	281	267	252	238	225	212	200	189	179	169	
82.0	23.98	3.09	360	360	355	340	323	307	291	276	261	246	232	219	207	195	184	
88.0	25.86	3.11	388	388	384	367	350	332	315	298	282	267	252	238	225	212	200	
94.0	27.63	3.12	414	414	411	393	374	356	338	320	302	286	270	255	241	227	215	
100.0	29.54	3.14	443	443	440	421	401	382	362	343	325	307	290	274	259	245	231	
107.0	31.45	3.16	472	472	470	449	429	408	387	367	348	329	311	294	278	263	248	
113.0	33.25	3.17	499	499	497	476	454	432	410	389	368	348	330	312	295	279	263	
125.0	36.89	3.65	553	553	553	553	535	514	493	472	451	431	411	392	373	356	339	
133.0	39.02	3.66	585	585	585	585	567	545	523	500	478	457	436	416	396	377	359	
140.0	41.29	3.68	619	619	619	619	601	578	555	531	508	486	463	442	421	401	382	
148.0	43.46	3.69	652	652	652	652	633	609	585	560	535	512	488	466	444	423	403	
155.0	45.62	3.70	684	684	684	684	666	640	614	588	563	538	514	490	467	445	424	
162.0	47.78	3.72	717	717	717	717	699	672	645	618	592	566	540	516	492	469	447	
170.0	49.98	3.73	750	750	750	750	731	704	676	648	620	593	566	540	515	491	468	
177.0	52.18	3.74	783	783	783	783	764	736	706	677	648	620	592	566	540	514	490	
185.0	54.37	3.76	816	816	816	816	798	768	738	708	678	648	620	592	564	538	513	
192.0	56.45	3.77	847	847	847	847	829	799	767	736	705	675	645	615	588	561	535	
200.0	58.80	3.78	882	882	882	882	864	833	800	768	736	704	673	642	613	585	559	
208.0	61.17	3.79	918	918	918	918	900	867	834	800	766	733	701	670	640	610	582	
215.0	63.27	3.80	949	949	949	949	932	898	863	828	794	760	727	694	663	633	604	
222.0	65.38	3.81	981	981	981	981	964	929	893	858	822	787	752	719	686	655	626	
230.0	67.77	3.83	1017	1017	1017	1017	1002	965	928	891	855	818	783	748	714	682	651	
238.0	70.04	3.84	1051	1051	1051	1051	1036	999	961	922	885	847	810	775	740	707	675	
246.0	72.30	3.85	1085	1085	1085	1085	1070	1032	993	954	915	876	838	801	766	731	698	

Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 10" ROLLED COLUMNS

BETHLEHEM SECTIONS

DIMENSIONS											AXIS X-X				AXIS Y-Y			
Weight per foot	10" BETHLEHEM H COLUMNS										I	S	r	I	S	r	I	S
	d	b	t	h	m	n	f	c	g	u	Riv.							
62.0	10.000	11.99	.38	8.654	.673	.557	.50	7.688	9"	9/16	1"	350.1	70.0	168.7	28.1	3.04	168.7	28.1
68.0	10.125	12.03	.42	8.654	.733	.617	.50	7.688	9"	5/8	1"	390.0	77.1	187.8	31.2	3.05	390.0	31.2
75.0	10.250	12.06	.45	8.654	.798	.682	.50	7.688	9"	11/16	1"	438.2	84.5	208.3	34.5	3.08	438.2	34.5
82.0	10.375	12.10	.49	8.654	.863	.747	.50	7.688	9"	3/4	1"	478.6	92.2	229.6	37.9	3.09	478.6	37.9
88.0	10.500	12.14	.53	8.654	.923	.807	.50	7.688	9"	13/16	1"	522.1	99.4	249.8	41.2	3.11	522.1	41.2
94.0	10.625	12.17	.56	8.654	.983	.867	.50	7.688	9"	7/8	1"	565.7	106.5	269.7	44.3	3.12	565.7	44.3
100.0	10.750	12.20	.59	8.654	1.048	.932	.50	7.688	9"	15/16	1"	613.9	114.2	291.5	47.8	3.14	613.9	47.8
107.0	10.875	12.23	.62	8.654	1.113	.997	.50	7.688	9"	1"	1"	663.5	122.0	313.5	51.3	3.16	663.5	51.3
113.0	11.000	12.26	.65	8.654	1.173	1.057	.50	7.688	9"	1 1/16	1"	710.8	129.2	334.3	54.5	3.17	710.8	54.5
125.0	11.000	14.00	.65	8.654	1.173	1.040	.50	7.688	10"	1 1/16	1"	801.4	145.7	491.7	70.2	3.65	801.4	70.2
133.0	11.125	14.04	.69	8.654	1.233	1.100	.50	7.688	10"	1 1/8	1"	857.4	154.2	523.7	74.6	3.66	857.4	74.6
140.0	11.250	14.08	.73	8.654	1.298	1.165	.50	7.688	10"	1 3/8	1"	919.2	163.4	558.5	79.3	3.68	919.2	79.3
148.0	11.375	14.11	.76	8.654	1.363	1.230	.50	7.688	10"	1 1/2	1"	981.5	172.5	592.6	84.0	3.69	981.5	84.0
155.0	11.500	14.15	.80	8.654	1.423	1.290	.50	7.688	10"	1 5/8	1"	1042.0	181.2	626.0	88.5	3.70	1042.0	88.5
162.0	11.625	14.19	.84	8.654	1.483	1.350	.50	7.688	10"	1 3/4	1"	1103.9	190.0	660.0	93.0	3.72	1103.9	93.0
170.0	11.750	14.22	.87	8.654	1.548	1.415	.50	7.688	10"	1 7/8	1"	1170.9	199.3	695.5	97.8	3.73	1170.9	97.8
177.0	11.875	14.25	.90	8.654	1.613	1.480	.50	7.688	10"	1 7/8	1"	1239.6	208.7	731.3	102.6	3.74	1239.6	102.6
185.0	12.000	14.29	.94	8.654	1.673	1.540	.50	7.688	10"	1 7/8	1"	1306.3	217.7	766.8	107.3	3.76	1306.3	107.3
192.0	12.125	14.32	.97	8.654	1.733	1.600	.50	7.688	10"	1 5/8	1"	1373.2	226.6	801.1	111.9	3.77	1373.2	111.9
200.0	12.250	14.36	1.01	8.654	1.798	1.665	.50	7.688	10"	1 11/16	1"	1443.4	236.5	840.0	117.0	3.78	1443.4	117.0
208.0	12.375	14.40	1.05	8.654	1.863	1.730	.50	7.688	10"	1 3/4	1"	1525.5	246.4	879.9	122.2	3.79	1525.5	122.2
215.0	12.500	14.43	1.08	8.654	1.923	1.790	.50	7.688	10"	1 13/16	1"	1597.2	255.6	915.2	126.9	3.80	1597.2	126.9
222.0	12.625	14.46	1.11	8.654	1.983	1.850	.50	7.688	10"	1 7/8	1"	1670.5	264.7	951.3	131.6	3.81	1670.5	131.6
230.0	12.750	14.50	1.15	8.654	2.048	1.915	.50	7.688	10"	1 15/16	1"	1753.1	275.0	992.4	136.9	3.83	1753.1	136.9
238.0	12.875	14.53	1.18	8.654	2.113	1.980	.50	7.688	10"	2"	1"	1835.8	285.1	1031.9	142.0	3.84	1835.8	142.0
246.0	13.000	14.57	1.22	8.654	2.173	2.040	.50	7.688	10"	2 1/16	1"	1916.1	294.8	1071.6	147.1	3.85	1916.1	147.1



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 12" ROLLED COLUMNS

BETHLEHEM
SECTIONS

Weight per Foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET														34	36
			4	8	12	14	16	18	20	22	24	26	28	30	32			
12" BETHLEHEM B _s .																		
28.0	8.28	1.41	124	118	94	83	73	65	57	51								
36.0	10.58	1.46	159	154	124	110	97	86	76	68	60							
40.0	11.80	1.53	177	174	142	127	113	101	90	80	72							
48.5	14.28	1.57	214	213	175	157	140	125	112	100	90							
12" BETHLEHEM G _s .																		
55.5	16.35	2.28	245	245	241	226	211	196	182	169	156	144	134	123				
61.0	17.92	2.31	269	269	265	249	233	217	202	187	173	160	148	137	127			
70.5	20.79	2.40	312	312	312	294	276	258	241	224	208	193	179	166	154			
76.5	22.50	2.42	338	338	338	319	300	281	262	244	227	210	196	182	169			
12" BETHLEHEM H COLUMNS.																		
40.5	11.85	1.90	178	178	162	149	136	124	113	103	94	85	78					
45.5	13.31	1.92	200	200	183	168	154	141	128	117	106	97	89					
50.5	14.79	1.93	222	222	203	187	172	157	143	131	119	109	99					
55.0	16.27	1.94	244	244	224	207	190	173	158	144	132	120	110					
52.5	15.40	2.44	231	231	231	219	206	193	180	168	156	145	135	126	117	109		
58.0	17.12	2.45	257	257	257	244	230	215	201	187	174	162	151	140	130	121		
64.0	18.85	2.47	283	283	283	270	254	238	223	208	193	180	167	156	145	135		
70.0	20.59	2.49	309	309	309	296	279	261	244	228	213	198	184	172	160	149		
65.5	19.29	2.96	289	289	289	280	281	268	254	241	228	215	202	191	179	169	159	
72.5	21.25	2.98	319	319	319	310	311	296	281	266	252	238	224	211	199	187	176	
79.0	23.23	2.99	348	348	348	348	340	324	308	292	276	261	246	232	218	206	194	
85.5	25.21	3.01	378	378	378	378	370	353	335	318	301	284	268	253	238	225	212	
92.5	27.21	3.03	408	408	408	408	400	382	363	345	328	308	291	275	259	244	230	
99.5	29.21	3.04	438	438	438	438	430	411	391	371	351	332	313	296	279	263	248	
106.0	31.23	3.06	468	468	468	468	461	440	419	398	377	356	337	318	300	283	267	
113.0	33.25	3.07	499	499	499	499	492	469	447	424	402	380	359	339	320	302	285	
119.5	35.16	3.09	527	527	527	527	521	498	474	450	427	404	382	361	341	321	303	
126.5	37.21	3.10	558	558	558	558	552	528	502	477	453	429	405	383	362	341	322	
133.5	39.26	3.11	589	589	589	589	583	557	531	505	479	453	429	405	383	361	341	
140.5	41.32	3.13	620	620	620	620	615	588	561	533	506	479	453	428	405	382	361	
147.5	43.40	3.14	651	651	651	651	647	619	590	561	532	504	477	451	427	403	381	
154.5	45.48	3.15	682	682	682	682	679	649	619	589	559	530	502	474	448	423	400	
162.0	47.57	3.17	714	714	714	714	711	681	649	618	587	557	527	499	472	446	421	
169.0	49.68	3.18	745	745	745	745	744	712	679	647	614	583	552	522	494	467	442	
176.0	51.79	3.19	777	777	777	777	776	743	709	675	642	609	577	546	516	488	462	
183.0	53.78	3.20	807	807	807	807	807	773	738	702	668	633	600	568	538	509	481	
190.0	55.91	3.22	839	839	839	839	839	805	769	733	697	661	627	594	562	532	503	

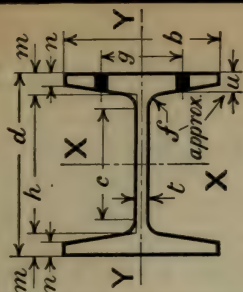
Loads to right of heavy vertical lines for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 12" ROLLED COLUMNS

BETHELEHM
SECTIONS

Weight per Foot	DIMENSIONS										AXIS X-X				AXIS Y-Y			
	d	b	t	h	m	n	f	c	g	u	Rivet	I	S	r	I	S	r	
12" BETHELEHEM Bs																		
28.0	12.00	6.500	.245	10.900	.550	.290	.35	10.250	3	7/16	3/4	213.6	35.60	5.08	16.4	5.04	1.41	
36.0	12.25	6.555	.300	10.900	.675	.415	.35	10.250	3	9/16	3/4	281.8	46.01	5.16	22.7	6.93	1.46	
40.0	12.00	6.750	.330	10.530	.735	.468	.40	9.750	3	23/32	3/4	301.2	50.20	5.05	27.6	8.18	1.53	
48.5	12.25	6.815	.395	10.530	.860	.593	.40	9.750	3	27/32	3/4	373.2	60.93	5.11	35.1	10.29	1.57	
12" BETHELEHEM Gs																		
55.5	12.00	10.000	.380	10.388	.806	.405	.45	9.500	5 1/2	5/8	1"	435.6	72.60	5.16	84.9	17.0	2.28	
61.0	12.12	10.030	.410	10.388	.866	.465	.45	9.500	5 1/2	11/16	1"	483.6	79.80	5.20	95.9	19.1	2.31	
70.5	12.00	10.250	.470	10.066	.967	.560	.55	9.000	5 1/2	25/32	1"	543.6	90.60	5.11	119.7	23.4	2.40	
76.5	12.12	10.290	.510	10.066	1.027	.620	.55	9.000	5 1/2	13/16	1"	594.2	98.05	5.14	132.1	25.7	2.42	
12" BETHELEHEM H COLUMNS																		
40.5	11.500	8.00	.31	10.384	.558	.481		9.188	5 1/2	1/2	1"	287.7	50.0	4.93	42.8	10.7	1.90	
45.5	11.625	8.04	.35	10.384	.620	.543		9.188	5 1/2	9/16	1"	326.4	56.1	4.95	48.9	12.2	1.92	
50.5	11.750	8.08	.39	10.384	.683	.606		9.188	5 1/2	5/8	1"	366.1	62.3	4.98	55.1	13.6	1.93	
55.0	11.875	8.12	.43	10.384	.745	.668		9.188	5 1/2	11/16	1"	406.9	68.5	5.00	61.5	15.2	1.94	
52.5	11.625	10.00	.35	10.384	.620	.524		9.188	5 1/2	9/16	1"	390.7	67.2	5.04	91.5	18.3	2.44	
58.0	11.750	10.04	.39	10.384	.683	.586		9.188	5 1/2	5/8	1"	438.8	74.7	5.06	103.2	20.6	2.45	
64.0	11.875	10.08	.43	10.384	.745	.649		9.188	5 1/2	11/16	1"	488.2	82.2	5.09	115.1	22.8	2.47	
70.0	12.000	10.12	.47	10.384	.808	.711		9.188	5 1/2	3/4	1"	538.8	89.8	5.12	127.3	25.2	2.49	
65.5	11.750	11.92	.39	10.384	.683	.567		9.188	9"	5/8	1"	506.6	86.2	5.12	168.6	28.3	2.96	
72.5	11.875	11.96	.43	10.384	.745	.630		9.188	9"	11/16	1"	564.1	95.0	5.15	188.2	31.5	2.98	
79.0	12.000	12.00	.47	10.384	.808	.692		9.188	9"	3/4	1"	623.1	103.9	5.18	208.2	34.7	2.99	
85.5	12.125	12.04	.51	10.384	.870	.755		9.188	9"	13/16	1"	683.6	112.8	5.21	228.5	38.0	3.01	
92.5	12.250	12.08	.55	10.384	.933	.817		9.188	9"	7/8	1"	745.7	121.7	5.23	249.2	41.3	3.03	
99.5	12.375	12.12	.59	10.384	.995	.880		9.188	9"	15/16	1"	809.2	130.8	5.26	270.3	44.6	3.04	
106.0	12.500	12.16	.63	10.384	1.058	.942		9.188	9"	1"	1"	874.3	139.9	5.29	291.8	48.0	3.06	
113.0	12.625	12.20	.67	10.384	1.120	1.005		9.188	9"	1 1/16	1"	941.0	149.1	5.32	313.7	51.4	3.07	
119.5	12.750	12.23	.70	10.384	1.183	1.067		9.188	9"	1 1/8	1"	1007.5	158.0	5.35	335.1	54.8	3.09	
126.5	12.875	12.27	.74	10.384	1.245	1.130		9.188	9"	1 3/16	1"	1077.4	167.4	5.38	357.7	58.3	3.10	
133.5	13.000	12.31	.78	10.384	1.308	1.192		9.188	9"	1 1/2	1"	1148.9	176.8	5.41	380.8	61.9	3.11	
140.5	13.125	12.35	.82	10.384	1.370	1.255		9.188	9"	1 5/8	1"	1222.1	186.2	5.44	404.2	65.5	3.13	
147.5	13.250	12.39	.86	10.384	1.433	1.317		9.188	9"	1 3/4	1"	1296.9	195.8	5.47	428.1	69.1	3.14	
154.5	13.375	12.43	.90	10.384	1.495	1.380		9.188	9"	1 7/8	1"	1373.5	205.4	5.50	452.3	72.8	3.15	
162.0	13.500	12.47	.94	10.384	1.558	1.442		9.188	9"	1 1/2	1"	1451.9	215.1	5.52	477.0	76.5	3.17	
169.0	13.625	12.51	.98	10.384	1.620	1.505		9.188	9"	1 9/16	1"	1532.0	224.9	5.55	502.2	80.3	3.18	
176.0	13.750	12.55	1.02	10.384	1.683	1.567		9.188	9"	1 5/8	1"	1613.9	234.7	5.58	527.7	84.1	3.19	
183.0	13.875	12.58	1.05	10.384	1.745	1.630		9.188	9"	1 11/16	1"	1695.4	244.4	5.61	552.4	87.8	3.20	
190.0	14.000	12.62	1.09	10.384	1.808	1.692		9.188	9"	1 3/4	1"	1780.9	254.4	5.64	578.7	91.7	3.22	



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration

12"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14" ROLLED COLUMNS

BETHLEHEM
SECTIONS

Weight Per Foot	Area Square Inches	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																
			9	10	12	14	16	18	20	22	24	26	28	30	32	36	40	44	48
14" BETHLEHEM H COLUMNS 8-10 and 12" Nominal Flange Widths																			
43.0	12.58	1.86	189	184	170	156	142	129	118	107	97	88	81						
48.0	14.12	1.88	212	207	192	170	161	147	133	121	110	101	92						
53.5	15.67	1.89	235	231	213	196	179	163	149	135	123	112	102						
58.5	17.23	1.90	258	254	235	216	198	181	164	150	136	124	113						
55.0	16.25	2.39	244	244	243	229	215	201	188	174	162	150	139						
61.5	18.04	2.41	271	271	271	256	240	224	209	195	181	168	156	145					
67.5	19.85	2.43	298	298	298	282	265	248	232	216	201	186	173	161	150				
73.5	21.66	2.44	325	325	325	305	290	272	254	236	220	204	190	177	164				
69.0	20.34	2.95	305	305	305	305	281	267	252	238	225	212	199	187	166	147			
76.0	22.89	2.97	356	356	356	356	326	311	295	279	264	249	234	221	208	184	163		
83.0	24.45	2.97	367	367	367	367	357	340	323	306	289	273	257	242	228	202	179		
90.0	26.52	2.98	398	398	398	398	388	369	351	333	314	297	280	264	248	220	195		
14" BETHLEHEM H COLUMNS 14" Nominal Flange Width																			
84.0	24.76	3.45	371	371	371	371	371	366	351	336	321	306	292	278	264	238	215	194	
92.0	27.05	3.47	406	406	406	406	406	401	385	368	352	336	320	305	290	262	236	213	
100.0	29.36	3.49	440	440	440	440	440	436	418	401	383	366	349	332	316	285	257	233	
107.5	31.67	3.50	475	475	475	475	471	452	433	414	396	377	359	342	309	279	252	233	
115.5	34.00	3.52	510	510	510	510	510	506	486	466	446	426	407	387	369	333	301	272	
123.5	36.33	3.54	545	545	545	545	545	542	521	500	478	457	436	415	392	358	323	292	
131.5	38.68	3.55	580	580	580	580	580	577	555	533	510	487	465	443	422	382	345	312	
139.0	40.98	3.57	613	613	613	613	613	612	588	565	540	517	493	470	448	406	367	332	
147.0	43.25	3.58	649	649	649	649	649	647	623	598	573	548	523	499	475	430	389	352	
155.0	45.62	3.60	684	684	684	684	684	684	659	633	606	579	553	528	503	456	413	374	
163.0	47.93	3.80	710	710	710	710	710	710	697	672	646	620	594	568	544	496	452	411	
168.0	49.51	3.82	743	743	743	743	743	743	731	705	677	650	623	597	571	521	475	432	
177.0	51.99	3.83	780	780	780	780	780	780	768	740	712	684	656	628	600	548	500	455	
185.0	54.48	3.84	817	817	817	817	817	817	806	777	747	718	688	659	630	576	525	478	
194.0	56.99	3.86	855	855	855	855	855	855	845	814	784	753	722	692	662	605	552	503	
202.0	59.50	3.87	893	893	893	893	893	893	882	851	819	787	755	724	692	632	577	527	
210.0	61.86	3.88	928	928	928	928	928	928	918	886	852	819	786	753	721	659	602	549	
219.0	64.40	3.89	966	966	966	966	966	966	957	923	888	854	820	786	752	688	628	573	
227.0	66.94	3.91	1004	1004	1004	1004	1004	1004	996	961	926	890	854	819	785	718	656	598	
236.0	69.40	3.92	1042	1042	1042	1042	1042	1042	1035	999	962	925	888	852	816	747	682	623	
245.0	71.95	3.93	1081	1081	1081	1081	1081	1081	1074	1038	999	960	922	885	847	776	709	648	
254.0	74.52	3.94	1119	1119	1119	1119	1119	1119	1113	1075	1036	996	957	918	879	805	736	672	
263.0	77.10	3.96	1158	1158	1158	1158	1158	1158	1153	1115	1075	1035	993	953	913	836	765	698	
271.0	79.79	3.97	1197	1197	1197	1197	1197	1197	1194	1153	1111	1069	1028	986	945	866	792	724	
280.0	82.39	3.98	1236	1236	1236	1236	1236	1236	1233	1191	1149	1106	1062	1020	978	896	821	750	
289.0	85.01	3.99	1275	1275	1275	1275	1275	1275	1274	1231	1187	1142	1097	1053	1011	927	848	775	
298.0	87.63	4.01	1314	1314	1314	1314	1314	1314	1314	1272	1226	1180	1135	1089	1045	959	878	804	
307.0	90.25	4.02	1353	1353	1353	1353	1353	1353	1353	1310	1264	1218	1172	1127	1081	994	911	834	

Loads to right of heavy vertical lines are for Secondary Members ONLY;

LOADS BY AIS C SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 14" ROLLED COLUMNS

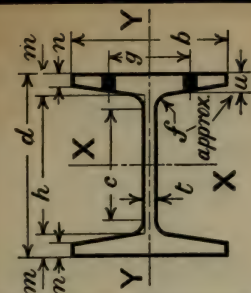
BETHLEHEM
SECTIONS

Weight
per
foot

DIMENSIONS

AXIS X-X

AXIS Y-Y



per foot		14" BETHLEHEM H COLUMNS 8—10 and 12" Nominal Flange Widths																
d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r	I	S	r		
43.0	13.375	8.00	.31	12.240	.567	.491	.60	11.063	5 1/2	1 1/2	1*	408.2	61.0	5.70	43.6	10.9	1.86	
48.0	13.500	8.04	.35	12.240	.630	.553	.60	11.063	5 1/2	9/16	1*	461.5	68.4	5.72	49.7	12.4	1.88	
53.5	13.625	8.08	.39	12.240	.692	.616	.60	11.063	5 1/2	5/8	1*	516.2	75.8	5.74	56.0	13.9	1.89	
58.5	13.750	8.12	.43	12.240	.755	.678	.60	11.063	5 1/2	11/16	1*	572.2	83.2	5.76	62.4	15.4	1.90	
55.0	13.500	10.00	.35	12.240	.630	.533	.60	11.063	5 1/2	9/16	1*	551.0	81.6	5.82	93.1	18.6	2.39	
61.5	13.625	10.04	.39	12.240	.692	.596	.60	11.063	5 1/2	5/8	1*	616.9	90.6	5.85	104.8	20.9	2.41	
67.5	13.750	10.08	.43	12.240	.755	.658	.60	11.063	5 1/2	11/16	1*	684.3	99.5	5.87	116.8	23.2	2.43	
73.5	13.875	10.12	.47	12.240	.817	.721	.60	11.063	5 1/2	3/4	1*	753.3	108.6	5.90	129.1	25.5	2.44	
69.0	13.625	12.00	.39	12.240	.692	.576	.60	11.063	9"	5/8	1*	714.6	104.9	5.93	174.7	29.1	2.93	
76.0	13.750	12.04	.43	12.240	.755	.639	.60	11.063	9"	11/16	1*	793.5	115.4	5.95	194.7	32.3	2.95	
83.0	13.875	12.08	.47	12.240	.817	.701	.60	11.063	9"	3/4	1*	874.2	126.0	5.98	215.1	35.6	2.97	
90.0	14.000	12.12	.51	12.240	.880	.764	.60	11.063	9"	13/16	1*	956.7	136.7	6.01	235.8	38.9	2.98	

14" BETHLEHEM H COLUMNS 14" Nominal Flange Width

	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r	I	S	r
84.0	13.750	13.92	.43	12.240	.755	.620	.60	11.063	10"	1 1/8	1	895.5	130.2	6.01	294.5	42.3	3.45
92.0	13.875	13.96	.47	12.240	.817	.683	.60	11.063	10"	3/4	1	987.4	142.3	6.04	325.5	46.6	3.47
100.0	14.000	14.00	.51	12.240	.880	.745	.60	11.063	10"	7/8	1	1081.2	154.5	6.07	356.9	51.0	3.49
107.5	14.125	14.04	.55	12.240	.942	.808	.60	11.063	10"	1 1/4	1	1177.2	166.7	6.10	388.9	55.4	3.50
115.5	14.250	14.08	.59	12.240	1.005	.870	.60	11.063	10"	1 1/2	1	1275.1	179.0	6.12	421.4	59.9	3.52
123.5	14.375	14.12	.63	12.240	1.067	.933	.60	11.063	10"	1 5/8	1	1375.1	191.3	6.15	454.4	64.4	3.54
131.5	14.500	14.16	.67	12.240	1.130	.995	.60	11.063	10"	1 3/4	1	1477.3	203.8	6.18	488.0	68.9	3.55
139.0	14.625	14.19	.70	12.240	1.192	1.058	.60	11.063	10"	1 7/8	1	1578.9	215.9	6.21	520.9	73.4	3.57
147.0	14.750	14.23	.74	12.240	1.255	1.120	.60	11.063	10"	2	1	1685.3	228.5	6.24	555.5	78.1	3.58
155.0	14.875	14.27	.78	12.240	1.317	1.183	.60	11.063	10"	1 1/4	1	1793.8	241.2	6.27	590.6	82.8	3.60
161.0	14.875	15.00	.78	12.240	1.317	1.175	.60	11.063	10"	1 1/2	1	1874.4	252.0	6.29	682.5	91.0	3.80
168.0	15.000	15.02	.80	12.240	1.380	1.237	.60	11.063	10"	1 5/8	1	1984.6	264.6	6.33	720.6	96.0	3.82
177.0	15.125	15.06	.84	12.240	1.442	1.300	.60	11.063	10"	1 3/4	1	2102.6	278.0	6.36	762.1	101.2	3.83
185.0	15.250	15.10	.88	12.240	1.505	1.362	.60	11.063	10"	1 7/8	1	2223.0	291.5	6.39	804.2	106.5	3.84
194.0	15.375	15.14	.92	12.240	1.567	1.425	.60	11.063	10"	2	1	2345.8	305.1	6.42	846.9	111.9	3.86
202.0	15.500	15.18	.96	12.240	1.630	1.487	.60	11.063	10"	1 1/2	1	2470.9	318.8	6.44	890.3	117.3	3.87
210.0	15.625	15.21	.99	12.240	1.692	1.550	.60	11.063	10"	1 5/8	1	2595.4	332.2	6.48	932.4	122.6	3.88
219.0	15.750	15.25	1.01	12.240	1.755	1.612	.60	11.063	10"	1 3/4	1	2726.3	346.1	6.51	976.9	128.1	3.89
227.0	15.875	15.29	1.07	12.240	1.817	1.675	.60	11.063	10"	1 7/8	1	2857.8	360.0	6.53	1022.0	133.7	3.91
236.0	16.000	15.33	1.11	12.240	1.880	1.737	.60	11.063	10"	2	1	2992.9	374.1	6.56	1067.8	139.3	3.92
245.0	16.125	15.37	1.15	12.240	1.942	1.800	.60	11.063	10"	1 5/8	1	3130.4	388.3	6.59	1114.2	145.0	3.93
254.0	16.250	15.41	1.19	12.240	2.005	1.862	.60	11.063	10"	1 3/4	1	3270.6	402.6	6.62	1161.2	150.7	3.94
262.0	16.375	15.45	1.23	12.240	2.067	1.925	.60	11.063	10"	2	1	3413.4	416.9	6.65	1209.0	156.5	3.96
271.0	16.500	15.49	1.27	12.240	2.130	1.987	.60	11.063	10"	2 1/8	1	3558.8	431.4	6.68	1257.3	162.3	3.98
280.0	16.625	15.53	1.31	12.240	2.192	2.050	.60	11.063	10"	2 1/4	1	3706.9	445.9	6.71	1306.4	168.2	3.98
289.0	16.750	15.57	1.35	12.240	2.255	2.112	.60	11.063	10"	2 3/8	1	3857.7	460.6	6.74	1356.1	174.2	3.99
298.0	16.875	15.61	1.39	12.240	2.317	2.175	.60	11.063	10"	2 1/2	1	4011.3	475.4	6.77	1406.5	180.2	4.01

14"



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

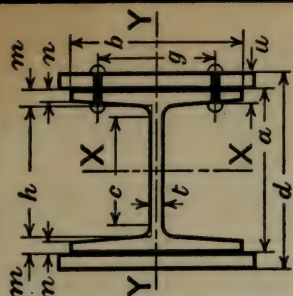
ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14" BETHLEHEM H COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per foot	Area Inches	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET															
				20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	
14" X 26 1/2" BETHLEHEM H COLUMN																			
17 X	3/16	305	89.95	4.11	1349	1317	1272	1227	1181	1135	1090	1046	1003	962	921	882	845	809	774
	7/16	312	92.08	4.13	1381	1351	1305	1258	1212	1165	1120	1075	1030	988	947	907	868	831	797
	1/2	320	94.20	4.14	1413	1383	1336	1289	1242	1194	1147	1102	1057	1013	971	930	891	853	817
	9/16	327	96.33	4.16	1445	1415	1370	1321	1273	1224	1177	1130	1085	1039	997	955	915	877	840
	5/8	334	98.45	4.18	1477	1447	1403	1353	1304	1255	1207	1159	1112	1067	1023	981	939	900	862
17 X	11/16	342	100.58	4.20	1509	1485	1435	1386	1336	1285	1236	1188	1141	1094	1049	1006	964	924	885
	3/4	349	102.70	4.21	1541	1517	1468	1416	1365	1315	1264	1215	1167	1119	1073	1029	986	946	906
	13/16	356	104.83	4.23	1572	1551	1500	1449	1397	1346	1295	1244	1195	1147	1101	1055	1012	970	930
	7/8	363	106.95	4.24	1604	1584	1533	1480	1427	1374	1323	1272	1221	1172	1125	1078	1034	991	951
	15/16	370	109.08	4.26	1636	1619	1565	1512	1458	1405	1353	1301	1249	1200	1151	1104	1058	1016	974
14" X 29 3/8" BETHLEHEM H COLUMN																			
18 X	5/16	375	110.13	4.28	1652	1637	1584	1531	1477	1423	1369	1317	1265	1216	1166	1119	1073	1031	988
	3/4	382	112.38	4.30	1686	1672	1619	1565	1510	1456	1401	1349	1296	1245	1194	1147	1100	1056	1013
	1/2	390	114.63	4.32	1719	1709	1655	1600	1544	1490	1434	1380	1326	1275	1224	1175	1127	1082	1039
	9/16	397	116.88	4.33	1753	1744	1689	1633	1577	1521	1465	1408	1355	1302	1251	1200	1151	1106	1061
	5/8	405	119.13	4.35	1787	1780	1725	1668	1611	1553	1496	1440	1385	1332	1279	1228	1178	1132	1086
18 X	11/16	413	121.38	4.37	1821	1816	1760	1702	1645	1586	1528	1472	1415	1362	1308	1256	1205	1158	1112
	3/4	420	123.63	4.39	1854	1853	1796	1737	1679	1620	1561	1503	1446	1391	1338	1285	1234	1184	1137
	1/2	428	125.88	4.40	1888	1888	1830	1771	1712	1652	1592	1533	1475	1419	1365	1310	1259	1208	1161
	9/16	436	128.13	4.42	1922	1922	1866	1807	1746	1685	1625	1566	1507	1449	1394	1339	1286	1235	1186
	5/8	443	130.38	4.54	1956	1956	1918	1859	1799	1739	1679	1619	1562	1503	1447	1392	1340	1288	1239
19 X	1 1/16	451	132.75	4.56	1991	1991	1955	1896	1836	1775	1714	1654	1594	1536	1479	1423	1369	1317	1266
	1/2	460	135.13	4.58	2027	2027	1995	1934	1873	1811	1749	1688	1627	1569	1511	1454	1399	1346	1295
	9/16	468	137.50	4.60	2063	2063	2032	1972	1910	1847	1785	1722	1661	1601	1543	1485	1429	1375	1323
	5/8	476	139.88	4.61	2098	2098	2069	2007	1944	1881	1817	1754	1693	1631	1571	1514	1456	1402	1348
	11/16	484	142.25	4.63	2134	2134	2108	2044	1982	1916	1852	1790	1725	1664	1603	1543	1487	1431	1377
19 X	3/4	492	144.63	4.65	2169	2169	2146	2083	2018	1953	1887	1824	1760	1697	1636	1575	1517	1461	1406
	1 1/16	500	147.00	4.66	2205	2205	2183	2118	2052	1986	1921	1856	1790	1727	1664	1604	1545	1486	1432
	1/2	508	149.38	4.67	2241	2241	2220	2154	2088	2021	1955	1888	1822	1758	1694	1633	1573	1513	1458
	9/16	516	151.75	4.69	2276	2276	2258	2193	2126	2058	1991	1923	1856	1791	1727	1665	1602	1543	1486
	5/8	524	154.13	4.70	2312	2312	2295	2229	2161	2093	2024	1956	1888	1822	1757	1692	1631	1571	1512
19 X	11/16	532	156.50	4.71	2348	2348	2332	2265	2196	2127	2058	1988	1920	1853	1786	1722	1659	1598	1538
	3/4	540	158.88	4.73	2383	2383	2372	2304	2234	2164	2094	2024	1954	1886	1819	1754	1690	1629	1568
	1 1/16	548	161.25	4.74	2419	2419	2409	2340	2269	2198	2127	2056	1987	1917	1850	1782	1719	1654	1595
	1/2	556	163.63	4.75	2454	2454	2446	2376	2306	2234	2162	2090	2019	1949	1880	1811	1748	1682	1622
	9/16	564	166.00	4.76	2489	2489	2481	2411	2340	2269	2197	2125	2054	1983	1912	1841	1770	1700	1630

Loads to right of heavy vertical lines are for Secondary Members ONLY. For 14" Bethlehem 149# Special H.Column with cover plates see following pages.

DIMENSIONS AND FUNCTIONS OF 14" BETHLEHEM H COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per foot	DIMENSIONS										AXIS X - X				AXIS Y - Y			
		d	b	t	a	h	m	n	c	g	u	Riv.	I	S	r	I	S	r	
14" × 262" BETHLEHEM H COLUMN																			
17 × $\frac{3}{8}$ 305	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 4307.8	503.1 517.7	6.92 6.96	1516.0 1567.2	178.4 184.4	4.11 4.13							
17 × $\frac{7}{16}$ 313	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 4464.8	532.3 546.9	7.01 7.05	1618.4 1669.6	190.4 196.4	4.14 4.16							
17 × $\frac{9}{16}$ 327	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 4785.5	561.6 576.4	7.09 7.13	1669.6 1720.7	202.4 208.5	4.18 4.20							
17 × $\frac{5}{8}$ 334	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5115.6	576.4 591.2	7.13 7.17	1720.7 1771.9	202.4 208.5	4.18 4.20							
17 × $\frac{11}{16}$ 342	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5284.1	591.2 606.1	7.13 7.21	1771.9 1823.1	208.5 214.5	4.20 4.21							
17 × $\frac{13}{16}$ 349	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5455.1	606.1 621.1	7.21 7.25	1823.1 1874.3	214.5 220.5	4.21 4.23							
17 × $\frac{15}{16}$ 356	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5628.4	621.1 636.1	7.25 7.29	1874.3 1925.5	220.5 226.5	4.23 4.24							
17 × $\frac{17}{16}$ 363	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5804.1	636.1 651.6	7.29 7.33	1925.5 1976.6	226.5 232.5	4.24 4.26							
17 × $\frac{19}{16}$ 370	17 $\frac{1}{4}$ 15.45	1.23 163	12.24 163	2.067 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5804.1	636.1 651.6	7.29 7.33	1976.6 2027.7	232.5 238.5	4.26 4.28							
14" × 298" BETHLEHEM H COLUMN																			
18 × $\frac{5}{8}$ 375	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5734.7	632.8 648.8	7.22 7.26	2014.0 2074.7	223.8 230.5	4.28 4.30							
18 × $\frac{11}{16}$ 382	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 5920.7	648.8 665.0	7.26 7.30	2074.7 2135.5	230.5 237.3	4.30 4.32							
18 × $\frac{3}{4}$ 390	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 6109.4	665.0 681.1	7.30 7.34	2135.5 2196.2	237.3 244.0	4.32 4.33							
18 × $\frac{13}{16}$ 397	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 6300.6	681.1 697.4	7.34 7.38	2196.2 2257.0	244.0 250.8	4.33 4.35							
18 × $\frac{15}{16}$ 405	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 6494.4	697.4 713.7	7.38 7.42	2257.0 2317.7	250.8 257.5	4.35 4.37							
18 × $\frac{17}{16}$ 413	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 6690.8	713.7 730.1	7.42 7.47	2317.7 2378.5	257.5 264.3	4.37 4.39							
18 × $\frac{19}{16}$ 420	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 6889.9	730.1 746.5	7.47 7.51	2378.5 2439.2	264.3 271.0	4.39 4.40							
18 × $\frac{11}{8}$ 428	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 7091.6	746.5 763.0	7.51 7.55	2439.2 2500.0	271.0 277.8	4.40 4.42							
18 × $\frac{5}{8}$ 436	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 7296.0	763.0 779.4	7.55 7.59	2500.0 2560.8	277.8 284.6	4.42 4.44							
18 × $\frac{3}{4}$ 443	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 7478.5	779.4 795.7	7.59 7.63	2560.8 2621.6	284.6 291.4	4.44 4.46							
18 × $\frac{7}{8}$ 451	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 7697.1	795.7 812.0	7.63 7.67	2621.6 2682.4	291.4 298.2	4.46 4.48							
18 × $\frac{9}{8}$ 460	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 7918.6	812.0 828.3	7.67 7.71	2682.4 2743.2	298.2 305.0	4.48 4.50							
18 × $\frac{5}{8}$ 468	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 8142.9	828.3 844.6	7.71 7.75	2743.2 2804.0	305.0 311.8	4.50 4.52							
18 × $\frac{11}{8}$ 476	18 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 8370.1	844.6 860.9	7.75 7.79	2804.0 2864.8	311.8 318.6	4.52 4.54							
19 × $\frac{1}{8}$ 484	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 8600.3	860.9 877.2	7.79 7.83	2864.8 2925.6	318.6 325.4	4.54 4.56							
19 × $\frac{1}{4}$ 492	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 8833.3	877.2 893.5	7.83 7.87	2925.6 2986.4	325.4 332.2	4.56 4.58							
19 × $\frac{3}{8}$ 500	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 9069.4	893.5 909.8	7.87 7.91	2986.4 3047.2	332.2 339.0	4.58 4.60							
19 × $\frac{1}{2}$ 508	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 9308.3	909.8 926.1	7.91 7.95	3047.2 3108.0	339.0 345.8	4.60 4.62							
19 × $\frac{5}{8}$ 508	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 9550.3	926.1 942.4	7.95 7.99	3108.0 3168.8	345.8 352.6	4.62 4.64							
19 × $\frac{3}{4}$ 516	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 9550.3	942.4 958.7	7.99 8.03	3168.8 3229.6	352.6 359.4	4.64 4.66							
19 × $\frac{7}{8}$ 524	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 9795.3	958.7 975.0	8.03 8.07	3229.6 3290.4	359.4 366.2	4.66 4.68							
19 × $\frac{15}{16}$ 530	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 10043.3	975.0 991.3	8.07 8.11	3290.4 3351.2	366.2 373.0	4.68 4.70							
19 × $\frac{17}{16}$ 540	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 10294.4	991.3 1007.6	8.11 8.15	3351.2 3412.0	373.0 379.8	4.70 4.72							
19 × $\frac{19}{16}$ 548	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 10548.5	1007.6 1023.9	8.15 8.19	3412.0 3472.8	379.8 386.6	4.72 4.74							
19 × $\frac{11}{8}$ 556	19 $\frac{1}{4}$ 15.61	1.39 167	12.24 167	2.317 1925	11 $\frac{1}{16}$ 10 $\frac{2}{8}$	10 $\frac{2}{8}$ 2 $\frac{3}{8}$	1 $\frac{1}{8}$ 10805.7	1023.9 1040.2	8.19 8.23	3472.8 3533.6	386.6 393.4	4.74 4.76							



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



For 14" Bethlehem 149" Special H Column with cover plates see following pages.

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14" BETHLEHEM SPECIAL H COLUMN WITH COVER PLATES

UNSUPPORTED LENGTH IN FEET																		
14" X 149% BETHLEHEM SPECIAL H COLUMN																		
2 Cover Plates	Weight per foot	Area Square Inches	Least Radius Gyration	14" X 149% BETHLEHEM SPECIAL H COLUMN														
				18	20	22	24	26	28	30	32	34	36	38	40	42	44	48
None	149.	43.82	3.27	1295	1295	1270	1227	1183	1140	1097	1055	1013	972	931	893	855	820	753
17 X 1 1/4	293.5	86.32	4.16	1327	1327	1303	1260	1215	1172	1128	1084	1041	999	959	919	881	844	775
1 3/8	300.7	88.44	4.18	1359	1359	1337	1292	1248	1203	1157	1113	1070	1027	985	945	906	868	797
1 1/2	307.9	90.57	4.20	1390	1390	1369	1325	1278	1232	1186	1141	1097	1053	1010	969	929	890	818
1 5/8	315.2	92.69	4.21	1422	1422	1403	1357	1310	1264	1217	1171	1126	1081	1037	996	954	925	841
1 3/2	322.4	94.82	4.23	1454	1454	1437	1390	1343	1295	1248	1200	1155	1109	1064	1021	979	938	864
17 X 1 9/16	329.6	96.94	4.25	1486	1486	1470	1422	1373	1325	1276	1228	1182	1134	1090	1045	1003	961	885
1 5/8	336.8	99.07	4.26	1518	1518	1504	1455	1407	1357	1307	1258	1210	1163	1117	1072	1028	986	908
1 11/16	344.1	101.19	4.28	1550	1550	1536	1487	1437	1387	1337	1286	1238	1189	1143	1097	1053	1009	929
1 3/4	351.3	103.32	4.29	1582	1582	1569	1519	1469	1417	1367	1315	1265	1216	1168	1122	1077	1032	950
1 13/16	358.5	105.44	4.30	1602	1602	1602	1567	1519	1469	1420	1371	1321	1273	1226	1180	1135	1092	1008
18 X 1 3/4	363.2	106.82	4.51	1636	1636	1636	1602	1552	1502	1452	1402	1351	1302	1254	1207	1162	1117	1032
1 13/16	370.8	109.07	4.52	1670	1670	1670	1638	1587	1536	1485	1434	1383	1334	1284	1236	1189	1144	1058
1 7/8	378.5	111.32	4.54	1704	1704	1704	1672	1621	1568	1516	1464	1413	1362	1312	1263	1215	1169	1081
1 15/16	386.1	113.57	4.55	1737	1737	1737	1706	1654	1602	1549	1495	1443	1391	1340	1290	1242	1194	1105
2	393.8	115.82	4.56	1771	1771	1771	1743	1690	1636	1582	1528	1475	1422	1371	1320	1270	1222	1131
18 X 2 1/16	401.4	118.07	4.58	1805	1805	1805	1777	1723	1669	1613	1559	1505	1451	1399	1348	1297	1248	1155
2 1/8	409.1	120.32	4.59	1839	1839	1839	1812	1758	1702	1646	1591	1535	1481	1427	1375	1324	1274	1179
2 3/8	416.7	122.57	4.60	1872	1872	1872	1846	1791	1735	1679	1621	1565	1510	1455	1402	1351	1299	1203
2 1/2	424.4	124.82	4.61	1906	1906	1906	1882	1825	1768	1710	1655	1596	1539	1484	1430	1376	1325	1227
2 5/16	432.0	127.07	4.62	1940	1940	1940	1914	1857	1799	1740	1682	1621	1561	1508	1453	1403	1351	1305
19 X 2 1/8	439.7	129.32	4.85	1975	1975	1975	1947	1889	1830	1770	1710	1649	1588	1528	1474	1424	1371	1331
2 5/8	447.8	131.69	4.86	2011	2011	2011	1982	1923	1862	1801	1740	1678	1616	1554	1493	1439	1384	1358
2 3/4	455.8	134.07	4.87	2047	2047	2047	2017	1957	1895	1832	1769	1706	1643	1580	1516	1459	1403	1384
2 7/8	463.9	136.44	4.88	2082	2082	2082	2052	1991	1928	1864	1801	1737	1673	1608	1543	1478	1421	1410
2 1/2	472.0	138.82	4.89	2118	2118	2118	2087	2025	1962	1898	1833	1768	1703	1638	1572	1506	1449	1440
19 X 2 9/16	480.1	141.19	4.91	2154	2154	2154	2122	2059	1995	1931	1866	1800	1734	1668	1602	1536	1479	1467
2 5/8	488.1	143.57	4.92	2190	2190	2190	2157	2093	2028	1963	1897	1831	1765	1699	1632	1566	1509	1494
2 11/8	496.2	145.94	4.93	2225	2225	2225	2191	2126	2060	1994	1928	1861	1795	1729	1662	1604	1546	1520
2 3/4	504.3	148.32	4.94	2260	2260	2260	2225	2159	2092	2025	1958	1891	1824	1757	1690	1623	1565	1545
2 13/16	512.4	150.69	4.94	2296	2296	2296	2259	2192	2125	2057	1989	1921	1853	1785	1718	1650	1591	1572
2 7/8	520.4	153.07	4.95	2331	2331	2331	2294	2227	2159	2091	2022	1954	1885	1817	1749	1681	1618	1595

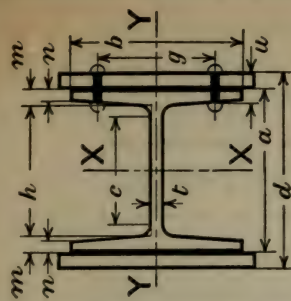
Loads to right of heavy vertical lines are for Secondary Members ONLY.

For 14" Bethlehem 262# and 298# H Columns with cover plates see preceding pages.

DIMENSIONS AND FUNCTIONS OF 14" BETHLEHEM SPECIAL H COLUMN WITH COVER PLATES

2 Cover Plates		Weight per foot	DIMENSIONS											AXIS X-X			AXIS Y-Y			
			d	b	t	a	h	m	n	c	g	u	Riv.	I	S	r	I	S	r	
14" X 149" BETHLEHEM SPECIAL H COLUMN																				
None	149.0	14 1/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	7/8	1379.1	195.3	5.61	468.8	62.9	4.16	3.27
	17 X 1 1/8	293.5	16 5/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	3896.3	468.7	6.72	1492.4	175.6	4.18	4.16
	17 X 1 3/8	300.7	16 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	4044.2	482.9	6.81	1543.5	181.6	4.20	4.18
	17 X 1 7/8	307.9	16 7/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	4194.4	497.1	6.81	1594.7	187.6	4.20	4.20
	17 X 1 1/2	315.2	17	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	4346.8	511.4	6.85	1645.9	193.6	4.21	4.21
17 X 1 9/16	322.4	17 1/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	4501.5	525.7	6.89	1697.1	199.7	4.23	4.23
	329.6	17 1/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	4658.4	540.1	6.93	1748.3	205.7	4.25	4.25
	336.8	17 1/2	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	4817.6	554.5	6.97	1799.4	211.7	4.26	4.26
	344.1	17 3/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	4979.2	569.0	7.01	1850.6	217.7	4.28	4.28
	351.3	17 1/2	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	5143.0	583.6	7.06	1901.8	223.7	4.29	4.29
17 X 1 3/4	358.5	17 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	7/8	5309.2	598.2	7.10	1953.0	229.8	4.30	4.30
	363.2	17 5/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 5/8	7/8	7/8	5364.4	608.7	7.09	2169.8	241.1	4.51	4.51
	370.8	17 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 1/8	7/8	7/8	5540.4	624.3	7.13	2230.6	247.8	4.52	4.52
	378.5	17 1/2	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	5718.9	639.9	7.17	2291.3	254.6	4.54	4.54
	386.1	18	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	5899.9	655.5	7.21	2352.1	261.3	4.55	4.55
18 X 2 1/8	393.8	18 1/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 3/8	7/8	7/8	6083.4	671.3	7.25	2412.8	268.1	4.56	4.56
	401.4	18 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	2 5/8	7/8	7/8	6269.5	687.1	7.29	2473.6	274.8	4.58	4.58
	409.1	18 5/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3"	7/8	7/8	6458.1	702.9	7.33	2534.3	281.6	4.59	4.59
	416.7	18 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/8	7/8	7/8	6649.3	718.8	7.37	2595.1	288.3	4.60	4.60
	424.4	18 5/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/8	7/8	7/8	6843.1	734.8	7.40	2655.8	295.1	4.61	4.61
18 X 2 3/8	432.0	18 3/2	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	7039.6	750.9	7.44	2716.6	301.8	4.62	4.62
	439.7	18 5/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/8	7/8	7/8	7146.7	767.4	7.43	3040.9	320.1	4.85	4.85
	447.8	18 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	7354.1	784.4	7.47	3112.4	327.6	4.86	4.86
	455.8	18 5/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/2	7/8	7/8	7564.2	801.5	7.51	3183.8	335.1	4.87	4.87
	463.9	19	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/2	7/8	7/8	7777.1	818.6	7.55	3255.3	342.7	4.88	4.88
19 X 2 5/8	472.0	19 1/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	7992.9	835.9	7.59	3326.7	350.2	4.89	4.89
	480.1	19 1/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	8211.5	853.1	7.63	3398.2	357.7	4.91	4.91
	488.1	19 3/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	8432.9	870.5	7.66	3469.6	365.2	4.92	4.92
	496.2	19 1/2	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/8	7/8	7/8	8657.3	887.9	7.70	3541.1	372.7	4.93	4.93
	504.3	19 3/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 5/8	7/8	7/8	8884.5	905.4	7.74	3612.5	380.3	4.94	4.94
19 X 2 7/8	512.4	19 1/4	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 1/2	7/8	7/8	9114.6	923.0	7.78	3684.0	387.8	4.94	4.94
	520.4	19 3/8	14.90	1.41	14 1/8	12.24	.942	.808	11 1/8	10"	3 3/4	7/8	7/8	9347.7	940.6	7.81	3755.4	395.3	4.95	4.95

For 14" Bethlehem 262's and 298's H Columns with cover plates see preceding pages.



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

14"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 16" ROLLED COLUMNS

BETHLEHEM
SECTIONS

Weight per foot	Area Square Inch.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET															
			16" BETHLEHEM H COLUMNS															
			16	18	20	22	24	26	28	30	32	34	36	38	40	44	48	
143.0	42.03	3.90	630	625	603	580	558	536	514	492	470	450	430	411	375	342		
151.0	44.56	3.92	668	664	641	617	593	569	546	523	501	479	458	438	400	365		
160.0	47.10	3.93	707	702	678	653	628	603	578	554	530	507	485	463	423	387		
169.0	49.65	3.95	745	742	716	690	664	638	612	586	561	537	513	491	448	410		
177.0	52.20	3.96	783	780	754	727	698	671	644	617	591	565	541	517	472	432		
186.0	54.77	3.98	822	820	792	763	735	706	678	650	622	596	570	546	498	456		
195.0	57.35	4.00	860	860	832	801	771	742	712	683	654	626	599	574	524	479		
203.0	59.94	4.01	899	899	870	839	807	776	745	715	685	656	628	601	550	503		
212.0	62.53	4.02	938	938	909	875	844	811	778	747	716	685	657	628	575	526		
221.0	65.10	4.04	977	977	948	914	881	848	814	780	748	717	687	657	602	550		
230.0	67.60	4.05	1014	1014	984	950	915	880	846	811	778	746	714	683	626	573		
238.0	70.07	4.07	1051	1051	1022	987	951	914	879	844	809	776	743	711	652	597		
247.0	72.70	4.08	1091	1091	1061	1025	988	950	913	877	841	806	773	739	678	621		
256.0	75.35	4.10	1130	1130	1102	1065	1026	988	949	912	875	839	804	770	706	647		
265.0	78.00	4.11	1170	1170	1142	1103	1064	1024	984	945	907	870	834	799	732	672		
274.0	80.67	4.12	1210	1210	1183	1142	1101	1060	1020	979	940	901	864	828	759	696		
283.0	84.69	4.14	1270	1270	1243	1201	1159	1116	1073	1032	991	950	910	873	801	734		
301.0	88.56	4.16	1328	1328	1303	1259	1214	1170	1126	1082	1039	997	956	917	841	772		
314.0	92.45	4.18	1387	1387	1362	1317	1270	1225	1179	1133	1088	1045	1002	961	882	810		
328.0	96.53	4.20	1448	1448	1425	1377	1330	1282	1234	1186	1140	1095	1050	1007	925	849		
342.0	100.63	4.22	1509	1509	1487	1439	1390	1339	1290	1241	1192	1145	1099	1055	969	891		
356.0	104.75	4.24	1571	1571	1551	1501	1450	1397	1346	1296	1245	1196	1148	1102	1013	931		
370.0	108.90	4.26	1634	1634	1616	1563	1509	1456	1403	1350	1299	1247	1198	1149	1056	972		
384.0	113.07	4.27	1696	1696	1679	1625	1569	1514	1459	1404	1350	1297	1246	1195	1099	1012		
399.0	117.26	4.29	1759	1759	1744	1687	1631	1574	1517	1460	1405	1350	1297	1245	1146	1054		
413.0	121.48	4.31	1822	1822	1810	1753	1695	1635	1577	1517	1460	1403	1348	1295	1197	1108		
427.0	125.72	4.33	1886	1886	1876	1817	1756	1696	1636	1575	1515	1457	1401	1348	1238	1142		

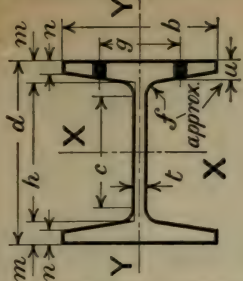
Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 16" ROLLED COLUMNS

BETHLEHEM
SECTIONS

Weight per foot	DIMENSIONS										16" BETHLEHEM H COLUMNS					AXIS X-X					AXIS Y-Y				
	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r	I	S	r	I	S	r					
143.0	14.500	15.54	.72	12.240	1.130	.982	.60	11.063	10"	1 1/16	1"	1610.4	222.1	6.19	638.9	82.2	3.90	1610.4	222.1	6.19	638.9	82.2	3.90		
151.0	14.625	15.58	.76	12.240	1.193	1.044	.60	11.063	10"	1 1/8	1"	1723.8	235.7	6.22	683.4	87.7	3.92	1723.8	235.7	6.22	683.4	87.7	3.92		
160.0	14.750	15.62	.80	12.240	1.255	1.107	.60	11.063	10"	1 3/16	1"	1839.5	249.4	6.25	728.5	93.3	3.93	1839.5	249.4	6.25	728.5	93.3	3.93		
169.0	14.875	15.66	.84	12.240	1.318	1.169	.60	11.063	10"	1 1/4	1"	1957.6	263.2	6.28	774.2	98.9	3.95	1957.6	263.2	6.28	774.2	98.9	3.95		
177.0	15.000	15.70	.88	12.240	1.380	1.232	.60	11.063	10"	1 5/16	1"	2078.0	277.1	6.31	820.7	104.5	3.96	2078.0	277.1	6.31	820.7	104.5	3.96		
186.0	15.125	15.74	.92	12.240	1.443	1.294	.60	11.063	10"	1 3/8	1"	2200.9	291.0	6.34	867.7	110.3	3.98	2200.9	291.0	6.34	867.7	110.3	3.98		
195.0	15.250	15.78	.96	12.240	1.505	1.357	.60	11.063	10"	1 7/16	1"	2326.1	305.1	6.37	915.5	116.0	4.00	2326.1	305.1	6.37	915.5	116.0	4.00		
203.0	15.375	15.82	1.00	12.240	1.568	1.419	.60	11.063	10"	1 1/2	1"	2453.9	319.2	6.40	963.9	121.9	4.01	2453.9	319.2	6.40	963.9	121.9	4.01		
212.0	15.500	15.86	1.04	12.240	1.630	1.482	.60	11.063	10"	1 9/16	1"	2584.1	333.4	6.43	1013.0	127.7	4.02	2584.1	333.4	6.43	1013.0	127.7	4.02		
221.0	15.625	15.90	1.08	12.240	1.693	1.544	.60	11.063	10"	1 5/8	1"	2716.9	347.8	6.46	1062.7	133.7	4.04	2716.9	347.8	6.46	1062.7	133.7	4.04		
230.0	15.750	15.93	1.11	12.240	1.755	1.607	.60	11.063	10"	1 11/16	1"	2848.9	361.8	6.49	1111.0	139.5	4.05	2848.9	361.8	6.49	1111.0	139.5	4.05		
238.0	15.875	15.96	1.14	12.240	1.818	1.669	.60	11.063	10"	1 3/4	1"	2983.4	375.9	6.53	1159.8	145.3	4.07	2983.4	375.9	6.53	1159.8	145.3	4.07		
247.0	16.000	16.00	1.18	12.240	1.880	1.732	.60	11.063	10"	1 13/16	1"	3123.7	390.5	6.55	1211.4	151.4	4.08	3123.7	390.5	6.55	1211.4	151.4	4.08		
256.0	16.125	16.04	1.22	12.240	1.943	1.794	.60	11.063	10"	1 7/8	1"	3266.7	405.2	6.58	1263.8	157.6	4.10	3266.7	405.2	6.58	1263.8	157.6	4.10		
265.0	16.250	16.08	1.26	12.240	2.005	1.857	.60	11.063	10"	1 15/16	1"	3412.4	420.0	6.61	1316.8	163.8	4.11	3412.4	420.0	6.61	1316.8	163.8	4.11		
274.0	16.375	16.12	1.30	12.240	2.068	1.919	.60	11.063	10"	2 ⁻	1"	3560.7	434.9	6.64	1370.6	170.0	4.12	3560.7	434.9	6.64	1370.6	170.0	4.12		
288.0	16.563	16.18	1.36	12.240	2.161	2.013	.60	11.063	10"	2 1/16	1"	3788.4	457.5	6.69	1452.5	179.5	4.14	3788.4	457.5	6.69	1452.5	179.5	4.14		
301.0	16.750	16.23	1.41	12.240	2.255	2.107	.60	11.063	10"	2 3/16	1"	4018.4	479.8	6.74	1533.2	188.9	4.16	4018.4	479.8	6.74	1533.2	188.9	4.16		
314.0	16.938	16.28	1.46	12.240	2.349	2.201	.60	11.063	10"	2 1/4	1"	4254.5	502.4	6.78	1615.2	198.4	4.18	4254.5	502.4	6.78	1615.2	198.4	4.18		
328.0	17.125	16.34	1.52	12.240	2.443	2.294	.60	11.063	10"	2 5/8	1"	4500.9	525.7	6.83	1701.8	208.3	4.20	4500.9	525.7	6.83	1701.8	208.3	4.20		
342.0	17.313	16.40	1.58	12.240	2.536	2.388	.60	11.063	10"	2 7/8	1"	4754.0	549.2	6.87	1790.1	218.3	4.22	4754.0	549.2	6.87	1790.1	218.3	4.22		
356.0	17.500	16.46	1.64	12.240	2.630	2.482	.60	11.063	10"	2 9/16	1"	5013.7	573.0	6.92	1880.0	228.4	4.24	5013.7	573.0	6.92	1880.0	228.4	4.24		
370.0	17.688	16.52	1.70	12.240	2.724	2.576	.60	11.063	10"	2 ⁺	1"	5280.2	597.1	6.96	1971.7	238.7	4.26	5280.2	597.1	6.96	1971.7	238.7	4.26		
384.0	17.875	16.58	1.76	12.240	2.818	2.669	.60	11.063	10"	2 3/4	1"	5553.6	621.4	7.01	2065.1	249.1	4.27	5553.6	621.4	7.01	2065.1	249.1	4.27		
399.0	18.063	16.64	1.82	12.240	2.911	2.763	.60	11.063	10"	2 13/16	1"	5834.0	646.0	7.05	2160.3	259.6	4.29	5834.0	646.0	7.05	2160.3	259.6	4.29		
413.0	18.250	16.70	1.88	12.240	3.005	2.857	.60	11.063	10"	2 15/16	1"	6121.5	670.8	7.10	2257.2	270.3	4.31	6121.5	670.8	7.10	2257.2	270.3	4.31		
427.0	18.438	16.76	1.94	12.240	3.099	2.951	.60	11.063	10"	3 ⁻	1"	6416.2	696.0	7.14	2355.9	281.1	4.33	6416.2	696.0	7.14	2355.9	281.1	4.33		

I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration

16"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 16" BETHLEHEM H COLUMNS WITH COVER PLATES

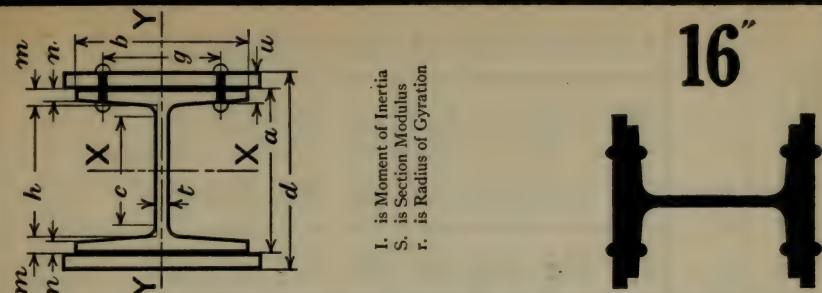
2 Cover Plates		Weight per Foot	Area Square Inches	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET															
					18	20	22	24	26	28	30	32	34	36	38	40	42	44	48	
16" X 293# BETHLEHEM H COLUMN																				
18 X	5/16 11/16 3/4	370	108.74	4.36-	1631	1626	1626	1576	1523	1471	1420	1368	1317	1267	1218	1170	1123	1078	994	
		377	110.99	4.38	1665	1663	1663	1612	1558	1506	1453	1400	1349	1296	1248	1199	1151	1105	1019	
18 X	7/16 15/16	385	113.24	4.40	1699	1699	1699	1647	1593	1540	1486	1432	1379	1327	1276	1228	1179	1132	1044	
		392	115.49	4.42	1732	1732	1732	1682	1628	1574	1519	1464	1411	1358	1306	1257	1207	1160	1069	
18 X	1 1/16 1 1/8	400	117.74	4.43	1766	1766	1766	1715	1661	1606	1549	1495	1441	1387	1334	1282	1233	1184	1093	
		408	119.99	4.45	1800	1800	1800	1752	1697	1640	1584	1527	1472	1417	1364	1311	1261	1212	1118	
18 X	1 1/8	415	122.24	4.46	1834	1834	1834	1786	1730	1672	1616	1559	1502	1446	1392	1339	1287	1237	1142	
		423	124.49	4.48	1867	1867	1867	1823	1765	1707	1649	1591	1534	1478	1422	1368	1316	1265	1168	
18 X	1 1/8	431	126.74	4.49	1901	1901	1901	1857	1798	1739	1681	1622	1564	1506	1450	1395	1342	1290	1191	
16" X 363# BETHLEHEM H COLUMN																				
18 X	5/16 11/16 3/4	440	129.36	4.42	1940	1940	1940	1883	1824	1763	1701	1640	1581	1521	1463	1407	1352	1299	1198	
		447	131.61	4.43	1974	1974	1974	1918	1857	1795	1732	1671	1611	1550	1491	1433	1378	1324	1221	
18 X	7/16 15/16	455	133.86	4.44	2008	2008	2008	1953	1891	1829	1764	1703	1641	1580	1519	1460	1404	1349	1245	
		463	136.11	4.46	2042	2042	2042	1989	1926	1862	1799	1735	1673	1610	1550	1490	1433	1377	1271	
18 X	1 1/16 1 1/8	470	138.36	4.47	2075	2075	2075	2023	1959	1894	1831	1765	1703	1640	1579	1518	1460	1403	1295	
		478	140.61	4.48	2109	2109	2109	2059	1994	1928	1863	1797	1732	1669	1606	1545	1486	1429	1319	
18 X	1 1/8	486	142.86	4.49	2143	2143	2143	2093	2027	1960	1894	1829	1763	1697	1634	1573	1513	1454	1343	
		493	145.11	4.51	2177	2177	2177	2129	2063	1995	1929	1862	1795	1730	1666	1603	1543	1483	1370	
19 X	1 1/8	501	147.36	4.52	2210	2210	2210	2165	2097	2029	1961	1894	1826	1759	1695	1631	1569	1509	1394	
19 X	1 1/4	509	149.61	4.63	2244	2244	2244	2217	2150	2084	2015	1948	1882	1815	1750	1686	1623	1563	1448	
		517	151.99	4.64	2280	2280	2280	2254	2186	2119	2049	1980	1914	1847	1780	1716	1652	1591	1474	
19 X	1 1/2	525	154.36	4.65	2315	2315	2315	2291	2223	2153	2084	2014	1946	1879	1811	1746	1681	1619	1500	
		533	156.74	4.67	2351	2351	2351	2329	2260	2191	2121	2052	1981	1912	1845	1777	1713	1650	1530	
19 X	1 3/4	541	159.11	4.68	2387	2387	2387	2366	2298	2226	2156	2084	2014	1944	1874	1807	1742	1677	1555	
		549	161.49	4.69	2422	2422	2422	2403	2334	2262	2190	2119	2046	1975	1906	1838	1772	1705	1581	
19 X	1 5/8	557	163.86	4.71	2458	2458	2458	2442	2371	2300	2227	2155	2081	2011	1940	1870	1802	1737	1611	
		565	166.24	4.72	2494	2494	2494	2479	2407	2334	2263	2188	2115	2041	1970	1900	1832	1765	1637	
19 X	1 5/8	573	168.61	4.73	2529	2529	2529	2517	2445	2371	2296	2222	2148	2074	2001	1931	1861	1794	1664	

Loads to right of heavy vertical lines are for Secondary Members ONLY.
For 16" Bethlehem H Columns with 20" cover plates see following pages.

DIMENSIONS AND FUNCTIONS OF 16" BETHLEHEM H COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per Foot		DIMENSIONS										AXIS X-X				AXIS Y-Y			
	d	b	t	a	h	m	n	c	g	u	Riv.	I	S	r	I	S	r	I	S	r
16" X 293# BETHLEHEM H COLUMN																				
18 X $\frac{5}{16}$	17 $\frac{3}{4}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	5311.5	602.7	6.99	2069.5	229.9	4.36			
18 X $\frac{3}{4}$	17 $\frac{3}{4}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	5487.5	618.3	7.03	2130.2	236.7	4.38			
18 X $\frac{13}{16}$	17 $\frac{3}{4}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	5665.9	633.9	7.07	2191.0	243.4	4.40			
18 X $\frac{1}{2}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	5846.9	649.7	7.12	2251.7	250.2	4.42			
18 X $\frac{7}{8}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	6030.4	665.4	7.16	2312.5	256.9	4.43			
18 X $\frac{1}{4}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	6216.5	681.3	7.20	2373.2	263.7	4.45			
18 X $\frac{1}{8}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	6405.1	697.2	7.24	2434.0	270.4	4.46			
18 X $\frac{1}{16}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	6596.4	713.1	7.28	2494.7	277.2	4.48			
18 X $\frac{1}{32}$	18 $\frac{1}{8}$	16.46	1.64	16.36	12.24	2.068	1.919	11 $\frac{1}{16}$	10 $\frac{1}{16}$	2 $\frac{3}{8}$	1"	6790.2	729.1	7.32	2555.5	283.9	4.49			
16" X 363# BETHLEHEM H COLUMN																				
18 X $\frac{5}{16}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	6720.2	724.1	7.21	2522.0	280.2	4.42			
18 X $\frac{3}{4}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	6915.4	740.1	7.25	2582.8	287.0	4.43			
18 X $\frac{13}{16}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	7113.1	756.2	7.29	2643.5	293.7	4.44			
18 X $\frac{1}{2}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	7313.5	772.4	7.33	2704.3	300.5	4.46			
18 X $\frac{7}{8}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	7516.6	788.6	7.37	2765.0	307.2	4.47			
18 X $\frac{1}{4}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	7722.3	804.9	7.41	2825.8	314.0	4.48			
18 X $\frac{1}{8}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	7930.8	821.3	7.45	2886.5	320.7	4.49			
18 X $\frac{1}{16}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	8141.9	837.8	7.49	2947.3	327.5	4.51			
18 X $\frac{1}{32}$	18 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	8355.8	854.3	7.53	3008.0	334.2	4.52			
19 X $\frac{1}{4}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	8547.3	873.8	7.56	3200.6	336.9	4.63			
19 X $\frac{3}{8}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	8775.9	891.5	7.60	3272.0	344.4	4.64			
19 X $\frac{1}{2}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	9007.5	909.3	7.64	3343.5	351.9	4.65			
19 X $\frac{5}{8}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	9242.1	927.1	7.68	3414.9	359.5	4.67			
19 X $\frac{3}{4}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	9479.6	945.0	7.72	3486.4	367.0	4.68			
19 X $\frac{7}{8}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	9720.1	963.0	7.76	3557.8	374.5	4.69			
19 X $\frac{1}{4}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	9963.5	981.0	7.80	3629.3	382.0	4.71			
19 X $\frac{3}{8}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	10210.0	999.1	7.84	3700.7	389.5	4.72			
19 X $\frac{1}{2}$	19 $\frac{9}{16}$	16.76	1.94	17 $\frac{5}{16}$	12.24	2.536	2.388	11 $\frac{1}{16}$	10 $\frac{1}{16}$	3 $\frac{1}{16}$	1"	10459.6	1017.3	7.88	3772.2	397.1	4.73			

For 16" Bethlehem H Columns with 20" cover plates see following pages.



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

16"

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 16" BETHLEHEM H COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per Square Foot	Area Square Inches	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																16" X 363% BETHLEHEM H COLUMN																	
				22	24	26	28	30	32	34	36	38	40	42	44	46	48	50	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50				
20 X 1 5/16 1 1/4	584	171.86	4.87	2578	2578	2519	2447	2373	2299	2226	2152	2080	2009	1940	1872	1805	1741	1679	20 X 1 3/16 1 1/8	610	179.36	4.91	2690	2690	2637	2561	2486	2411	2333	2258	2183	2107	2038	1966	1898	1829	1765
	593	174.36	4.89	2615	2615	2560	2486	2411	2338	2263	2190	2117	2043	1974	1904	1838	1771	1709		618	181.86	4.93	2728	2728	2677	2602	2526	2450	2371	2295	2219	2144	2071	1999	1930	1862	1795
	601	176.86	4.90	2653	2653	2598	2524	2448	2373	2297	2223	2149	2075	2006	1935	1868	1800	1737		627	184.36	4.94	2765	2765	2716	2640	2563	2485	2408	2328	2253	2177	2102	2030	1958	1890	1823
20 X 2 1/16 2 1/8	635	186.86	4.95	2803	2803	2754	2678	2599	2521	2442	2364	2285	2209	2134	2061	1988	1919	1852	20 X 2 3/16 2 1/4	661	194.36	4.99	2915	2915	2875	2795	2713	2632	2550	2470	2391	2311	2233	2157	2082	2010	1940
	644	189.36	4.96	2840	2840	2795	2715	2638	2556	2479	2399	2320	2242	2166	2092	2019	1949	1880		669	196.86	5.00	2953	2953	2914	2833	2752	2669	2587	2504	2423	2345	2266	2187	2112	2039	1969
	652	191.86	4.97	2878	2878	2834	2753	2675	2594	2513	2433	2352	2275	2199	2122	2049	1978	1909		678	199.36	5.01	2990	2990	2953	2871	2789	2705	2622	2538	2456	2376	2297	2219	2143	2069	1998
20 X 2 5/16 2 1/2	686	201.86	5.02	3028	3028	2992	2909	2826	2741	2658	2574	2491	2410	2329	2251	2174	2099	2027	20 X 2 7/16 2 3/4	712	209.36	5.05	3140	3140	3109	3025	2939	2851	2766	2680	2594	2508	2426	2345	2265	2188	2112
	695	204.36	5.03	3065	3065	3031	2949	2863	2777	2693	2610	2526	2442	2362	2283	2203	2127	2054		720	211.86	5.06	3178	3178	3148	3063	2977	2888	2801	2714	2627	2542	2458	2375	2294	2216	2140
	703	206.86	5.04	3103	3103	3070	2987	2900	2815	2728	2644	2559	2474	2393	2313	2234	2158	2083		729	214.36	5.06	3215	3215	3185	3100	3012	2922	2834	2746	2658	2572	2487	2403	2322	2242	2165
20 X 2 9/16 2 7/8	737	216.86	5.07	3253	3253	3225	3138	3049	2960	2871	2782	2693	2607	2520	2435	2353	2273	2195	20 X 2 11/16 3	763	224.36	5.10	3365	3365	3343	3253	3163	3071	2980	2888	2796	2706	2618	2531	2446	2363	2284
	746	219.36	5.08	3290	3290	3264	3176	3086	2996	2907	2817	2727	2639	2553	2468	2384	2303	2224		754	221.86	5.09	3328	3328	3303	3215	3126	3033	2942	2850	2760	2671	2585	2498	2414	2332	2254
	754	221.86	5.09	3328	3328	3303	3215	3126	3033	2942	2850	2760	2671	2585	2498	2414	2332	2254		771	226.86	5.11	3403	3403	3382	3292	3201	3108	3015	2922	2829	2738	2650	2561	2477	2393	2312

Loads to right of heavy vertical lines are for Secondary Members ONLY.

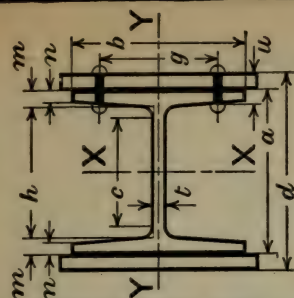
For 16" Bethlehem H Columns with 18" and 19" cover plates see preceding pages.

DIMENSIONS AND FUNCTIONS OF 16" BETHLEHEM H COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per Foot	DIMENSIONS										AXIS X-X			AXIS Y-Y			
		d	b	t	a	h	m	n	c	g	u	Riv.	I	S	r	I	S	r
16" X 363# BETHLEHEM H COLUMN																		
20 X 1 5/8 1 11/16	584	20 9/16	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 1/16	1"	10752	1045.7	7.91	4081.2	408.1	4.87
	593	20 11/16	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 1/8	1"	11018	1065.1	7.95	4164.5	416.5	4.89
	601	20 3/4	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 3/16	1"	11287	1084.6	7.99	4247.8	424.8	4.90
20 X 1 13/16 1 1/8	610	20 15/16	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 1/4	1"	11559	1104.1	8.03	4331.2	433.1	4.91
	618	21 1/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 5/16	1"	11835	1123.8	8.07	4414.5	441.5	4.93
	627	21 3/16	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 3/8	1"	12114	1143.5	8.11	4497.8	449.8	4.94
20 X 2 2 1/8	635	21 5/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 7/16	1"	12396	1163.2	8.14	4581.2	458.1	4.95
	644	21 7/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 1/2	1"	12681	1183.1	8.18	4664.5	466.5	4.96
	652	21 9/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 9/16	1"	12970	1203.0	8.22	4747.8	474.8	4.97
20 X 2 3/8 2 1/4	661	21 11/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 5/8	1"	13262	1223.0	8.26	4831.2	483.1	4.99
	669	21 13/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 11/16	1"	13558	1243.2	8.30	4914.5	491.5	5.00
	678	21 15/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 3/4	1"	13857	1263.3	8.34	4997.8	499.8	5.01
20 X 2 3/4 2 1/2	686	22 1/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 13/16	1"	14160	1283.6	8.38	5081.2	508.1	5.02
	695	22 3/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 7/8	1"	14466	1303.9	8.41	5164.5	516.5	5.03
	703	22 5/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	4 15/16	1"	14775	1324.4	8.45	5247.8	524.8	5.04
20 X 2 7/8 2 5/8	712	22 7/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5	1"	15088	1344.9	8.49	5331.2	533.1	5.05
	720	22 9/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 1/16	1"	15404	1365.5	8.53	5414.5	541.5	5.06
	729	22 11/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 1/8	1"	15724	1386.2	8.56	5497.8	549.8	5.06
20 X 2 3/2 2 3/4	737	23 1/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 3/16	1"	16048	1406.9	8.60	5581.2	558.1	5.07
	746	23 1/4	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 1/4	1"	16375	1427.8	8.64	5664.5	566.5	5.08
	754	23 3/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 5/16	1"	16705	1448.7	8.68	5747.8	574.8	5.09
20 X 2 15/8 3	763	23 5/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 3/8	1"	17040	1469.7	8.71	5831.2	583.1	5.10
	771	23 7/8	16.76	1.94	17 5/16	12.24	2.536	2.388	11 1/16	10"	5 7/16	1"	17378	1490.8	8.75	5914.5	591.5	5.11

I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

For 16" Bethlehem H Columns with 18" and 19" cover plates see preceding pages.

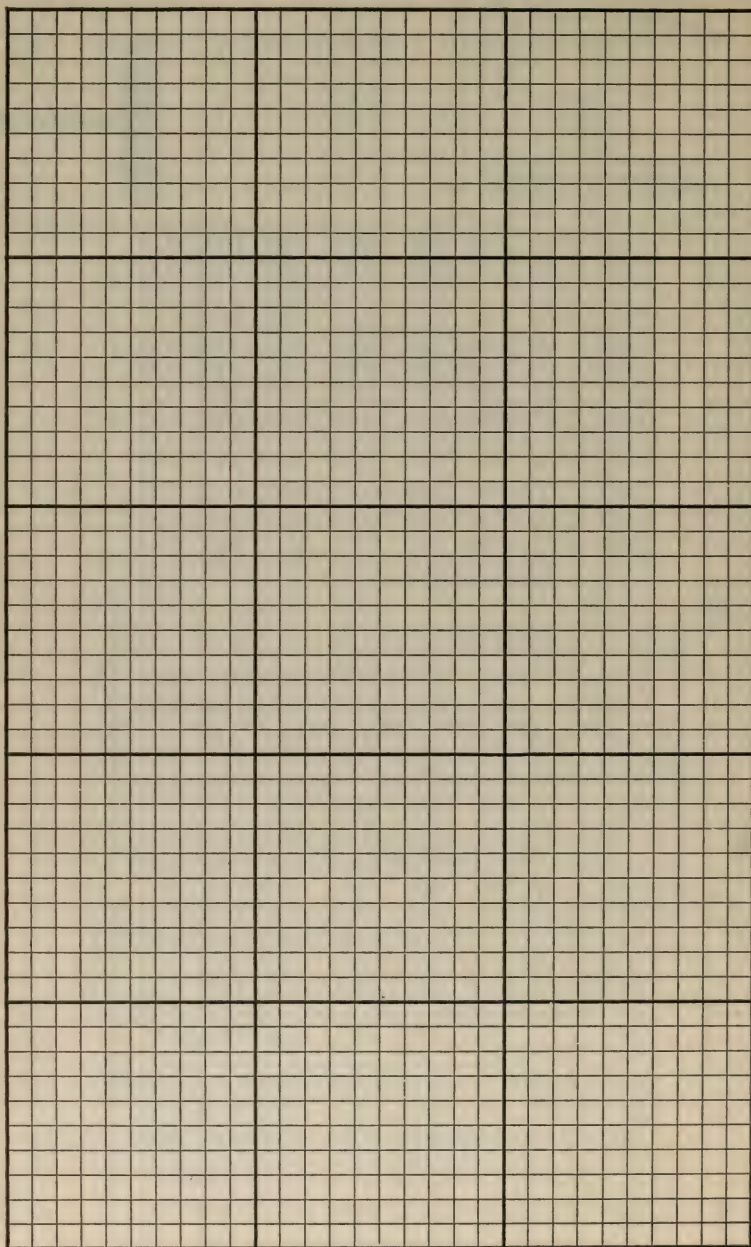


I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

16"



NOTES and DIAGRAMS



Part IV

Section 12

CARNEGIE BEAM COLUMN SECTIONS

Dimensions—Technical Functions

Allowable Concentric Loads by A. I. S. C. Specification

Manufacturers Section Index

Sec. Index	Depth	Weight													
H 1	4"	13.8													
H 2	5"	18.9													
H 3	6"	20.0	22.5												
H 3A	6"	25.0	27.5												
CB 61	6"	40.0	50.0	60.0	70.0	80.0	88.0								
B 39	8"	17.5	21.0												
H 4	8"	32.6	34.3	37.7											
CB 82	8"	24.0	27.0	30.0											
CB 83	8"	31.0	36.0	42.0	48.0	54.0	60.0	66.0	72.0	78.0	84.0	90.0			
B 40	9"	20.5	25.0												
CB 92	9"	29.0	32.0	35.0											
CB 93	9"	38.0	43.0	48.0											
CB 101	10"	21.0	23.0	26.0	30.0										
CB 102	10"	31.0	36.0	42.0											
CB 103A	10"	49.0	54.0	59.0	64.0										
CB 104	10"	70.0	77.0	84.0	92.0										
CB 105	10"	100.0	108.0	116.0	124.0	132.0	140.0								
CB 121	12"	25.0													
CB 122	12"	28.0	32.0	34.0	36.0										
CB 123	12"	40.0	45.0	50.0											
CB 123B	12"	55.0	60.0	66.0											
CB 124B	12"	65.0	70.0	76.0											
CB 124C	12"	82.0	88.0	95.0	102.0										
CB 125	12"	110.0	120.0	130.0	140.0										
CB 126	12"	150.0	160.0	170.0	180.0										
CB 127	12"	190.0	200.0	210.0	220.0	230.0									
CB 141	14"	30.0													
CB 142	14"	33.0	36.0	38.0	39.0	42.0									
CB 143	14"	48.0	53.0	58.0											
CB 144	14"	61.0	68.0	75.0											
CB 145	14"	85.0	95.0	105.0											
CB 146	14"	86.0	96.0	106.0	115.0	125.0	131.0	135.0	145.0	155.0	165.0	175.0	185.0		
CB 146	14"	195.0	205.0	215.0	225.0	235.0	245.0	255.0	265.0	275.0	285.0	295.0	305.0		
CB 146	14"	325.0	345.0	365.0	385.0	405.0	425.0								

CARNegie SMALL AND
SPECIAL SECTIONS

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 4", 5", 6", 8", AND 9" ROLLED COLUMNS

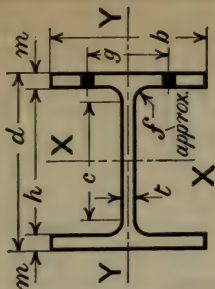
Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																			
			4	6	8	9	10	11	12	13	14	15	16	17	18	19	20	22	24	26	28	30
4" CARNEGIE H BEAMS																						
13.8	3.99	0.95	60	54	46	42	38	35	32	29	26	24										
5" CARNEGIE H BEAMS																						
18.9	5.47	1.20	82	82	73	68	63	59	55	51	47	44	41	38	35	33	31					
6" CARNEGIE H BEAMS																						
20.0	5.86	1.39	88	88	83	79	75	70	66	62	58	55	51	48	45	42	40	35				
22.5	6.61	1.36	99	99	93	88	83	78	73	69	64	60	56	53	50	46	44	38				
25.0	7.33	1.43	110	110	106	100	95	90	84	79	75	70	66	62	58	55	51	46				
27.5	8.08	1.41	121	121	116	110	104	98	92	87	81	76	72	67	63	59	56	49				
6" CARNEGIE SPECIAL BEAM SECTIONS																						
40.0	11.76	2.43	176	176	176	176	176	176	176	172	167	162	157	152	147	142	137	128	119	110	103	95
50.0	14.70	2.48	221	221	221	221	221	221	221	217	211	205	198	192	186	180	174	162	151	141	131	122
60.0	17.63	2.51	264	264	264	264	264	264	264	261	254	247	239	232	225	218	211	197	183	171	159	148
70.0	20.58	2.54	309	309	309	309	309	309	309	306	298	290	281	273	264	256	248	232	216	201	188	175
80.0	23.52	2.58	353	353	353	353	353	353	353	352	343	333	324	314	305	295	286	268	250	234	218	203
88.0	25.87	2.60	388	388	388	388	388	388	388	388	388	378	368	357	347	337	326	316	296	277	259	242
8" CARNEGIE MILL SECTIONS.																						
17.5	5.14	1.08	77	74	64	59	55	51	47	43	39	36	34	31								
21.0	6.17	1.03	93	87	75	69	63	58	53	49	45	41	38	35								
8" CARNEGIE H BEAMS																						
32.6	9.50	1.90	143	143	143	143	140	135	130	124	119	114	109	104	100	95	91	83	75	68	62	57
34.3	10.00	1.87	150	150	150	150	146	141	136	130	124	119	114	108	103	99	94	85	78	71	64	59
37.7	11.00	1.83	165	165	165	165	160	154	147	141	135	129	123	117	112	106	101	92	83	76	69	63
9" CARNEGIE MILL SECTIONS																						
20.5	6.02	1.15	90	89	78	73	68	63	58	54	50	46	43	39	37	34						
25.0	7.34	1.09	110	106	92	85	79	73	67	62	57	53	49	45	42							

Loads to right of heavy vertical lines are for Secondary Members ONLY.

CARNEGIE SMALL AND
SPECIAL SECTIONS

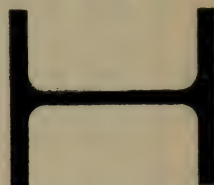
DIMENSIONS AND FUNCTIONS OF 4", 5", 6", 8" AND 9" ROLLED COLUMNS

Weight per foot	DIMENSIONS.											AXIS X-X				AXIS Y-Y			
	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r		I	S	r	
	4" CARNEGIE H BEAMS																		
13.8	4 000	4 000	.313	3.094	.453	.290	.31	2.522	2 1/4	3/8	3/4	10.7	5.35	1.64		3.6	1.80	0.95	
5" CARNEGIE H BEAMS																			
18.9	5 000	5 000	.313	3.994	.503	.330	.31	3.413	2 3/4	13/32	3/4	23.8	9.52	2.08		7.8	3.12	1.20	
6" CARNEGIE H BEAMS																			
20.0	6 000	5 938	.250	5.042	.479	.280	.31	4.458	3 1/2	3/8	3/4	38.8	12.93	2.57		11.4	3.84	1.39	
22.5	6 000	6 063	.375	5.042	.479	.280	.31	4.458	3 1/2	3/8	3/4	41.0	13.67	2.49		12.2	4.02	1.36	
25.0	6 000	5 938	.313	4.840	.580	.381	.31	4.256	3 1/2	15/32	3/4	47.0	15.67	2.53		14.9	5.02	1.43	
27.5	6 000	6 063	.438	4.840	.580	.381	.31	4.256	3 1/2	15/32	3/4	49.3	16.43	2.47		16.0	5.28	1.41	
6" CARNEGIE SPECIAL BEAM SECTIONS																			
40.0	5 750	9 500	.489	4.772	.489		.45	3.872	5 1/2	1 1/2	7/8	69.6	24.21	2.43		69.9	14.72	2.44	
50.0	5 986	9 617	.606	4.772	.607		.45	3.872	5 1/2	1 1/2	7/8	91.0	30.40	2.49		90.1	18.74	2.48	
60.0	6 216	9 733	.722	4.772	.722		.45	3.872	5 1/2	23/32	7/8	113.9	36.65	2.54		111.1	22.83	2.51	
70.0	6 444	9 846	.835	4.772	.836		.45	3.872	5 1/2	27/32	7/8	138.7	43.05	2.60		133.3	27.08	2.54	
80.0	6 666	9 959	.948	4.772	.947		.45	3.872	5 1/2	15/16	7/8	164.9	49.47	2.65		156.3	31.39	2.58	
88.0	6 842	10 046	1.035	4.772	1.035		.45	3.872	5 1/2	1 1/32	7/8	187.3	54.75	2.69		175.4	34.92	2.60	
8" CARNEGIE MILL SECTIONS																			
17.5	8 000	4 981	.231	7.108	.446	.238	.25	6.608	2 3/4	5/16	3/4	57.4	14.35	3.36		6.0	2.44	1.08	
21.0	8 000	5 110	.360	7.108	.446	.238	.25	6.608	2 3/4	5/16	3/4	63.4	15.85	3.21		6.6	2.58	1.03	
8" CARNEGIE H BEAMS																			
32.6	8 000	7 938	.313	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	112.8	28.20	3.45		34.2	8.62	1.90	
34.3	8 000	8 000	.375	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	115.5	28.88	3.40		35.1	8.78	1.87	
37.7	8 000	8 125	.500	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	120.8	30.20	3.31		36.9	9.08	1.83	
9" CARNEGIE MILL SECTIONS																			
20.5	9 000	5 234	.234	8.008	.496	.277	.28	7.458	2 3/4	3/8	3/4	86.6	19.24	3.79		8.0	3.09	1.15	
25.0	9 000	5 380	.380	8.008	.496	.277	.28	7.458	2 3/4	3/8	3/4	95.5	21.22	3.61		8.8	3.27	1.09	



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

4" to 9"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 8" AND 9" ROLLED COLUMNS

CARNEGIE
SECTIONS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																				
			4	6	8	9	10	11	12	13	14	15	16	17	18	19	20	22	24	26	28	30	
8" AMERICAN STANDARD I BEAMS																							
8" CARNEGIE H BEAMS																							
18.4	5.34	.84	80	68	56	50	45	41	37	33													
20.5	5.97	.82	90	75	61	55	49	44	40	36													
32.6	9.50	1.90	143	143	143	143	140	135	130	124	119	114	109	104	100	95	91	83	75	68	62	57	
34.5	10.00	1.87	150	150	150	150	146	141	136	130	124	119	114	108	103	99	94	85	78	71	64	59	
37.7	11.00	1.83	165	165	165	165	160	154	147	141	135	129	123	117	112	106	101	92	83	76	69	63	
8" CARNEGIE BEAM SECTIONS																							
24.0	7.06	1.61	106	106	106	102	97	93	88	84	79	75	71	67	64	60	57	51	46	41			
27.0	7.93	1.62	119	119	119	114	109	104	99	94	89	85	80	76	72	68	64	58	52	47			
30.0	8.81	1.63	132	132	132	127	122	116	111	105	100	95	90	85	80	76	72	65	58	52			
31.0	9.10	2.01	137	137	137	137	137	132	127	123	118	113	109	104	100	96	91	84	77	70	64	59	
36.0	10.58	2.02	159	159	159	159	154	149	143	138	132	127	122	116	112	107	98	89	82	75	69		
42.0	12.34	2.04	185	185	185	185	180	174	168	161	155	149	143	137	131	126	115	105	97	89	81		
48.0	14.10	2.06	212	212	212	212	212	207	200	192	185	178	171	164	158	151	145	133	122	112	102	94	
54.0	15.87	2.07	238	238	238	238	233	225	217	209	201	193	186	178	171	164	150	138	126	116	107		
60.0	17.63	2.09	264	264	264	264	260	251	242	234	225	216	208	199	191	183	168	154	142	130	120		
66.0	19.40	2.11	291	291	291	291	287	277	268	258	249	239	230	221	212	203	187	172	158	145	133		
72.0	21.17	2.12	318	318	318	318	318	314	303	293	282	272	262	252	242	232	223	205	188	173	159	146	
78.0	22.93	2.14	344	344	344	344	344	341	330	319	307	296	285	274	264	253	243	224	206	189	174	160	
84.0	24.71	2.15	371	371	371	371	371	368	356	344	332	320	308	296	285	274	263	242	223	205	189	174	
90.0	26.47	2.17	397	397	397	397	397	395	383	370	357	345	332	320	307	295	284	261	241	222	204	188	
9" CARNEGIE BEAM SECTIONS																							
29.0	8.53	1.59	128	128	128	122	117	111	105	100	95	90	85	80	76	72	68	61	54	49			
32.0	9.40	1.60	141	141	141	135	129	123	117	111	105	99	94	89	84	80	75	67	60	54			
35.0	10.29	1.61	154	154	154	148	142	135	128	122	115	109	103	98	93	88	83	74	67	60			
38.0	11.17	2.26	168	168	168	168	168	168	164	159	154	149	144	138	133	128	124	114	106	95	90	83	
43.0	12.65	2.28	190	190	190	190	190	186	181	175	169	163	157	152	146	141	130	120	111	103	95		
48.0	14.11	2.29	212	212	212	212	212	212	208	202	196	189	183	176	170	164	158	146	135	125	116	107	

Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 8" AND 9" ROLLED COLUMNS

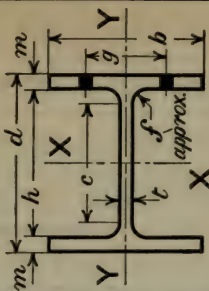
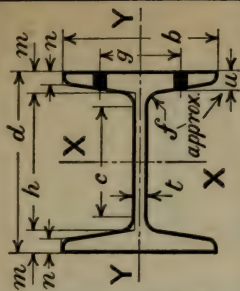
 CARNEGIE
SECTIONS

*CARNEGIE BEAM SECTIONS have flanges of uniform thickness throughout their width.

Weight per foot	DIMENSIONS										AXIS X-X				AXIS Y-Y			
	d	b	t	h	m	n	f	c	g	u	Riv.	I	S	r	I	S	r	
8" AMERICAN STANDARD I BEAMS																		
18.4	8.000	4.000	.270	6.838	.581	.270	.37	6.211	2 1/4	7/16	3/4	56.9	14.22	3.26	3.8	1.90	.84	
20.5	8.000	4.080	.349	6.838	.581	.270	.37	6.211	2 1/4	7/16	3/4	60.2	15.05	3.18	4.0	2.00	.82	
8" CARNEGIE H BEAMS																		
32.6	8.000	7.938	.313	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	112.8	28.20	3.45	34.2	8.62	1.90	
34.3	8.000	8.000	.375	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	115.5	28.88	3.40	35.1	8.78	1.87	
37.7	8.000	8.125	.500	6.880	.560	.358	.31	6.287	5 1/2	15/32	7/8	120.8	30.20	3.31	36.9	9.08	1.83	
8" CARNEGIE BEAM SECTIONS																		
24.0	8.000	6.500	.239	7.200	.400	.45	6.300	3 1/2			7/8	84.3	21.08	3.46	18.3	5.63	1.61	
27.0	8.098	6.529	.268	7.200	.449	.45	6.300	3 1/2			7/8	95.9	23.68	3.48	20.8	6.37	1.62	
30.0	8.196	6.559	.298	7.200	.498	.45	6.300	3 1/2			7/8	107.8	26.31	3.50	23.4	7.14	1.63	
31.0	8.060	8.000	.290	7.200	.430	.45	6.300	5 1/2			7/8	110.9	27.52	3.49	36.7	9.18	2.01	
36.0	8.198	8.046	.336	7.200	.499	.45	6.300	5 1/2			7/8	131.3	32.03	3.52	43.4	10.79	2.02	
42.0	8.360	8.100	.390	7.200	.580	.45	6.300	5 1/2			7/8	156.2	37.37	3.56	51.4	12.69	2.04	
48.0	8.520	8.155	.445	7.200	.660	.45	6.300	5 1/2			7/8	182.2	42.77	3.59	59.7	14.64	2.06	
54.0	8.680	8.208	.498	7.200	.740	.45	6.300	5 1/2			7/8	209.2	48.20	3.63	68.3	16.64	2.07	
60.0	8.838	8.261	.551	7.200	.819	.45	6.300	5 1/2			7/8	237.1	53.65	3.67	77.1	18.67	2.09	
66.0	8.994	8.314	.604	7.200	.897	.45	6.300	5 1/2			7/8	265.9	59.13	3.70	86.1	20.71	2.11	
72.0	9.150	8.366	.656	7.200	.975	.45	6.300	5 1/2			7/8	295.9	64.68	3.74	95.3	22.78	2.12	
78.0	9.302	8.418	.708	7.200	1.051	.45	6.300	5 1/2			7/8	326.5	70.20	3.77	104.7	24.88	2.14	
84.0	9.456	8.469	.759	7.200	1.128	.45	6.300	5 1/2			7/8	358.6	75.85	3.81	114.5	27.04	2.15	
90.0	9.606	8.520	.810	7.200	1.203	.45	6.300	5 1/2			7/8	391.2	81.45	3.84	124.4	29.20	2.17	
9" CARNEGIE BEAM SECTIONS																		
29.0	9.000	6.500	.279	8.060	.470	.50	7.060	3 1/2			7/8	126.0	28.00	3.84	21.5	6.62	1.59	
32.0	9.096	6.528	.307	8.060	.518	.50	7.060	3 1/2			7/8	140.5	30.89	3.87	24.0	7.35	1.60	
35.0	9.192	6.556	.335	8.060	.566	.50	7.060	3 1/2			7/8	155.4	33.81	3.89	26.6	8.11	1.61	
38.0	9.000	9.000	.316	8.060	.470	.50	7.060	5 1/2			7/8	170.4	37.87	3.91	57.1	12.69	2.26	
43.0	9.122	9.041	.357	8.060	.531	.50	7.060	5 1/2			7/8	195.5	42.86	3.93	65.4	14.47	2.28	
48.0	9.242	9.082	.398	8.060	.591	.50	7.060	5 1/2			7/8	221.1	47.85	3.96	73.8	16.25	2.29	

I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

*CARNEGIE BEAM SECTIONS have flanges of uniform thickness throughout their width.



I_x is Moment of Inertia
 S_x is Section Modulus
 r_x is Radius of Gyration

8" & 9"

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 10" ROLLED COLUMNS

CARNegie
SECTIONS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																					
			8	10	12	13	14	15	16	17	18	19	20	22	24	26	28	30	32	34	36	38		
10" CARNEGIE BEAM SECTIONS																								
21	6.17	1.39	88	79	70	65	61	57	54	51	47	45	42	37										
23	6.76	1.43	97	87	78	73	69	65	61	57	54	50	47	42										
26	7.64	1.43	110	99	88	83	78	73	69	65	61	57	54	48	42									
30	8.82	1.45	128	115	103	97	91	86	80	76	71	69	63	56	50									
31	9.11	1.89	137	134	124	119	114	109	104	100	95	91	86	79	72	65	60	54						
36	10.58	1.80	159	153	140	134	128	122	117	111	106	101	96	87	79	71	65	59						
42	12.35	1.73	185	175	161	153	146	139	132	125	119	113	107	97	88	79	72							
49	14.40	2.54	216	216	216	214	209	203	197	191	185	179	173	162	151	141	131	123	114	107	99	93		
54	15.87	2.48	238	238	238	234	228	221	214	208	201	194	188	175	163	152	141	132	123	114	106	99		
59	17.34	2.42	260	260	260	254	246	239	231	224	216	209	202	188	175	162	151	140	130	121	113	105		
64	18.81	2.38	282	282	281	273	265	257	249	240	232	224	216	201	187	173	161	149	138	129	120	111		
70	20.59	2.55	309	309	309	307	299	290	282	273	265	257	248	232	217	202	189	176	164	153	143	133		
77	22.65	2.51	340	340	340	336	326	317	308	298	289	280	270	253	235	219	204	190	177	165	154	144		
84	24.70	2.48	371	371	371	364	354	344	334	323	313	303	292	273	254	237	220	205	191	178	166	154		
92	27.06	2.45	406	406	406	398	386	375	363	352	340	329	318	296	275	256	238	221	206	192	179	166		
100	29.40	3.16	441	441	441	441	441	441	439	430	420	410	401	381	362	343	325	307	291	275	260	245		
108	31.76	3.13	476	476	476	476	476	476	473	463	452	442	431	410	389	368	349	330	311	294	278	262		
116	34.11	3.11	512	512	512	512	512	512	507	496	484	473	461	438	416	394	372	352	332	314	296	280		
124	36.46	3.09	547	547	547	547	547	547	540	528	516	504	492	467	443	419	396	374	353	333	315	297		
132	38.81	3.09	582	582	582	582	582	582	575	562	549	536	523	497	472	446	422	398	376	355	335	316		
140	41.17	3.08	618	618	618	618	618	618	609	596	582	568	554	526	499	472	446	421	398	375	354	334		

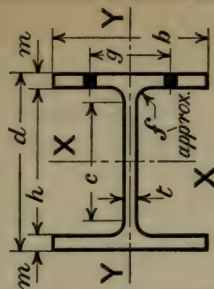
Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 10" ROLLED COLUMNS

CARNEGIE
SECTIONS

Weight per foot	DIMENSIONS						10" CARNEGIE BEAM SECTIONS						AXIS X-X			AXIS Y-Y		
	d	b	t	h	m	f	c	g	Riv.	I	S	r	I	S	r	I	S	r
21	9.902	6.000	.230	9.238	.332	.30	8.638	3"	3/4	107.6	21.7	4.18	12.0	4.0	1.39	12.0	4.0	1.39
23	10.000	6.000	.230	9.238	.381	.30	8.638	3"	3/4	122.2	24.4	4.25	13.7	4.6	1.43	13.7	4.6	1.43
26	10.098	6.029	.259	9.238	.430	.30	8.638	3"	3/4	139.5	27.6	4.27	15.7	5.2	1.43	15.7	5.2	1.43
30	10.228	6.068	.298	9.238	.495	.30	8.638	3"	3/4	163.2	31.9	4.30	18.5	6.1	1.45	18.5	6.1	1.45
31	10.000	8.000	.320	9.238	.381	.30	8.638	5 1/2	7/8	163.4	32.7	4.23	32.5	8.1	1.89	32.5	8.1	1.89
36	10.000	8.147	.467	9.238	.381	.30	8.638	5 1/2	7/8	175.6	35.1	4.07	34.4	8.5	1.80	34.4	8.5	1.80
42	10.000	8.324	.644	9.238	.381	.30	8.638	5 1/2	7/8	190.4	38.1	3.93	36.8	8.9	1.73	36.8	8.9	1.73
49	10.000	10.000	.350	8.884	.558	.45	7.984	5 1/2	7/8	272.0	54.4	4.35	93.0	18.6	2.54	93.0	18.6	2.54
54	10.000	10.147	.497	8.884	.558	.45	7.984	5 1/2	7/8	284.3	56.9	4.23	97.3	19.2	2.48	97.3	19.2	2.48
59	10.000	10.294	.644	8.884	.558	.45	7.984	5 1/2	7/8	296.5	59.3	4.13	101.7	19.8	2.42	101.7	19.8	2.42
64	10.000	10.441	.791	8.884	.558	.45	7.984	5 1/2	7/8	308.8	61.8	4.05	106.3	20.4	2.38	106.3	20.4	2.38
70	10.000	10.000	.515	8.390	.805	.50	7.390	5 1/2	7/8	369.3	73.9	4.24	134.3	26.9	2.55	134.3	26.9	2.55
77	10.000	10.206	.721	8.390	.805	.50	7.390	5 1/2	7/8	386.5	77.3	4.13	142.9	28.0	2.51	142.9	28.0	2.51
84	10.000	10.411	.926	8.390	.805	.50	7.390	5 1/2	7/8	403.6	80.7	4.04	152.0	29.2	2.48	152.0	29.2	2.48
92	10.000	10.647	1.162	8.390	.805	.50	7.390	5 1/2	7/8	423.2	84.6	3.96	163.1	30.6	2.45	163.1	30.6	2.45
100	10.000	12.000	.600	7.968	1.016	.60	6.768	9"	1"	525.1	105.0	4.23	292.8	48.8	3.16	292.8	48.8	3.16
108	10.000	12.236	.836	7.968	1.016	.60	6.768	9"	1"	544.8	109.0	4.14	310.7	50.8	3.13	310.7	50.8	3.13
116	10.000	12.471	1.071	7.968	1.016	.60	6.768	9"	1"	564.3	112.9	4.07	329.4	52.8	3.11	329.4	52.8	3.11
124	10.000	12.706	1.306	7.968	1.016	.60	6.768	9"	1"	583.9	116.8	4.00	349.0	54.9	3.09	349.0	54.9	3.09
132	10.000	12.941	1.541	7.968	1.016	.60	6.768	9"	1"	603.5	120.7	3.94	369.6	57.1	3.09	369.6	57.1	3.09
140	10.000	13.177	1.777	7.968	1.016	.60	6.768	9"	1"	623.2	124.6	3.89	391.4	59.4	3.08	391.4	59.4	3.08



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

10"

ALLOWABLE CONCENTRIC LOAD IN KIPS FOR 12" ROLLED COLUMNS

**CARNEGIE
SECTIONS**

Weight per foot	Area Sq. In.	Least Radius Gyrat.	UNSUPPORTED LENGTH IN FEET																			
			8	10	12	14	15	16	17	18	19	20	22	24	26	28	30	32	34	36	38	40
12" CARNEGIE BEAM SECTIONS																						
25	7.34	1.37	104	93	82	72	67	63	59	55	52	49	43									
28	8.22	1.53	121	110	99	89	84	79	74	70	66	63	56	50								
32	9.40	1.54	139	127	114	102	96	91	86	81	76	72	64	57								
36	10.59	1.45	145	130	116	103	97	91	86	81	76	71	63	56								
40	11.76	1.55	157	143	129	115	109	103	97	92	87	82	73	65								
45	13.23	1.95	176	175	163	150	144	138	132	125	121	115	105	96	88	80	73	67				
50	14.69	1.97	198	197	184	170	163	156	149	143	137	131	119	109	99	91	83	77				
55	16.17	1.98	220	220	204	189	181	174	166	159	152	146	133	122	111	102	93	86				
60	17.65	2.24	243	243	237	222	214	207	199	192	185	178	164	152	140	129	120	111	102			
66	19.41	2.25	265	265	259	243	234	226	218	210	202	195	180	166	154	142	131	121	112	104		
70		2.26	291	291	285	267	258	249	241	232	223	215	199	184	170	157	145	134	124	115		
76	19.11	3.03	287	287	287	287	287	281	275	268	262	255	242	229	216	204	193	182	171	162	152	144
82	20.58	2.96	309	309	309	309	307	300	293	286	279	271	257	243	229	216	204	191	180	170	160	151
88	22.35	2.90	332	332	332	332	331	324	316	308	299	291	275	260	245	230	217	204	192	180	169	160
95	24.11	3.09	362	362	362	362	362	357	349	341	333	325	309	293	277	262	247	234	220	208	196	185
102	25.88	3.04	388	388	388	388	388	381	373	364	355	346	328	311	294	278	262	247	233	220	207	195
110	27.93	2.99	419	419	419	419	418	409	399	390	380	370	351	332	313	295	278	262	247	233	219	207
120	32.34	3.10	485	485	485	485	485	480	469	458	448	437	415	393	373	352	333	314	297	280	264	250
130	38.24	3.06	529	529	529	529	529	521	509	497	485	473	449	426	403	380	359	339	319	301	284	268
140	41.18	3.03	574	574	574	574	574	563	550	537	524	510	484	458	433	409	386	364	343	323	305	287
150	44.12	3.01	618	618	618	618	618	605	591	576	562	548	519	491	464	438	413	389	367	346	326	307
160	47.06	3.69	662	662	662	662	662	662	662	662	655	643	618	593	568	544	519	496	471	451	430	409
170	50.00	3.67	706	706	706	706	706	706	706	706	698	684	658	631	604	578	552	527	502	479	456	434
180	52.94	3.65	750	750	750	750	750	750	750	750	740	726	697	669	640	612	584	557	531	506	482	459
190	55.88	3.64	794	794	794	794	794	794	794	794	782	768	737	707	677	647	617	589	561	535	509	485
200	58.82	3.71	838	838	838	838	838	838	838	838	831	816	785	754	722	691	660	631	602	574	547	521
210	61.76	3.71	882	882	882	882	882	882	882	882	882	875	859	826	793	760	727	695	664	633	604	576
220	64.70	3.72	926	926	926	926	926	926	926	926	926	920	903	869	834	799	765	731	698	666	636	606
230	67.64	3.73	971	971	971	971	971	971	971	971	971	964	947	911	875	839	803	767	733	700	667	636
240	70.64	3.74	1015	1015	1015	1015	1015	1015	1015	1015	1015	1009	991	954	916	878	841	804	768	733	699	667

Loads to right of heavy vertical lines are for Secondary Members ONLY.

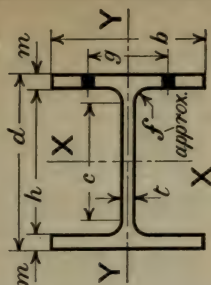
† Special Section. Web Thickness 3/8".

LOADS BY A. I. S. C. SPECIFICATION

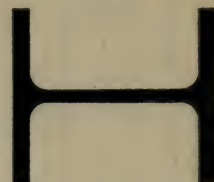
DIMENSIONS AND FUNCTIONS OF 12" ROLLED COLUMNS

CARNEGIE
SECTIONS

12"



I_x is Moment of Inertia
 S_x is Section Modulus
 r_x is Radius of Gyration



Weight per foot		DIMENSIONS										AXIS X-X					AXIS Y-Y				
		d	b	t	h	m	f	c	g	Riv.	I	S	r	I	S	r					
12" CARNEGIE BEAM SECTIONS																					
25	11.924	6.000	.240	11.160	0.382	.35	10.460	3"	3/4	183.0	30.7	4.99	13.8	4.6	1.37						
28	12.000	6.500	.240	11.160	.420	.35	10.460	3"	3/4	213.4	35.6	5.10	19.2	5.3	1.53						
32	12.118	6.534	.274	11.160	.479	.35	10.460	3"	3/4	246.3	40.7	5.12	22.3	6.8	1.54						
34	12.022	6.635	.375	11.160	.431	.35	10.460	3"	3/4	238.1	39.6	4.88	21.0	6.3	1.45						
36	12.236	6.368	.308	11.160	.538	.35	10.460	3"	3/4	280.1	45.8	5.14	25.4	7.7	1.55						
40	12.000	8.000	.290	10.948	.526	.50	9.948	5 1/2	7/8	313.7	52.3	5.17	44.9	11.2	1.95						
43	12.130	8.036	.326	10.948	.591	.50	9.948	5 1/2	7/8	356.9	58.8	5.19	51.2	12.7	1.97						
50	12.258	8.071	.361	10.948	.655	.50	9.948	5 1/2	7/8	400.5	65.4	5.22	57.5	14.2	1.98						
55	12.000	9.000	.375	10.670	.665	.55	9.570	5 1/2	7/8	428.4	71.4	5.15	80.9	18.0	2.24						
60	12.118	9.034	.409	10.670	.724	.55	9.570	5 1/2	7/8	472.0	77.9	5.17	89.0	19.7	2.25						
66	12.260	9.073	.448	10.670	.795	.55	9.570	5 1/2	7/8	525.7	85.8	5.20	99.1	21.8	2.26						
65	12.000	12.000	.400	10.784	.608	.55	9.684	9"	1"	521.3	86.9	5.22	175.2	29.2	3.03						
70	12.000	12.123	.523	10.784	.608	.55	9.684	9"	1"	539.0	89.8	5.12	180.7	29.8	2.96						
76	12.000	12.270	.670	10.784	.608	.55	9.684	9"	1"	560.2	93.4	5.01	187.5	30.6	2.90						
82	12.000	12.000	.453	10.400	.800	.55	9.300	9"	1"	650.8	108.5	5.20	230.5	38.4	3.09						
88	12.000	12.147	.600	10.400	.800	.55	9.300	9"	1"	672.0	112.0	5.10	239.2	39.4	3.04						
95	12.000	12.318	.771	10.400	.800	.55	9.300	9"	1"	696.6	116.1	4.99	249.7	40.5	2.99						
102	12.000	12.490	.943	10.400	.800	.55	9.300	9"	1"	721.4	120.2	4.90	260.6	41.7	2.95						
110	12.000	12.000	.640	9.850	1.075	.60	8.650	9"	1"	828.8	138.1	5.06	309.9	51.6	3.10						
120	12.000	12.245	.885	9.850	1.075	.60	8.650	9"	1"	864.1	144.0	4.95	329.6	53.8	3.06						
130	12.000	12.491	1.131	9.850	1.075	.60	8.650	9"	1"	899.5	149.9	4.85	350.5	56.1	3.03						
140	12.000	12.736	1.376	9.850	1.075	.60	8.650	9"	1"	934.8	155.8	4.76	372.4	58.5	3.01						
150	12.000	14.000	.757	9.376	1.312	.65	8.076	10"	1"	1112.2	185.4	5.02	600.4	85.8	3.69						
160	12.000	14.245	1.002	9.376	1.312	.65	8.076	10"	1"	1147.5	191.3	4.94	633.0	88.9	3.67						
170	12.000	14.490	1.247	9.376	1.312	.65	8.076	10"	1"	1182.8	197.1	4.86	666.9	92.1	3.65						
180	12.000	14.735	1.492	9.376	1.312	.65	8.076	10"	1"	1218.1	203.0	4.80	702.4	95.3	3.64						
190	12.000	14.980	1.000	8.646	1.677	.65	7.346	10"	1"	1320.8	220.1	4.86	767.8	109.7	3.71						
200	12.000	14.245	1.245	8.646	1.677	.65	7.346	10"	1"	1356.1	226.0	4.80	809.5	113.7	3.71						
210	12.000	14.490	1.490	8.646	1.677	.65	7.346	10"	1"	1391.3	231.9	4.75	852.9	117.7	3.72						
220	12.000	14.735	1.735	8.646	1.677	.65	7.346	10"	1"	1426.6	237.8	4.70	898.2	121.9	3.73						
230	12.000	14.980	1.980	8.646	1.677	.65	7.346	10"	1"	1461.9	243.7	4.65	945.5	126.2	3.74						

† Special Section, Web Thickness 3/4"

ALLOWABLE CONCENTRIC LOAD IN KIPS FOR 14" ROLLED COLUMNS

CARNEGIE SECTIONS

Weight per foot	Area Sq. In.	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET																14" CARNEGIE BEAM SECTIONS															
			8	10	12	14	15	16	17	18	19	20	22	24	26	28	30	32	34	36	38	40												
30	8.82	1.33	123	109	96	84	79	74	69	64	60	57	50	59																				
33	9.71	1.54	144	131	118	105	99	94	88	84	79	74	66	65																				
36	10.58	1.55	157	143	129	115	109	103	97	92	86	82	73	65																				
† 38	11.18	1.47	163	147	131	117	110	113	106	100	94	89	80	71	64	64																		
39	11.47	1.56	171	155	140	126	119	112	106	100	94	89	80	71																				
42	12.35	1.56	184	167	151	135	128	121	114	108	102	96	86	77	69																			
48	14.12	1.91	212	200	193	177	170	162	155	148	141	135	123	112	102	93	85																	
53	15.59	1.91	234	230	213	196	188	180	172	164	157	149	136	124	113	103	94																	
58	17.05	1.92	256	252	234	215	206	197	189	180	172	164	150	136	124	114	104	95																
61	17.94	2.44	269	269	269	256	248	240	233	225	217	210	196	182	169	157	146	136	126															
68	19.99	2.46	300	300	300	286	277	269	260	252	244	235	219	204	190	177	164	153	142															
75	22.05	2.47	331	331	331	316	306	297	288	279	269	260	243	226	210	196	182	169	158															
85	24.99	3.05	375	375	375	375	375	369	360	352	343	335	318	301	284	269	254	239	226															
95	27.93	3.06	419	419	419	419	419	413	403	394	384	375	356	337	319	301	284	268	253															
105	30.88	3.08	463	463	463	463	463	457	447	437	426	416	395	374	354	335	316	298	281															
86	25.28	3.84	379	379	379	379	379	379	379	379	379	374	360	347	333	319	306	293	280	267	255	244												
96	28.23	3.86	423	423	423	423	423	423	423	423	423	418	403	388	373	358	343	328	314	300	286	273												
106	31.18	3.87	468	468	468	468	468	468	468	468	468	463	446	430	412	396	379	363	347	332	317	303												
115	33.82	3.89	507	507	507	507	507	507	507	507	507	502	485	467	448	430	413	395	378	361	345	330												
125	36.75	3.90	551	551	551	551	551	551	551	551	551	547	527	508	488	468	449	430	411	393	376	359												
† 131	38.52	3.77	578	578	578	578	578	578	578	578	576	566	545	524	502	481	460	440	420	401	382	365												
135	39.70	3.92	596	596	596	596	596	596	596	596	596	591	570	549	528	507	486	466	446	426	407	389												
145	42.64	3.93	640	640	640	640	640	640	640	640	640	636	614	591	568	546	523	502	480	459	439	420												
155	45.58	3.94	684	684	684	684	684	684	684	684	684	680	657	633	608	584	560	537	514	492	470	450												
165	48.52	3.96	728	728	728	728	728	728	728	728	728	725	700	675	649	624	599	574	549	526	503	481												
175	51.47	3.97	772	772	772	772	772	772	772	772	772	770	744	717	690	663	636	610	584	559	535	511												
185	54.41	3.98	816	816	816	816	816	816	816	816	816	815	787	759	731	702	674	646	619	593	567	542												
195	57.34	4.00	860	860	860	860	860	860	860	860	860	858	831	801	771	741	712	683	654	626	599	573												
205	60.28	4.01	904	904	904	904	904	904	904	904	904	904	874	843	812	781	749	719	689	660	631	604												
215	63.23	4.03	949	949	949	949	949	949	949	949	949	949	919	886	853	821	788	756	725	694	664	636												
225	66.17	4.04	993	993	993	993	993	993	993	993	993	993	963	929	895	860	826	793	760	728	697	668												
235	69.11	4.05	1037	1037	1037	1037	1037	1037	1037	1037	1037	1037	1006	971	936	900	864	830	795	762	730	699												
245	72.06	4.06	1081	1081	1081	1081	1081	1081	1081	1081	1081	1081	1051	1014	977	940	903	867	832	797	763	731												
255	74.99	4.08	1125	1125	1125	1125	1125	1125	1125	1125	1125	1125	1095	1057	1019	980	942	905	868	832	797	763												
265	77.93	4.09	1169	1169	1169	1169	1169	1169	1169	1169	1169	1169	1139	1100	1060	1020	981	942	903	866	830	795												
NOTE: For the convenience of the designer beams from 68 lb. to 265 lb. per foot are duplicated on the following page in conjunction with those from 275 lb. to 425 lb. per foot. Loads to right of heavy vertical lines are for Secondary Members ONLY. † Special Section: Web Thickness 3/8". ‡ Special Section for Column use.																																		

NOTE: For the convenience of the designer beams from 68 lb. to 265 lb. per foot are duplicated on the following page in conjunction with those from 275 lb. to 425 lb. per foot.

Loads to right of heavy vertical lines are for Secondary Members ONLY.

† Special Section; Web Thickness $\frac{3}{8}$ ".

‡ Special Section for Column Core.

DIMENSIONS AND FUNCTIONS OF 14" ROLLED COLUMNS

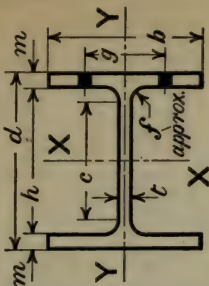
CARNegie
SECTIONS

DIMENSIONS

AXIS X - X

AXIS Y - Y

14" CARNegie BEAM SECTIONS



Weight per foot	d	b	t	h	m	f	c	g	Riv.	I	S	r	I	S	r
30	13.964	6.000	.270	13.102	.431	.40	12.302	3"	3/4	292.0	41.8	5.75	15.5	5.2	1.33
33	14.000	6.750	.270	13.102	.449	.40	12.302	3"	3/4	333.4	47.6	5.86	23.0	6.8	1.54
36	14.080	6.774	.294	13.102	.489	.40	12.302	3"	3/4	365.6	51.9	5.88	25.4	7.5	1.55
38	14.000	6.855	.375	13.102	.449	.40	12.302	3"	3/4	357.5	51.1	5.66	24.2	7.1	1.47
39	14.160	6.798	.318	13.102	.529	.40	12.302	3"	3/4	398.3	56.3	5.89	27.7	8.2	1.56
42	14.240	6.822	.342	13.102	.569	.40	12.302	3"	3/4	431.5	60.6	5.91	30.2	8.8	1.56
48	14.000	8.000	.343	12.810	.595	.55	11.710	5 1/2"	7/8	496.0	70.9	5.93	50.8	12.7	1.90
53	14.122	8.035	.378	12.810	.656	.55	11.710	5 1/2"	7/8	552.5	78.2	5.95	56.8	14.1	1.91
58	14.242	8.070	.413	12.810	.716	.55	11.710	5 1/2"	1"	609.4	85.6	5.98	62.8	15.6	1.92
61	14.094	10.000	.382	12.810	.642	.55	11.710	5 1/2"	1"	656.2	93.1	6.03	107.1	21.4	2.44
68	14.238	10.043	.425	12.810	.716	.55	11.710	5 1/2"	1"	738.8	103.8	6.08	120.6	24.0	2.46
75	14.382	10.086	.468	12.810	.784	.55	11.710	5 1/2"	1"	823.5	114.5	6.11	134.5	26.7	2.47
82	14.000	12.000	.435	12.300	.805	.65	11.090	9"	1"	921.3	131.6	6.07	232.0	38.7	3.05
95	14.186	12.050	.483	12.300	.898	.65	11.090	9"	1"	1044.0	147.2	6.11	262.0	43.5	3.06
105	14.370	12.101	.536	12.300	.990	.65	11.090	9"	1"	1169.6	162.8	6.15	292.6	48.4	3.08
86	13.714	15.008	.414	12.300	.662	.65	11.090	10"	1"	923.0	136.6	6.04	373.1	49.7	3.84
96	13.866	15.056	.462	12.300	.738	.65	11.090	10"	1"	1042.1	150.3	6.08	419.9	55.8	3.86
106	14.018	15.103	.509	12.300	.814	.65	11.090	10"	1"	1164.1	166.1	6.11	467.6	61.9	3.87
115	14.154	15.145	.551	12.300	.882	.65	11.090	10"	1"	1275.9	180.3	6.14	510.9	67.5	3.89
125	14.304	15.191	.597	12.300	.957	.65	11.090	10"	1"	1402.1	196.0	6.18	559.4	73.7	3.90
†131	14.162	15.468	.874	12.300	.886	.65	11.090	10"	1"	1358.4	191.8	5.94	547.3	70.8	3.77
135	14.452	15.239	.645	12.300	1.031	.65	11.090	10"	1"	1530.4	211.8	6.21	608.4	79.9	3.92
145	14.602	15.284	.690	12.300	1.106	.65	11.090	10"	1"	1662.7	227.7	6.24	658.5	86.2	3.93
155	14.750	15.330	.736	12.300	1.180	.65	11.090	10"	1"	1796.8	243.6	6.28	709.9	92.5	3.94
165	14.896	15.377	.783	12.300	1.253	.65	11.090	10"	1"	1932.6	259.5	6.31	759.9	98.8	3.96
175	15.042	15.424	.830	12.300	1.326	.65	11.090	10"	1"	2071.7	275.5	6.34	811.6	105.2	3.97
185	15.188	15.469	.875	12.300	1.399	.65	11.090	10"	1"	2213.5	291.5	6.38	863.9	111.7	3.98
195	15.334	15.513	.919	12.300	1.472	.65	11.090	10"	1"	2358.2	307.6	6.41	916.8	118.2	4.00
205	15.478	15.559	.965	12.300	1.544	.65	11.090	10"	1"	2505.0	323.7	6.45	970.3	124.7	4.01
215	15.622	15.604	1.010	12.300	1.616	.65	11.090	10"	1"	2654.7	339.9	6.48	1024.5	131.3	4.03
225	15.764	15.650	1.056	12.300	1.687	.65	11.090	10"	1"	2806.2	356.0	6.51	1079.1	137.9	4.04
235	15.908	15.693	1.099	12.300	1.759	.65	11.090	10"	1"	2961.9	372.4	6.55	1134.5	144.6	4.05
245	16.050	15.738	1.144	12.300	1.830	.65	11.090	10"	1"	3119.6	388.7	6.58	1190.6	151.3	4.06
255	16.192	15.781	1.187	12.300	1.901	.65	11.090	10"	1"	3280.0	405.1	6.61	1247.1	158.0	4.08
265	16.332	15.826	1.232	12.300	1.971	.65	11.090	10"	1"	3442.4	421.6	6.65	1304.2	164.8	4.09

NOTE: For the convenience of the designer beams from 68 lb. to 265 lb. per foot are duplicated on the following page in conjunction with those from 275 lb. to 425 lb. per foot.

† Special Section Web Thickness 3/8"
‡ Special Section for Column core

14"



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

DIMENSIONS AND FUNCTIONS OF 14" ROLLED COLUMNS

CARNEGIE
SECTIONS

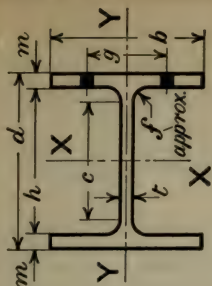
DIMENSIONS															AXIS X-X					AXIS Y-Y						
Weight per foot	14" CARNEGIE BEAM SECTIONS														I	S	r	I	S	r	I	S	r			
	d	b	t	h	m	f	c	g	Riv.	I	S	r	I	S	r	I	S	r	I	S	r	I	S	r		
68	14.238	10.043	.425	12.810	.714	.55	11.710	5½	1"	738.8	103.8	6.08	120.6	24.0	2.46	738.8	103.8	6.08	120.6	24.0	2.46	738.8	103.8	6.08	120.6	24.0
75	14.382	10.086	.468	12.810	.786	.55	11.710	5½	1"	823.5	114.5	6.11	134.5	26.7	2.47	823.5	114.5	6.11	134.5	26.7	2.47	823.5	114.5	6.11	134.5	26.7
85	14.000	12.000	.435	12.390	.805	.65	11.090	9"	1"	921.3	131.6	6.07	232.0	38.7	3.05	921.3	131.6	6.07	232.0	38.7	3.05	921.3	131.6	6.07	232.0	38.7
95	14.186	12.050	.485	12.390	.898	.65	11.090	9"	1"	1044.0	147.2	6.11	262.0	43.5	3.06	1044.0	147.2	6.11	262.0	43.5	3.06	1044.0	147.2	6.11	262.0	43.5
105	14.370	12.101	.536	12.390	.990	.65	11.090	9"	1"	1169.6	162.8	6.15	292.6	48.4	3.08	1169.6	162.8	6.15	292.6	48.4	3.08	1169.6	162.8	6.15	292.6	48.4
86	13.714	15.008	.414	12.390	.662	.65	11.090	10"	1"	923.0	136.6	6.04	373.1	49.7	3.84	923.0	136.6	6.04	373.1	49.7	3.84	923.0	136.6	6.04	373.1	49.7
96	13.866	15.056	.462	12.390	.738	.65	11.090	10"	1"	1042.1	150.3	6.08	419.9	55.8	3.86	1042.1	150.3	6.08	419.9	55.8	3.86	1042.1	150.3	6.08	419.9	55.8
106	14.018	15.103	.509	12.390	.814	.65	11.090	10"	1"	1164.1	166.1	6.11	467.6	61.9	3.87	1164.1	166.1	6.11	467.6	61.9	3.87	1164.1	166.1	6.11	467.6	61.9
115	14.154	15.145	.551	12.390	.882	.65	11.090	10"	1"	1275.9	180.3	6.14	510.9	67.5	3.89	1275.9	180.3	6.14	510.9	67.5	3.89	1275.9	180.3	6.14	510.9	67.5
125	14.304	15.191	.597	12.390	.957	.65	11.090	10"	1"	1402.1	196.0	6.18	559.4	73.7	3.90	1402.1	196.0	6.18	559.4	73.7	3.90	1402.1	196.0	6.18	559.4	73.7
131	14.162	15.468	.874	12.390	.886	.65	11.090	10"	1"	1358.4	191.8	5.94	547.3	70.8	3.77	1358.4	191.8	5.94	547.3	70.8	3.77	1358.4	191.8	5.94	547.3	70.8
135	14.452	15.239	.645	12.390	1.031	.65	11.090	10"	1"	1530.4	211.8	6.21	608.4	79.9	3.92	1530.4	211.8	6.21	608.4	79.9	3.92	1530.4	211.8	6.21	608.4	79.9
145	14.602	15.284	.690	12.390	1.106	.65	11.090	10"	1"	1662.7	227.7	6.24	658.5	86.2	3.93	1662.7	227.7	6.24	658.5	86.2	3.93	1662.7	227.7	6.24	658.5	86.2
155	14.750	15.330	.736	12.390	1.180	.65	11.090	10"	1"	1796.8	243.6	6.28	709.0	92.5	3.94	1796.8	243.6	6.28	709.0	92.5	3.94	1796.8	243.6	6.28	709.0	92.5
165	14.896	15.377	.783	12.390	1.253	.65	11.090	10"	1"	1932.6	259.5	6.31	759.9	98.8	3.96	1932.6	259.5	6.31	759.9	98.8	3.96	1932.6	259.5	6.31	759.9	98.8
175	15.042	15.424	.830	12.390	1.326	.65	11.090	10"	1"	2071.7	275.5	6.34	811.6	105.2	3.97	2071.7	275.5	6.34	811.6	105.2	3.97	2071.7	275.5	6.34	811.6	105.2
185	15.188	15.469	.875	12.390	1.399	.65	11.090	10"	1"	2213.5	291.5	6.38	863.9	111.7	3.98	2213.5	291.5	6.38	863.9	111.7	3.98	2213.5	291.5	6.38	863.9	111.7
195	15.334	15.513	.919	12.390	1.472	.65	11.090	10"	1"	2358.2	307.6	6.41	916.8	118.2	4.00	2358.2	307.6	6.41	916.8	118.2	4.00	2358.2	307.6	6.41	916.8	118.2
205	15.478	15.559	.965	12.390	1.544	.65	11.090	10"	1"	2505.0	323.7	6.45	970.3	124.7	4.01	2505.0	323.7	6.45	970.3	124.7	4.01	2505.0	323.7	6.45	970.3	124.7
215	15.622	15.604	1.010	12.390	1.616	.65	11.090	10"	1"	2654.7	339.9	6.48	1024.5	131.3	4.03	2654.7	339.9	6.48	1024.5	131.3	4.03	2654.7	339.9	6.48	1024.5	131.3
225	15.764	15.650	1.056	12.390	1.687	.65	11.090	10"	1"	2806.2	356.0	6.51	1079.1	137.9	4.04	2806.2	356.0	6.51	1079.1	137.9	4.04	2806.2	356.0	6.51	1079.1	137.9
235	15.908	15.693	1.099	12.390	1.759	.65	11.090	10"	1"	2961.9	372.4	6.55	1134.5	144.6	4.05	2961.9	372.4	6.55	1134.5	144.6	4.05	2961.9	372.4	6.55	1134.5	144.6
245	16.050	15.738	1.144	12.390	1.830	.65	11.090	10"	1"	3119.6	388.7	6.58	1190.6	151.3	4.06	3119.6	388.7	6.58	1190.6	151.3	4.06	3119.6	388.7	6.58	1190.6	151.3
255	16.192	15.781	1.187	12.390	1.901	.65	11.090	10"	1"	3280.0	405.1	6.61	1247.1	158.0	4.08	3280.0	405.1	6.61	1247.1	158.0	4.08	3280.0	405.1	6.61	1247.1	158.0
265	16.332	15.826	1.232	12.390	1.971	.65	11.090	10"	1"	3442.4	421.6	6.65	1304.2	164.8	4.09	3442.4	421.6	6.65	1304.2	164.8	4.09	3442.4	421.6	6.65	1304.2	164.8
275	16.472	15.870	1.276	12.390	2.041	.65	11.090	10"	1"	3607.8	438.1	6.68	1362.0	171.6	4.10	3607.8	438.1	6.68	1362.0	171.6	4.10	3607.8	438.1	6.68	1362.0	171.6
285	16.614	15.912	1.318	12.390	2.112	.65	11.090	10"	1"	3778.1	454.8	6.71	1420.7	178.6	4.12	3778.1	454.8	6.71	1420.7	178.6	4.12	3778.1	454.8	6.71	1420.7	178.6
295	16.752	15.956	1.362	12.390	2.181	.65	11.090	10"	1"	3948.1	471.4	6.75	1479.4	185.4	4.13	3948.1	471.4	6.75	1479.4	185.4	4.13	3948.1	471.4	6.75	1479.4	185.4
305	16.890	16.000	1.406	12.390	2.250	.65	11.090	10"	1"	4121.5	488.0	6.78	1539.1	192.4	4.14	4121.5	488.0	6.78	1539.1	192.4	4.14	4121.5	488.0	6.78	1539.1	192.4
325	17.104	16.087	1.493	12.390	2.387	.65	11.090	10"	1"	4475.9	521.6	6.84	1659.9	206.4	4.17	4475.9	521.6	6.84	1659.9	206.4	4.17	4475.9	521.6	6.84	1659.9	206.4
345	17.438	16.172	1.578	12.390	2.524	.65	11.090	10"	1"	4843.4	555.5	6.91	1783.5	220.6	4.19	4843.4	555.5	6.91	1783.5	220.6	4.19	4843.4	555.5	6.91	1783.5	220.6
365	17.710	16.255	1.661	12.390	2.660	.65	11.090	10"	1"	5221.4	589.7	6.97	1909.1	234.9	4.22	5221.4	589.7	6.97	1909.1	234.9	4.22	5221.4	589.7	6.97	1909.1	234.9
385	17.978	16.340	1.746	12.390	2.794	.65	11.090	10"	1"	5609.4	624.0	7.04	2037.4	249.4	4.24	5609.4	624.0	7.04	2037.4	249.4	4.24	5609.4	624.0	7.04	2037.4	249.4
405	18.246	16.423	1.829	12.390	2.928	.65	11.090	10"	1"	6010.5	658.8	7.10	2168.2	264.0	4.27	6010.5	658.8	7.10	2168.2	264.0	4.27	6010.5	658.8	7.10	2168.2	264.0
425	18.510	16.506	1.912	12.390	3.060	.65	11.090	10"	1"	6420.5	693.7	7.17	2301.0	278.8	4.29	6420.5	693.7	7.17	2301.0	278.8	4.29	6420.5	693.7	7.17	2301.0	278.8

I. is Moment of Inertia
 S. is Section Modulus
 r. is Radius of Gyration

14"

NOTE: For the convenience of the designer beams from 68 lb. to 265 lb. per foot are duplicated on the preceding page in conjunction with those from 30 lb. to 61 lb. per foot.

† Special Section for Column core



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration

14"

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14" CARNEGIE COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per Foot	Area Sq. Inches	Least Radius Gyration	UNSUPPORTED LENGTH IN FEET															
				20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50
14" × 131# CARNEGIE BEAM SECTION																			
16 × 3/16	171.8	50.5	3.99	757	731	705	679	652	626	600	575	551	527	504	482	461	441	421	403
16 × 7/16	178.6	52.5	4.01	788	762	735	707	680	653	626	600	575	550	526	504	482	461	440	421
16 × 1/2	185.4	54.5	4.04	818	793	765	737	709	681	653	626	600	575	550	526	504	482	461	441
16 × 9/16	192.2	56.5	4.06	848	824	795	766	737	708	680	652	625	598	573	548	525	502	480	460
16 × 5/8	199.0	58.5	4.08	878	855	825	795	765	735	706	677	649	622	596	570	546	522	500	478
16 × 11/16	205.8	60.5	4.10	908	885	855	824	793	763	732	703	674	646	618	592	567	543	520	497
16 × 3/4	212.6	62.5	4.12	938	916	885	853	822	790	759	728	699	670	642	615	588	563	539	517
16 × 13/16	219.4	64.5	4.13	968	947	914	882	849	817	785	753	722	692	663	636	609	583	558	535
16 × 7/8	226.2	66.5	4.15	998	978	945	911	878	844	811	779	747	717	687	658	630	604	578	554
16 × 1 1/8	233.0	68.5	4.16	1028	1008	974	940	905	871	837	804	771	740	709	679	651	623	597	572
16 × 1 1/4	239.8	70.5	4.18	1058	1039	1004	969	934	899	864	830	797	764	733	702	673	645	618	592
16 × 1 1/2	246.6	72.5	4.19	1088	1069	1034	998	962	926	890	855	821	787	755	724	694	665	637	610
16 × 1 3/8	253.4	74.5	4.20	1118	1100	1064	1027	990	953	916	880	845	811	777	745	714	684	656	629
16 × 1 1/2	260.2	76.5	4.21	1148	1130	1093	1055	1017	979	942	905	869	834	800	767	735	705	675	647
16 × 1 5/8	267.0	78.5	4.22	1178	1161	1123	1084	1045	1006	968	930	893	857	822	788	756	725	695	666
16 × 1 3/4	273.8	80.5	4.23	1208	1192	1153	1113	1073	1033	994	956	918	881	845	810	777	745	714	684
16 × 1 7/8	280.6	82.5	4.24	1238	1222	1182	1142	1101	1061	1020	981	942	904	868	832	798	765	733	703
16 × 1 9/8	287.4	84.5	4.25	1268	1253	1212	1171	1129	1088	1047	1006	967	928	890	854	819	785	753	722
16 × 1 1/2	294.2	86.5	4.26	1298	1284	1242	1200	1157	1115	1073	1032	991	952	913	876	840	806	773	741
16 × 1 5/8	301.0	88.5	4.27	1328	1314	1272	1229	1186	1142	1099	1057	1016	975	936	898	862	826	792	760
16 × 1 3/4	307.8	90.5	4.28	1358	1345	1302	1258	1214	1170	1126	1083	1040	999	959	920	883	847	812	779
16 × 1 7/8	314.6	92.5	4.29	1388	1376	1332	1287	1242	1197	1152	1108	1065	1023	982	943	904	867	832	798
16 × 1 9/8	321.4	94.5	4.29	1418	1406	1361	1315	1269	1223	1177	1132	1088	1045	1003	963	924	886	850	815
16 × 1 3/4	328.2	96.5	4.30	1448	1437	1391	1344	1297	1250	1204	1158	1113	1069	1027	985	945	907	870	835
16 × 1 7/8	335.0	98.5	4.31	1478	1467	1421	1373	1326	1278	1231	1184	1135	1093	1050	1008	967	928	890	854
16 × 1 9/8	341.8	100.5	4.31	1508	1497	1450	1401	1353	1304	1256	1208	1161	1116	1071	1028	987	947	908	871
16 × 1 3/4	348.6	102.5	4.32	1538	1528	1480	1431	1381	1332	1282	1234	1186	1140	1095	1051	1008	968	928	891
14" × 225# CARNEGIE BEAM SECTION																			
22 × 1 7/16	440.0	129.4	5.30	1941	1941	1941	1941	1904	1854	1804	1753	1701	1651	1600	1551	1502	1454	1407	1361
22 × 1 9/16	458.7	134.9	5.34	2024	2024	2024	2024	1991	1939	1887	1834	1781	1728	1676	1625	1574	1524	1475	1427
22 × 1 1/2	477.4	140.4	5.39	2106	2106	2106	2106	2070	2026	1972	1917	1863	1808	1755	1701	1649	1597	1546	1497
22 × 1 3/4	496.1	145.9	5.43	2189	2189	2189	2189	2166	2111	2055	1999	1943	1887	1831	1776	1722	1669	1616	1565
22 × 1 5/8	514.8	151.4	5.46	2271	2271	2271	2271	2252	2195	2138	2080	2022	1964	1907	1850	1794	1738	1684	1631
14" × 325# CARNEGIE BEAM SECTION																			
17 × 1"	440.6	129.6	4.37	1944	1939	1879	1818	1756	1694	1632	1571	1512	1453	1396	1341	1288	1236	1187	1139
17 × 1 3/16	462.2	136.0	4.40	2039	2039	1977	1913	1848	1784	1719	1656	1594	1533	1473	1415	1360	1306	1254	1204
17 × 1 1/2	483.9	142.3	4.42	2135	2135	2073	2007	1939	1872	1805	1737	1674	1610	1548	1487	1429	1373	1318	1266
17 × 1 3/4	505.6	148.7	4.45	2231	2231	2171	2102	2033	1963	1893	1825	1757	1690	1626	1563	1502	1443	1386	1332
17 × 1 5/8	527.3	155.1	4.47	2326	2326	2268	2197	2125	2052	1980	1908	1838	1767	1702	1636	1573	1511	1452	1395
17 × 1 3/4	548.9	161.5	4.48	2422	2422	2363	2289	2214	2139	2064	1989	1916	1844	1774	1706	1640	1576	1515	1456

Loads to right of heavy vertical lines are for Secondary Members ONLY.

Loads to right of heavy vertical lines are for Secondary Members ONLY.


LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 14" CARNEGIE COLUMNS WITH COVER PLATES

2 Cover Plates	Weight per Foot	DIMENSIONS										AXIS X - X				AXIS Y - Y			
		d	b	t	a	h	m	c	g	Riv.	I	S	r	I	S	r			
14" x 131# CARNEGIE BEAM SECTION																			
16 x 3/4 7/8 1 1/8 1 1/4 1 1/2 1 3/4 1 7/8 2	171.8	14 1/2	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	1993	267	6.28	803	100	3.99			
	178.6	15 1/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2105	280	6.33	846	106	4.01			
	185.4	15 3/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2219	293	6.38	889	111	4.04			
	192.2	15 5/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2335	305	6.43	931	116	4.06			
16 x 5/8 1 1/8 1 1/4 1 1/2 1 3/4 1 7/8 2	199.0	15 7/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2452	318	6.47	974	122	4.08			
	205.8	15 9/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2572	331	6.52	1017	127	4.10			
	212.6	15 11/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2694	344	6.56	1059	132	4.12			
	219.4	15 13/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2817	357	6.61	1102	138	4.13			
16 x 7/8 1 1/8 1 1/4 1 1/2 1 3/4 1 7/8 2	226.2	15 15/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	2943	370	6.65	1145	143	4.15			
	233.0	16 1/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3071	383	6.69	1187	148	4.16			
	239.8	16 3/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3200	396	6.74	1230	154	4.18			
	246.6	16 5/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3332	409	6.78	1273	159	4.19			
16 x 1 1/8 1 1/4 1 1/2 1 3/4 1 7/8 2	253.4	16 7/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3465	422	6.82	1315	164	4.20			
	260.2	16 9/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3601	436	6.86	1358	170	4.21			
	267.0	16 11/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3739	449	6.90	1401	175	4.22			
	273.8	16 13/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	3879	462	6.94	1443	180	4.23			
16 x 1 3/8 1 1/2 1 3/4 1 7/8 2	280.6	16 15/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4021	475	6.98	1486	186	4.24			
	287.4	17 1/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4165	489	7.02	1529	191	4.25			
	294.2	17 3/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4311	502	7.06	1571	196	4.26			
	301.0	17 5/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4459	516	7.10	1614	202	4.27			
16 x 1 7/8 2	307.8	17 7/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4610	530	7.14	1657	207	4.28			
	314.6	17 9/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4763	543	7.17	1699	212	4.29			
	321.4	17 11/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	4917	557	7.21	1742	218	4.30			
	328.2	17 13/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	5074	571	7.25	1785	223	4.31			
16 x 1 9/8 2	335.0	17 15/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	5234	584	7.29	1827	228	4.31			
	341.8	18 1/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	5395	598	7.33	1870	234	4.32			
	348.6	18 3/8	15 4/8	874	14 1/2	12.39	886	11.09	10"	1"	5559	612	7.36	1913	239	4.33			

I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

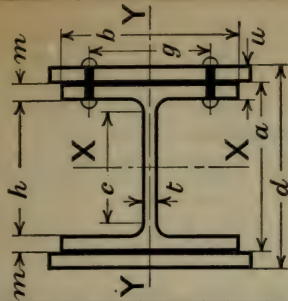
14" x 225# CARNEGIE BEAM SECTION

																			
22 x 1 7/16	440.0	DIMENSIONS										AXIS X - X				AXIS Y - Y			
		d	b	t	a	h	m	c	g	Riv.	I	S	r	I	S	r			
22 x 1 7/16	440.0	18 11/8	15 6/8	1056	15 7/4	12.39	1687	11.09	10"	1"	7496	804	7.61	3630	330	5.30			
22 x 1 9/16	458.7	18 5/8	15 6/8	1056	15 7/4	12.39	1687	11.09	10"	1"	7980	845	7.69	3852	350	5.34			
22 x 1 3/4	477.4	19 3/8	15 6/8	1056	15 7/4	12.39	1687	11.09	10"	1"	8477	886	7.77	4074	370	5.39			
22 x 1 13/16	496.1	19 7/8	15 6/8	1056	15 7/4	12.39	1687	11.09	10"	1"	8987	927	7.85	4296	391	5.43			
22 x 1 5/8	514.8	19 11/8	15 6/8	1056	15 7/4	12.39	1687	11.09	10"	1"	9511	969	7.93	4517	411	5.46			

14" x 325# CARNEGIE BEAM SECTION

4

17 ×	440.6	19 3/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	7283	AXIS X - X				AXIS Y - Y			
												I	S	r	I	S	r	I	S
17 × 1 3/8	462.2	19 5/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	7880	807	7.61	2632	310	4.40			
17 × 1 3/4	483.9	19 9/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	8500	854	7.73	2786	328	4.42			
17 × 1 13/16	505.6	20 5/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	9144	901	7.84	2939	346	4.45			
17 × 1 5/8	527.3	20 9/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	9813	950	7.95	3093	364	4.47			
17 × 1 11/8	548.9	21 1/8	16 0/8	1.493	17 1/4	12.39	2.387	11 09	10"	1"	10505	999	8.07	3246	382	4.48			



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

14"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14" CARNEGIE COLUMNS WITH COVER PLATES

UNSUPPORTED LENGTH IN FEET

2 Cover Plates	Weight Per Foot	Area Sq. Inches	Least Radius Gyrations	UNSUPPORTED LENGTH IN FEET															
				20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50
				14" × 325# CARNEGIE BEAM SECTION															
18 × 2 1/2" 2 3/16	569.8	167.6	4.64	2514	2514	2485	2411	2336	2260	2185	2110	2036	1963	1892	1822	1754	1689	1625	1564
	592.7	174.3	4.66	2615	2615	2589	2512	2435	2357	2278	2201	2124	2048	1974	1902	1832	1763	1697	1633
	615.7	181.1	4.68	2716	2716	2693	2614	2534	2453	2372	2292	2212	2134	2057	1982	1909	1839	1770	1704
18 × 2 9/16 2 1/2"	638.6	187.8	4.70	2817	2817	2797	2716	2633	2550	2466	2383	2301	2220	2141	2063	1987	1914	1843	1774
	661.6	194.6	4.72	2919	2919	2902	2818	2733	2647	2561	2475	2390	2307	2224	2144	2066	1990	1917	1846
	684.5	201.3	4.74	3020	3020	3007	2921	2833	2745	2656	2567	2480	2393	2309	2226	2145	2067	1991	1917
24 × 1 1/4 1 1/8"	529.0	155.6	5.40	2334	2334	2334	2334	2305	2246	2186	2126	2066	2006	1946	1887	1829	1772	1716	1661
	549.4	161.6	5.47	2424	2424	2424	2424	2404	2344	2283	2222	2160	2098	2037	1976	1917	1858	1800	1743
	569.8	167.6	5.53	2514	2514	2514	2514	2503	2442	2379	2316	2253	2189	2126	2064	2002	1942	1882	1824
24 × 1 3/4 1 5/8"	590.2	173.6	5.58	2604	2604	2604	2604	2601	2538	2474	2409	2344	2279	2214	2150	2087	2024	1963	1902
	610.6	179.6	5.63	2694	2694	2694	2694	2694	2634	2569	2502	2436	2369	2303	2237	2171	2107	2044	1982
	631.0	185.6	5.68	2784	2784	2784	2784	2784	2724	2658	2596	2528	2460	2392	2324	2257	2191	2126	2062
24 × 2 1/8 2 1/2"	651.4	191.6	5.72	2874	2874	2874	2874	2874	2816	2758	2688	2619	2549	2479	2409	2341	2273	2206	2140
	671.8	197.6	5.76	2964	2964	2964	2964	2964	2922	2852	2781	2710	2638	2566	2495	2425	2355	2286	2219

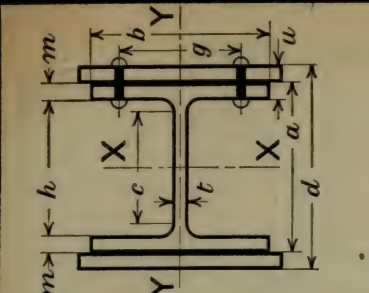
14" X 425# CARNEGIE BEAM SECTION

18 X 2 5/16	708.0	208.2	4.67	3124	3124	3094	3003	2911	2818	2725	2632	2541	2450	2362	2276	2192	2110	2031	1955
2 1/2 X 2 1/2"	731.0	215.0	4.69	3225	3225	3199	3106	3011	2915	2820	2724	2630	2537	2446	2357	2271	2187	2105	2027
2 1/2 X 1 1/2"	753.9	221.7	4.71	3326	3326	3305	3209	3112	3013	2915	2817	2720	2625	2531	2440	2350	2264	2180	2099
18 X 2 7/8"	776.9	228.5	4.72	3427	3427	3408	3309	3209	3108	3007	2906	2807	2709	2612	2518	2426	2337	2251	2167
3 X 1 1/2"	799.8	235.2	4.74	3529	3529	3514	3413	3310	3207	3103	3000	2897	2797	2697	2601	2506	2415	2326	2240
3 X 1 1/4"	822.8	242.0	4.75	3630	3630	3617	3514	3409	3302	3195	3089	2984	2881	2779	2680	2583	2489	2397	2309
18 X 3 7/16	845.7	248.7	4.76	3731	3731	3721	3615	3507	3398	3288	3180	3072	2965	2861	2759	2660	2563	2469	2378
3 5/8 X 1 1/2"	868.7	255.5	4.77	3832	3832	3824	3716	3605	3493	3381	3270	3159	3050	2943	2838	2736	2637	2541	2448
3 1/2 X 1 1/2"	891.6	262.2	4.79	3934	3934	3931	3820	3707	3593	3478	3364	3251	3140	3030	2923	2818	2716	2617	2522
4" X 1 1/2"	914.6	269.0	4.80	4035	4035	4035	3921	3806	3689	3572	3455	3339	3225	3112	3003	2895	2791	2690	2592
24 X 1 5/8"	690.2	203.0	5.46	3045	3045	3045	3045	3019	2943	2866	2789	2711	2633	2556	2480	2405	2331	2258	2187
1 X 3/4"	710.6	209.0	5.50	3135	3135	3135	3135	3116	3039	2960	2881	2802	2722	2643	2565	2488	2412	2338	2265
1 1/8 X 1 1/2"	731.0	215.0	5.55	3225	3225	3225	3225	3215	3137	3057	2976	2895	2814	2734	2654	2575	2497	2421	2346
2" X 2"	751.4	221.0	5.59	3315	3315	3315	3315	3313	3233	3152	3069	2987	2904	2822	2740	2660	2580	2502	2425
24 X 2 1/8"	771.8	227.0	5.63	3405	3405	3405	3405	3405	3329	3247	3163	3079	2994	2910	2827	2745	2664	2584	2505
2 1/2 X 2 1/2"	792.2	233.0	5.67	3495	3495	3495	3495	3495	3426	3342	3257	3171	3085	3000	2914	2830	2747	2666	2585
2 1/2 X 2 1/4"	812.6	239.0	5.70	3585	3585	3585	3585	3585	3522	3435	3349	3261	3174	3086	2999	2913	2828	2745	2663
2 1/2 X 2 1/2"	833.0	245.0	5.74	3675	3675	3675	3675	3675	3619	3532	3443	3354	3265	3176	3087	3000	2913	2828	2744
24 X 2 5/8"	853.4	251.0	5.77	3765	3765	3765	3765	3765	3714	3626	3536	3445	3354	3263	3173	3083	2995	2908	2822
2 3/4 X 2 1/2"	873.8	257.0	5.80	3855	3855	3855	3855	3855	3810	3720	3628	3536	3443	3351	3259	3167	3079	2989	2901
2 3/4 X 2 3/4"	894.2	263.0	5.83	3945	3945	3945	3945	3945	3906	3814	3721	3627	3533	3439	3345	3252	3160	3069	2980
3" X 2 1/2"	914.6	269.0	5.85	4035	4035	4035	4035	4035	4000	3907	3812	3716	3620	3524	3428	3333	3239	3147	3056

Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 14" CARNEGIE COLUMNS WITH COVER PLATES



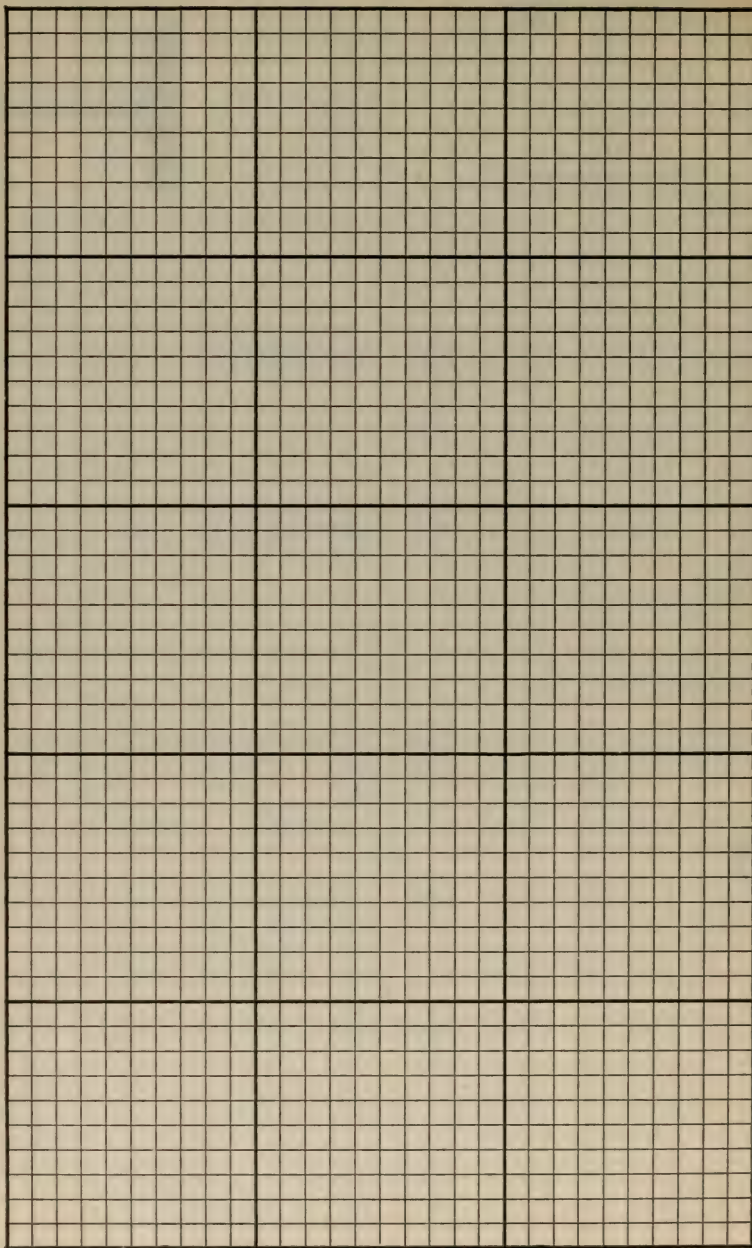
I, is Moment of Inertia
S, is Section Modulus
r, is Radius of Gyration

14"



2 Cover Plates	Weight per Foot	DIMENSIONS							AXIS X - X			AXIS Y - Y				
		d	b	t	a	h	m	c	g	Riv.	I	S	r	I	S	r
14" X 325# CARNEGIE BEAM SECTION																
18 X 2 3/16	569.8	21 3/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	11109	1050	8.14	3604	400	4.64
	592.7	21 9/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	11878	1103	8.25	3786	421	4.66
	615.7	21 15/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	12674	1157	8.37	3968	441	4.68
18 X 2 9/16	638.6	22 5/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	13498	1211	8.48	4151	461	4.70
	661.6	22 11/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	14350	1266	8.59	4333	481	4.72
	684.5	23 1/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	15230	1322	8.70	4515	502	4.74
24 X 1 1/4	529.0	19 11/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	9570	973	7.84	4540	378	5.40
	549.4	19 15/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	10157	1020	7.93	4828	400	5.47
	569.8	20 3/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	10760	1067	8.01	5116	426	5.53
24 X 1 1/2	590.2	20 7/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	11377	1115	8.10	5404	450	5.58
	610.6	20 11/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	12010	1162	8.18	5692	474	5.63
	631.0	20 15/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	12658	1210	8.26	5980	498	5.68
24 X 1 3/4	651.4	21 3/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	13322	1259	8.34	6268	522	5.72
	671.8	21 7/16	16.087	1.493	17.164	12.39	2.387	11.09	10"	1"	14002	1308	8.42	6556	546	5.76
	14" X 425# CARNEGIE BEAM SECTION															
18 X 2 5/16	708.0	23 3/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	15481	1338	8.62	4549	505	4.62
	731.0	23 9/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	16399	1395	8.73	4731	526	4.69
	753.9	23 15/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	17347	1453	8.84	4913	546	4.71
18 X 2 7/8	776.9	24 5/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	18325	1511	8.96	5096	566	4.72
	799.8	24 11/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	19333	1570	9.07	5278	586	4.74
	822.8	25 1/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	20373	1629	9.18	5460	607	4.75
18 X 3 7/16	845.7	25 7/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	21445	1690	9.29	5642	627	4.76
	868.7	25 13/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	22548	1751	9.39	5825	647	4.77
	891.6	26 3/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	23684	1812	9.50	6007	667	4.79
24 X 1 5/8	914.6	26 9/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	24854	1875	9.61	6189	688	4.80
	690.2	21 13/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	14343	1318	8.41	6045	504	5.46
	710.6	22 1/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	15062	1369	8.49	6333	528	5.50
24 X 1 7/8	731.0	22 5/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	15797	1419	8.57	6621	552	5.55
	751.4	22 9/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	16548	1470	8.65	6909	576	5.59
	771.8	22 13/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	17317	1522	8.73	7197	600	5.63
24 X 2 1/8	792.2	23 1/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	18102	1573	8.81	7485	624	5.67
	812.6	23 5/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	18905	1626	8.89	7773	648	5.70
	833.0	23 9/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	19726	1678	8.97	8061	672	5.74
24 X 2 5/8	853.4	23 13/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	20564	1731	9.05	8349	696	5.77
	873.8	24 1/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	21419	1784	9.13	8637	720	5.80
	894.2	24 5/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	22293	1838	9.21	8925	744	5.83
24 X 3"	914.6	24 9/16	16.506	1.912	18.510	12.39	3.060	11.09	10"	1"	23185	1892	9.28	9213	768	5.85

NOTES and DIAGRAMS



Part IV

Section 13

Plate and Angle Columns

**Plate and Angle Columns with
Cover Plates**

Channel and Plate Columns

Dimensions

Technical Functions

Allowable Concentric Loads

by

A. I. S. C. Specification

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 8 1/2" PLATE AND ANGLE COLUMNS

1 Web Plate	4 Angles	Weight Per Foot	Area Sq. in.	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET																	
					4	8	10	11	12	13	14	15	16	17	18	20	22	24	26	30		
8×1/4	2½×2½×¼	23.2	6.76	.96	101	78	65	59	54	49	45	41	38		
	3×2½×¼	24.8	7.24	1.19	109	96	83	77	72	66	62	57	53		
	3½×2½×¼	29.2	8.48	1.23	127	114	100	95	90	85	80	75	70	65		
	3½×2½×⅜	26.4	7.16	1.44	137	133	120	114	108	102	96	90	85	80	76	67	60		
	3½×3×¼	35.6	10.44	1.52	157	154	140	132	125	118	112	106	100	94	89	79	70		
8×1/4	3½×3×¼	38.4	8.24	1.40	124	118	105	99	93	87	82	77	73	68	64	56	50		
	3½×3×⅜	33.2	9.72	1.44	146	140	126	119	112	106	100	94	88	83	78	69	61		
	4×3×¼	38.4	11.20	1.47	168	163	147	139	131	124	117	110	103	97	92	81	72		
	4×3×¼	30.0	8.76	1.64	131	131	122	116	110	105	100	95	90	85	80	72	65		
	4×3×⅜	35.6	10.36	1.69	155	155	146	139	133	127	120	113	109	103	98	88	79		
8×5/16	4×3½×⅜	40.8	11.92	1.72	179	179	169	162	154	147	140	133	127	120	114	103	93		
	5×3½×⅜	43.2	12.68	1.68	190	190	178	170	162	154	147	140	133	127	120	107	96		
	5×3½×⅝	41.6	12.24	2.19	184	184	184	182	176	171	165	159	153	147	141	130	120		
	2½×2½×5/16	28.5	8.38	.98	126	98	82	75	69	63	57	52	48		
	3×2½×5/16	30.9	8.98	1.22	135	120	105	98	91	85	79	73	68		
8×5/16	3½×2½×⅝	34.9	10.18	1.26	153	139	122	114	106	99	92	86	80		
	3½×2½×⅝	32.9	9.62	1.47	144	140	126	119	113	106	100	94	89	84	79	70	62		
	3½×3×⅝	37.3	10.94	1.51	164	161	146	138	131	124	117	110	104	98	92	82	73		
	3½×3×⅝	34.9	10.22	1.42	153	147	132	124	117	110	103	97	91	85	80	71	63		
	4×3×⅝	40.1	11.70	1.46	176	170	153	144	137	129	121	114	107	101	95	84	75		
8×5/16	4×3×⅝	37.3	10.86	1.67	163	163	152	145	138	132	125	119	113	107	101	91	82		
	4×3×⅝	42.5	12.42	1.71	186	186	175	168	160	153	145	138	132	125	118	107	96		
	4×3½×⅝	44.9	13.18	1.67	198	198	184	176	168	160	152	144	137	130	123	110	99		
	5×3½×⅝	43.3	12.74	2.13	191	191	191	189	183	177	170	164	158	152	146	135	124	105	89	...		
	5×3½×⅝	50.1	14.70	2.17	221	221	221	219	213	206	198	191	184	177	171	158	145	123	105	...		
8×3/8	3×2½×⅝	36.6	10.68	1.25	160	145	127	119	111	103	96	89	83	77	72		
	3×3×⅝	39.0	11.44	1.21	172	152	133	124	115	107	99	92	86	80	74		
	3½×2½×⅝	39.0	11.44	1.50	172	168	152	144	136	128	121	114	108	102	96		
	3½×3×⅝	41.8	12.20	1.45	183	177	159	150	142	134	126	118	111	104	98		
	4×3×⅝	46.6	13.60	1.49	204	199	180	170	161	152	143	135	127	120	113	100	89		
8×3/8	4×3×⅝	44.2	12.92	1.70	194	194	182	174	166	158	151	143	136	129	123	110	99		
	4×3×⅝	49.4	14.48	1.73	217	217	206	197	188	180	171	163	155	147	140	126	114		
	4×3½×⅝	46.6	13.68	1.66	205	205	191	182	174	165	157	149	141	134	127	114	102		
	5×3½×⅝	51.8	15.20	2.15	228	228	226	219	212	204	196	188	179	171	162	149	137	126	107	...		
	5×3½×⅝	58.2	17.12	2.19	257	257	257	256	248	240	232	224	216	208	200	185	171	157	145	123		

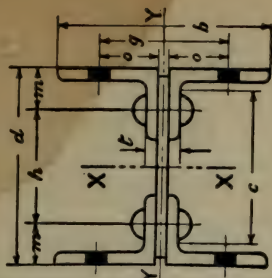
Unequal Angles have short leg against web plate.
Weights given do not include rivets or other details.
Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

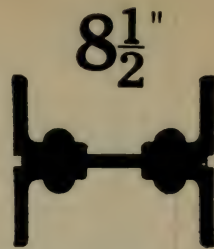
DIMENSIONS AND FUNCTIONS OF $8\frac{1}{2}$ " PLATE AND ANGLE COLUMNS

I Web Plate	Angles	DIMENSIONS										AXIS X-X				AXIS Y-Y			
		d	b	t	h	m	o	g	c	Riv.	I	S	r	I	S	r	I	S	r
$8 \times 1\frac{1}{4}$	$2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	$8\frac{1}{2}$	$5\frac{1}{4}$	$\frac{3}{4}$	$5\frac{3}{4}$	$1\frac{3}{8}$	$1\frac{3}{8}$	3	$7\frac{1}{8}$	$\frac{3}{4}$	73	17.1	3.28	6.2	2.4	.96			
	$3 \times 2\frac{1}{2} \times \frac{1}{4}$	"	$6\frac{1}{4}$	$\frac{3}{4}$	"	"	$1\frac{3}{8}$	$3\frac{3}{4}$	$7\frac{3}{8}$	"	82	19.2	3.35	10.3	3.3	1.19			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	$7\frac{1}{4}$	$\frac{3}{4}$	"	"	2	$4\frac{1}{4}$	$7\frac{3}{8}$	"	97	22.8	3.38	12.9	4.1	1.23			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	"	$\frac{7}{8}$	"	"	"	"	$7\frac{3}{8}$	"	108	25.1	3.40	16.0	4.4	1.44			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	"	"	"	"	"	"	$7\frac{3}{8}$	"	124	29.4	3.43	20.2	5.6	1.49			
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	$1\frac{3}{4}$	5	$1\frac{3}{4}$	"	"	$7\frac{3}{8}$	$\frac{7}{8}$	101	21.3	3.44	24.2	6.7	1.52			
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	$\frac{7}{8}$	"	"	"	"	$7\frac{3}{8}$	"	98	25.5	3.34	20.2	4.4	1.40			
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	1	"	"	"	"	$7\frac{3}{8}$	"	126	29.6	3.35	24.3	6.7	1.47			
	$4 \times 3 \times \frac{1}{4}$	$8\frac{1}{2}$	$8\frac{1}{4}$	$\frac{3}{4}$	5	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{1}{4}$	$7\frac{1}{8}$	$\frac{7}{8}$	100	23.5	3.38	23.7	5.8	1.64			
	$4 \times 3 \times \frac{1}{4}$	"	"	$\frac{7}{8}$	"	"	"	"	$7\frac{1}{8}$	"	119	28.0	3.38	29.6	7.2	1.69			
$8 \times 5\frac{1}{16}$	$4 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	1	$4\frac{1}{2}$	"	"	"	"	"	138	32.4	3.40	35.4	8.6	1.72			
	$5 \times 3\frac{1}{2} \times \frac{1}{4}$	"	$10\frac{1}{4}$	$\frac{7}{8}$	"	"	3	$6\frac{1}{4}$	"	"	141	33.1	3.39	35.8	8.7	1.68			
	$2\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	$8\frac{1}{2}$	$5\frac{5}{16}$	$1\frac{5}{16}$	$5\frac{3}{4}$	$1\frac{3}{8}$	$1\frac{3}{8}$	$3\frac{1}{8}$	$7\frac{1}{8}$	$\frac{3}{4}$	89	21.0	3.26	8.1	3.1	.98			
	$3 \times 2\frac{1}{2} \times \frac{1}{4}$	"	$6\frac{5}{16}$	$1\frac{1}{16}$	"	"	$1\frac{3}{8}$	$3\frac{1}{8}$	$7\frac{1}{8}$	"	99	23.4	3.33	13.3	4.2	1.22			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	$7\frac{5}{16}$	$1\frac{1}{16}$	"	"	"	$4\frac{5}{16}$	$7\frac{1}{8}$	"	113	26.7	3.34	16.2	5.1	1.26			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{16}$	"	"	2	"	$7\frac{1}{8}$	"	110	25.9	3.38	20.7	5.6	1.47			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{16}$	"	"	"	"	$7\frac{1}{8}$	"	126	29.7	3.40	24.9	6.8	1.51			
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	$1\frac{1}{16}$	5	$1\frac{3}{4}$	"	"	$7\frac{1}{8}$	$\frac{7}{8}$	111	26.1	3.30	20.7	5.7	1.42			
	$4 \times 3 \times \frac{1}{4}$	$8\frac{1}{2}$	$8\frac{5}{16}$	$1\frac{5}{16}$	5	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{5}{16}$	$7\frac{1}{8}$	$\frac{7}{8}$	121	28.6	3.34	30.3	7.3	1.67			
	$4 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{16}$	$4\frac{1}{2}$	"	"	"	"	"	140	33.0	3.36	36.3	8.7	1.71			
$8 \times 3\frac{3}{8}$	$4 \times 3\frac{1}{2} \times \frac{1}{4}$	"	$10\frac{5}{16}$	$1\frac{1}{16}$	"	"	3	$6\frac{5}{16}$	"	"	141	33.2	3.35	36.7	8.8	1.67			
	$5 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{16}$	"	"	"	"	$6\frac{7}{8}$	"	143	33.7	3.35	37.6	11.2	2.13			
	$3 \times 2\frac{1}{2} \times \frac{1}{4}$	$8\frac{1}{2}$	$6\frac{3}{8}$	$1\frac{1}{8}$	$5\frac{3}{4}$	$1\frac{3}{8}$	$1\frac{3}{8}$	$3\frac{7}{8}$	$7\frac{1}{8}$	$\frac{3}{4}$	116	27.3	3.29	16.8	5.3	1.25			
	$3 \times 3 \times \frac{1}{4}$	"	$6\frac{3}{8}$	"	5	$1\frac{3}{4}$	2	$4\frac{3}{8}$	$7\frac{1}{8}$	$\frac{7}{8}$	118	27.8	3.21	16.8	5.3	1.21			
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	"	$7\frac{3}{8}$	"	$5\frac{3}{4}$	$1\frac{3}{4}$	"	"	$7\frac{1}{8}$	$\frac{3}{4}$	131	30.4	3.36	25.6	6.9	1.50			
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	$1\frac{1}{4}$	"	"	"	"	$6\frac{7}{8}$	$\frac{7}{8}$	147	34.5	3.29	30.0	8.1	1.49			
	$4 \times 3 \times \frac{1}{4}$	$8\frac{1}{2}$	$8\frac{3}{8}$	$1\frac{1}{8}$	5	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{3}{8}$	"	$\frac{7}{8}$	143	33.7	3.33	37.2	8.9	1.70			
	$4 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{4}$	$4\frac{1}{2}$	"	"	"	$6\frac{7}{8}$	"	161	37.9	3.34	43.5	10.4	1.73			
	$5 \times 3\frac{1}{2} \times \frac{1}{4}$	"	$10\frac{9}{8}$	$1\frac{1}{8}$	"	"	3	$6\frac{3}{8}$	"	"	144	33.8	3.34	37.7	9.0	1.66			
	$5 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	$1\frac{1}{4}$	"	"	"	"	$6\frac{7}{8}$	"	169	39.8	3.33	70.5	13.6	2.15			

Unequal Angles have short leg against web plate.
Dimensions h, m, o and g can be varied considerably.



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration



$8\frac{1}{2}$ "

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 10 1/2" PLATE AND ANGLE COLUMNS

Web Plate	Angles	Weight Per Foot	Area Sq. in.	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET															
					6	7	8	9	10	12	14	16	18	20	22	24	26	28	30	32
10x1/4	3 1/2 x 2 1/2 x 1/4	28.1	8.26	1.39	124	123	118	111	105	93	82	72	63	56
	3 1/2 x 2 1/2 x 5/16	32.9	9.62	1.45	144	144	139	132	125	112	99	88	78	69
	3 1/2 x 3 x 3/8	37.3	10.94	1.49	164	164	160	153	145	130	115	102	91	81
	3 1/2 x 3 x 1/2	40.1	12.11	1.56	184	184	180	173	165	149	133	119	106	95
	3 1/2 x 3 x 5/8	43.9	13.41	1.61	204	204	200	193	185	168	151	137	123	110
10x3/8	4 x 3 x 1/4	31.7	9.26	1.60	139	139	139	133	127	115	103	93	83	74	66
	4 x 3 x 5/16	37.3	10.86	1.65	163	163	163	158	151	137	124	112	100	90	81
	4 x 3 x 3/8	42.5	12.42	1.69	186	186	186	182	175	159	144	130	117	105	95
	4 x 3 x 1/2	44.3	13.18	1.65	198	198	198	192	184	167	151	135	122	109	98
	5 x 3 x 1/2	49.3	15.14	1.74	221	221	221	215	207	189	172	155	141	127	113	104	96	88
10x5/16	3 1/2 x 2 1/2 x 1/4	35.0	10.25	1.42	154	154	147	140	132	117	104	92	81	71	63
	3 1/2 x 2 1/2 x 5/16	39.4	11.57	1.47	174	174	168	160	152	136	121	107	95	84	75
	3 1/2 x 3 x 3/8	42.2	12.33	1.42	185	185	177	168	159	141	125	110	97	86	76
	4 x 3 x 1/4	39.4	11.49	1.62	172	172	172	166	159	144	129	116	104	93	84
	4 x 3 x 5/16	44.6	13.05	1.67	196	196	196	191	183	166	150	135	122	109	98
10x3/8	4 x 3 x 3/8	47.0	13.81	1.63	207	207	207	200	191	173	156	140	126	113	101
	4 x 3 x 1/2	48.4	14.37	1.68	221	221	221	214	205	187	170	153	138	124	110
	5 x 3 x 1/2	52.2	15.33	1.22	230	230	230	223	214	196	177	163	151	138	127	117	107	98	90	...
	3 1/2 x 3 x 3/8	44.4	12.95	1.41	194	194	185	176	166	148	130	115	101	89	79
	4 x 3 x 3/8	46.8	13.67	1.65	205	205	205	199	190	173	156	140	126	113	102
10x1/2	4 x 3 x 1/2	49.2	14.43	1.62	217	217	217	208	199	181	163	146	131	117	105
	5 x 3 x 3/8	54.4	15.95	2.10	239	239	239	239	239	228	212	196	181	166	153	140	129	118	109	...
	6 x 3 x 1/2	60.8	17.87	2.14	268	268	268	268	268	257	240	222	206	189	174	160	147	136	125	...
	6 x 4 x 1/2	67.2	19.75	2.19	296	296	296	296	296	287	268	249	231	213	197	181	167	154	142	...
	6 x 4 x 3/8	72.0	21.89	2.26	323	323	323	323	323	313	294	275	256	237	220	206	192	179	167	156
10x5/8	6 x 4 x 1/2	77.6	22.75	2.65	341	341	341	341	341	331	312	293	274	255	236	220	205	192	179	167
	6 x 4 x 5/8	81.8	24.00	2.62	360	360	360	360	360	350	331	312	293	274	255	236	220	205	192	180
	6 x 4 x 3/4	89.4	26.24	2.66	394	394	394	394	394	384	365	346	327	308	289	270	251	232	213	197
	6 x 4 x 7/8	97.0	28.44	2.69	427	427	427	427	427	417	398	379	360	341	322	303	284	265	246	227
	6 x 4 x 1	101.3	29.69	2.68	445	445	445	445	445	435	416	397	378	359	340	321	302	283	264	245
10x3/4	6 x 4 x 5/8	115.7	34.01	2.75	510	510	510	510	510	500	481	462	443	424	405	386	367	348	329	310
	6 x 4 x 3/4	119.9	35.26	2.74	529	529	529	529	529	519	500	481	462	443	424	405	386	367	348	329
	6 x 4 x 7/8	134.3	39.42	2.80	591	591	591	591	591	581	562	543	524	505	486	467	448	429	410	391
	6 x 4 x 1	138.7	40.67	2.80	610	610	610	610	610	600	581	562	543	524	505	486	467	448	429	410
	6 x 4 x 1 1/8	143.1	41.92	2.80	629	629	629	629	629	619	600	581	562	543	524	505	486	467	448	429

Unequal Angles have short leg against web plate.

Weights given do not include rivets or other details.

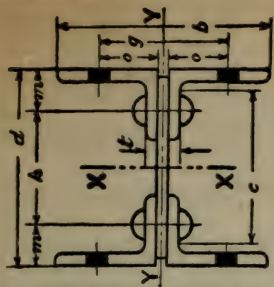
Loads to right of heavy vertical lines are for Secondary Members ONLY.

DIMENSIONS AND FUNCTIONS OF 10½" PLATE AND ANGLE COLUMNS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration

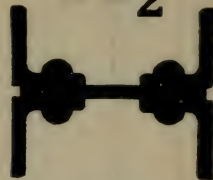
		DIMENSIONS		AXIS X-X		AXIS Y-Y										
I Web Plate	Angles	d	b	t	h	m	o	g	c	Riv.	I	S	r	I	S	r
10×1/4	3 1/2 × 2 1/2 × 1/4	10 1/2	7 1/4	3/4	7 3/4	1 3/4	2	4 1/4	9 3/4	3/4	148	28.2	4.23	16.0	4.4	1.39
10×1/4	3 1/2 × 2 1/2 × 3/8	"	"	1	7 7/8	"	"	"	9 1/4	"	176	33.5	4.28	16.0	5.6	1.45
10×1/4	3 1/2 × 3 × 1/4	"	"	1	7 3/4	1 3/4	"	"	9 1/4	7/8	203	38.6	4.30	24.2	6.7	1.49
10×1/4	3 1/2 × 3 × 3/8	"	"	1	7 3/4	1 3/4	"	"	9 1/4	7/8	150	28.6	4.15	16.1	4.4	1.36
10×1/4	5 × 3 1/2 × 1/4	"	"	1	"	"	"	"	9	"	179	34.2	4.19	20.2	5.6	1.41
10×1/4	4 × 3 × 1/4	10 1/2	8 1/4	3/4	7	1 3/4	2 1/2	5 1/4	9 1/4	7/8	164	31.2	4.20	23.7	5.8	1.60
10×1/4	4 × 3 × 3/8	"	"	1	"	"	"	"	9 1/4	"	196	37.3	4.24	29.6	7.2	1.65
10×1/4	4 × 3 1/2 × 3/8	"	"	1	6 1/2	2	"	"	9	"	227	43.2	4.27	35.4	8.6	1.69
10×1/4	5 × 3 1/2 × 1/4	"	10 1/4	7/8	"	"	3	6 1/4	8 7/8	"	229	43.7	4.17	35.8	8.7	1.65
10×1/4	5 × 3 1/2 × 3/8	"	"	1	"	"	"	"	8 7/8	"	269	51.0	4.27	67.8	13.3	2.15
10×5/16	3 1/2 × 2 1/2 × 5/16	10 1/2	7 5/16	15/16	7 3/4	1 3/4	2	4 5/16	9 1/4	3/4	181	34.5	4.20	20.7	5.7	1.42
10×5/16	3 1/2 × 2 1/2 × 3/8	"	"	1 1/16	7 1/2	1 3/4	"	"	9 1/4	7/8	208	39.6	4.24	24.9	6.8	1.47
10×5/16	3 1/2 × 3 × 1/4	"	"	1 1/16	7	1 3/4	"	"	9	"	185	35.2	4.13	20.7	5.7	1.38
10×5/16	3 1/2 × 3 × 3/8	"	"	1 1/16	7	1 3/4	"	"	9	"	213	40.4	4.15	25.0	6.8	1.42
10×5/16	4 × 3 × 1/4	10 1/2	8 5/16	15/16	7	1 3/4	2 1/2	5 1/16	9 1/4	7/8	201	38.3	4.18	30.3	7.3	1.62
10×5/16	4 × 3 1/2 × 3/8	"	"	1 1/16	6 1/2	2	"	"	9	"	232	44.2	4.22	36.3	8.7	1.67
10×5/16	5 × 3 1/2 × 1/4	"	10 5/16	15/16	"	"	3	6 5/16	8 7/8	"	235	44.7	4.19	36.7	8.9	1.63
10×5/16	5 × 3 1/2 × 3/8	"	"	1 1/16	"	"	"	"	8 7/8	"	236	45.0	4.20	57.6	11.2	2.08
10×5/16	3 1/2 × 3 × 1/4	10 1/2	7 3/8	1 1/8	7	1 3/4	2	4 3/8	9	1/2	218	41.6	4.11	25.7	7.0	1.41
10×5/16	4 × 3 × 3/8	"	8 3/8	"	6 1/2	2	2 1/2	5 3/8	9	"	237	45.2	4.17	37.2	8.9	1.65
10×5/16	4 × 3 1/2 × 3/8	"	"	"	"	"	"	"	9	"	240	45.7	4.08	37.7	9.0	1.62
10×3/8	5 × 3 1/2 × 1/4	10 1/2	10 3/8	1 1/4	6 1/2	2	3	6 3/8	8 7/8	7/8	279	53.2	4.18	70.5	13.6	2.10
10×3/8	5 × 3 1/2 × 3/8	"	"	1 1/4	"	"	"	"	8 3/4	"	315	60.0	4.20	82.2	15.8	2.14
10×3/8	6 × 3 1/2 × 1/4	"	"	1 3/8	5 1/2	"	"	"	8 5/8	"	349	66.6	4.21	94.6	18.2	2.19
10×3/8	6 × 3 1/2 × 3/8	"	12 3/8	1 1/8	5 1/2	2 1/2	3 1/2	7 3/8	8 3/4	"	319	60.8	4.19	119.2	19.3	2.56
10×3/8	6 × 4 × 1/4	"	"	1 1/4	"	"	"	"	8 5/8	7/8	361	68.8	4.20	139.0	22.5	2.61
10×3/8	6 × 4 × 3/8	"	"	1 3/8	"	"	"	"	8 1/2	"	401	76.4	4.20	159.7	25.8	2.65
10×3/8	6 × 4 × 1/2	10 1/2	12 1/2	1 1/2	5 1/2	2 1/2	3 1/2	7 1/2	8 1/2	7/8	412	78.5	4.14	164.9	26.3	2.62
10×3/8	6 × 4 × 3/4	"	"	1 5/8	"	"	"	"	8 3/4	"	451	85.9	4.15	185.5	29.7	2.66
10×3/8	6 × 4 × 5/8	"	"	1 3/4	"	"	"	"	8 1/4	"	490	93.3	4.15	206.1	33.0	2.69
10×5/8	6 × 4 × 3/8	10 1/2	12 3/8	1 1/8	5 1/2	2 1/2	3 1/2	7 5/8	8 3/4	7/8	500	95.3	4.10	212.9	33.7	2.68
10×5/8	6 × 4 × 1/2	"	"	2 1/8	"	"	"	"	8	"	569	108.4	4.09	256.9	40.7	2.75
10×5/8	6 × 4 × 3/4	10 1/2	12 3/4	2 1/4	5 1/2	2 1/2	3 1/2	7 3/4	7 3/4	7/8	580	110.3	4.05	265.4	41.6	2.74
10×5/8	6 × 4 × 7/8	"	"	2 1/2	"	"	"	"	7 3/4	"	646	123.0	4.05	309.6	48.6	2.80

Unequal angles have short leg against web plate.
Dimensions *h*, *m*, *o* and *g* can be varied considerably.



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration

10½"



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 12 1/2" PLATE AND ANGLE COLUMNS

[For 12 1/2" Columns with Cover Plates see following pages]

UNSUPPORTED LENGTH IN FEET

1 Web Plate	4 Angles	Weight Per Foot	Area Sq. in.	Least Radius Gyr.	6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
12 x 1/4	3 1/2 x 2 1/2 x 1/4	29.8	8.76	1.36	131	124	110	97	86	75	66	58	51
	3 1/2 x 2 1/2 x 3/8	39.0	11.44	1.45	172	165	149	133	118	104	92	82	73
	3 1/2 x 3 x 1/4	31.8	9.24	1.32	139	129	114	100	88	76	67	59	52
	3 1/2 x 3 x 3/8	41.8	12.20	1.41	183	175	157	139	123	108	95	84	74
	4 x 3 x 1/4	33.4	9.76	1.56	146	145	132	119	107	95	85	76	68
12 x 5/16	3 1/2 x 2 1/2 x 5/16	37.2	10.87	1.38	163	154	138	122	107	94	83	73	64
	3 1/2 x 2 1/2 x 3/8	41.6	12.19	1.43	183	176	158	140	124	110	97	86	76
	3 1/2 x 3 x 1/4	39.2	11.47	1.34	172	161	143	126	110	96	84	74	65
	3 1/2 x 3 x 3/8	49.4	12.95	1.39	194	184	165	146	129	113	99	88	78
	4 x 3 x 5/16	41.6	12.11	1.58	182	181	165	149	134	120	107	96	85
12 x 3/8	3 1/2 x 2 1/2 x 3/8	46.8	13.67	1.63	205	205	189	172	155	139	125	112	100
	3 1/2 x 2 1/2 x 5/16	49.2	14.43	1.59	217	216	197	178	160	143	128	115	102
	4 x 3 1/2 x 1/4	47.6	13.99	2.03	210	210	210	197	182	168	155	142	130
	4 x 3 1/2 x 3/8	54.4	15.95	2.08	239	239	239	227	211	195	180	165	152
	4 x 3 x 3/8	49.3	14.42	1.61	216	216	198	180	162	145	130	116	104
12 x 3/8	4 x 3 1/2 x 1/4	51.7	15.18	1.57	228	226	206	186	167	149	133	119	106
	4 x 3 1/2 x 3/8	56.9	16.70	2.05	251	251	251	236	219	202	186	171	156
	5 x 3 1/2 x 1/4	63.3	18.62	2.10	279	279	279	266	247	229	211	194	178
	5 x 3 1/2 x 3/8	69.7	20.50	2.15	308	308	308	295	275	256	237	218	201
	6 x 4 x 3/8	64.5	18.94	2.51	284	284	284	273	257	241	226	211	197
12 x 1/2	3 1/2 x 2 1/2 x 1/2	72.5	21.22	2.56	318	318	318	318	309	291	274	257	240
	3 1/2 x 2 1/2 x 3/8	80.1	23.50	2.61	353	353	353	353	344	325	306	288	270
	4 x 3 1/2 x 1/4	74.8	22.10	2.11	350	330	330	315	293	271	250	230	212
	4 x 3 1/2 x 3/8	81.6	25.68	2.19	385	385	385	372	348	324	300	277	252
	6 x 4 x 1/2	85.2	25.60	2.57	375	375	375	375	364	344	323	303	284
12 x 5/8	3 1/2 x 2 1/2 x 5/8	92.8	27.24	2.61	409	409	409	409	399	377	355	334	313
	4 x 3 1/2 x 1/2	100.4	29.44	2.65	442	442	442	442	432	412	387	364	342
	4 x 3 1/2 x 3/8	105.5	30.94	2.62	464	464	464	464	453	429	404	380	356
	6 x 4 x 5/8	119.5	35.76	2.70	529	529	529	529	522	495	468	441	415
	6 x 4 x 3/4	125.0	36.76	2.69	551	551	551	551	544	516	487	459	431
12 x 3/4	3 1/2 x 2 1/2 x 3/4	139.4	40.92	2.75	614	614	614	614	611	579	549	518	487
	4 x 3 1/2 x 1/2	145.4	42.76	2.51	641	641	641	641	616	581	545	511	477
	4 x 3 1/2 x 3/8	163.0	47.92	2.57	719	719	719	719	697	658	620	581	544
	6 x 4 x 3/4	139.4	40.92	2.75	614	614	614	614	611	579	549	518	487
	6 x 6 x 3/4	163.0	47.92	2.57	719	719	719	719	697	658	620	581	544

Unequal Angles have short leg against web plate.

Weights given do not include rivets or other details.

Loads to right of heavy vertical lines are for Secondary Members ONLY.

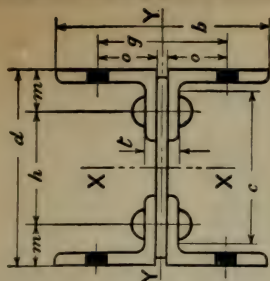
LOADS BY A. I. S. C. SPECIFICATION

For $12\frac{1}{2}$ " Columns with Cover
Plates see following pages

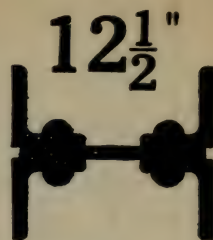
DIMENSIONS AND FUNCTIONS OF $12\frac{1}{2}$ " PLATE AND ANGLE COLUMNS

Web Plate	Angles	DIMENSIONS										AXIS X-X				AXIS Y-Y			
		d	b	t	h	m	o	q	c	Riv.	I	S	r	I	S	r	I	S	r
$12 \times \frac{1}{4}$	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{4}$	$12\frac{1}{2}$	$7\frac{1}{4}$	$\frac{3}{4}$	$9\frac{3}{4}$	$1\frac{3}{8}$	2	$4\frac{1}{4}$	$11\frac{3}{8}$	$\frac{3}{4}$	222	36	5.04	16.0	4.4	1.36	4.4	1.36	
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	$\frac{3}{4}$	9	$1\frac{3}{4}$	"	"	$11\frac{1}{4}$	$\frac{7}{8}$	304	49	5.15	24.2	6.7	1.45	6.7	1.45	
	$3\frac{1}{2} \times 3 \times \frac{1}{4}$	"	"	1	"	"	"	"	11	"	227	36	4.96	16.1	4.4	1.32	4.4	1.32	
	$4 \times 3 \times \frac{1}{4}$	$12\frac{1}{2}$	$8\frac{1}{4}$	$\frac{3}{4}$	9	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{1}{4}$	$11\frac{1}{4}$	$\frac{7}{8}$	247	40	5.03	23.7	5.8	1.56	5.8	1.56	
	$4 \times 3\frac{1}{2} \times \frac{1}{4}$	"	"	1	$8\frac{1}{2}$	2	"	"	11	"	341	55	5.14	35.4	8.6	1.62	8.6	1.62	
$12 \times \frac{5}{16}$	$5 \times 3\frac{1}{2} \times \frac{5}{16}$	"	$10\frac{1}{4}$	$\frac{7}{8}$	"	"	3	$6\frac{1}{4}$	$10\frac{7}{8}$	"	347	56	5.03	35.8	8.7	1.66	8.7	1.66	
	$3\frac{1}{2} \times 2\frac{1}{2} \times \frac{5}{16}$	$12\frac{1}{2}$	$7\frac{5}{16}$	$\frac{13}{16}$	$9\frac{3}{4}$	$1\frac{3}{8}$	2	$4\frac{5}{16}$	$11\frac{1}{4}$	$\frac{3}{4}$	273	44	5.01	20.7	5.7	1.38	5.7	1.38	
	$3\frac{1}{2} \times 3 \times \frac{5}{16}$	"	"	$1\frac{1}{16}$	9	$1\frac{3}{4}$	"	"	$11\frac{1}{8}$	$\frac{7}{8}$	313	50	5.07	24.9	6.8	1.43	6.8	1.43	
	$4 \times 3 \times \frac{5}{16}$	$12\frac{1}{2}$	$8\frac{5}{16}$	$\frac{15}{16}$	9	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{5}{16}$	$11\frac{1}{8}$	$\frac{7}{8}$	280	45	4.94	20.7	5.7	1.34	5.7	1.34	
	$4 \times 3\frac{1}{2} \times \frac{5}{16}$	"	"	$1\frac{1}{16}$	$8\frac{1}{2}$	2	"	"	11	"	323	52	4.91	25.0	6.8	1.39	6.8	1.39	
$12 \times \frac{3}{8}$	$5 \times 3\frac{1}{2} \times \frac{3}{8}$	"	$10\frac{5}{16}$	$\frac{15}{16}$	"	"	3	$6\frac{5}{16}$	$10\frac{7}{8}$	"	412	66	5.08	69.2	13.4	2.08	13.4	2.08	
	$4 \times 3 \times \frac{3}{8}$	$12\frac{1}{2}$	$8\frac{3}{8}$	$\frac{11}{8}$	9	$1\frac{3}{4}$	$2\frac{1}{2}$	$5\frac{3}{8}$	11	$\frac{7}{8}$	359	58	4.99	37.2	8.9	1.61	8.9	1.61	
	$4 \times 3\frac{1}{2} \times \frac{3}{8}$	"	"	"	$8\frac{1}{2}$	2	3	$6\frac{3}{8}$	$10\frac{7}{8}$	"	365	58	4.90	37.7	9.0	1.57	9.0	1.57	
	$5 \times 3\frac{1}{2} \times \frac{3}{8}$	"	$10\frac{3}{8}$	$\frac{11}{4}$	"	"	"	"	$10\frac{3}{8}$	"	421	67	5.02	70.5	13.6	2.05	13.6	2.05	
	$\frac{1}{2}$	"	"	$\frac{13}{8}$	"	"	"	"	$10\frac{5}{8}$	"	476	76	5.05	82.2	15.8	2.10	15.8	2.10	
$12 \times \frac{1}{2}$	$6 \times 4 \times \frac{1}{2}$	$12\frac{1}{2}$	$12\frac{3}{8}$	$\frac{15}{8}$	$7\frac{1}{2}$	$2\frac{1}{2}$	$3\frac{1}{2}$	$7\frac{3}{8}$	$10\frac{3}{4}$	$\frac{7}{8}$	481	77	5.04	119.2	19.3	2.51	19.3	2.51	
	$5 \times 3\frac{1}{2} \times \frac{1}{2}$	$12\frac{1}{2}$	$10\frac{1}{2}$	$\frac{13}{8}$	$8\frac{1}{2}$	2	3	$6\frac{1}{2}$	$10\frac{3}{8}$	$\frac{7}{8}$	544	87	5.06	139.0	22.5	2.56	22.5	2.56	
	$6 \times 4 \times \frac{1}{2}$	"	"	1	$8\frac{1}{2}$	"	"	"	$10\frac{1}{2}$	"	605	97	5.07	159.7	25.8	2.61	25.8	2.61	
	$5 \times 3\frac{1}{2} \times \frac{1}{2}$	$12\frac{1}{2}$	$10\frac{1}{2}$	$\frac{13}{8}$	"	"	"	"	$10\frac{3}{8}$	"	544	87	4.97	98.3	18.7	2.11	18.7	2.11	
	$6 \times 4 \times \frac{1}{2}$	"	"	$\frac{15}{8}$	$7\frac{1}{2}$	$2\frac{1}{2}$	$3\frac{1}{2}$	$7\frac{1}{2}$	$10\frac{1}{2}$	"	623	100	4.99	164.9	26.4	2.57	26.4	2.57	
$12 \times \frac{5}{8}$	$6 \times 4 \times \frac{5}{8}$	$12\frac{1}{2}$	$12\frac{3}{8}$	$\frac{17}{8}$	"	"	"	"	$10\frac{3}{4}$	"	683	109	5.01	185.5	29.7	2.61	29.7	2.61	
	$5 \times 3\frac{1}{2} \times \frac{5}{8}$	"	"	$\frac{13}{4}$	"	"	"	"	$10\frac{1}{4}$	"	741	119	5.02	206.1	33.0	2.65	33.0	2.65	
	$6 \times 4 \times \frac{5}{8}$	$12\frac{1}{2}$	$12\frac{3}{8}$	$\frac{17}{8}$	$7\frac{1}{2}$	$2\frac{1}{2}$	$3\frac{1}{2}$	$7\frac{5}{8}$	$10\frac{1}{4}$	$\frac{7}{8}$	759	122	4.95	212.9	33.7	2.62	33.7	2.62	
	$5 \times 3\frac{1}{2} \times \frac{5}{8}$	"	"	$\frac{13}{4}$	"	"	"	"	10	"	867	139	4.96	256.9	40.7	2.70	40.7	2.70	
	$6 \times 4 \times \frac{5}{8}$	$12\frac{1}{2}$	$12\frac{3}{8}$	$\frac{17}{8}$	$7\frac{1}{2}$	$2\frac{1}{2}$	$3\frac{1}{2}$	$7\frac{3}{4}$	$9\frac{3}{4}$	$\frac{7}{8}$	885	142	4.91	265.4	41.7	2.69	41.7	2.69	
$12 \times \frac{3}{4}$	$6 \times 4 \times \frac{3}{4}$	"	"	$\frac{13}{4}$	$5\frac{1}{2}$	$3\frac{1}{2}$	"	"	$9\frac{3}{4}$	"	987	158	4.91	309.6	48.6	2.75	48.6	2.75	
	$5 \times 3\frac{1}{2} \times \frac{3}{4}$	"	"	$\frac{13}{4}$	"	"	"	"	10	"	895	143	4.57	269.4	42.3	2.51	42.3	2.51	
	$6 \times 4 \times \frac{3}{4}$	"	"	$\frac{13}{4}$	"	"	"	"	$9\frac{3}{4}$	"	999	160	4.57	315.2	49.5	2.57	49.5	2.57	
	$5 \times 3\frac{1}{2} \times \frac{3}{4}$	"	"	$\frac{13}{4}$	"	"	"	"	"	"									
	$6 \times 4 \times \frac{3}{4}$	"	"	$\frac{13}{4}$	"	"	"	"	"	"									

Unequal Angles have short leg against web plate.
Dimensions h , m , o and g can be varied considerably.



I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 12½" PLATE AND ANGLE COLUMNS WITH COVER PLATES

1 Web Plate	4 Angles	2 Cover Plates	Weight Per Foot	Area Sq. in.	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET															
						12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	44
12×3/8	6×4×3/8	14×3/8	100.2	29.44	3.14	442	442	439	420	400	380	361	342	324	306	289	273	258	244
	6×4×3/8	14×1/2	112.1	32.94	3.25	494	494	494	476	455	434	413	392	372	352	334	316	299	283
	6×4×3/8	14×1/2	120.1	35.22	3.23	528	528	528	508	485	462	440	418	396	375	355	336	318	301
12×1/2	6×4×1/2	14×1/2	127.7	37.50	3.22	563	563	563	540	516	491	467	444	421	398	377	357	338	319
	6×4×1/2	14×1/2	132.8	39.00	3.18	585	585	584	559	533	508	482	457	433	410	388	367	347	328
	6×4×1/2	14×1/2	144.7	42.50	3.20	638	638	638	615	588	561	534	507	481	456	432	409	387	366
12×5/8	6×4×5/8	14×5/8	152.3	44.74	3.25	671	671	671	646	618	589	561	532	505	479	453	429	406	385
	6×4×5/8	14×5/8	159.9	46.94	3.24	704	704	704	678	647	617	587	558	529	501	474	449	425	402
	6×4×5/8	14×5/8	165.0	48.44	3.21	727	727	727	697	665	634	602	572	542	513	485	459	434	411
12×3/4	6×4×3/4	14×3/4	176.9	51.94	3.27	779	779	779	753	719	686	653	621	590	559	529	501	475	449
	6×4×3/4	14×3/4	188.9	55.44	3.33	832	832	832	808	774	740	705	670	637	605	574	544	516	488
	6×4×3/4	14×3/4	200.7	58.94	3.37	884	884	884	858	827	791	755	719	684	650	617	585	555	526
12×5/8	6×4×5/8	14×5/8	196.4	57.76	3.25	866	866	866	835	798	761	724	687	652	618	585	554	524	497
	6×4×5/8	14×5/8	208.4	61.26	3.30	919	919	919	891	852	814	775	737	700	664	629	596	565	536
	6×4×5/8	14×5/8	220.2	64.76	3.34	971	971	971	946	906	865	825	785	746	708	672	637	604	572
12×5/8	6×4×5/8	14×5/8	234.6	68.92	3.33	1034	1034	1034	1005	963	919	876	833	792	752	713	676	641	607
	6×4×5/8	14×5/8	212.6	62.44	3.41	937	937	937	919	882	843	805	767	730	694	659	626	594	564
	6×4×5/8	14×5/8	224.5	65.94	3.45	989	989	989	975	935	895	855	816	777	739	703	668	634	602
12×5/8	6×4×5/8	14×5/8	236.3	69.44	3.48	1042	1042	1042	1030	989	947	905	865	824	784	746	709	674	640
	6×4×5/8	14×5/8	248.3	72.94	3.51	1094	1094	1094	1085	1042	999	956	912	870	829	788	750	713	678
	6×4×5/8	14×5/8	260.3	76.44	3.54	1147	1147	1147	1140	1096	1051	1006	961	917	874	832	792	753	716
12×5/8	6×4×5/8	14×5/8	272.3	79.94	3.56	1199	1199	1199	1194	1149	1102	1055	1009	962	917	874	831	791	753
	6×4×5/8	14×5/8	283.9	83.44	3.58	1252	1252	1252	1252	1207	1153	1105	1056	1008	962	917	873	830	790
	6×4×5/8	14×5/8	295.9	86.94	3.60	1304	1304	1304	1304	1255	1205	1155	1104	1055	1006	959	913	869	828

Columns above heavy horizontal line have no metal above 1" thick.

Unequal Angles have short leg against web plate.

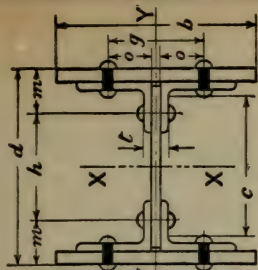
Weights given do not include rivets or other details.

Loads to right of heavy vertical lines are for Secondary Members ONLY.

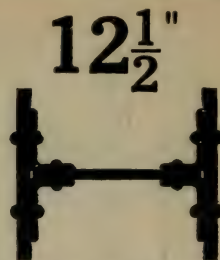
LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 12½" PLATE AND ANGLE COLUMNS WITH COVER PLATES

1 Web Plate	4 Angles	2 Cover Plates	DIMENSIONS							AXIS X-X				AXIS Y-Y			
			d	b	t	h	m	o	g	c	Riv.	I	S	r	I	S	r
12×3/8	6×4×3/8	14×3/8	13¼	14	1½	7½	2½	3½	7½	10¾	7/8	916	138.2	5.58	291	41.6	3.14
	6×4×5/16	14×1/2	13½	"	1½	"	"	"	"	"	"	1073	159.0	5.71	348	49.7	3.25
12×1/2	6×4×1/2	14×1/2	13½	14	1½	7½	2½	3½	7½	10¾	7/8	1136	168.3	5.68	368	52.6	3.23
	6×4×5/8	14×5/8	14	"	1½	"	"	"	"	10½	"	1197	177.4	5.65	388	55.4	3.22
12×5/8	6×4×5/8	14×5/8	14	14	1½	7½	2½	3½	7½	10¾	7/8	1215	180.0	5.58	394	56.3	3.18
	6×4×3/4	14×3/4	14	"	1½	"	"	"	"	10¾	"	1377	200.4	5.69	451	64.4	3.26
12×3/4	6×4×3/4	14×3/4	14½	14	1½	7½	2½	3½	7½	10¾	7/8	1437	209.0	5.67	472	67.4	3.25
	6×4×7/8	14×7/8	14½	"	1½	"	"	"	"	10¾	"	1495	217.5	5.64	492	70.3	3.24
12×5/8	6×4×5/8	14×5/8	14½	14	1½	7½	2½	3½	7½	10¾	7/8	1513	220.2	5.59	499	71.3	3.21
	6×4×3/4	14×3/4	14½	"	1½	"	"	"	"	10¾	"	1882	240.3	5.69	556	79.4	3.27
12×3/4	6×4×3/4	14×3/4	14½	14	1½	7½	2½	3½	7½	10¾	7/8	1856	260.6	5.79	613	87.6	3.33
	6×4×7/8	14×7/8	14½	"	1½	"	"	"	"	10¾	"	2035	280.7	5.88	671	95.8	3.37
12×5/8	6×4×5/8	14×5/8	14½	14	1½	7½	2½	3½	7½	10¾	7/8	1808	258.3	5.60	609	87.0	3.25
	6×4×3/4	14×3/4	14½	"	1½	"	"	"	"	10¾	"	1982	278.2	5.69	666	95.1	3.30
12×3/4	6×4×3/4	14×3/4	14½	14	1½	7½	2½	3½	7½	10¾	7/8	2161	298.1	5.78	723	103.3	3.34
	6×4×7/8	14×7/8	14½	"	1½	"	"	"	"	10¾	"	2085	292.6	5.64	710	101.4	3.29
12×5/8	6×4×5/8	14×5/8	14½	14	1½	7½	2½	3½	7½	10¾	7/8	2265	312.4	5.74	767	109.6	3.33
	6×4×3/4	14×3/4	14½	"	1½	"	"	"	"	10¾	"	2224	302.0	5.97	728	104.0	3.41
12×3/4	6×4×3/4	14×3/4	14½	14	1½	7½	2½	3½	7½	10¾	7/8	2418	322.4	6.06	785	112.1	3.45
	6×4×7/8	14×7/8	14½	"	1½	"	"	"	"	10¾	"	2618	343.3	6.14	842	120.3	3.48
12×5/8	6×4×5/8	14×5/8	14½	14	1½	7½	2½	3½	7½	10¾	7/8	2825	364.5	6.22	899	128.4	3.51
	6×4×3/4	14×3/4	14½	"	1½	"	"	"	"	10¾	"	3038	385.8	6.30	956	136.6	3.54
12×3/4	6×4×3/4	14×3/4	14½	14	1½	7½	2½	3½	7½	10¾	7/8	3259	407.4	6.38	1014	144.8	3.56
	6×4×7/8	14×7/8	14½	"	1½	"	"	"	"	10¾	"	3486	429.2	6.46	1071	153.0	3.58
12×5/8	6×4×5/8	14×5/8	14½	14	1½	7½	2½	3½	7½	10¾	7/8	3721	451.0	6.54	1128	161.1	3.60
	6×4×3/4	14×3/4	14½	"	1½	"	"	"	"	10¾	"						



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



Columns above heavy horizontal line have no metal above 1" thick.
Unequal Angles have short leg against web plate.
Dimensions h , m , o , and g can be varied considerably.

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14½" PLATE AND ANGLE COLUMNS

[For 14½" Columns with Cover Plates see following pages]

Web Plate	Angles	Weight Per Foot	Area Sq. in.	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET															
					6	8	10	12	14	16	18	20	22	24	26	28	30	32	34	36
14×1¼	3½×3×¼	33.5	9.74	1.29	146	134	118	104	90	79	68	60
	4×3×¾	35.1	12.70	1.38	151	180	151	142	125	110	97	85
	4×3×¾	35.1	10.26	1.32	151	151	137	123	110	96	87	78	69
	4×3×¾	43.9	13.42	1.62	201	201	185	168	151	136	122	109	98
14×5/16	4×3½×¾	48.3	14.18	1.59	213	212	194	175	157	141	126	113	101	90
	5×3½×¾	46.7	13.74	2.03	206	206	206	194	179	165	152	139	127	117	107	98	106
	4×3×¾	53.5	15.70	2.08	236	236	236	223	207	192	177	162	149	137	126	116	106
	4×3×¾	43.7	12.74	1.54	191	189	171	154	138	123	110	98	87
14×3/8	4×3½×¾	48.0	14.30	1.59	215	214	195	177	159	142	127	114	102
	4×3½×¾	51.3	15.06	1.56	226	224	204	184	165	147	131	117	105
	5×3½×¾	49.7	14.62	1.98	219	219	219	204	188	173	158	145	132	121	111	101	93
	6×4×7/8	56.5	16.58	2.04	249	249	249	234	217	201	184	169	155	142	130	119	109	109
14×3/8	4×3×¾	64.1	18.82	2.50	282	282	282	282	271	255	239	224	209	195	182	169	157
	4×3×¾	72.1	21.10	2.55	317	317	317	317	306	291	272	254	238	222	207	193	180
	4×3½×¾	51.9	15.17	1.57	228	226	206	186	167	149	133	119	106
	5×3½×¾	58.3	15.92	1.54	239	236	214	193	173	154	137	122	109
14×1/2	4×3½×¾	59.5	17.45	2.01	262	262	262	244	226	209	192	175	160	147	134	123	113
	4×3½×¾	65.9	19.37	2.06	291	291	291	274	255	235	217	199	182	167	153	140	129
	4×3½×¾	72.3	21.25	2.11	319	319	319	304	283	262	242	223	204	188	173	159	146
	6×4×7/8	67.1	19.69	2.46	295	295	295	295	282	265	248	232	216	201	187	174	162	151	140	...
14×1/2	4×3½×¾	75.1	21.97	2.52	330	330	330	330	317	299	281	263	246	229	214	199	185	173	161	...
	4×3½×¾	82.7	24.25	2.57	364	364	364	364	353	333	314	294	275	257	240	224	209	195	182	...
	6×6×7/8	77.5	22.69	2.30	340	340	340	335	315	294	274	255	236	218	202	187	173	160
	6×6×7/8	86.3	25.49	2.34	382	382	382	379	357	334	311	290	269	249	231	214	198	184
14×1/2	5×3½×¾	78.2	23.00	2.38	424	424	424	423	398	373	349	325	302	280	260	241	224	208
	6×4×7/8	91.0	26.68	2.07	345	345	345	326	303	280	258	237	218	199	183	168	155
	6×4×7/8	86.6	26.00	2.52	390	390	390	390	375	353	332	311	291	271	253	235	219	204	188	...
	6×6×7/8	96.2	28.24	2.56	424	424	424	424	410	387	364	341	320	298	278	260	242	226	211	178
14×5/8	4×3½×¾	103.8	30.44	2.60	457	457	457	457	445	420	396	372	348	326	304	284	265	248	231	216
	6×6×7/8	102.2	30.00	2.35	450	450	450	447	420	394	368	342	317	294	273	253	234	217
	6×6×7/8	111.4	32.72	2.39	491	491	491	490	462	434	405	378	351	326	303	281	260	242
	6×6×7/8	120.6	35.44	2.42	532	532	532	532	503	472	442	412	384	357	331	308	286	266
14×5/8	6×6×7/8	126.6	37.19	2.41	558	558	558	558	527	495	463	431	402	373	347	322	299	278
	6×6×7/8	144.6	42.51	2.47	638	638	638	638	609	573	537	502	468	436	406	377	351	326
	6×6×7/8	150.5	44.26	2.47	664	664	664	664	634	596	559	522	487	454	422	393	365	340
	6×6×7/8	168.1	49.42	2.53	741	741	741	741	714	674	633	593	554	517	482	449	419	390	364	340
14×3/4	6×6×7/8	168.1	49.42	2.53	741	741	741	741	714	674	633	593	554	517	482	449	419	390	364	340

Unequal Angles have short leg against web plate.

Weights given do not include rivets or other details.

Loads to right of heavy vertical lines are for Secondary Members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF $14\frac{1}{2}$ " PLATE AND ANGLE COLUMNS[For $14\frac{1}{2}$ " Columns with Cover Plates see following pages]

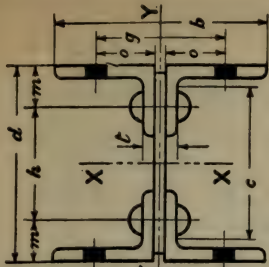
I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration

14½"

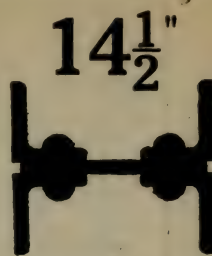
Web Plate	Angles	DIMENSIONS										AXIS X-X			AXIS Y-Y		
		d	b	t	h	m	o	g	c	Riv.	I	S	r	I	S	r	
14×1/4	3½ × 3 × ¼	14½	7¼	¾	11	13¼	2	4¼	13¼	¾	323	44.5	5.76	16	4.5	1.29	
	4 × 3 × ¼	"	8¼	¾	"	"	2½	5¼	13¼	"	444	61.2	5.91	24	5.8	1.38	
	4 × 3½ × ¾	"	8¼	1	"	"	3	5¼	13	"	349	44.7	5.83	24	5.8	1.52	
	5 × 3½ × ¾	14½	8¼	1	10½	2	2½	5¼	13	¾	492	67.8	5.98	35	8.6	1.62	
	5 × 3½ × ¾	"	10¼	1	"	"	3	6¼	13	"	489	67.5	5.97	36	8.7	1.59	
14×5/16	4 × 3 × 5/16	14½	8⅝	15/16	11	13¼	2½	5⅝	13¼	¾	431	59.4	5.82	30	7.3	1.54	
	4 × 3½ × ¾	"	"	11/16	10½	2	"	"	13	"	495	68.2	5.88	36	8.7	1.59	
	4 × 3½ × 5/16	14½	10⅝	15/16	10½	2	3	6⅝	13	¾	504	69.5	5.87	58	11.2	1.98	
	5 × 3½ × ¾	"	"	11/16	"	"	3½	7⅝	12⅞	"	583	80.4	5.93	69	13.4	2.04	
	6 × 4 × ¾	"	12⅝	13/16	9½	2½	3½	"	12⅝	"	667	92.0	5.95	117	19.0	2.50	
14×3/8	4 × 3 × ¾	14½	8⅝	11/8	11	13¼	2½	5⅝	13	¾	509	70.2	5.79	37	8.9	1.57	
	4 × 3½ × ¾	"	"	"	10½	2	3	6⅝	13	"	520	71.8	5.72	38	9.0	1.54	
	5 × 3½ × ¾	"	"	13/16	"	"	"	"	12⅞	"	597	82.3	5.85	71	13.6	2.01	
	5 × 3½ × 1½	"	"	13/8	"	"	"	"	12⅝	"	673	92.8	5.89	82	15.9	2.06	
	6 × 4 × ¾	"	"	"	"	"	"	"	"	"	745	102.7	5.92	95	18.3	2.11	
14×1/2	6 × 4 × ¾	14½	12⅝	11/8	9½	2½	3½	7⅝	12¾	¾	681	94.0	5.88	119	19.3	2.46	
	6 × 4 × 1½	"	"	11/4	"	"	"	"	12⅝	"	770	106.2	5.92	139	22.5	2.52	
	6 × 4 × 1½	"	"	13/8	"	"	"	"	12½	"	856	117.7	5.94	160	25.8	2.57	
	6 × 6 × ¾	"	"	11/8	7½	3½	"	"	12¾	"	696	95.9	5.53	120	19.4	2.30	
	6 × 6 × 1½	"	"	11/4	"	"	"	"	12⅝	"	789	108.8	5.56	140	22.6	2.34	
14×5/8	5 × 3½ × 1½	14½	10½	1½	10½	2	3	6½	12½	¾	879	121.2	5.58	160	25.8	2.38	
	6 × 4 × 5/8	"	12½	13/8	9½	2½	3½	7½	12¾	"	773	106.0	5.80	99	18.8	2.07	
	6 × 4 × 5/8	"	"	13/8	"	"	"	"	12¾	"	914	126.1	5.86	123	23.5	2.15	
	6 × 4 × 5/8	"	12½	15/8	"	"	3½	7½	12¾	"	884	122.0	5.83	165	26.4	2.52	
	6 × 6 × 5/8	"	"	13/4	"	"	"	"	12¾	"	969	133.6	5.86	186	29.7	2.56	
14×3/4	6 × 6 × 1½	14½	12½	1½	7½	3½	3½	7½	12½	¾	1031	145.0	5.88	206	33.0	2.60	
	6 × 6 × 5/8	"	"	13/8	"	"	"	"	12¾	"	907	125.1	5.50	166	26.5	2.35	
	6 × 6 × 5/8	"	"	15/8	"	"	"	"	12¾	"	992	136.8	5.51	187	30.0	2.39	
	6 × 6 × ¾	"	12⅝	11/4	7½	3½	3½	7⅝	12½	"	1077	148.6	5.52	208	33.3	2.42	
	6 × 6 × ¾	"	"	13/8	"	"	"	"	12½	"	1106	152.6	5.46	216	34.1	2.41	
14×3/4	6 × 6 × ¾	14½	12¾	11/2	7½	3½	3½	7¾	12	¾	1266	174.7	5.46	261	41.2	2.47	
	6 × 6 × ¾	"	"	13/8	"	"	"	"	11¾	"	1295	178.5	5.41	270	42.3	2.47	
14×3/4	6 × 6 × ¾	"	"	11/2	"	"	"	"	11¾	"	1447	199.6	5.41	316	49.5	2.53	

Unequal Angles have short leg against web plate.
Dimensions h, m, o, and g can be varied considerably.

Unequal Angles have short leg against web plate.
Dimensions h , m , o , and g can be varied considerably.



I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration



$14\frac{1}{2}$ "

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 14 1/2" PLATE AND ANGLE COLUMNS WITH COVER PLATES

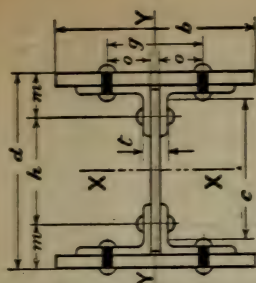
1 Web Plate	4 Angles	2 Cover Plates	Weight Per Foot	Area Sq. In.	Least Radius Gyr.	Unsupported Length In Feet															
						12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	44
14×3/8	6×4×3/8 1/2	14×3/8 1/2	102.8	30.19	3.10	453	453	448	428	408	387	367	348	329	311	293	277	261	247	233	
			110.8	32.47	3.09	487	487	481	460	438	416	394	373	353	333	314	297	280	264	248	
			118.4	34.75	3.09	521	521	515	492	468	445	422	399	377	357	336	318	300	283	266	
			124.3	36.50	3.14	548	548	544	520	496	472	448	424	402	380	359	339	320	303	285	
14×1/2	6×4×1/2 1/2	14×1/2 1/2	130.3	38.25	3.19	574	574	573	549	524	499	474	449	426	403	381	361	341	322	305	
			136.2	40.00	3.23	600	600	600	577	551	525	500	474	450	426	403	382	361	342	323	
			142.2	41.75	3.27	626	626	626	603	578	552	525	499	474	449	425	403	382	361	342	
			148.1	43.50	3.22	653	653	653	629	603	578	552	525	499	474	449	425	403	382	361	
14×5/8	6×4×5/8 1/2	14×5/8 1/2	169.3	49.69	3.17	745	745	743	711	678	645	613	581	551	521	492	466	440	416		
			181.2	53.19	3.23	798	798	798	767	732	698	664	631	598	566	536	507	480	454	430	
			193.2	56.69	3.29	850	850	850	823	787	751	716	680	646	613	581	550	521	494	467	
			205.0	60.19	3.34	903	903	903	879	842	804	767	729	693	658	625	592	562	532	504	
14×3/4	6×6×3/4 1/2	14×3/4 1/2	221.9	65.26	3.06	979	979	964	920	876	831	787	743	703	664	626	591	557	525		
			233.9	68.76	3.12	1031	1031	1022	978	932	885	840	796	752	711	672	635	599	566		
			245.7	72.26	3.17	1084	1084	1080	1034	986	939	892	845	801	757	716	677	640	606		
			263.3	77.42	3.43	1161	1161	1161	1142	1095	1048	1001	955	909	865	821	780	741	702		
14×5/8	6×6×5/8 1/2	14×5/8 1/2	276.9	81.42	3.50	1221	1221	1221	1210	1162	1114	1065	1017	970	923	879	835	794	754		
			288.3	84.69	3.56	1270	1270	1270	1265	1217	1168	1119	1069	1020	971	926	881	838	798		
			300.2	88.19	3.58	1323	1323	1323	1320	1270	1219	1168	1119	1069	1020	971	926	881	838		
			313.8	92.19	4.02	1383	1383	1383	1383	1340	1291	1244	1196	1148	1102	1056	1010	968	926		
14×5/8	6×6×5/8 1/2	14×5/8 1/2	327.4	96.19	4.05	1443	1443	1443	1443	1401	1351	1302	1252	1203	1154	1107	1061	1016			
			344.2	101.19	3.95	1518	1518	1518	1512	1459	1407	1353	1299	1247	1194	1143	1094	1046			
			357.8	105.19	3.98	1578	1578	1578	1575	1521	1466	1411	1356	1302	1249	1195	1144	1095			
			371.4	109.19	4.01	1638	1638	1638	1638	1584	1528	1471	1414	1357	1303	1248	1195	1144			
14×5/8	6×6×5/8 1/2	14×5/8 1/2	385.0	113.19	4.03	1698	1698	1698	1698	1647	1587	1532	1470	1412	1355	1298	1244				
			398.6	117.19	4.05	1758	1758	1758	1758	1706	1647	1587	1526	1466	1406	1349	1293				

Columns above heavy horizontal line have no metal above 1" thick.
Unequal angles have short leg against web plate.
Weights given do not include rivets or other details.
Loads to right of heavy vertical lines are for secondary members ONLY.

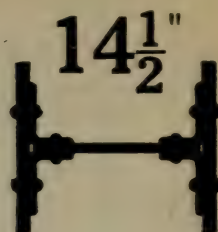
LOADS BY A. L. S. C. SPECIFICATION.

DIMENSIONS AND FUNCTIONS OF 14 1/2" PLATE AND ANGLE COLUMNS WITH COVER PLATES

1 Web Plate	4 Angles	2 Cover Plates	DIMENSIONS										AXIS X-X			AXIS Y-Y		
			d	b	t	h	m	o	g	c	Riv.	I	S	r	I	S	r	
14×3/8	6×4×3/8	14×3/8	15 1/4	14	1 1/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1262	166	6.46	391	41.6	4.10	
	6×4×3/8	14×3/8	15 1/4	14	1 1/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1351	177	6.45	311	44.4	3.09	
	6×4×3/8	14×3/8	15 1/4	14	1 1/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1437	189	6.42	331	47.3	3.09	
	6×4×3/8	14×3/8	15 1/4	14	1 1/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1539	200	6.50	360	51.4	3.14	
14×1/2	6×4×1/2	14×1/2	15 1/2	14	1 3/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1644	212	6.56	389	55.6	3.19	
	6×4×1/2	14×1/2	15 1/2	14	1 3/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1749	224	6.61	417	59.6	3.23	
	6×4×1/2	14×1/2	15 1/2	14	1 3/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1857	236	6.67	446	63.7	3.27	
	6×4×1/2	14×1/2	15 1/2	14	1 3/8	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1885	240	6.58	451	64.4	3.22	
14×5/8	6×4×5/8	14×5/8	16 1/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	1970	250	6.56	472	60.7	3.21	
	6×4×5/8	14×5/8	16 1/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2053	261	6.54	492	70.3	3.20	
	6×4×5/8	14×5/8	16 1/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2081	265	6.47	499	71.3	3.17	
	6×4×5/8	14×5/8	16 1/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2302	288	6.58	556	79.4	3.23	
14×3/4	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2529	311	6.68	613	87.6	3.29	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2762	335	6.78	671	95.8	3.34	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2517	315	6.21	613	87.6	3.06	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2741	338	6.32	670	95.7	3.12	
14×3/4	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	2977	361	6.42	727	103.8	3.17	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	3103	382	6.33	913	114.1	3.43	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	3371	409	6.43	998	124.8	3.50	
	6×4×3/4	14×3/4	16 1/2	14	1 3/4	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	3006	359	6.87	728	104.0	3.38	
14×5/8	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	3255	383	6.96	785	112.1	3.42	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	4087	432	7.05	842	120.3	3.45	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	3776	432	7.13	899	128.4	3.48	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	4048	456	7.22	956	136.5	3.51	
14×5/8	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	4327	481	7.30	1014	144.8	3.53	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	4615	506	7.38	1071	153.0	3.56	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	4910	531	7.46	1128	161.1	3.58	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	5120	561	7.45	1193	168.6	3.62	
14×5/8	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	5457	590	7.53	1257	197.4	3.65	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	5484	593	7.36	1581	197.6	3.95	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	5830	622	7.44	1666	208.2	3.98	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	6187	651	7.53	1752	219.0	4.01	
14×5/8	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	6552	681	7.61	1837	229.6	4.04	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	6928	711	7.66	1922	240.2	4.05	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	6928	711	7.66	1922	240.2	4.05	
	6×4×5/8	14×5/8	16 3/4	14	1 1/2	9 1/2	2 1/2	3 1/2	7 3/8	1 3/4	7/8	6928	711	7.66	1922	240.2	4.05	



I. is Moment of Inertia
S. is Section Modulus
r. is Radius of Gyration



Sections above heavy horizontal line have no metal above 1" thick.
Unequal angles have short leg against web plate.
Dimensions b, m, o and g can be varied considerably.

ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 10" CHANNEL COLUMNS WITH COVER PLATES

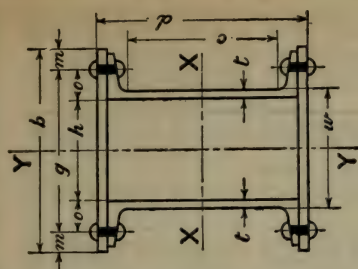
Channels	2 Cover Plates	Weight Per Foot	Area Sq. Inches	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET													
					14	16	18	20	22	24	26	28	30	32	34	36	38	40
10" × 15.3 #	12 × 1/4	51.0	14.19	3.62	213	213	213	205	197	189	181	173	165	157	150	143	136	129
		56.1	16.44	3.60	247	247	247	237	228	218	209	199	190	181	173	164	157	149
		61.2	17.94	3.59	269	269	269	259	248	238	228	217	207	197	188	179	170	162
		66.3	19.44	3.58	292	292	291	280	269	257	246	235	224	214	203	193	184	175
10" × 20.0 #	12 × 1/4	60.4	16.97	3.53	255	255	253	243	233	223	213	203	194	184	175	167	159	151
		65.5	19.22	3.52	288	288	286	275	264	252	241	230	219	208	198	188	179	170
		70.7	20.72	3.51	311	311	308	296	284	271	259	247	235	224	213	202	192	183
		75.7	22.22	3.51	333	333	330	317	304	291	278	265	252	240	228	217	206	196
10" × 25.0 #	12 × 1/4	80.8	23.72	3.51	356	356	353	339	325	311	297	283	269	256	244	232	220	209
		85.8	26.00	3.45	399	399	396	382	367	351	336	321	306	291	276	261	246	231
		90.8	28.66	3.45	400	400	394	378	362	346	330	314	299	284	270	257	243	231
		101.0	29.66	3.45	445	445	438	421	403	385	367	349	333	316	301	285	271	257
10" × 30.0 #	12 × 1/4	80.4	22.85	3.33	343	343	333	319	305	290	276	263	249	237	224	213	201	191
		85.5	25.10	3.34	377	377	367	351	335	320	304	289	275	261	250	234	222	210
		90.6	26.60	3.35	399	399	389	373	356	339	323	307	292	277	265	249	236	224
		100.8	29.60	3.36	444	444	433	415	397	378	360	343	325	309	293	278	263	250
10" × 35.0 #	12 × 1/4	111.0	32.60	3.37	489	489	478	458	438	418	398	378	359	341	323	307	291	276
		121.2	35.60	3.38	534	534	522	501	479	457	435	414	393	373	354	336	319	302
		90.4	25.79	3.25	387	387	373	356	340	323	307	291	276	261	247	234	222	210
		95.5	28.04	3.27	421	421	406	389	370	353	335	318	302	286	271	256	243	230
10" × 35.0 #	12 × 1/4	100.6	29.54	3.28	443	443	429	410	391	372	354	336	318	302	286	271	256	243
		110.8	32.54	3.30	488	488	473	453	432	412	392	372	353	334	317	300	284	269
		121.0	35.54	3.31	533	533	518	495	473	450	428	407	386	366	347	329	311	295
		131.2	38.54	3.33	578	578	562	539	514	490	466	443	421	399	378	358	340	322

The 1/4" Plates are tabulated with all weights of Channels, as adding some sectional area, without costing appreciably more than lattice bars and batten plates; 8 1/2% of their area is included in the functions and column areas.
Weights given do not include rivets or other details.
Loads to right of heavy vertical lines are for secondary members ONLY.

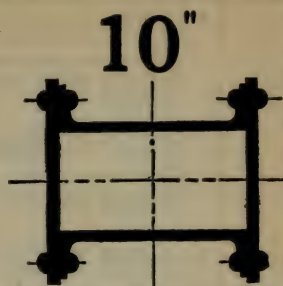
DIMENSIONS AND FUNCTIONS OF 10" CHANNEL COLUMNS WITH COVER PLATES

Channels	2 Cover Plates	DIMENSIONS										AXIS X-X			AXIS Y-Y		
		d	b	w	c	g	m	h	o	t	Riv.	I	S	r	I	S	r
10" × 15.3#	12 × 1/4	10 1/2	12	6 1/2	8 3/16	9	1 1/2	6	1 1/2	.240	3/4	272	51.8	4.38	186	31.0	3.62
	5/16	10 5/8	"	"	"	"	"	"	"	"	"	333	62.7	4.50	213	35.5	3.60
	3/8	10 3/4	"	"	"	"	"	"	"	"	"	376	70.0	4.58	231	38.5	3.59
	7/16	10 7/8	"	"	"	"	"	"	"	"	"	420	77.2	4.65	249	41.5	3.58
10" × 20.0#	1/2	11	12	6 1/2	8 3/16	9	1 1/2	5 3/4	1 5/8	.379	3/4	295	56.2	4.17	211	35.2	3.53
	5/16	10 5/8	"	"	"	"	"	"	"	"	"	356	67.1	4.31	238	39.7	3.52
	3/8	10 3/4	"	"	"	"	"	"	"	"	"	399	74.3	4.39	256	42.7	3.51
	7/16	10 7/8	"	"	"	"	"	"	"	"	"	443	81.5	4.46	274	45.7	3.51
10" × 25.0#	1/2	11	12	6 1/2	8 3/16	9	1 1/2	5 1/2	1 3/8	.526	3/4	319	60.8	4.00	236	39.4	3.45
	5/16	10 5/8	"	"	"	"	"	"	"	"	"	381	71.7	4.15	263	43.0	3.45
	3/8	10 3/4	"	"	"	"	"	"	"	"	"	424	78.8	4.23	281	46.0	3.45
	7/16	11 1/4	"	"	"	"	"	"	"	"	"	512	93.1	4.38	317	52.9	3.45
10" × 30.0#	5/8	11 1/4	"	"	"	"	"	"	"	"	"	605	107.5	4.52	353	58.9	3.45
	12 × 1/4	10 1/2	12	6 1/2	8 3/16	9	1 1/2	5 1/8	1 15/16	.673	3/4	344	65.5	3.88	253	42.1	3.33
	5/16	10 5/8	"	"	"	"	"	"	"	"	"	405	76.3	4.02	280	46.6	3.34
	3/8	10 3/4	"	"	"	"	"	"	"	"	"	448	83.4	4.10	298	49.6	3.35
10" × 35.0#	12 × 1/2	11 1/4	12	6 1/2	8 3/16	9	1 1/2	5 1/8	1 15/16	.673	3/4	537	97.6	4.26	334	55.6	3.36
	5/8	11 1/4	"	"	"	"	"	"	"	"	"	629	111.9	4.39	370	61.6	3.37
	3/4	11 1/2	"	"	"	"	"	"	"	"	"	726	126.3	4.52	406	67.6	3.38
	12 × 5/16	10 1/2	12	6 1/2	8 3/16	9	1 1/2	4 7/8	2 1/16	.820	3/4	368	70.2	3.78	275	45.9	3.25
10" × 35.0#	3/8	10 3/4	"	"	"	"	"	"	"	"	"	430	80.9	3.92	300	50.0	3.27
	5/8	11 1/4	"	"	"	"	"	"	"	"	"	473	87.9	4.00	318	53.0	3.28
	3/4	11 1/2	"	"	"	"	"	"	"	"	"	561	102.0	4.15	354	59.0	3.30
	5/4	11 3/4	"	"	"	"	"	"	"	"	"	654	116.2	4.29	390	65.0	3.31
10" × 35.0#	3/4	11 1/2	"	"	"	"	"	"	"	"	"	751	130.6	4.41	426	71.0	3.33

.875 of 12" × 1/4" plates used in areas and functions.



I. is Moment of Inertia.
S. is Section Modulus.
r. is Radius of Gyration.



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 12" CHANNEL COLUMNS WITH COVER PLATES

Channels	2 Cover Plates	Weight Per Foot	Area Sq. Inches	Least Radius Gyr.	UNSUPPORTED LENGTH IN FEET															
					18	20	22	24	26	28	30	32	34	36	38	40	42	44		
12" × 20.7#	14 × 1/4 5/16 3/8	65.2	17.31	4.38	260	260	259	251	243	235	227	218	210	202	195	187	180	172		
		71.2	20.81	4.33	312	312	310	301	291	281	271	261	251	241	232	223	214	205		
		77.1	22.56	4.30	338	338	336	325	314	303	292	281	271	260	250	240	230	221		
14 × 20.7#	14 × 7/16 1/2 5/8	83.1	24.31	4.29	365	365	361	350	338	326	315	303	291	280	269	258	248	238		
		89.0	26.06	4.27	391	391	387	374	362	349	336	324	311	299	287	275	264	253		
		100.9	29.56	4.24	443	443	438	424	409	394	380	366	351	338	324	311	298	286		
14 × 25.0#	14 × 1/4 5/16 3/8	73.8	19.89	4.29	298	298	296	286	277	267	257	248	238	229	220	211	203	194		
		79.8	23.39	4.25	351	351	347	335	324	312	301	290	279	268	257	246	236	226		
		85.7	25.14	4.24	377	377	372	360	348	335	323	311	299	287	276	265	253	243		
14 × 30.0#	14 × 1/2 5/8 3/4	91.7	26.89	4.23	404	404	398	385	372	358	345	332	319	307	294	282	271	259		
		97.6	28.64	4.22	430	430	423	410	396	381	367	353	339	326	313	300	288	276		
		109.5	32.14	4.20	482	482	474	459	443	427	411	395	380	365	350	335	321	308		
14 × 35.0#	14 × 1/4 5/16 3/8	83.8	22.83	4.20	343	343	337	326	315	303	292	281	270	259	248	238	228	219		
		89.8	26.33	4.18	395	395	388	375	362	349	336	323	310	298	285	273	262	251		
		95.7	28.08	4.17	421	421	413	400	386	372	358	344	330	317	304	291	279	267		
14 × 30.0#	14 × 1/2 5/8 3/4	107.6	31.58	4.16	474	474	465	449	433	417	401	386	370	356	341	327	313	300		
		119.5	35.08	4.15	526	526	516	498	481	463	445	428	411	394	378	362	347	333		
		131.4	38.58	4.14	579	579	566	547	528	508	489	470	451	433	415	398	381	365		
14 × 35.0#	14 × 1/4 5/16 3/8	93.8	25.77	4.12	387	387	378	365	352	339	326	313	300	288	276	264	253	242		
		99.8	29.27	4.11	439	439	429	414	399	384	369	355	341	326	313	300	287	275		
		105.7	31.02	4.10	465	465	454	438	422	407	391	375	360	345	331	317	304	291		
14 × 35.0#	14 × 5/8 3/4 1/2	117.6	34.52	4.10	518	518	505	488	470	453	435	418	401	384	368	353	338	323		
		129.5	38.02	4.09	570	570	556	536	517	498	478	459	441	422	405	388	371	355		
		141.4	41.52	4.08	623	623	607	586	565	543	522	502	481	461	442	424	406	388		
14 × 40.0#	14 × 1/4 5/16 3/8	153.4	45.02	4.08	675	675	657	635	612	588	565	543	521	499	479	458	438	420		
		165.2	48.52	4.08	728	728	708	684	659	634	609	585	561	538	516	493	473	452		
		181.4	52.02	4.07	781	781	759	733	707	681	655	629	603	577	551	525	500	474		
14 × 40.0#	14 × 1/2 5/8 3/4	103.8	28.71	4.04	431	431	418	403	388	373	359	344	330	316	303	289	277	265		
		109.8	32.21	4.04	483	483	469	452	436	419	402	386	370	355	340	325	311	298		
		115.7	33.96	4.04	509	509	494	477	459	441	424	407	390	374	358	342	328	314		
14 × 40.0#	14 × 1/2 5/8 3/4	127.6	37.46	4.04	562	562	545	526	506	487	468	449	430	412	395	378	361	346		
		139.5	40.96	4.04	614	614	596	575	554	532	512	491	471	451	432	413	395	378		
		151.4	44.46	4.04	667	667	647	624	601	578	555	533	511	490	469	448	429	411		
14 × 40.0#	14 × 3/4 1/2 5/8	163.4	47.96	4.04	719	719	698	673	648	623	599	575	551	528	505	483	463	443		
		175.2	51.46	4.04	772	772	749	722	696	669	643	616	591	567	542	519	497	475		

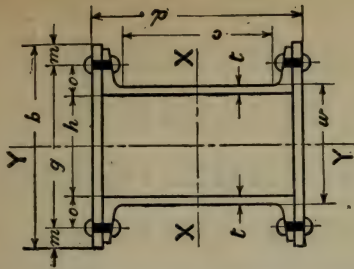
The 1/4" Plates are tabulated with all weights of Channels, as adding some sectional area, without costing appreciably more than lattice bars and batten plates:
 75% of their area is included in the weights of Channels and column areas.
 Weights given do not include Rivets or other details.
 Loads to right of heavy vertical lines are for secondary members ONLY.

LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 12" CHANNEL COLUMNS WITH COVER PLATES

Channels	Cover Plates	DIMENSIONS										AXIS X-X			AXIS Y-Y		
		d	b	w	c	g	m	h	o	t	Riv.	I	S	r	I	S	r
12" × 20.7#	14 × 1/4	12 1/2	14	8	10	11	1 1/2	7 1/2	1 3/4	.280	3/4	453	72.5	5.12	332	47.5	4.38
	14 × 5/16	12 5/8	"	"	"	"	"	"	"	"	"	588	93.1	5.31	390	55.6	4.33
	14 × 3/8	13 1/4	"	"	"	"	"	"	"	"	"	658	103.3	5.40	418	59.7	4.30
	14 × 7/16	12 7/8	14	8	10	11	1 1/2	7 1/2	1 3/4	.280	3/4	731	113.6	5.48	447	63.8	4.29
12" × 25.0#	14 × 1/2	13	14	8	10	11	1 1/2	7 1/2	1 3/4	.387	3/4	804	123.7	5.56	475	67.9	4.27
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	954	143.9	5.68	532	76.1	4.24
	14 × 3/4	12 1/2	14	8	10	11	1 1/2	7 1/4	1 7/8	.387	3/4	484	77.4	4.93	366	52.3	4.29
	14 × 7/8	12 5/8	"	"	"	"	"	"	"	"	"	619	98.0	5.14	423	60.5	4.25
12" × 30.0#	14 × 1	13 1/4	14	8	10	11	1 1/2	7 1/4	1 7/8	.387	3/4	689	108.1	5.23	452	64.5	4.24
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	835	128.4	5.40	509	72.7	4.22
	14 × 3/4	12 5/8	14	8	10	11	1 1/2	7	2	.510	3/4	984	148.6	5.53	566	80.9	4.20
	14 × 7/8	13	14	8	10	11	1 1/2	7	2	.510	3/4	870	133.9	5.25	546	78.0	4.16
12" × 35.0#	14 × 1	13 1/2	14	8	10	11	1 1/2	6 3/4	2 1/8	.632	3/4	1020	153.9	5.39	603	86.2	4.15
	14 × 5/8	13 1/4	"	"	"	"	"	"	"	"	"	1176	174.2	5.52	661	94.4	4.14
	14 × 3/4	12 7/8	14	8	10	11	1 1/2	6 3/4	2 1/8	.632	3/4	555	88.7	4.64	437	62.4	4.12
	14 × 7/8	13	"	"	"	"	"	"	"	"	"	689	109.2	4.85	494	70.5	4.11
12" × 40.0#	14 × 1	13 3/4	14	8	10	11	1 1/2	6 3/4	2 1/8	.632	3/4	760	119.2	4.95	522	74.6	4.10
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	905	139.2	5.12	580	82.8	4.10
	14 × 3/4	12 5/8	14	8	10	11	1 1/2	6 3/4	2 1/8	.632	3/4	1055	159.2	5.27	637	91.0	4.09
	14 × 7/8	13	"	"	"	"	"	"	"	"	"	1212	179.5	5.40	694	99.1	4.09
12" × 40.0#	14 × 1	13 3/4	14	8	10	11	1 1/2	6 1/2	2 1/4	.755	3/4	1374	199.8	5.52	751	107.3	4.08
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	1543	220.3	5.64	808	115.5	4.08
	14 × 3/4	12 7/8	14	8	10	11	1 1/2	6 1/2	2 1/4	.755	3/4	590	94.4	4.53	469	67.0	4.04
	14 × 7/8	13	"	"	"	"	"	"	"	"	"	725	114.8	4.71	526	75.1	4.04
12" × 40.0#	14 × 1	13 3/4	14	8	10	11	1 1/2	6 1/2	2 1/4	.755	3/4	795	124.7	4.84	554	79.2	4.04
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	940	144.6	5.01	612	87.4	4.04
	14 × 3/4	12 5/8	14	8	10	11	1 1/2	6 1/2	2 1/4	.755	3/4	1090	164.6	5.16	669	95.5	4.04
	14 × 7/8	13	"	"	"	"	"	"	"	"	"	1247	184.7	5.29	726	103.7	4.04
12" × 40.0#	14 × 1	13 3/4	14	8	10	11	1 1/2	6 1/2	2 1/4	.755	3/4	1409	204.9	5.42	783	111.9	4.04
	14 × 5/8	13 1/2	"	"	"	"	"	"	"	"	"	1578	225.4	5.53	840	120.0	4.04
	14 × 3/4	12 7/8	"	"	"	"	"	"	"	"	"						
	14 × 7/8	13	"	"	"	"	"	"	"	"	"						

.75 of 14" × 1/4" plates used in areas and functions.



L is Moment of Inertia.
S is Section Modulus.
r is Radius of Gyration



ALLOWABLE CONCENTRIC LOADS IN KIPS FOR 15" CHANNEL COLUMNS WITH COVER PLATES

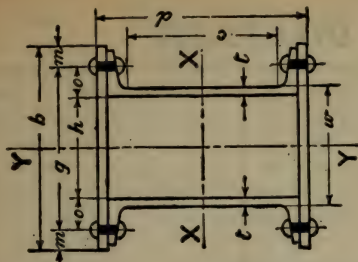
Channels	2 Cover Plates	Weight Per Foot	Area Sq. Inches	Least Radius Gyri.	UNSUPPORTED LENGTH IN FEET															
					20	22	24	26	28	30	32	34	36	38	40	42	44	46		
15" × 33.9 #	16 × 1/4	95.0	25.05	5.12	376	376	376	374	364	354	343	333	323	313	303	293	283	274		
		108.6	31.80	5.02	477	477	477	471	458	445	432	419	405	392	379	367	355	342		
		115.4	33.80	5.00	507	507	507	500	486	473	458	444	430	416	402	389	376	363		
		122.2	35.80	4.98	537	537	537	529	514	499	484	469	454	439	425	411	397	383		
15" × 35.0 #	16 × 1/2	135.8	39.80	4.94	597	597	597	586	570	553	537	520	503	486	470	454	438	423		
		149.4	43.80	4.91	657	657	657	644	625	607	589	570	551	533	515	498	480	463		
		97.2	25.71	5.07	386	386	386	382	372	361	351	340	330	319	309	299	289	279		
		110.8	32.46	4.98	487	487	487	480	467	453	439	426	412	398	385	372	360	348		
15" × 40.0 #	16 × 5/8	124.4	36.46	4.94	547	547	547	537	522	507	491	476	461	446	430	416	401	387		
		138.0	40.46	4.91	607	607	607	595	578	561	544	526	509	492	475	460	443	428		
		151.6	44.46	4.89	667	667	667	653	634	615	596	577	558	540	521	503	486	469		
		165.2	48.46	4.87	727	727	727	710	690	669	648	628	607	586	566	547	528	509		
15" × 45.0 #	16 × 3/4	107.2	28.65	5.02	430	430	430	425	413	401	389	377	365	354	342	331	319	308		
		120.8	35.40	4.95	531	531	531	522	507	492	478	463	448	433	418	404	391	377		
		134.4	39.40	4.92	591	591	591	580	563	546	530	513	496	480	464	448	433	417		
		148.0	43.40	4.89	651	651	651	637	619	600	582	563	545	527	509	491	474	457		
15" × 50.0 #	16 × 1 1/8	161.6	47.40	4.87	711	711	711	695	675	655	634	614	593	574	554	535	516	498		
		175.2	51.40	4.85	771	771	771	752	730	708	686	664	642	620	599	578	558	538		
		117.2	31.59	4.93	474	474	474	465	452	439	426	412	399	385	372	360	347	335		
		144.4	42.34	4.86	635	635	635	620	602	584	568	548	530	512	495	477	460	444		
15" × 50.0 #	16 × 1 1/2	158.0	46.34	4.84	695	695	695	677	658	638	618	598	578	558	539	520	502	484		
		171.6	50.34	4.82	755	755	755	735	713	692	670	648	627	605	584	564	544	524		
		185.2	54.34	4.80	815	815	815	792	769	745	722	698	674	652	629	606	585	564		
		198.8	58.34	4.79	875	875	875	849	824	799	774	749	723	698	674	650	627	604		
15" × 50.0 #	16 × 1 3/4	212.4	62.34	4.78	935	935	934	907	880	853	826	799	772	745	719	694	669	645		
		226.0	66.34	4.77	995	995	993	965	936	907	878	849	820	792	764	737	711	685		
		127.2	34.53	4.89	518	518	518	507	492	478	463	448	434	419	405	391	377	364		
		154.4	45.28	4.83	679	679	679	662	643	623	603	584	564	545	526	508	490	472		
15" × 50.0 #	16 × 1 7/8	168.0	49.28	4.81	739	739	739	719	698	677	655	634	613	592	571	551	531	512		
		181.6	53.28	4.80	799	799	799	777	754	731	708	684	661	639	616	595	573	553		
		195.2	57.28	4.79	859	859	859	834	809	785	760	735	710	686	662	638	616	593		
		208.8	61.28	4.78	919	919	918	892	865	838	812	785	759	732	707	682	658	634		
15" × 50.0 #	18 × 1 1/2	222.4	65.28	4.77	979	979	977	949	921	892	864	836	807	779	752	725	699	674		
		236.0	69.28	4.76	1039	1039	1036	1007	977	946	916	885	856	826	797	768	741	714		
		130.6	34.53	5.07	518	518	518	518	507	492	478	463	448	434	419	405	391	377		
		191.8	56.28	5.59	844	844	844	844	844	823	803	782	761	740	719	698	677	657		
15" × 50.0 #	18 × 1 3/4	207.2	60.78	5.56	912	912	912	912	909	887	865	842	819	796	774	751	729	707		
		222.4	65.28	5.54	979	979	979	979	979	957	932	908	885	862	839	816	793	770		
		237.7	69.78	5.51	1047	1047	1047	1047	1041	1015	989	963	936	910	883	858	832	807		
		253.0	74.28	5.49	1114	1114	1114	1114	1107	1079	1051	1023	995	966	938	911	883	856		
15" × 50.0 #	18 × 1 7/8	268.4	78.78	5.48	1182	1182	1182	1182	1173	1144	1114	1084	1054	1024	994	964	935	906		
		283.6	83.28	5.46	1249	1249	1249	1249	1238	1208	1176	1144	1112	1080	1048	1018	987	956		

The 1/4" plates are tabulated with all weights of Channels, as adding some sectional area, without costing appreciably more than lattice bars and batten plates; 65% of the 16" × 1/4" and 58 1/3% of the 18" × 1/4" plates are included in the functions and column areas. Weights given do not include Rivets or other details.

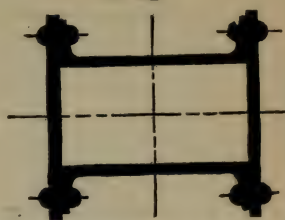
LOADS BY A. I. S. C. SPECIFICATION

DIMENSIONS AND FUNCTIONS OF 15" CHANNEL COLUMNS WITH COVER PLATES

15"



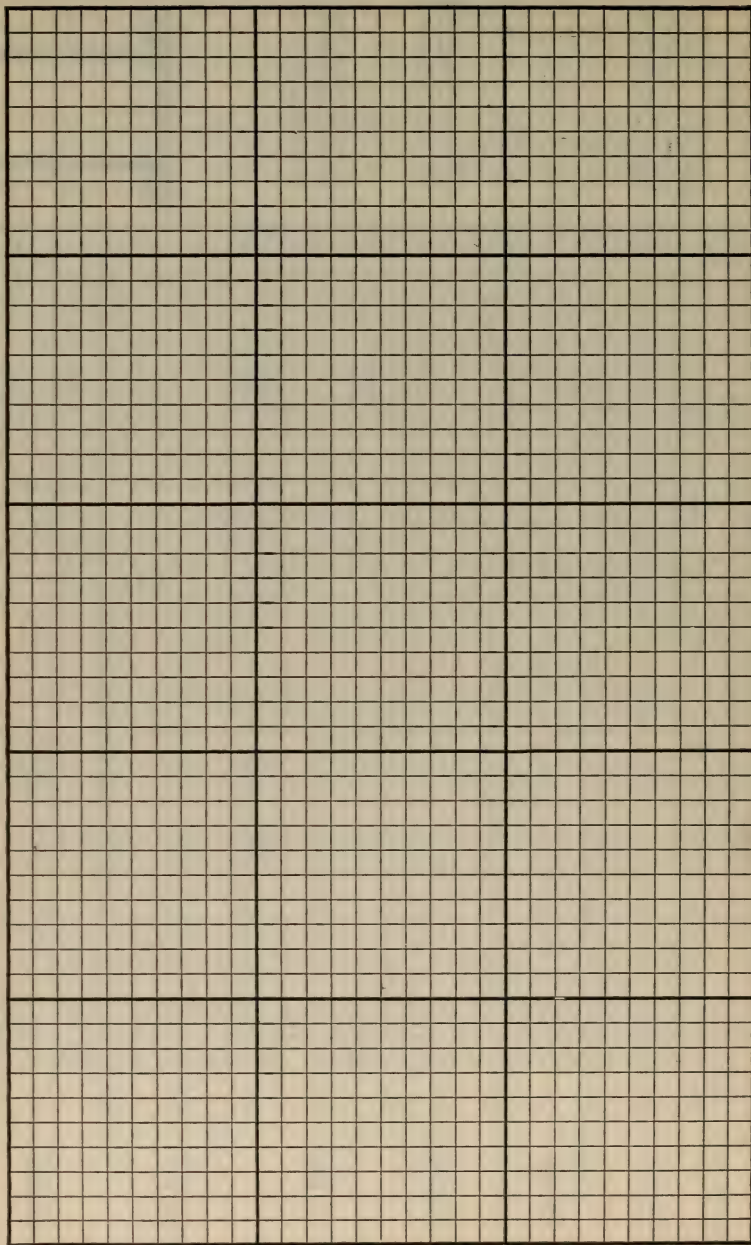
I is Moment of Inertia.
S is Section Modulus.
r is Radius of Gyration.



Channels	Cover Plates	DIMENSIONS										AXIS X-X			AXIS Y-Y		
		d	b	w	c	g	m	h	o	t	Riv.	I	S	r	I	S	r
15" x 33.9#	16 x 1/4	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.400	7/8	930	120.1	6.09	657	82.1	5.12
	15 3/4	15 3/4	"	"	"	"	"	"	"	"	"	1334	169.4	6.48	801	105.1	5.02
	15 7/8	15 7/8	"	"	"	"	"	"	"	"	"	1459	183.9	6.57	843	105.4	5.00
	16 x 1/2	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.400	7/8	1587	198.3	6.66	886	110.7	4.98
	16 1/4	16 1/4	"	"	"	"	"	"	"	"	"	1846	227.3	6.81	971	121.4	4.94
15" x 35.0#	16 1/2	16 1/2	"	"	"	"	"	"	"	"	"	2115	256.3	6.95	1057	132.1	4.91
	16 x 3/8	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.422	7/8	943	121.6	6.06	661	82.7	5.07
	15 3/4	15 3/4	"	"	"	"	"	"	"	"	"	1347	171.0	6.44	805	100.7	4.98
	16	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.422	7/8	1599	199.9	6.62	891	111.4	4.94
	16 x 5/8	16 1/4	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	"	"	1859	228.8	6.78	976	122.0	4.91
15" x 40.0#	16 x 3/4	16 1/2	"	"	"	"	"	"	"	"	"	2107	257.8	6.92	1061	132.7	4.89
	16 3/4	16 3/4	"	"	"	"	"	"	"	"	"	2403	287.0	7.04	1147	143.4	4.87
	16 x 7/8	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.520	7/8	998	128.7	5.90	723	90.3	5.02
	15 3/4	15 3/4	"	"	"	"	"	"	"	"	"	1402	178.0	6.29	867	108.3	4.95
	16	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.520	7/8	1654	206.8	6.48	952	119.0	4.92
15" x 45.0#	16 x 1 1/8	16 1/4	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	"	"	1914	235.5	6.64	1037	129.7	4.89
	17	16 3/4	"	"	"	"	"	"	"	"	"	2182	264.5	6.78	1123	140.3	4.87
	17 1/4	16 3/4	"	"	"	"	"	"	"	"	"	2458	293.5	6.92	1208	151.0	4.85
	17 1/2	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.618	7/8	1053	135.9	5.77	769	96.1	4.93
	16 x 1 1/2	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	"	"	1709	213.7	6.35	998	124.8	4.86
15" x 50.0#	16 1/2	16 1/2	"	"	"	"	"	"	"	"	"	1969	242.4	6.52	1084	135.5	4.84
	16 3/4	16 3/4	"	"	"	"	"	"	"	"	"	2237	271.2	6.67	1169	146.1	4.82
	16 x 7/8	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.618	7/8	2514	300.1	6.80	1254	156.8	4.80
	17	16 1/4	"	"	"	"	"	"	"	"	"	2798	329.2	6.93	1340	167.5	4.79
	17 1/4	16 1/4	"	"	"	"	"	"	"	"	"	3092	358.4	7.04	1425	178.1	4.78
15" x 50.0#	17 1/2	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.716	7/8	3393	387.8	7.15	1510	188.8	4.77
	16 x 1 3/4	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	"	"	1108	143.0	5.67	827	103.3	4.89
	17	16 1/2	"	"	"	"	"	"	"	"	"	1764	220.5	6.24	1056	132.0	4.83
	17 1/4	16 1/4	"	"	"	"	"	"	"	"	"	2024	249.1	6.41	1141	142.7	4.81
	17 1/2	16 3/4	"	"	"	"	"	"	"	"	"	2292	277.8	6.56	1227	153.3	4.80
15" x 50.0#	16 x 1 1/2	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.716	7/8	2569	306.7	6.70	1312	164.0	4.79
	17	16 1/4	"	"	"	"	"	"	"	"	"	2854	335.8	6.82	1397	174.7	4.78
	17 1/4	16 1/4	"	"	"	"	"	"	"	"	"	3147	364.8	6.94	1483	185.3	4.77
	17 1/2	16 3/4	"	"	"	"	"	"	"	"	"	3448	394.1	7.06	1568	196.0	4.76
	18	15 1/2	18	11 1/2	12 3/8	15	1 1/2	10 3/4	2 1/8	.716	7/8	1108	143.0	5.67	1170	130.1	5.82
15" x 50.0#	16 x 3/4	15 1/2	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.716	7/8	2478	300.4	6.64	1758	195.3	5.59
	16 1/2	16 1/2	"	"	"	"	"	"	"	"	"	2789	333.1	6.77	1879	208.8	5.56
	16 3/4	16 3/4	"	"	"	"	"	"	"	"	"	3110	365.9	6.90	2001	222.3	5.54
	17	16	16	9 1/2	12 3/8	13	1 1/2	8 3/4	2 1/8	.716	7/8	3440	398.8	7.02	2122	235.8	5.51
	17 1/4	16 1/4	"	"	"	"	"	"	"	"	"	3719	431.9	7.13	2244	249.3	5.49
15" x 50.0#	17 1/2	16 3/4	"	"	"	"	"	"	"	"	"	4129	465.2	7.24	2365	262.8	5.48
	18	16 1/2	"	"	"	"	"	"	"	"	"	4488	498.7	7.34	2487	276.3	5.46

.65625 of 16" x 1/4" plates used in areas and functions.
.58333 of 18" x 1/4" plates used in areas and functions.

NOTES and DIAGRAMS



Part IV

Section 14

Steel Slab Column Bases

SOLID STEEL SLABS FOR COLUMN BASES

The size of slabs that can now be rolled is limited by the size of the ingot produced and the capacity of the rolling mill. Slabs have been rolled up to 120" x 120" x 9" thick, weighing 36,000 #, and can be rolled up to 12" thick and weighing 40,000 #.

Rolled steel slabs, especially those 2" thick and over, are likely to be more or less bowed flatwise. If the material is sheared hot there will be 3" to 5" of deformation adjacent to the shear. All slabs over 2½" thick and those 2½" thick with a carbon content of more than .25% must be cut with a flame cutting torch. Slabs cut with the flame cutting torch do not show deformation adjacent to the cut. All slabs 4" and under in thickness can be straightened by a press, but those thicker than 4" must be machine faced where accuracy is required.

When ordering material for rolled steel slabs the following is suggested:

Specify ordinary Open Hearth steel with a carbon content of .10% to .25% and without incorporating the same physical requirements as fixed for structural steel.

Show finished dimensions only and state whether material is required hot sheared or flame cut to length.

Show what machining is to be done, namely on one face, both faces, or possibly both faces and four edges.

The mill should be instructed to add to these specified dimensions sufficient material to allow for machined finish.

Below is a table giving the width and thickness of material as usually rolled for slab use. The range of sizes will be found sufficient to cover any but very special cases, and as stated above the mills are now able to furnish slabs up to 12" in thickness and 40,000 # in weight.

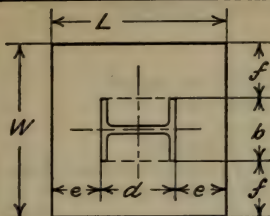
TABLE I
AVAILABLE SIZES OF STEEL SLABS

Width	Thick- ness	Length	Weight per Linear In.	Width	Thick- ness	Length	Weight per Linear In.
16"	2"	6'-8" to 60'-0"	9.07	44"	6	11'-3" to 14'-2"	74.80
20	2	6'-8" to 50'-0"	11.33	48	5½	11'-3" to 14'-0"	74.80
20	2½	6'-8" to 36'-8"	14.17	48	6	11'-3" to 14'-0"	81.60
24	2½	6'-8" to 36'-8"	17.00	48	6½	9'-7" to 12'-0"	88.40
24	3	6'-8" to 24'-2"	20.40	52	6	11'-3" to 14'-7"	88.40
28	3	6'-8" to 24'-2"	23.80	52	6½	9'-7" to 12'-6"	95.77
28	3½	6'-8" to 18'-4"	27.77	56	6½	10'-0" to 11'-8"	103.10
32	3½	6'-8" to 18'-4"	31.73	56	7	10'-0" to 11'-8"	111.07
32	4	6'-8" to 18'-4"	36.27	60	7		119.00
36	4	6'-8" to 22'-11"	40.80	60	8		136.00
36	4½	6'-8" to 22'-11"	45.90	66	8		149.60
40	4½	6'-8" to 20'-10"	51.00	66	9		168.30
40	5	6'-8" to 20'-10"	56.67	72	9		183.60
44	5	13'-9" to 17'-1"	62.33	72	10		204.00
44	5½	11'-3" to 14'-2"	68.57				

TABLE II
AVERAGE ALLOWABLE UNIT PRESSURES ON MASONRY IN POUNDS PER SQUARE INCH

Common Brick	—	Lime Mortar	=	100	Sandstone	—	Port. Cem. Mortar	=	400
Rubble Masonry	—	Lime Mortar	=	150	Limestone	—	Port. Cem. Mortar	=	500
Common Brick	—	Port. Cem. Mortar	=	200	Concrete	—	Port. Cement 1:2:4	=	600
Rubble Masonry	—	Port. Cem. Mortar	=	200	Granite	—	Port. Cem. Mortar	=	800
Hard Brick	—	Port. Cem. Mortar	=	250					

SOLID STEEL SLABS FOR COLUMN BASES



- C = Total Load on Column in pounds
 L = Length of Slab in inches
 W = Width of Slab in inches
 d = depth of Column in inches
 b = width of Column in inches
 A = Area of the Slab = $L \times W$
 U = Unit pressure per square inch on lower side of slab = $C \div A$

The column is assumed as having uniform bearing on the slab over the entire area of the milled end of the column shaft. It is also assumed that a part of the slab which is the smallest rectangle which will enclose the column cross section will act as a continuation of the column and that the maximum bending moment in the slab will occur at the sides of this rectangle. While these assumptions are empirical they are considered conservative since for the sake of simplicity in the calculations various other factors are omitted which if considered would materially add to the strength of the slab.

The determining bending moment will occur on that side of the enclosing rectangle for which the overhang "e" or "f" is greatest. In the following calculation a section of the slab is considered which is one inch in width and "t" inches in depth.

The square of the required slab thickness "t" is obtained as given below:—

$$M = \text{Moment for 1" width of slab} = U \times e \times \frac{e}{2} = \frac{U \times e^2}{2} \text{ or } \frac{U \times f^2}{2} \quad (1)$$

$$S = \text{Sec. Mod. for 1" width of slab} = \frac{M}{18000} = \frac{U \times e^2}{36000} \text{ or } \frac{U \times f^2}{36000} \quad (2)$$

$$\text{Since } S = t^2 \div 6 \therefore t^2 = \frac{U \times e^2}{6000} \text{ or } \frac{U \times f^2}{6000} \quad (3)$$

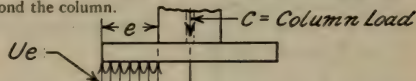
Having the value of t^2 , the required slab may be selected from table III, which is arranged to show the value of t^2 or usual available thicknesses.

Slabs 4" and less in thickness can be straightened and do not require planing. For slabs over 4" there has been deducted $\frac{1}{4}$ " for planing under the column and also $\frac{3}{8}$ " for planing the bottom surface when required.

EXPLANATION OF STRESS FORMULAE

Slabs:—The stresses on the slab are considered as those of an inverted cantilever in which the length of the cantilever is the amount of the projection of the slab beyond the column.

$$\text{Max. Moment} = Ue \times \frac{e}{2}$$



Grillage:—The stresses on the grillage beams are considered as those of a simple beam, and the Max. Moment therefore occurs at the center.

$$\begin{aligned}
 \text{Max. Moment} &= \frac{C}{2} \times \frac{l}{4} - \frac{C}{2} \times \frac{l}{4} \\
 &= \frac{C}{2} \left(\frac{l-l}{4} \right) \\
 &= \frac{C(l-l)}{8}
 \end{aligned}$$

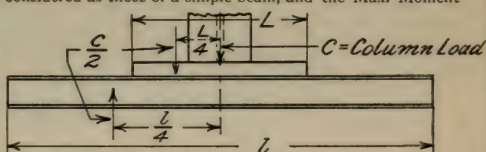
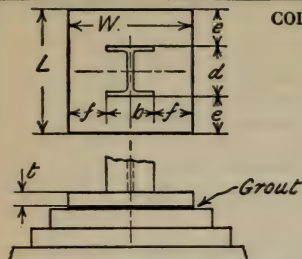


TABLE III
VALUES FOR t^2 FOR VARIOUS THICKNESSES

t²	Slab thickness			t²	Slab thickness		
	Rough	Machine faced			Rough	Machine faced	
		Top only	Top & Bottom			Top only	Top & Bottom
6.25	2½			39.06	6½		
9.00	3			40.64	7		6¾
12.25	3½			45.56	7	6¾	
16.00	4			54.39	8		7¾
15.02	4½		3⅞	60.06	8	7¾	
18.06	4½	4¼		70.14	9		8¾
19.14	5		4¾	76.56	9	8¾	
22.56	5	4¾		87.89	10		9¾
23.77	5½		4⅞	95.06	10	9¾	
27.56	5½	5¼		107.64	11		10¾
28.90	6		5¾	115.56	11	10¾	
33.06	6	5¾		129.39	12		11¾
34.51	6½		5⅞	138.06	12	11¾	

SOLID STEEL SLABS FOR COLUMN BASES

COLUMN BASE RESTING UPON MASONRY



- C** = Total Load on Column in pounds
L = Length of Slab in inches
W = Width of Slab in inches
t = Thickness of Slab in inches
U = Allowable Unit Pressure on Masonry (Table II)
A = Area of the Slab base in square inches = $C \div U$

The area of the slab base must first be computed from the Unit Pressure allowed on the type of Masonry to be used for the foundation and the Load on the Column. $A = C \div U$

Select a slab having a rolled width of one of the dimensions L or W (see Table I). The thickness of the slab is then computed as shown on the preceding page.

Slab bases resting on masonry need not be machine faced on the bottom but should be grouted.

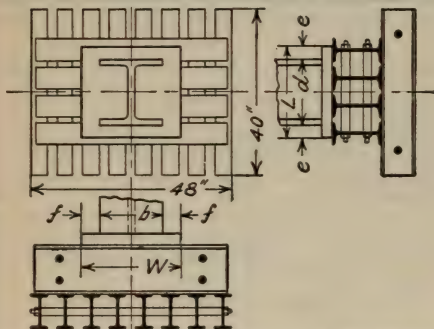
Example:—

Column Load = 960000 # ; Column dimensions, $d = 15.75"$ and $b = 15.25"$; Unit Pressure on Masonry, $U = 600$
 Then $A = 960000 \div 600 = 1600$ sq. inches = $40" \times 40"$ Slab base

Then $e = \frac{40 - 15.75}{2} = 12.125$ and $f = \frac{40 - 15.25}{2} = 12.375$ $\therefore t^2 = 600 \times 12.375 \times 12.375 \div 6000 = 15.31$

This value of t^2 requires a slab $4\frac{1}{2}"$ thick machine faced on top. (Table III)

COLUMN BASE RESTING UPON GRILLAGE



- C** = Total Load on Column in pounds
L = Length of Slab in inches
W = Width of Slab in inches
t = Thickness of Slab in inches
U = Allowable Unit Pressure on Masonry (Table II)
A = Area of the Slab base in square inches = $C \div U$

The area of the grillage is determined by the Unit pressure allowed on the type of Masonry to be used for the foundation, and the shape is often determined by the building conditions.

Select a slab having a rolled width of one of the dimensions L or W . (See Table I). W should not be less than 30% of the length of the grillage and L must extend at least $\frac{3}{4}"$ beyond the center lines of the outside grillage beams. The thickness of the slab is computed as shown on the preceding page.

Slab bases resting on grillage must be true and flat and if over $4"$ thick must be machine faced on top and bottom.

Upper tier grillage beams should be spaced with $1"$ minimum clear distance between the flanges. Lower tier beams should have $2"$ minimum clearance and a maximum of $\frac{3}{4}"$ of the flange width.

Example:—

Column Load = 960000 # ; Column dimensions, $d = 15.75"$ and $b = 15.25"$; Size of Grillage = $4' - 0" \times 3' - 4"$
 Grillage = $48" \times 40" = 1920$ sq. inches. Therefore:—Unit pressure on masonry foundation = $500\#$ per sq. inch.
 Column base:— $W = 24"$ and $L = 22"$. Then $A = 528$ sq. inches and $U = C \div A = 1818$

Then $e = \frac{22 - 15.75}{2} = 3.125$ and $f = \frac{24 - 15.25}{2} = 4.375$ $\therefore t^2 = \frac{1818}{6000} \times \frac{4.375}{1} \times \frac{4.375}{1} = 5.80$

This requires use of a slab $2\frac{1}{2}"$ thick (Table III)

Upper tier grillage beams

$$\text{Max. Bending Moment} = \frac{960000(48-24)}{8} = 2880000\#$$

$$4\text{-}1\frac{1}{2}"\ 12\text{-}45\# \text{ good for } 852300\# \text{ each} = 3409200\#$$

$$\text{Max. Shear} = \frac{960000}{48} \times \frac{(48-24)}{2} = 240000\#$$

$$4\text{-}1\frac{1}{2}"\ 12\text{-}45\# \text{ good for } 81400\# \text{ each} = 325600\#$$

$$\text{*Web Buckling. Total Load} = 960000\#$$

$$1\frac{1}{2}"\ 12\text{-}45\# \text{ good for } 8475\# \text{ per inch of web} + 8475 \times d/2$$

$$4\text{-}1\frac{1}{2}"\ 12\text{-}45\# \text{ good for } 4 \times 8475 \times \left(24 + \frac{12}{2}\right) = 1017000\#$$

Lower tier grillage beams

$$\text{Max. Bending Moment} = \frac{960000(40-25.235)}{8} = 1771800\#$$

$$1\frac{1}{2}"\ 8\text{-}20.5\# \text{ good for } 270900\# \text{ each} = 2167200\#$$

$$\text{Max. Shear} = \frac{960000}{40} \times \frac{40-25.235}{2} = 177180\#$$

$$1\frac{1}{2}"\ 8\text{-}20.5\# \text{ good for } 33500\# \text{ each} = 268000\#$$

$$\text{*Web Buckling. Total Load} = 960000\#$$

$$1\frac{1}{2}"\ 8\text{-}20.5\# \text{ good for } 5235\# \text{ per inch of web} + 5235 \times d/2$$

$$1\frac{1}{2}"\ 8\text{-}20.5\# \text{ good for } 8 \times 5235 \times \left(25.235 + \frac{8}{2}\right) = 1224360\#$$

*See table of end reactions and notes below.

†Seven beams have the required strength. Eight are necessary due to the limit allowed for space between flanges.

Part IV

Section 15

Miscellaneous Rolled Steel Sections

Dimensions

Technical Functions

T Bars

Z Bars

J & L Stair Stringer Channel

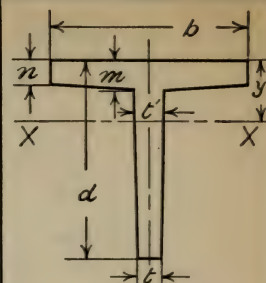
$\frac{3}{4}$ " to $1\frac{3}{4}$ "


T BARS

EQUAL LEGS

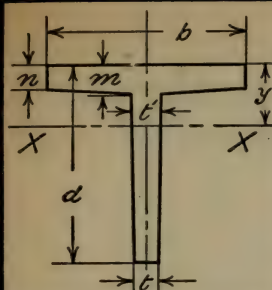
I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Stem Shear in Pounds

T Bar Sections have not been standardized.
Those listed below are representative sections rolled
by various mills.
Slight variations in dimensions occur.



Size (width of flange)			¾"	1"		
Weight			.61	.73	.80 .85 .89 1.25	
Depth = d".....			¾	7/8	1" 1" 1" 1"	
Area.....			.18	.21	.22 .25 .26 .37	
b.....			¾	7/8	1" 1" 1" 1"	
T to T'.....			1/8*	1/8*	7/64 to 1/8 1/8* 1/8 to 5/32 3/16 to 7/32	
M to N.....			1/8	1/8	1/8 1/8 1/8 to 5/32 3/16 to 7/32	
y.....			.24	.27	.28 .30 .29 .32	
AXES	X-X	I.....	.01	.01	.02 .02 .02 .03	
		S.....	.02	.02	.03 .03 .03 .05	
		r.....	.22	.26	.31 .30 .30 .29	
	Y-Y	I.....	.005	.01	.01 .01 .01 .02	
		S.....	.01	.02	.02 .02 .02 .04	
		r.....	.16	.18	.21 .21 .21 .22	
Coef. Strength.....			240	200	330 340 340 530	
Max. Mom. " #.....			350	300	500 510 510 790	
V.....			1130	1310	1400 1500 1690 2440	
Size (width of flange)			1 1/8"	1 3/16"	1 1/4"	
Weight			1.37	1.51	1.59 1.60 1.70 2.02	
Depth = d".....			1 1/8	1 3/16	1 1/4 1 1/4 1 1/4 1 1/4	
Area.....			.40	.44	.47 .47 .50 .59	
b.....			1 1/8	1 3/16	1 1/4 1 1/4 1 1/4 1 1/4	
T to T'.....			5/32 to 7/32	5/32 to 7/32	3/16 to 7/32 5/32 to 7/32 3/16 to 9/32 1/4 to 9/32	
M to N.....			3/16 to 7/32	3/16 to 1/4	3/16 to 7/32 5/32 to 1/4 3/16 to 7/32 1/4 to 9/32	
y.....			.33	.34	.38 .36 .40 .40	
AXES	X-X	I.....	.04	.05	.06 .06 .07 .08	
		S.....	.05	.06	.07 .06 .08 .10	
		r.....	.31	.33	.37 .35 .37 .37	
	Y-Y	I.....	.02	.03	.03 .03 .03 .05	
		S.....	.04	.05	.05 .05 .05 .07	
		r.....	.24	.26	.27 .27 .26 .28	
Coef. Strength.....			600	710	830 810 990 1130	
Max. Mom. " #.....			910	1060	1240 1210 1480 1694	
V.....			2530	2670	3050 2810 3520 3980	
Size (width of flange)			1 1/2"		1 3/4"	
Weight			1.94	2.47	2.28 2.93 3.09	
Depth = d".....			1 1/2	1 1/2	1 3/4 1 3/4 1 3/4	
Area.....			.57	.73	.67 .86 .91	
b.....			1 1/2	1 1/2	1 3/4 1 3/4 1 3/4	
T to T'.....			3/16 to 7/32	1/4 to 9/32	3/16 to 7/32 1/4 to 9/32 1/4 to 5/16	
M to N.....			3/16 to 7/32	1/4 to 9/32	3/16 to 7/32 1/4 to 9/32 1/4 to 5/16	
y.....			.44	.47	.50 .53 .54	
AXES	X-X	I.....	.11	.15	.19 .23 .23	
		S.....	.11	.14	.15 .19 .19	
		r.....	.45	.45	.53 .52 .51	
	Y-Y	I.....	.06	.08	.09 .12 .12	
		S.....	.08	.10	.10 .13 .14	
		r.....	.32	.32	.35 .37 .37	
Coef. Strength.....			1250	1750	1820 2260 2280	
Max. Mom. " #.....			1870	2620	2740 3390 3420	
V.....			3660	4780	4270 5580 5910	

*Each side of Stem has taper of about one degree.

**T BARS****EQUAL LEGS**

- I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Stem Shear in Pounds

T Bar Sections have not been standardized.
 Those listed below are representative sections rolled
 by various mills.
 Slight variations in dimensions occur.

2" to 6 1/2"

Size (width of flange)			2"				2 1/4"			
Weight			3.38	3.56	4.1	4.3	3.83	4.1	4.7	4.9
Depth = d".....			2"	2"	2"	2"	2 1/4	2 1/4	2 1/4	2 1/4
Area.....			1.00	1.05	1.20	1.26	1.13	1.19	1.38	1.43
b".....			2"	2"	2"	2"	2 1/4	2 1/4	2 1/4	2 1/4
T to T'.....			1/4 to 9/32	1/4 to 5/16	5/16 to 11/32	5/16 to 3/8	1/4 to 9/32	1/4 to 5/16	5/16 to 11/32	5/16 to 3/8
M to N.....			1/4 to 9/32	1/4 to 5/16	5/16 to 11/32	5/16 to 3/8	1/4 to 9/32	1/4 to 5/16	5/16 to 11/32	5/16 to 3/8
y.....			.59	.59	.61	.61	.65	.65	.67	.68
AXES	X-X	I.....	.36	.37	.42	.44	.52	.52	.62	.65
		S.....	.25	.26	.31	.31	.32	.32	.39	.41
		r.....	.60	.59	.59	.59	.68	.66	.67	.67
	Y-Y	I.....	.18	.18	.22	.23	.25	.25	.31	.33
		S.....	.18	.18	.22	.23	.22	.22	.28	.29
		r.....	.42	.42	.43	.43	.47	.46	.47	.48
	Coef. Strength.....		3060	3150	3630	3800	3900	3900	4710	4970
	Max. Mom. " #.....		4600	4720	5440	5700	5850	5850	7060	7450
	V.....		6370	6750	7870	8250	7170	7590	8860	9280

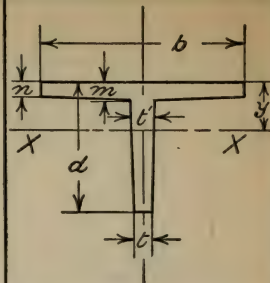
Size (width of flange)			2 1/2"			3"				
Weight			4.6	5.5	6.4	5.5	6.7	7.8	9.0	12.2
Depth = d".....			2 1/2	2 1/2	2 1/2	3"	3"	3"	3"	3"
Area.....			1.33	1.60	1.88	1.61	1.95	2.27	2.65	3.52
b".....			2 1/2	2 1/2	2 1/2	3"	3"	3"	3"	3"
T to T'.....			1/4 to 5/16	5/16 to 3/8	3/8 to 7/16	1/4 to 5/16	5/16 to 3/8	3/8 to 7/16	7/16 to 1/2	1/2 to 9/16
M to N.....			1/4 to 5/16	5/16 to 3/8	3/8 to 7/16	1/4 to 5/16	5/16 to 3/8	3/8 to 7/16	7/16 to 1/2	1/2 to 13/16
y.....			.71	.74	.76	.82	.86	.88	.90	.89
AXES	X-X	I.....	.74	.88	1.02	1.33	1.61	1.84	2.06	2.32
		S.....	.42	.50	.59	.61	.74	.86	.98	1.10
		r.....	.75	.74	.74	.91	.90	.90	.88	.81
	Y-Y	I.....	.34	.44	.52	.61	.75	.90	1.05	1.76
		S.....	.27	.35	.42	.40	.50	.60	.70	1.17
		r.....	.51	.52	.53	.61	.62	.63	.63	.71
Coef. Strength.....			4960	6000	7030	7320	9030	10420	11770	13190
Max. Mom. " #.....			7440	9000	10550	10980	13540	15620	17660	19790
V.....			8440	10310	12190	10130	12380	14630	16880	19130

Size (width of flange)		3 1/2"			4"			6 1/2"	
Weight		9.2	10.5	11.7	10.5	12.1	13.5	19.8	
Depth = d"		3 1/2	3 1/2	3 1/2	4"	4"	4"	6 1/2	
Area.....		2.70	3.09	3.44	3.09	3.56	3.97	5.80	
b"		3 1/2	3 1/2	3 1/2	4"	4"	4"	6 1/2	
T to T'		3/8 to 7/16	7/16 to 1/8	1/2 to 9/16	3/8 to 7/16	7/16 to 1/2	1/2 to 9/16	0.45	
M to N.....		3/8 to 7/16	7/16 to 1/2	1/2 to 9/16	3/8 to 7/16	7/16 to 1/2	1/2 to 9/16	40 to 55	
y.....		1.00	1.02	1.05	1.13	1.14	1.18	1.76	
AXES	X-X	I.....	3.00	3.38	3.73	4.5	5.17	5.72	23.5
		S.....	1.20	1.36	1.53	1.6	1.81	2.03	5.0
		r.....	1.05	1.05	1.04	1.21	1.20	1.20	2.01
	Y-Y	I.....	1.39	1.65	1.91	2.1	2.46	2.81	10.1
		S.....	.80	.95	1.09	1.1	1.23	1.40	3.1
		r.....	.72	.73	.74	.83	.83	.84	1.32
Coef. Strength.....		14400	16350	18270	18820	21690	24340	59490	
Max. Mom. " #.....		21600	24530	27400	28220	32540	36510	89240	
V.....		17060	19690	22310	19500	22500	25500	35100	

1 $\frac{1}{4}$ " to 3"**T BARS****UNEQUAL LEGS**

I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Stem Shear in Pounds

T Bar Sections have not been standardized.
 Those listed below are representative sections rolled
 by various mills.
 Slight variations in dimensions occur.

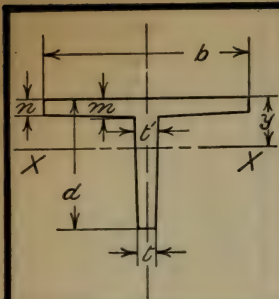


Size (width of flange)			1 ¼"		1 ½"		
Weight			1.48	1.56	1.54	1.25	2.45
Depth = d".....			1 1/16	1 1/8	1 1/16	1 1/4	2"
Area.....			.43	.46	.45	.37	.72
b.....			1 1/4	1 1/4	1 1/2	1 1/2	1 1/2
T to T'.....			5/32 to 7/32	3/16 to 1/4	3/16 to 5/32	1/8 to 5/32	3/16 to 1/4
M to N.....			3/16 to .30	3/16 to 7/32	3/16 to 1/4	1/8 to 5/32	3/16 to 1/4
y.....			.34	.34	.29	.33	.63
AXES	X-X	I.....	.04	.05	.04	.05	.27
		S.....	.05	.06	.05	.05	.19
		r.....	.29	.32	.30	.37	.61
	Y-Y	I.....	.03	.03	.05	.04	.06
		S.....	.05	.05	.07	.05	.08
		r.....	.28	.27	.34	.32	.92
Coef. Strength.....			630	770	620	660	2360
Max. Mom. " #.....			940	1150	930	980	3550
V.....			2390	2950	2390	2110	5250

Size (width of flange)			1 3/4"	2 7/16"		2 1/2"
Weight			1.43	3.62	4.2	6.1
Depth = d".....			19/32	2"	2"	3"
Area.....			.42	1.06	1.23	1.77
b.....			1 3/4	2 7/16	2 7/16	2 1/2
T to T'.....			1/4 to 5/16	3/16 to 1/4	17/64 to 21/64	5/16 to 3/8
M to N.....			5/32 to 3/16	17/64 to 21/64	17/64 to 21/64	5/16 to 3/8
y.....			.17	.59	.55	.92
AXES	X-X	I.....	.01	.39	.41	1.5
		S.....	.02	.28	.28	.72
		r.....	.15	.61	.58	.92
	Y-Y	I.....	.07	.25	.35	.44
		S.....	.09	.21	.28	.35
		r.....	.42	.49	.53	.50
Coef. Strength.....			290	3320	3390	8660
Max. Mom. " #.....			430	4980	5090	12990
V.....			2000	5250	7120	12380

Size (width of flange)			2 ¾"	3"			
Weight			2.52	6.1	8.5	9.7	10.8
Depth = d".....			1 ¾	2 ½	3 ½	3 ½	3 ½
Area.....			.74	1.77	2.50	2.85	3.17
b.....			2 ¾	3"	3"	3"	3"
T to T'.....			3/16 to ¼	5/16 to 3/8	3/8 to 7/16	7/16 to ½	½ to 9/16
M to N.....			9/64 to 5/64	5/16 to 3/8	3/8 to 7/16	7/16 to ½	½ to 9/16
y.....			.47	.68	1.07	1.10	1.12
AXES	X-X	I.....	.21	.94	2.8	3.20	3.50
		S.....	.16	.52	1.20	1.30	1.50
		r.....	.53	.73	1.07	1.06	1.06
	Y-Y	I.....	.25	.75	.93	1.00	1.20
		S.....	.18	.50	.62	.69	.80
		r.....	.58	.65	.60	.61	.62
Coef. Strength.....			1970	6200	13830	16000	17650
Max. Mom. " #.....			2960	9300	20740	24000	26480
V.....			4590	10310	17060	19690	22310

*Each side of Stem has taper of about one-half degree.



T BARS

UNEQUAL LEGS

- I is Moment of Inertia
 S is Section Modulus
 r is Radius of Gyration
 V is Maximum Web Shear in Pounds

T Bar Sections have not been standardized.
 Those listed below are representative sections rolled
 by various mills.
 Slight variations in dimensions occur.


 $3\frac{1}{2}''$ to $5''$


Size (width of flange)			3 1/2"				
Weight			5.1	8.5	9.7	9.8	12.6
Depth = d".....			2 1/2	3	3	4	4
Area.....			1.48	2.50	2.85	2.88	3.70
b.....			3 1/2	3 1/2	3 1/2	3 1/2	3 1/2
T to T'.....			9/32 to 11/32	3/8 to 7/16	7/16 to 1/2	3/8 to 7/16	1/2 to 9/16
M to N.....			3/16 to 1/4	3/8 to 7/16	7/16 to 1/2	3/8 to 7/16	1/2 to 9/16
y.....			.69	.83	.85	1.19	1.24
AXES	X-X	I.....	.85	1.90	2.17	4.30	5.50
		S.....	.47	.89	1.01	1.50	2.00
		r.....	.76	.88	.87	1.23	1.21
	Y-Y	I.....	.74	1.40	1.65	1.40	1.90
		S.....	.42	.81	.94	.81	1.10
		r.....	.71	.75	.76	.70	.72
Coef. Strength.....		5640	10510	12120	18370	23920	
Max. Mom. " #.....		8460	15770	18170	27550	35870	
V.....		9380	14630	16880	19500	25500	

Size (width of flange)			4"					
Weight			6.7	7.8	7.2	8.5	7.8	9.2
Depth = d".....			2"	2"	2 1/2	2 1/2	3"	3"
Area.....			1.97	2.29	2.12	2.48	2.29	2.68
b.....			4"	4"	4"	4"	4"	4"
T to T'.....			5/16 to 3/8	3/8 to 7/16	5/16 to 3/8	3/8 to 7/16	5/16 to 3/8	3/8 to 7/16
M to N.....			5/16 to 3/8	3/8 to 7/16	5/16 to 3/8	3/8 to 7/16	5/16 to 3/8	3/8 to 7/16
y.....			.46	.48	.60	.62	.75	.78
AXES	X-X	I.....	.53	.60	1.0	1.2	1.7	2.0
		S.....	.34	.40	.53	.62	.77	.90
		r.....	.52	.52	.69	.69	.87	.86
	Y-Y	I.....	1.80	2.10	1.8	2.1	1.8	2.1
		S.....	.88	1.10	.88	1.0	.88	1.1
		r.....	.95	.96	.91	.92	.88	.89
Coef. Strength.....			4130	4740	6320	7660	9070	10820
Max. Mom. " #.....			6200	7110	9480	11490	13600	16220
V.....			8250	9750	10310	12190	12380	14630

Size (width of flange)		4"				5"	
Weight		11.2	14.4	11.9	15.3	11.5	
Depth = d".		4 1/2	4 1/2	5	5	3	
Area.		3.29	4.23	3.49	4.50	3.37	
b.		4"	4"	4"	4"	5	
T to T'.		3/8 to 7/16	1/2 to 9/16	3/8 to 7/16	1/2 to 9/16	13/32 to 5/8	
M to N.		3/8 to 7/16	1/2 to 9/16	3/8 to 7/16	1/2 to 9/16	3/8 to 7/16	
y.		1.31	1.37	1.51	1.56	.76	
AXES	X-X	I.....	6.3	7.9	.85	10.8	2.4
		S.....	2.0	2.5	2.4	3.1	1.1
		r.....	1.39	1.37	1.56	1.55	.84
	Y-Y	I.....	2.1	2.8	2.1	2.8	3.9
		S.....	1.1	1.4	1.1	1.4	1.6
		r.....	.80	.81	.78	.79	1.10
Coef. Strength.....		23700	30290	29230	37680	12860	
Max. Mom. " #		35550	45440	43840	56520	19290	
V.....		21940	28690	24380	31880	18560	

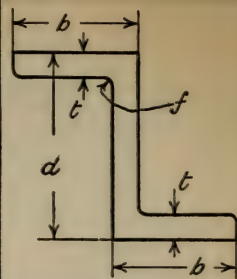
3" & 4"



Z BARS

EQUAL LEGS

I is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
V is Maximum Web Shear in Pounds



3' Z BARS

Weight per foot			6.7	8.5	9.8	11.5	12.6	14.3
Depth = d".....			3"	3 1/16"	3"	3 1/16"	3"	3 1/16"
Area.....			1.97	2.48	2.86	3.36	3.69	4.18
b.....			2 11/16"	2 3/4"	2 11/16"	2 3/4"	2 11/16"	2 3/4"
t.....			1/4"	5/16"	3/8"	7/16"	1/2"	5/8"
f.....			5/16"	5/16"	5/16"	5/16"	5/16"	5/16"
AXES	X-X	I.....	2.9	3.6	3.9	4.6	4.6	5.3
		S.....	1.9	2.4	2.6	3.0	3.1	3.4
		r.....	1.21	1.21	1.16	1.17	1.12	1.12
	Y-Y	I.....	2.8	3.6	3.9	4.8	4.9	5.7
		S.....	1.1	1.4	1.6	1.9	2.0	2.3
		r.....	1.19	1.21	1.17	1.19	1.15	1.17
	Z-Z	r.....	.55	.56	.54	.55	.53	.54
	Coef. Strength.....			23200	28200	31200	36000	36800
Max. Mom. # *.....			34800	42300	46800	54100	55200	62300
V.....			9000	11500	13500	16100	18000	20700

4' Z BARS

Weight per foot			8.2	10.3	12.5	13.8	15.9	18.0	18.9	20.9	23.0	
Depth = d".....			4"	4 1/16	4 1/8	4"	4 1/16	4 1/8	4"	4 1/16	4 1/8	
Area.....			2.41	3.03	3.66	4.05	4.66	5.27	5.55	6.14	6.75	
b.....			3 1/16	3 1/8	3 3/16	3 1/16	3 1/8	3 3/16	3 1/16	3 1/8	3 3/16	
t.....			1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	
f.....			5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	
AXES	X-X	I.....	6.3	7.9	9.6	9.7	11.2	12.7	12.1	13.5	15.0	
		S.....	3.1	3.9	4.7	4.8	5.5	6.2	6.1	6.7	7.3	
		r.....	1.62	1.62	1.62	1.55	1.55	1.55	1.48	1.48	1.49	
	Y-Y	I.....	4.2	5.5	6.8	6.7	8.0	9.3	8.7	10.0	11.2	
		S.....	1.4	1.8	2.3	2.4	2.8	3.2	3.2	3.6	4.0	
		r.....	1.33	1.34	1.36	1.29	1.31	1.33	1.25	1.27	1.29	
	Z-Z	r.....	.67	.68	.69	.66	.67	.68	.66	.67	.68	
		Coef. Strength.....		37800	46700	55900	58200	66200	73900	72600	79800	87300
		Max. Mom. " #.....		56700	70000	83800	87300	99200	110800	108900	119600	130900
V.....		12000	15200	18600	21000	24400	27800	30000	33500	37100		

For Uniformly Distributed Loads for laterally supported Z bars, simple span, divide the Coefficient of Strength by the length of the span in feet.

Z BARS**EQUAL LEGS**

- I** is Moment of Inertia
S is Section Modulus
r is Radius of Gyration
v is Maximum Web Shear in Pounds

5" & 6"**5" Z BARS**

Weight per foot		11.6	14.0	16.4	17.9	20.2	22.6	23.7	26.0	28.4
Depth = d"		5"	5 1/16	5 1/8	5"	5 1/16	5 1/8	5"	5 1/16	5 1/8
Area.....		3.40	4.10	4.81	5.25	5.94	6.64	6.96	7.64	8.33
b.....		3 1/4	3 5/16	3 3/8	3 1/4	3 5/16	3 3/8	3 1/4	3 5/16	3 3/8
t.....		5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16
f.....		5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16
AXES	X-X	I.....	13.4	16.2	19.1	19.2	21.8	24.5	23.7	26.2
		S.....	5.3	6.4	7.4	7.7	8.6	9.6	9.5	10.3
		r.....	1.98	1.99	1.99	1.91	1.91	1.92	1.84	1.85
	Y-Y	I.....	6.2	7.7	9.2	9.1	10.5	12.1	11.4	12.8
		S.....	2.0	2.5	2.9	3.0	3.5	3.9	3.9	4.4
		r.....	1.35	1.37	1.38	1.31	1.33	1.35	1.28	1.30
	Z-Z	r.....	.75	.76	.77	.74	.75	.76	.73	.74
	Coef. Strength.....		64300	76800	89400	92200	103300	114700	113800	124200
Max. Mom. " #.....		96500	115200	134200	138200	155000	172100	170600	186300	201600
V.....		18800	22800	26900	30000	34200	38400	41300	45600	50000

6" Z BARS

Weight per foot		15.7	18.4	21.1	22.8	25.4	28.1	29.4	32.0	34.6
Depth = d"		6"	6 1/16	6 1/8	6"	6 1/16	6 1/8	6"	6 1/16	6 1/8
Area.....		4.59	5.39	6.19	6.68	7.46	8.25	8.63	9.40	10.17
b.....		3 1/2	3 9/16	3 5/8	3 1/2	3 9/16	3 5/8	3 1/2	3 9/16	3 5/8
t.....		3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8
f.....		5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16	5/16
AXES	X-X	I.....	25.3	29.8	34.4	34.6	38.9	43.2	42.1	46.1
		S.....	8.4	9.8	11.2	11.5	12.8	14.1	14.0	15.2
		r.....	2.35	2.35	2.36	2.28	2.28	2.29	2.21	2.22
	Y-Y	I.....	9.1	11.0	12.9	12.6	14.4	16.3	15.4	17.3
		S.....	2.8	3.3	3.8	3.9	4.4	5.0	4.9	5.5
		r.....	1.41	1.43	1.44	1.37	1.39	1.41	1.34	1.36
	Z-Z	r.....	.83	.83	.84	.81	.82	.84	.81	.82
	Coef. Strength.....		101200	118000	134800	138400	154000	169300	168400	182500
Max. Mom. " #.....		151800	177000	202200	207600	231000	253900	252600	273700	295100
V.....		27000	31800	36800	40500	45500	50500	54000	59100	64300

For Uniformly Distributed Loads for laterally supported Z bars, simple span, divide the Coefficient of Strength by the length of the span in feet.

10" & 12"**J AND L STAIR STRINGER CHANNEL**

DIMENSIONS—FUNCTIONS—ALLOWABLE LOADS

I is Moment of Inertia

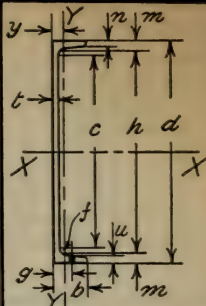
S is Section Modulus

r is Radius of Gyration

V is Maximum Web Shear in Pounds.

P is Minimum Span in feet, uniformly loaded to cause V.

Rivet given is Maximum Diameter in flange.
Allowable concentrated center loads are 50%
and their deflections 80% of those shown.



Depth = d".	10.0	10.0
Wt. per foot.	8.0	8.8
Area.....	2.34	2.57
b".....	1.500	1.523
t.....	.164	.1875
h.....	9.308	9.308
m.....	.346	.346
n.....	.180	.180
f.....	.187	.187
c.....	8.934	8.934
g.....	7/8	7/8
u.....	1/4	1/4

Live Load deflection must not exceed
1/360 of the Span.
Total Def. \times Live Load
Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

Depth = d".	12.0	12.0
Wt. per foot.	10.6	10.6
Area.....	3.12	3.12
b".....	1.500	1.500
t.....	.190	.190
h.....	11.164	11.164
m.....	.418	.418
n.....	.200	.200
f.....	.250	.250
c.....	10.664	10.664
g.....	7/8	7/8
u.....	5/16	5/16

Live Load deflection must not exceed
1/360 of the Span.
Total Def. \times Live Load
Live Load Def. = $\frac{\text{Total Def.} \times \text{Live Load}}{\text{Tabular Load}}$

AXES	X-X	I.....	30.3	32.2
	Y-Y	S.....	6.06	6.44
		r.....	3.60	3.54
		I.....	.33	.35
		S.....	.27	.28
		r.....	.38	.37
		y.....	.29	.28

AXES	X-X	I.....	55.8	55.8
	Y-Y	S.....	9.30	9.30
		r.....	4.23	4.23
		I.....	.39	.39
		S.....	.32	.32
		r.....	.35	.35
		y.....	.27	.27

Coef. Str....	77270	77280
Max.Mom. #	109080	115920
V.....	19680	22500
P. feet...	1.85	1.72
Rivet dia....	1/2	1/2

Deflection in
inches for Maximum
Load; Laterally fixed
beam.

Coef. Str....	111600	111600
Max.Mom. #	167400	167400
V.....	27360	27360
P. feet...	2.04	2.04
Rivet dia....	1/2	1/2

Deflection in
inches for Maximum
Load; Laterally fixed
beam.

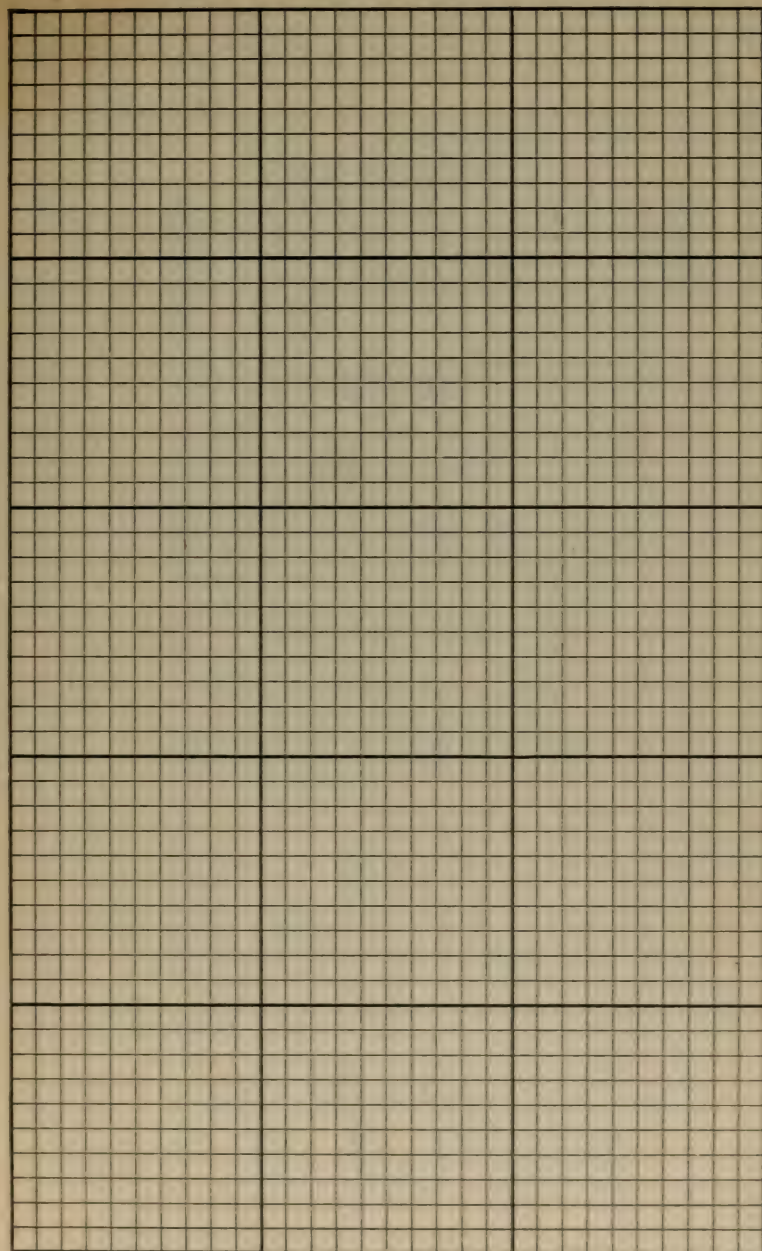
Span feet	Laterally		Laterally		Total inches for Maximum Load; Laterally fixed beam.
	fixed	free	fixed	free	
1	39.4	39.4	45.0	45.0	
2	36.4	35.8	38.6	38.1	
3	24.2	20.8	25.7	22.3	.017
4	18.2	13.4	19.3	14.3	.030
5	14.5	8.9	15.5	9.7	.047
6	12.1		12.9		.067
7	10.4		11.0		.091
8	9.1		9.7		.119
9	8.1		8.6		.151
10	7.3		7.7		.186
11	6.6		7.0		.225
12	6.1		6.4		.268
13	5.6		5.9		.315
14	5.2		5.5		.365
15	4.8		5.2		.419
16	4.5		4.8		.477
17	4.3		4.5		.538
18	4.0		4.3		.603
19	3.8		4.1		.672
20	3.6		3.9		.745

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the
Coefficient of Strength by Span in feet.

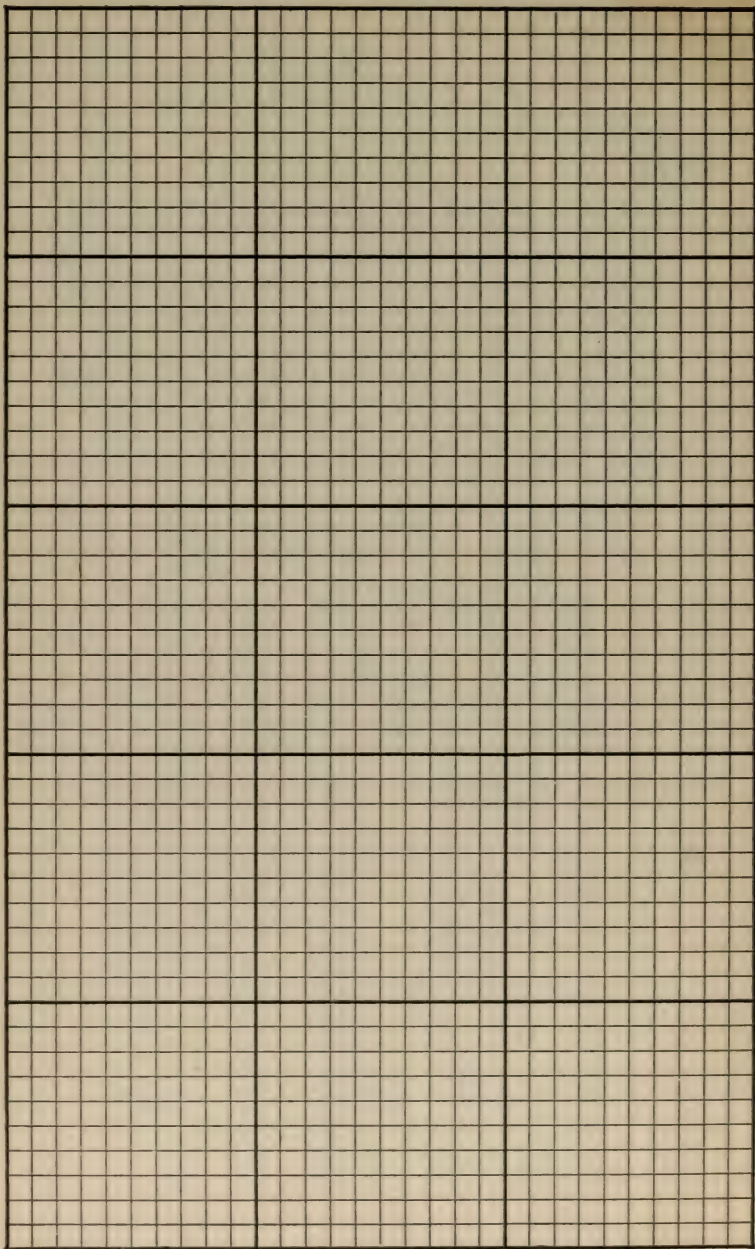
Span feet	Laterally		Total inches for Maximum Load; Laterally fixed beam.
	fixed	free	
1	54.7	54.7	
2	54.7	54.7	
3	37.2	32.5	.014
4	27.9	20.8	.025
5	22.3	13.8	.039
6	18.6		.056
7	15.9		.076
8	13.9		.099
9	12.4		.126
10	11.2		.155
11	10.1		.188
12	9.3		.223
13	8.6		.263
14	8.0		.304
15	7.4		.349
16	7.0		.398
17	6.6		.448
18	6.2		.503
19	5.9		.560
20	5.6		.621
21	5.3		.684
22	5.1		.751
23	4.9		.820
24	4.7		.894
25	4.5		.970

Allowable Uniform Load in Kips, as fixed by shear or flexure, whichever is least.
For laterally fixed beam loads not tabulated, divide the
Coefficient of Strength by Span in feet.

NOTES and DIAGRAMS



NOTES and DIAGRAMS



Part IV

Section 16

Rivets

Values in Plates

Values in Channel and Beam Webs

Dimensions, Weights, and Signs

Riveting Details

Lengths for various Grips

Reduction of Area in Plates

Bolts

Dimensions and Weights

SHEAR @ 13500		WORKING VALUES FOR POWER DRIVEN RIVETS AND TURNED BOLTS IN REAMED HOLES										BEARING Single @ 24000 Double @ 30000	
Rivet dia.		1/2"	5/8"	3/4"	7/8"	1"	1 1/8"	1 1/4"					
Area		.1963	.3068	.4418	.6013	.7854	.9940	1.2272					
Single Sh.		2650	4140	5960	8120	10600	13420	16570					
Double Sh.		5300	8280	11930	16240	21200	26840	33130					
Thickness of Plate		Bearing		Bearing		Bearing		Bearing		Bearing		Bearing	
		24000	30000	24000	30000	24000	30000	24000	30000	24000	30000	24000	30000
.170		2040	2550	2550	3190	3060	3830	3570	4460	4080	5100	4590	5740
.180		2160	2700	2700	3380	3240	4050	3780	4730	4320	5400	4860	6080
.1875	3/16	2250	2810	2810	3520	3380	4220	3940	4920	4500	5630	5060	6330
.190		2280	2850	2850	3560	3420	4280	3990	4990	4560	5700	5130	6410
.200		2400	3000	3000	3750	3600	4500	4200	5250	4800	6000	5400	6750
.210		2520	3150	3150	3940	3780	4730	4410	5510	5040	6300	5670	7090
.220		2640	3300	3300	4130	3960	4950	4620	5780	5280	6600	5940	7430
.230		3450	3450	4310	4140	5180	4830	6040	5520	6900	6210	7760
.240		3600	3600	4500	4320	5400	5040	6300	5720	7200	6480	8100
.250	1/4	3750	3750	4690	4500	5630	5250	6560	6000	7500	6750	8440
.260		3900	3900	4880	4680	5850	5460	6830	6240	7800	7020	8780
.270		4050	4050	5060	4860	6080	5670	7090	6480	8100	7290	9110
.280		4200	5250	5040	6300	5880	7350	6720	8400	7560	9450
.290		4350	5440	5220	6530	6090	7610	6960	8700	7830	9790
.300		4500	5630	5400	6750	6300	7880	7200	9000	8100	10130
.310		4650	5810	5580	6980	6510	8140	7440	9300	8370	10460
.312	5/16	4690	5860	5630	7030	6560	8200	7500	9380	8440	10550
.320		4800	6000	5760	7200	6720	8400	7680	9600	8640	10800
.330		4950	6190	5940	7430	6930	8660	7920	9900	8910	11140
.340		5100	6380	5960	7650	7140	8930	8160	10200	9180	11480
.350		5250	6560	7880	7350	9190	8400	10500	9450	11810
.360		6750	8100	7560	9450	8640	10800	9720	12150
.370		6940	8330	7770	9710	8880	11100	9990	12490
.375	3/8	7030	8440	7880	9840	9000	11250	10130	12660
.380		7130	8550	7980	9980	9120	11400	10260	12830
.390		7310	8780	10240	9360	11700	10530	13160
.400		7500	9000	10500	9600	12000	10800	13500
.410		7690	9230	10760	9840	12300	11070	13840
.420		7880	9450	11030	10080	12600	11340	14180
.430		8060	9680	11290	10320	12900	11610	14510
.4375	7/16	8200	9840	11480	10500	13130	11810	14770
.440		8250	9900	11550	10560	13200	11880	14850
.450		10130	11810	13500	12150	15190
.460		10350	12080	13800	12420	15530
.470		10580	12340	14100	12690	15860
.480		10800	12600	14400	12960	16200
.490		11030	12860	14700	13230	16540
.500	1/2	11250	13130	15000	16880
.510		11480	13390	15300	17210
.520		11700	13650	15600	17550
.530		11930	13910	15900	17890
.540		11930	14180	16200	18230
.550		14440	16500	18560
.560		14700	16800	18900
.5625	9/16	14770	16880	18980
.570		14960	17100	19240
.580		15230	17400	19580
.590		15490	17700	19910
.600		15750	18000	20250
.610		16010	18300	20590
.620		18600	20930
.625	5/8	18750	21090
.630		18900	21260
.640		19200	21600
.650		19500	21940
.660		19800	22280
.670		20100	22610
.680		20400	22950
.687	11/16	20630	23200
.690		20700	23290
.700		21000	23630
.710		23960
.720		24300
.730		24640
.740		24980
.750	3/4	25310
.812	13/16
.875	7/8
.937	1 5/16
1.00	1"	12000	15000	15000	18750	18000	22500	21000	26250	24000	30000	27000	33750

LOADS BY A. I. S. C. SPECIFICATION

SHEAR @ 10000	WORKING VALUES FOR HAND DRIVEN RIVETS AND UNFINISHED BOLTS												BEARING	
													Single @ 16000	
													Double @ 20000	
Rivet dia.	1/2"		5/8"		3/4"		7/8"		1"		1 1/8"		1 1/4"	
Area	1963		3068		4418		6013		7854		9940		12272	
Single Sh.	1960		3070		4420		6010		7850		9940		12270	
Double Sh	3930		6140		8840		12030		15710		19880		24540	
Thickness of Plate	Bearing		Bearing		Bearing		Bearing		Bearing		Bearing		Bearing	
	16000	20000	16000	20000	16000	20000	16000	20000	16000	20000	16000	20000	16000	20000
.170	1360	1700	1700	2130	2040	2550	2380	2980	2720	3400	3060	3830	3400	4250
.180	1440	1800	1800	2250	2160	2700	2520	3150	2880	3600	3240	4050	3600	4500
.1875 3/16	1500	1880	1880	2340	2250	2810	2630	3280	3000	3750	3380	4220	3750	4690
.190	1520	1900	1900	2380	2280	2850	2660	3330	3040	3800	3420	4280	3800	4750
.200	1600	2000	2000	2500	2400	3000	2800	3500	3200	4000	3600	4500	4000	5000
.210	1680	2100	2100	2630	2520	3150	2940	3680	3360	4200	3780	4730	4200	5250
.220	1760	2200	2200	2750	2640	3300	3080	3850	3520	4400	3960	4950	4400	5500
.230	1840	2300	2300	2880	2760	3450	3220	4030	3680	4600	4140	5180	4600	5750
.240	1920	2400	2400	3000	2880	3600	3360	4200	3840	4800	4320	5400	4800	6000
.250 1/4	2500	2500	3130	3000	3750	3500	4380	4000	5000	4500	5630	5000	6250
.260	2600	2600	3250	3120	3900	3640	4550	4160	5200	4680	5850	5200	6500
.270	2700	2700	3380	3240	4050	3780	4730	4320	5400	4860	6080	5400	6750
.280	2800	2800	3500	3360	4200	3920	4900	4480	5600	5040	6300	5600	7000
.290	2900	2900	3630	3480	4350	4060	5080	4640	5800	5220	6530	5800	7250
.300	3000	3000	3750	3600	4500	4200	5250	4800	6000	5400	6750	6000	7500
.310	3100	3880	3720	4650	4340	5430	4960	6200	5580	6980	6200	7750
.3125 5/16	3130	3910	3750	4690	4380	5470	5000	6250	5630	7030	6250	7810
.320	3200	4000	3840	4800	4480	5600	5120	6400	5760	7200	6400	8000
.330	3300	4130	3960	4950	4620	5780	5280	6600	5940	7430	6600	8250
.340	3400	4250	4080	5100	4760	5950	5440	6800	6120	7650	6800	8500
.350	3500	4380	4200	5250	4900	6130	5600	7000	6300	7880	7000	8750
.360	3600	4500	4320	5400	5040	6300	5760	7200	6480	8100	7200	9000
.370	3700	4630	5550	5180	6480	5920	7400	6660	8330	7400	9250
.375 3/8	3750	4690	5630	5250	6560	6000	7500	6750	8440	7500	9370
.380	3800	4750	5700	5320	6650	6080	7600	6840	8550	7600	9500
.390	3900	4880	5850	5460	6830	6240	7800	7020	8780	7800	9750
.400	5000	6000	5600	7000	6400	8000	7200	9000	8000	10000
.410	5130	6150	5740	7180	6560	8200	7380	9230	8200	10250
.420	5250	6300	5880	7350	6720	8400	7560	9450	8400	10500
.430	5380	6450	7530	6880	8600	7740	9680	8600	10750
.4375 7/16	5470	6560	7660	7000	8750	7880	9840	8750	10940
.440	5500	6600	7700	7040	8800	7920	9900	8800	11000
.450	5630	6750	7880	7200	9000	8100	10130	9000	11250
.460	5750	6900	8050	7360	9200	8280	10350	9200	11500
.470	5880	7050	8230	7520	9400	8460	10580	9400	11750
.480	6000	7200	8400	7680	9600	8640	10800	9600	12000
.490	6130	7350	8580	7840	9800	8820	11030	9800	12250
.500 1/2	7500	8750	10000	9000	11250	10000	12500
.510	7650	8930	10200	9180	11480	10200	12750
.520	7800	9100	10400	9360	11700	10400	13000
.530	7950	9280	10600	9540	11930	10600	13250
.540	8100	9450	10800	9720	12150	10800	13500
.550	8250	9630	11000	9900	12380	11000	13750
.560	8400	9800	11200	12600	11200	14000
.5625 9/16	8440	9850	11250	12660	11250	14060
.570	8550	9980	11400	12830	11400	14250
.580	8700	10150	11600	13050	11600	14500
.590	10330	11800	13280	11800	14750
.600	10500	12000	13500	12000	15000
.610	10680	12200	13730	12200	15250
.620	10850	12400	13950	15500
.625 5/8	10940	12500	14060	15630
.630	11030	12600	14180	15750
.640	11200	12800	14400	16000
.650	11380	13000	14630	16250
.660	11550	13200	14850	16500
.670	11730	13400	15080	16750
.680	11900	13600	15300	17000
.687 11/16	12030	13750	15470	17190
.690	13800	15530	17250
.700	14000	15750	17500
.710	14200	15980	17750
.720	14400	16200	18000
.730	14600	16430	18250
.740	14800	16650	18500
.750 3/4	15000	16880	18750
.812 13/16	18280	20310
.875 7/8	19690	21870
.937 1 1/8	23440
1.00	8000	10000	10000	12500	12000	15000	14000	17500	16000	20000	18000	22500	20000	25000

LOADS BY A. I. S. C. SPECIFICATION

WORKING VALUES FOR ONE 3/4" HAND DRIVEN RIVET OR UNFINISHED BOLT IN CHANNEL AND BEAM WEBS

Shear @ 10000

Single Shear Bearing @ 16000

Double Shear Bearing @ 20000

Depth in Inches	Amer. Std. Channels			Amer. Std. Beams			Bethlehem Beams			Beth. Girder Beams			Carnegie Beam Sect.		
	Weight Per Foot	Bearing		Weight Per Foot	Bearing		Weight Per Foot	Bearing		Weight Per Foot	Bearing		Weight Per Foot	Bearing	
		Single Shear	Double Shear		Single Shear	Double Shear		Single Shear	Double Shear		Single Shear	Double Shear		Single Shear	Double Shear
3	4.1 5.0 6.0	2040 3100 4270	2550 3870 5340	5.7 6.5 7.5	2040 3010 4190	2550 3770 5240									
4	5.4 6.25 7.25	2160 2960 3840	2700 3710 4800	7.7 8.5 9.5 10.5	2280 3040 3910 4420	2850 3800 4890 6000									
5	6.7 9.0 11.5	2280 3900 4420	2850 4880 7080	10.0 12.25 14.75	2520 4160 4420	3150 5210 7410									
6	8.2 10.5 13.0 15.5	2400 3770 4420 4420	3000 4710 6560 8390	12.5 14.75 17.25	2760 4120 4420	3450 5150 6980									
7	9.8 12.25 14.75 17.25 19.75	2520 3770 4420 4420 4420	3150 4710 6290 7860 8840	15.3 17.5 20.0	3000 4140 4420	3750 5180 6750									
8	11.50 13.75 16.25 18.75 21.25	2640 3640 4420 4420 4420	3300 4550 5930 7310 8690	18.4 20.5 23.0 25.5	3240 4190 4420 4420	4050 5240 6620 7980	17.5 19.0	3000 3240	3750 4050	29.5 33.0 36.5	3420 3480 3720	4280 4350 4650	24.0 27.0 30.0 31.0 42.0	2870 3220 3580 3480 4420	3590 4020 4470 4350 5850
9	13.40 15.0 20.0 25.0	2760 3420 4420 4420	3450 4280 6720 8840	21.8 25.0 30.0 35.0	3480 4420 4420 4420	4350 5960 8420 8840	20.5 22.0	3000 3120	3750 3900	36.0 38.5 43.5	3480 3720 4200	4350 4650 5250	29.0 32.0 35.0	3350 3680 4020	4190 4610 5030
10	15.3 20.0 25.0 30.0 35.0	2880 4420 4420 4420 4420	3600 5690 7890 8840 8840	25.4 30.0 35.0 40.0	3720 4420 4420 4420	4650 6710 8840 8840	21.0 23.5 26.0 28.5	2880 3000 3240 3420	3600 3750 4050 4280	41.5 44.5 50.0	3720 3840 4320	4650 4800 5400	21.0 23.0 26.0 30.0 31.0 36.0 42.0 49.0 54.0 59.0 64.0	2760 2760 3110 3580 3840 4420 4420 4420 4420 4420	3450 3450 3890 4470 4800 7010 8840 5250 7460 8840 8840
12	20.7 25.0 30.0 35.0 40.0	3360 4420 4420 4420 4420	4200 5810 7650 8840 8840	31.8 35.0 40.8 45.0 50.0 55.0	4200 4420 4420 4420 4420 4420	5250 6420 6900 8480 8840 8840	25.0 28.0 31.5 36.0 40.0 44.0 48.5	2880 2940 3240 3600 3960 4320 4420	3600 3680 4050 4500 4950 5400 5930	51.5 55.5 61.0 66.0 70.5 76.5	4320 4420 4420 4420 4420 4420	5400 5700 6150 6750 7050 7650	25.0 28.0 32.0 34.0 36.0 40.0 45.0 50.0 55.0 60.0 66.0 65.0 70.0 76.0	2880 2880 3290 4420 3700 3480 3910 4330 4420 4420 4420 4420 4420 4420	3600 3600 4110 5630 4620 4350 4890 5420 5630 6140 6720 6000 7850 8840

WORKING VALUES FOR ONE 3/4" POWER DRIVEN RIVET
OR TURNED BOLT IN REAMED HOLE IN CHANNEL AND BEAM WEBS

Shear @ 13500

Single Shear Bearing @ 24000

Double Shear Bearing @ 30000

Depth in Inches	Amer. Std. Channels			Amer. Std. Beams			Bethlehem Beams			Beth. Girder Beams			Carnegie Beam Sect.		
	Weight		Bearing	Weight		Bearing	Weight		Bearing	Weight		Bearing	Weight		Bearing
	Per Foot	Single Shear		Per Foot	Single Shear		Per Foot	Single Shear		Per Foot	Single Shear		Per Foot	Single Shear	
14							30.0	4770	5960				30.0	4860	6080
							33.0	4770	5960				33.0	4860	6080
							37.5	5490	6860				36.0	5290	6620
							42.0	5960	7650				38.0	5960	8440
													39.0	5720	7160
													42.0	5960	7700
													48.0	5960	7720
													53.0	5960	8510
													58.0	5960	9290
													61.0	5960	8600
15													68.0	5960	9560
													75.0	5960	10530
													85.0	5960	9790
													95.0	5960	10910
													105.0	5960	11930
	33.9	5960	9000	42.9	5960	9230	36.0	5040	6300	64.5	5960	8780			
	35.0	5960	9500	45.0	5960	10170	38.5	5220	6530	69.0	5960	9450			
	40.0	5960	11700	50.0	5960	11930	40.0	5490	6860	74.0	5960	9900			
	45.0	5960	11930	55.0	5960	11930	42.5	5850	7310	80.5	5960	10800			
	50.0	5960	11930	60.8	5960	11930	46.0	5960	8210	94.0	5960	11930			
16	55.0	5960	11930	65.0	5960	11930	50.5	5960	8660	99.0	5960	11930			
				70.0	5960	11930	54.5	5960	9230	105.0	5960	11930			
				75.0	5960	11930	59.5	5960	10130	111.0	5960	11930			
							71.5	5960	11700	127.0	5960	11930			
										135.0	5960	11930			
										141.0	5960	11930			
										147.0	5960	11930			
							35.0	5130	6410	74.5	5960	8780	35.0	5220	6530
							40.0	5310	6640	81.0	5960	9450	38.0	5650	7070
							45.0	5940	7425	87.0	5960	10130	40.0	5220	6530
18							50.0	6059	8210	94.0	5960	10910	43.0	5960	8440
							56.5	5960	8440				45.0	5870	7340
							60.5	5960	8780				50.0	5960	8150
							66.0	5960	9450				58.0	5960	8440
							71.5	5960	10240				63.0	5960	9140
													68.0	5960	9860
													76.0	5960	9430
													83.0	5960	10310
													90.0	5960	11140
													100.0	5960	10440
20													107.0	5960	11160
													115.0	5960	11930
				54.7	5960	10350	47.0	5850	7310	80.0	5960	9450	47.0	5760	7200
				60.0	5960	11930	49.0	5940	7430	86.0	5960	9900	51.0	5960	8440
				65.0	5960	11930	52.0	5960	7990	92.0	5960	10350	52.0	5960	7970
				70.0	5960	11930	54.5	5960	8330	99.0	5960	10910	58.0	5960	8840
				75.6	5960	11930	59.0	5960	8550				67.0	5960	9140
				80.0	5960	11930	64.5	5960	9000				72.0	5960	9810
				85.0	5960	11930	69.0	5960	9450				78.0	5960	10600
				90.0	5960	11930	74.0	5960	9900				86.0	5960	9650
20													93.0	5960	10420
													100.0	5960	11210
				65.4	5960	11250	56.0	5960	8440	99.0	5960	11480			
				70.0	5960	11930	59.5	5960	8440	107.0	5960	11930			
				75.0	5960	11930	62.0	5960	8780	113.0	5960	11930			
				81.4	5960	11930	64.5	5960	9000	120.0	5960	11930			
				85.0	5960	11930	68.5	5960	9230	127.0	5960	11930			
				90.0	5960	11930	73.0	5960	9680	135.0	5960	11930			
				95.0	5960	11930	78.0	5960	10350	142.0	5960	11930			
				100.0	5960	11930				149.0	5960	11930			

WORKING VALUES FOR ONE 3/4" POWER DRIVEN RIVET OR TURNED BOLT IN REAMED HOLE IN CHANNEL AND BEAM WEBS

Shear @ 13500

Single Shear Bearing @ 24000

Double Shear Bearing @ 30000

Depth in Inches	Amer. Std. Beams			Bethlehem Beams			Beth. Girder Beams			Carnegie Beam Sect.						
	Weight		Bearing	Weight		Bearing	Weight		Bearing	Weight		Bearing		Weight		Bearing
	Per Foot	Single Shear		Per Foot	Single Shear		Per Foot	Single Shear		Per Foot	Single Shear	Per Foot	Single Shear			
21										55.0	5960	8100	104.0	5960	10460	
										58.0	5960	8100	112.0	5960	11230	
										64.0	5960	8910	120.0	5960	11930	
										70.0	5960	9740	128.0	5960	11930	
										76.0	5960	10550	136.0	5960	11930	
										80.0	5960	9860				
										86.0	5960	10580				
22				54.5	5960	8100	101.0	5960	10130							
				58.0	5960	8100	108.0	5960	10800							
				62.5	5960	8330	116.0	5960	11480							
				67.5	5960	8780	124.0	5960	11930							
				73.0	5960	9340	132.0	5960	11930							
				77.0	5960	9560										
				83.0	5960	10240										
24	79.9	5960	11250	70.0	5960	8890	107.0	5960	10910	70.0	5960	9000	130.0	5960	11930	
	85.0	5960	11930	73.5	5960	8890	113.0	5960	11250	76.0	5960	9110	140.0	5960	11930	
	90.0	5960	11930	79.5	5960	9680	120.0	5960	11930	85.0	5960	10170	150.0	5960	11930	
	95.0	5960	11930	84.5	5960	10350	128.0	5960	11930	94.0	5960	11230	160.0	5960	11930	
	100.0	5960	11930	90.5	5960	10690	132.0	5960	11930	100.0	5960	10130				
	105.9	5960	11930	95.5	5960	11360	140.0	5960	11930	110.0	5960	11120				
	110.0	5960	11930	99.5	5960	11810	148.0	5960	11930	120.0	5960	11930				
26	115.0	5960	11930	104.5	5960	11930										
	120.0	5960	11930													
				81.0	5960	9900	138.0	5960	11930							
				85.5	5960	10130	144.0	5960	11930							
27				91.0	5960	10580	151.0	5960	11930							
				98.0	5960	11250	160.0	5960	11930							
										85.0	5960	10370	145.0	5960	11930	
										91.0	5960	10370	160.0	5960	11930	
										101.0	5960	11480	175.0	5960	11930	
28										112.0	5960	11930	190.0	5960	11930	
										124.0	5960	11930				
										137.0	5960	11930				
				85.0	5960	10130	145.0	5960	11930							
				91.0	5960	10130	156.0	5960	11930							
				97.0	5960	10580	165.0	5960	11930							
30				104.0	5960	11250	175.0	5960	11930							
				112.0	5960	11930	186.0	5960	11930							
				119.0	5960	11930										
				133.0	5960	11930										
				110.0	5960	11700	173.0	5960	11930	115.0	5960	11930	180.0	5960	11930	
				115.0	5960	11930	180.0	5960	11930	126.0	5960	11930	200.0	5960	11930	
				121.0	5960	11930	190.0	5960	11930	138.0	5960	11930	220.0	5960	11930	
33				129.0	5960	11930	200.0	5960	11930	151.0	5960	11930	240.0	5960	11930	
				137.0	5960	11930	220.0	5960	11930	165.0	5960	11930				
				149.0	5960	11930	240.0	5960	11930							
				163.0	5960	11930										
				125.0	5960	11930	200.0	5960	11930	125.0	5960	11930	200.0	5960	11930	
36				135.0	5960	11930	210.0	5960	11930	138.0	5960	11930	220.0	5960	11930	
				143.0	5960	11930	220.0	5960	11930	152.0	5960	11930	240.0	5960	11930	
				152.0	5960	11930	230.0	5960	11930	167.0	5960	11930	260.0	5960	11930	
				165.0	5960	11930	245.0	5960	11930							
36				260.0	5960	11930										
				147.0	5960	11930	230.0	5960	11930	147.0	5960	11930	230.0	5960	11930	
				155.0	5960	11930	240.0	5960	11930	160.0	5960	11930	250.0	5960	11930	
				164.0	5960	11930	250.0	5960	11930	175.0	5960	11930	275.0	5960	11930	
				173.0	5960	11930	260.0	5960	11930	192.0	5960	11930	300.0	5960	11930	
			190.0	5960	11930	280.0	5960	11930								
						300.0	5960	11930								

WORKING VALUES FOR ONE 3/4" HAND DRIVEN RIVET OR UNFINISHED BOLT IN CHANNEL AND BEAM WEBS

Shear @ 10000

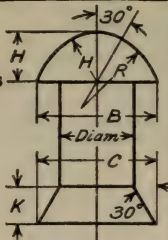
Single Shear Bearing @ 16000

Double Shear Bearing @ 20000

Depth in Inches	Amer. Std. Beams			Bethlehem Beams			Beth. Girder Beams			Carnegie Beam Sect.					
	Weight		Bearing		Weight		Bearing			Weight		Bearing		Weight	
	Per Foot	Single Shear	Double Shear	Per Foot	Single Shear	Double Shear	Per Foot	Single Shear	Double Shear	Per Foot	Single Shear	Double Shear	Per Foot	Single Shear	Double Shear
21										55.0	4320	5400	104.0	4420	6980
										58.0	4320	5400	112.0	4420	7490
										64.0	4420	5940	120.0	4420	8030
										70.0	4420	6500	128.0	4420	8550
										76.0	4420	7050	136.0	4420	8840
										80.0	4420	6570			
										86.0	4420	7050			
										92.0	4420	7530			
22										98.0	4420	8030			
				54.5	4320	5400	101.0	4420	6750						
				58.0	4320	5400	108.0	4420	7200						
				62.5	4420	5550	116.0	4420	7650						
				67.5	4420	5850	124.0	4420	8180						
				73.0	4420	6230	132.0	4420	8630						
				77.0	4420	6380									
				83.0	4420	6830									
24				89.0	4420	7280									
				96.5	4420	7880									
	79.9	4420	7500	70.0	4420	5930	107.0	4420	7280	70.0	4420	6000	130.0	4420	8210
	85.0	4420	8440	73.5	4420	5930	113.0	4420	7500	76.0	4420	6080	140.0	4420	8820
	90.0	4420	8840	79.5	4420	6450	120.0	4420	7950	83.0	4420	6780	150.0	4420	8840
	95.0	4420	8840	84.5	4420	6900	128.0	4420	8550	94.0	4420	7490	160.0	4420	8840
	100.0	4420	8840	90.5	4420	7130	132.0	4420	7550	100.0	4420	6750			
	105.9	4420	8840	95.5	4420	7580	140.0	4420	8840	110.0	4420	7410			
26	110.0	4420	8840	99.5	4420	7880	148.0	4420	8840	120.0	4420	8090			
	115.0	4420	8840	104.5	4420	8250									
	120.0	4420	8840												
				81.0	4420	6600	138.0	4420	8700						
27				85.5	4420	6750	144.0	4420	8840						
				91.0	4420	7050	151.0	4420	8840						
				98.0	4420	7500	160.0	4420	8840						
										85.0	4420	6920	145.0	4420	8700
28										91.0	4420	6920	160.0	4420	8840
										101.0	4420	7650	175.0	4420	8840
										112.0	4420	8490	190.0	4420	8840
										124.0	4420	8840			
										137.0	4420	8840			
30				85.0	4420	6750									
				91.0	4420	6750	145.0	4420	8780						
				97.0	4420	7050	156.0	4420	8840						
				104.0	4420	7500	165.0	4420	8840						
				112.0	4420	8030	175.0	4420	8840						
				119.0	4420	8480	186.0	4420	8840						
				133.0	4420	8840									
33				110.0	4420	7800	173.0	4420	8840	115.0	4420	7950	180.0	4420	8840
				115.0	4420	7950	180.0	4420	8840	126.0	4420	8720	200.0	4420	8840
				121.0	4420	8250	190.0	4420	8840	138.0	4420	8840	220.0	4420	8840
				129.0	4420	8700	200.0	4420	8840	151.0	4420	8840	240.0	4420	8840
				137.0	4420	8840	220.0	4420	8840	165.0	4420	8840			
				149.0	4420	8840	240.0	4420	8840						
				163.0	4420	8840									
36				125.0	4420	8100	200.0	4420	8840	125.0	4420	8840	200.0	4420	8840
				135.0	4420	8700	210.0	4420	8840	138.0	4420	8840	220.0	4420	8840
				143.0	4420	8840	220.0	4420	8840	152.0	4420	8840	240.0	4420	8840
				152.0	4420	8840	230.0	4420	8840	167.0	4420	8840	260.0	4420	8840
				165.0	4420	8840	245.0	4420	8840						
							260.0	4420	8840						
36				147.0	4420	8840	230.0	4420	8840	147.0	4420	8840	230.0	4420	8840
				155.0	4420	8840	240.0	4420	8840	160.0	4420	8840	250.0	4420	8840
				164.0	4420	8840	250.0	4420	8840	175.0	4420	8840	275.0	4420	8840
				173.0	4420	8840	260.0	4420	8840	192.0	4420	8840	300.0	4420	8840
				190.0	4420	8840	280.0	4420	8840						
							300.0	4420	8840						

DIMENSIONS, WEIGHTS AND CONVENTIONAL SIGNS FOR RIVETS

















DIMENSIONS OF RIVET HEADS (DRIVEN)

FORMULAE		Diam of Rivet	BUTTON HEAD			COUNTERSUNK	
			Diam. B	Height H	Radius R	Diam. C	Height K
Diam. Head B = $1.5 D + \frac{1}{8}$		$\frac{3}{8}$	$\frac{11}{16}$	$\frac{5}{16}$	$\frac{7}{16}$	$\frac{9}{16}$	$\frac{3}{16}$
Height of Hd. H = $.425 B$		$\frac{1}{2}$	$\frac{1}{8}$	$\frac{3}{8}$	$\frac{9}{16}$	$\frac{3}{4}$	$\frac{1}{4}$
Long Rad. R = $1.5 H$		$\frac{5}{8}$	$1 \frac{1}{4}$	$\frac{1}{2}$	$\frac{11}{16}$	1	$\frac{5}{16}$
Short Rad. = H		$\frac{3}{4}$	$1 \frac{1}{4}$	$\frac{1}{2}$	$\frac{13}{16}$	$1 \frac{3}{16}$	$\frac{3}{8}$
Depth of Countersunk K = $.5 D$		$\frac{7}{8}$	$1 \frac{7}{8}$	$\frac{5}{8}$	$\frac{15}{16}$	$1 \frac{3}{8}$	$\frac{7}{16}$
		1	$1 \frac{5}{8}$	$\frac{11}{16}$	1	$1 \frac{9}{16}$	$\frac{1}{2}$
		$1 \frac{1}{8}$	$1 \frac{13}{16}$	$\frac{3}{4}$	$1 \frac{1}{8}$	$1 \frac{3}{4}$	$\frac{9}{16}$
		$1 \frac{1}{4}$	2	$\frac{7}{8}$	$1 \frac{1}{4}$	2	$\frac{5}{8}$
		$1 \frac{3}{8}$	$2 \frac{3}{16}$	$\frac{15}{16}$	$1 \frac{3}{8}$	$2 \frac{3}{16}$	$1 \frac{1}{16}$
		$1 \frac{1}{2}$	$2 \frac{3}{8}$	1	$1 \frac{1}{2}$	$2 \frac{3}{8}$	$\frac{3}{4}$

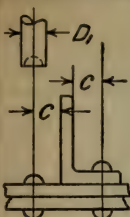
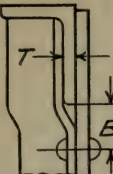


WEIGHTS OF 100 BUTTON HEAD STEEL RIVETS

Length in Inches under Head	Diameter of Rivets in Inches									
	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	1"	$1 \frac{1}{8}$	$1 \frac{1}{4}$	$1 \frac{3}{8}$	$1 \frac{1}{2}$
1	4.8	10.0	17	28						
$1 \frac{1}{4}$	5.6	11.4	20	31	44	60				
$1 \frac{1}{2}$	6.4	12.7	22	34	48	65	87			
$1 \frac{3}{4}$	7.2	14.1	24	37	52	70	93			
2	7.9	15.5	26	40	56	75	100	133	167	206
$2 \frac{1}{4}$	8.7	16.9	28	43	60	81	107	141	177	218
$2 \frac{1}{2}$	9.5	18.3	30	46	64	86	114	149	187	230
$2 \frac{3}{4}$	10.3	19.7	33	49	69	91	120	158	197	242
3	11.1	21.0	35	52	73	96	127	166	208	254
$3 \frac{1}{4}$	11.9	22.4	37	55	77	102	134	174	218	266
$3 \frac{1}{2}$	12.6	23.8	39	58	81	107	141	183	228	278
$3 \frac{3}{4}$	13.4	25.2	41	62	85	112	148	191	238	290
4	26.6	43	65	89	118	154	199	248	302
$4 \frac{1}{4}$	28.0	46	68	93	123	161	208	258	314
$4 \frac{1}{2}$	29.4	48	71	97	128	168	216	268	327
$4 \frac{3}{4}$	30.7	50	74	101	133	175	224	278	339
5	32.1	52	77	105	139	181	233	288	351
$5 \frac{1}{4}$	54	80	110	144	188	241	298	363
$5 \frac{1}{2}$	56	83	114	149	195	249	308	375
$5 \frac{3}{4}$	58	86	118	154	201	258	318	387
6	61	89	122	160	208	266	329	399
$6 \frac{1}{2}$	95	130	170	222	283	349	423
7	102	138	181	235	300	369	447
$7 \frac{1}{2}$	108	146	191	249	316	389	471
Weight of 100 Button Heads Only	1.7	4.4	9	15	23	33	46	66	87	110

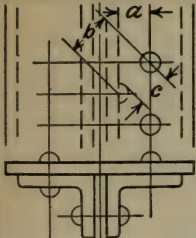
CONVENTIONAL SIGNS FOR RIVETING

SHOP RIVETS				FIELD RIVETS				
Two Full Heads	Countersunk and Chipped			Two Full Heads	Countersunk and Chipped			
	Near Side	Far Side	Both Sides		Near Side	Far Side	Both Sides	
								
SHOP RIVETS								
Countersunk, Not Chipped, 1/8 High			Flattened, 1/4 High, 1/2 and 5/8 Rivets			Flattened, 3/8 High, 3/4 to 1" Rivets		
Near Side	Far Side	Both Sides	Near Side	Far Side	Both Sides	Near Side	Far Side	Both Sides
								

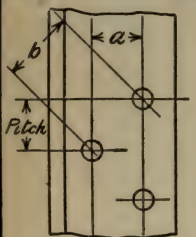
RIVETING DETAILS

DRIVING CLEARANCE				CRIMPS		GAGES FOR ANGLES																																											
	Riv. Diam.	Die D ₁	Clear C																																														
	$\frac{3}{8}$	$1\frac{1}{2}$	$\frac{7}{8}$																																														
	$\frac{1}{2}$	$1\frac{3}{4}$	1																																														
	$\frac{5}{8}$	2	$1\frac{1}{8}$																																														
	$\frac{3}{4}$	$2\frac{1}{4}$	$1\frac{1}{4}$																																														
	$\frac{7}{8}$	$2\frac{3}{4}$	$1\frac{3}{8}$																																														
	1	$2\frac{3}{2}$	$1\frac{1}{2}$																																														
	$1\frac{1}{8}$	3	$1\frac{5}{8}$																																														
	$1\frac{1}{4}$	$3\frac{1}{4}$	$1\frac{3}{4}$																																														
	$1\frac{3}{8}$	$3\frac{1}{2}$	$1\frac{7}{8}$																																														
	$1\frac{1}{2}$	$3\frac{3}{4}$	2																																														
	$B = T + 1\frac{1}{2}"$ (Min. 2")																																																
																																																	
<table><tr><td>Leg.</td><td>$1\frac{3}{4}$</td><td>2</td><td>$2\frac{1}{2}$</td><td>3</td><td>$3\frac{1}{2}$</td><td>4</td><td>5</td><td>6</td><td>7</td><td>8</td></tr><tr><td>g₁</td><td>1</td><td>$1\frac{1}{8}$</td><td>$1\frac{3}{8}$</td><td>$1\frac{5}{8}$</td><td>2</td><td>$2\frac{1}{2}$</td><td>3</td><td>$3\frac{1}{2}$</td><td>4</td><td>$4\frac{1}{2}$</td></tr><tr><td>g₂</td><td>...</td><td>...</td><td>...</td><td>...</td><td>...</td><td>...</td><td>2</td><td>...</td><td>$2\frac{1}{2}$</td><td>3</td></tr><tr><td>g₃</td><td>...</td><td>...</td><td>...</td><td>...</td><td>...</td><td>...</td><td>$1\frac{3}{4}$</td><td>$2\frac{1}{4}$</td><td>$2\frac{3}{4}$</td><td>3</td></tr></table>					Leg.	$1\frac{3}{4}$	2	$2\frac{1}{2}$	3	$3\frac{1}{2}$	4	5	6	7	8	g ₁	1	$1\frac{1}{8}$	$1\frac{3}{8}$	$1\frac{5}{8}$	2	$2\frac{1}{2}$	3	$3\frac{1}{2}$	4	$4\frac{1}{2}$	g ₂	2	...	$2\frac{1}{2}$	3	g ₃	$1\frac{3}{4}$	$2\frac{1}{4}$	$2\frac{3}{4}$	3	
Leg.	$1\frac{3}{4}$	2	$2\frac{1}{2}$		3	$3\frac{1}{2}$	4	5	6	7	8																																						
g ₁	1	$1\frac{1}{8}$	$1\frac{3}{8}$	$1\frac{5}{8}$	2	$2\frac{1}{2}$	3	$3\frac{1}{2}$	4	$4\frac{1}{2}$																																							
g ₂	2	...	$2\frac{1}{2}$	3																																							
g ₃	$1\frac{3}{4}$	$2\frac{1}{4}$	$2\frac{3}{4}$	3																																							
<table><tr><td>Max. Riv</td><td>$\frac{1}{2}$</td><td>$\frac{5}{8}$</td><td>$\frac{3}{4}$</td><td>$\frac{7}{8}$</td><td>$\frac{7}{8}$</td><td>$\frac{7}{8}$</td><td>$\frac{7}{8}$</td><td>$\frac{7}{8}$</td><td>1</td><td>$1\frac{1}{8}$</td></tr></table>					Max. Riv	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	1	$1\frac{1}{8}$																																		
Max. Riv	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	$\frac{7}{8}$	1	$1\frac{1}{8}$																																							

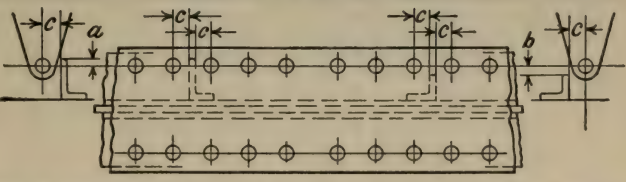
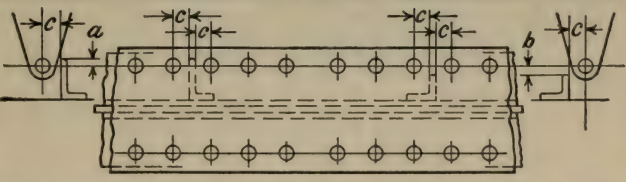
MINIMUM PITCH FOR MACHINE RIVETING

	Riv. Diam. D	Std. c	Std. b	a													
				$1\frac{1}{8}$	$1\frac{1}{4}$	$1\frac{3}{8}$	$1\frac{1}{2}$	$1\frac{5}{8}$	$1\frac{3}{4}$	$1\frac{7}{8}$	2	$2\frac{1}{8}$	$2\frac{1}{4}$	$2\frac{3}{8}$	$2\frac{1}{2}$	$2\frac{3}{4}$	
	$\frac{3}{8}$	$\frac{7}{8}$	1	$\frac{3}{16}$	$\frac{1}{4}$	0	$\frac{1}{2}$	0
	$\frac{1}{2}$	1	1	$\frac{1}{8}$	$\frac{3}{8}$	$\frac{1}{2}$
	$\frac{5}{8}$	$1\frac{1}{8}$	$1\frac{1}{8}$	$\frac{1}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	1
	$\frac{3}{4}$	$1\frac{1}{4}$	$1\frac{1}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	1	$\frac{1}{2}$
	$\frac{7}{8}$	$1\frac{3}{8}$	2	$1\frac{1}{2}$	$1\frac{1}{8}$	$\frac{3}{4}$	$\frac{7}{8}$	0
	1	$1\frac{1}{2}$	2	$\frac{3}{16}$	$1\frac{5}{8}$	$1\frac{1}{2}$	$1\frac{3}{8}$	$\frac{7}{8}$	$\frac{1}{2}$	0
	$1\frac{1}{8}$	$1\frac{5}{8}$	2	$\frac{1}{4}$	$1\frac{3}{4}$	$1\frac{1}{2}$	$1\frac{5}{8}$	$\frac{7}{8}$	$\frac{1}{2}$	$\frac{1}{8}$	0
	$1\frac{1}{4}$	$1\frac{3}{4}$	2	$\frac{3}{8}$	2	$1\frac{1}{2}$	$1\frac{3}{4}$	$\frac{1}{2}$	$1\frac{1}{4}$	$\frac{1}{8}$	0
	$1\frac{3}{8}$	$1\frac{7}{8}$	2	$\frac{1}{2}$	$1\frac{1}{2}$	$1\frac{3}{4}$	$\frac{1}{2}$	$1\frac{1}{4}$	$\frac{1}{8}$	$1\frac{1}{2}$	$1\frac{1}{4}$	$\frac{1}{2}$	0
	$1\frac{1}{2}$	2	3	$1\frac{1}{2}$	$\frac{1}{2}$	2	$1\frac{1}{4}$	$1\frac{1}{2}$	$1\frac{1}{4}$	$\frac{1}{2}$	$1\frac{1}{8}$

MINIMUM PITCH TO MAINTAIN 3 DIAMETERS C TO C

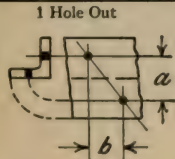
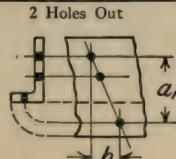
	Riv. Diam. D	Min. CtoC b	a													
			1	$1\frac{1}{4}$	$1\frac{1}{2}$	$1\frac{3}{4}$	2	$2\frac{1}{4}$	$2\frac{1}{2}$	$2\frac{3}{4}$	3	$3\frac{1}{4}$	$3\frac{1}{2}$	$3\frac{3}{4}$	4	$4\frac{1}{4}$
	$\frac{3}{8}$	$1\frac{1}{8}$	$\frac{1}{2}$	0
	$\frac{1}{2}$	$1\frac{1}{4}$	$\frac{3}{4}$	$\frac{1}{2}$
	$\frac{5}{8}$	$1\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{4}$
	$\frac{3}{4}$	$1\frac{3}{4}$	1	$\frac{1}{2}$
	$\frac{7}{8}$	$1\frac{7}{8}$	$1\frac{1}{4}$	$\frac{3}{4}$
	1	2	$1\frac{1}{2}$	1
	$1\frac{1}{8}$	$2\frac{1}{8}$	$1\frac{3}{4}$	$1\frac{1}{2}$
	$1\frac{1}{4}$	$2\frac{1}{4}$	$2\frac{1}{4}$	$1\frac{3}{4}$
	$1\frac{3}{8}$	$2\frac{3}{8}$	$2\frac{1}{2}$	$2\frac{1}{4}$
	$1\frac{1}{2}$	$2\frac{1}{2}$	3	$2\frac{3}{4}$

COVER PLATE RIVETING

	a	c		b	c
	$\frac{1}{2}$	$2\frac{1}{2}$...	$2\frac{1}{2}$
	1	$2\frac{3}{4}$		$\frac{3}{4}$	$2\frac{3}{4}$
	$1\frac{1}{2}$	$3\frac{1}{4}$		$1\frac{1}{4}$	$2\frac{1}{4}$
	2	$3\frac{3}{4}$		1	$2\frac{1}{2}$
	$2\frac{1}{2}$	$4\frac{1}{4}$		$1\frac{1}{2}$	$2\frac{3}{4}$
	3	$4\frac{3}{4}$		$1\frac{3}{4}$	3
	$3\frac{1}{2}$	$5\frac{1}{4}$		2	$3\frac{1}{4}$
	4	$5\frac{3}{4}$		$2\frac{1}{4}$	$3\frac{1}{2}$
	5	$6\frac{1}{4}$		$2\frac{3}{4}$	$3\frac{3}{4}$
	6	$6\frac{3}{4}$		$3\frac{1}{2}$	$4\frac{1}{4}$

The use of hand pneumatic hammers is avoided where construction permits these clearances.


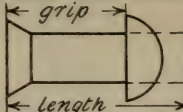

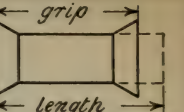
STAGGER OF RIVETS TO MAINTAIN NET SECTION

1 Hole Out		2 Holes Out		3 Rivet		7/8 Rivet		3/4 Rivet		7/8 Rivet	
				a	b	b	a1	b	b		
1 1/2		1 1/2		1	1 5/8	1 3/4	5	3 1/16	3 5/16		
2		2		2	1 7/8	2	5 1/2	3 1/4	3 1/2		
2 1/2		2 1/2		2	2 1/4	2 1/4	6	3 3/8	3 5/8		
3		3		2	2 3/4	2 3/4	6 1/2	3 1/2	3 3/4		
3 1/2		3 1/2		3	2 7/8	2 5/8	7	3 5/8	3 7/8		
4		4		3 1/2	2 9/16	2 3/4	7 1/2	3 3/4	4		
4 1/2		4 1/2		4	2 13/16	3	8	3 7/8	4 1/8		
5		5		4 1/2	2 15/16	3 1/8	8 1/2	4	4 1/4		

5/8" rivets, can be taken at 1/8" less than for 3/4".
1" rivets, can be taken at 1/8" more than for 7/8".

$\frac{5}{8}"$ rivets, can be taken at $\frac{1}{8}"$ less than for $\frac{3}{4}"$.
 $1"$ rivets, can be taken at $\frac{1}{8}"$ more than for $\frac{7}{8}"$.

LENGTHS OF UNDRIVEN RIVETS FOR VARIOUS LENGTHS OF GRIP

															
BUTTON HEAD								COUNTERSUNK							
Grip	Diameter of Rivet							Grip	Diameter of Rivet						
	1/2	5/8	3/4	7/8	1"	1 1/4	1 1/2		1/2	5/8	3/4	7/8	1"	1 1/4	1 1/2
1/2	1 5/8	1 3/4	1 7/8	2	2 1/8	2 1/4		1/2	1 1/8	1 1/4	1 1/8	1 1/4	1 3/8	1 1/2	
5/8	1 3/4	1 7/8	2	2 1/8	2 1/4	2 3/8		5/8	1 3/8	1 3/8	1 3/8	1 3/8	1 1/2	1 5/8	
3/4	1 7/8	2	2 1/8	2 1/4	2 3/8	2 1/2		3/4	1 1/2	1 1/2	1 1/2	1 1/2	1 5/8		
7/8	2	2 1/8	2 1/4	2 3/8	2 1/2			7/8							
1	2 1/4	2 3/8	2 3/8	2 1/2	2 5/8	2 7/8	3 1/8	1	1 5/8	1 5/8	1 5/8	1 3/4	1 3/4	1 7/8	2
1 1/8	2 3/8	2 1/2	2 1/2	2 5/8	2 3/4	2 7/8	3 1/8	1 1/8	1 3/4	1 3/4	1 7/8	1 7/8	1 7/8	2 1/8	2 1/8
1 1/4	2 1/2	2 5/8	2 5/8	2 3/4	2 7/8	3	3 1/8	1 1/4	2	2	2	2	2	2 1/8	2 1/4
1 1/2	2 5/8	2 3/4	2 3/4	2 7/8	3	3 1/4	3 1/2	1 1/2	2 1/8	2 1/8	2 1/8	2 1/4	2 1/4	2 3/8	2 1/2
1 5/8	2 7/8	2 7/8	3	3 1/8	3 1/4	3 3/8	3 5/8	1 5/8	2 1/4	2 1/4	2 1/4	2 3/8	2 3/8	2 5/8	2 5/8
1 3/4	3	3	3 1/4	3 1/4	3 3/8	3 1/2	3 3/8	1 3/4	2 3/8	2 3/8	2 3/8	2 1/2	2 1/2	2 3/4	2 3/4
1 7/8	3 1/4	3 1/8	3 1/4	3 1/4	3 1/2	3 5/8	3 7/8	1 7/8	2 5/8	2 5/8	2 5/8	2 5/8	2 5/8	2 7/8	2 7/8
2	3 1/4	3 3/8	3 3/8	3 3/8	3 5/8	3 7/8	4	2	2 3/4	2 3/4	2 3/4	2 3/4	2 3/4	2 7/8	3
1 1/8	3 5/8	3 5/8	3 3/4	3 7/8	4	4 1/8	4 1/4	2 1/8	2 7/8	2 7/8	2 7/8	2 7/8	3	3 1/8	3 1/8
1 1/4	3 3/4	3 7/8	3 7/8	4	4 1/8	4 1/4	4 1/2	1 1/4	3 1/4	3 1/8	3 1/8	3 1/8	3 1/4	3 3/8	3 3/8
1 1/2	4	4	4	4 1/8	4 1/4	4 3/8	4 5/8	1 1/2	3 3/8	3 3/8	3 3/8	3 3/8	3 3/8	3 3/8	3 1/2
1 5/8	4 1/8	4 1/8	4 1/8	4 1/8	4 3/8	4 5/8	5	1 5/8	3 1/2	3 1/2	3 1/2	3 1/2	3 1/2	3 5/8	3 5/8
1 3/4	4 1/4	4 1/4	4 1/4	4 1/4	4 3/8	4 5/8	5 1/8	1 3/4	3 5/8	3 5/8	3 5/8	3 5/8	3 5/8	3 3/4	3 3/4
1 7/8	4 3/8	4 3/8	4 3/8	4 3/8	4 5/8	5 1/8	5 1/8	1 7/8	3 3/4	3 3/4	3 3/4	3 3/4	3 3/4	3 7/8	4
2	4 5/8	4 5/8	4 5/8	4 5/8	5 1/8	5 1/8	5 1/8	2	4	3 7/8	3 7/8	3 7/8	3 7/8	4	4 1/8
1 1/8	4 7/8	4 7/8	4 7/8	4 7/8	5 1/8	5 1/8	5 1/8	1 1/8	4 1/8	4 1/8	4 1/8	4 1/8	4 1/8	4 1/8	4 1/4
1 1/4	5	5	5	5	5 1/8	5 1/8	5 1/2	1 1/4	4 3/8	4 3/8	4 3/8	4 3/8	4 3/8	4 3/8	4 1/2
1 1/2	5 1/8	5 1/8	5 1/8	5 1/8	5 1/8	5 1/2	5 5/8	1 1/2	4 1/2	4 1/2	4 1/2	4 1/2	4 1/2	4 1/2	4 1/2
1 5/8	5 3/8	5 3/8	5 3/8	5 3/8	5 1/2	5 5/8	6	1 5/8	4 5/8	4 5/8	4 5/8	4 5/8	4 5/8	4 5/8	4 3/4
1 3/4	5 1/2	5 1/2	5 1/2	5 1/2	5 3/4	5 7/8	6 1/8	1 3/4	4 3/4	4 3/4	4 3/4	4 3/4	4 3/4	4 7/8	4 7/8
1 7/8	5 3/4	5 3/4	5 3/4	5 3/4	5 7/8	6	6 1/4	1 7/8	5	5	5	5	5	5	5
2	5 7/8	5 7/8	5 7/8	5 7/8	6	6 1/4	6 1/4	2	5 1/8	5 1/8	5 1/8	5 1/8	5 1/8	5 1/8	5 1/8
1 1/8	6 1/4	6 1/4	6 1/4	6 1/4	6 1/4	6 1/4	6 3/8	1 1/8	5 1/4	5 1/4	5 1/4	5 1/4	5 1/4	5 1/4	5 1/4
1 1/4	6 3/8	6 3/8	6 3/8	6 3/8	6 3/8	6 3/8	6 5/8	1 1/4	5 3/8	5 3/8	5 3/8	5 3/8	5 3/8	5 3/8	5 1/2
1 1/2	6 5/8	6 5/8	6 5/8	6 5/8	6 3/4	6 7/8	6 7/8	1 1/2	5 5/8	5 5/8	5 5/8	5 5/8	5 5/8	5 5/8	5 3/4
1 5/8	6 7/8	6 7/8	6 7/8	6 7/8	6 7/8	7	7 1/8	1 5/8	5 7/8	5 7/8	5 7/8	5 7/8	5 7/8	5 7/8	5 7/8
1 3/4	7	7	7	7	7	7	7 1/4	1 3/4	6	6	6	6	6	6	6
1 7/8	7 1/8	7 1/8	7 1/8	7 1/8	7 1/8	7 1/4	7 1/2	1 7/8	6 1/8	6 1/8	6 1/8	6 1/8	6 1/8	6 1/8	6 1/4
2	7 1/4	7 1/4	7 1/4	7 1/4	7 1/4	7 1/4	7 5/8	2	6 3/8	6 3/8	6 3/8	6 3/8	6 3/8	6 3/8	6 3/8
1 1/8	7 3/8	7 3/8	7 3/8	7 3/8	7 3/8	7 3/8	7 7/8	1 1/8	6 1/2	6 1/2	6 1/2	6 1/2	6 1/2	6 1/2	6 1/2
1 1/4	7 5/8	7 5/8	7 5/8	7 5/8	7 5/8	7 5/8	8	1 1/4	6 5/8	6 5/8	6 5/8	6 5/8	6 5/8	6 5/8	6 5/8
1 1/2	7 7/8	7 7/8	7 7/8	7 7/8	7 7/8	7 7/8	8 1/8	1 1/2	6 3/4	6 3/4	6 3/4	6 3/4	6 3/4	6 3/4	6 7/8
1 5/8	8	8	8	8	8	8	8 1/4	1 5/8	6 7/8	6 7/8	6 7/8	6 7/8	6 7/8	6 7/8	7
1 3/4	8 1/8	8 1/8	8 1/8	8 1/8	8 1/8	8 1/8	8 3/8	1 3/4	7	7	7	7	7	7	7 1/8
1 7/8	8 3/8	8 3/8	8 3/8	8 3/8	8 3/8	8 3/8	8 7/8	1 7/8	7 1/4	7 1/4	7 1/4	7 1/4	7 1/4	7 1/4	7 1/4
2	8 7/8	8 7/8	8 7/8	8 7/8	8 7/8	8 7/8	9 1/8	2	7 3/8	7 3/8	7 3/8	7 3/8	7 3/8	7 3/8	7 3/8
1 1/8	9	9	9	9	9	9	9 1/4	1 1/8	7 7/8	7 7/8	7 7/8	7 7/8	7 7/8	7 7/8	7 7/8
1 1/4	9 1/8	9 1/8	9 1/8	9 1/8	9 1/8	9 1/4	9 3/8	1 1/4	8	8	8	8	8	8	8
1 1/2	9 3/8	9 3/8	9 3/8	9 3/8	9 3/8	9 3/8	9 5/8	1 1/2	8 1/4	8 1/4	8 1/4	8 1/4	8 1/4	8 1/4	8 1/4
1 5/8	9 5/8	9 5/8	9 5/8	9 5/8	9 5/8	9 5/8	10	1 5/8	8 3/8	8 3/8	8 3/8	8 3/8	8 3/8	8 3/8	8 3/8
1 3/4	9 7/8	9 7/8	9 7/8	9 7/8	9 7/8	9 7/8	10 1/8	1 3/4	8 7/8	8 7/8	8 7/8	8 7/8	8 7/8	8 7/8	8 7/8
1 7/8	10	10	10	10	10	10	10 1/4	1 7/8	9	9	9	9	9	9	9
2	10 1/8	10 1/8	10 1/8	10 1/8	10 1/8	10 1/8	10 3/8	2	9 1/4	9 1/4	9 1/4	9 1/4	9 1/4	9 1/4	9 1/4
1 1/8	10 3/8	10 3/8	10 3/8	10 3/8	10 3/8	10 3/8	10 5/8	1 1/8	9 3/8	9 3/8	9 3/8	9 3/8	9 3/8	9 3/8	9 3/8
1 1/4	10 5/8	10 5/8	10 5/8	10 5/8	10 5/8	10 5/8	11	1 1/4	9 5/8	9 5/8	9 5/8	9 5/8	9 5/8	9 5/8	9 5/8
1 1/2	11	11	11	11	11	11	11 1/4	1 1/2	10	10	10	10	10	10	10
1 5/8	11 1/4	11 1/4	11 1/4	11 1/4	11 1/4	11 1/4	11 3/8	1 5/8	10 1/4	10 1/4	10 1/4	10 1/4	10 1/4	10 1/4	10 1/4
1 3/4	11 3/8	11 3/8	11 3/8	11 3/8	11 3/8	11 3/8	11 5/8	1 3/4	10 3/8	10 3/8	10 3/8	10 3/8	10 3/8	10 3/8	10 3/8
1 7/8	11 5/8	11 5/8	11 5/8	11 5/8	11 5/8	11 5/8	12	1 7/8	10 5/8	10 5/8	10 5/8	10 5/8	10 5/8	10 5/8	10 5/8

For 1 1/8" Rivets use lengths given above for 1 1/4", and for 1 3/8" Rivets those given for 1 1/2".

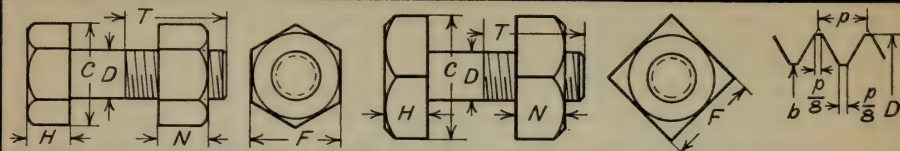
REDUCTION OF AREA IN PLATES FOR RIVET HOLES

Thickness of Plate	DIAMETER OF HOLE IN INCHES															
	1/4	5/16	3/8	7/16	1/2	9/16	5/8	11/16	3/4	13/16	7/8	15/16	1"	1 1/16	1 1/8	1 3/16
.170	.043	.053	.064	.074	.085	.096	.106	.117	.128	.138	.149	.159	.170	.181	.191	.202
.180	.045	.056	.068	.079	.090	.101	.113	.124	.135	.146	.158	.169	.180	.191	.203	.214
.1875	3/16	.047	.059	.070	.082	.094	.105	.117	.129	.141	.152	.164	.176	.188	.199	.211
.190		.048	.059	.071	.083	.095	.107	.119	.131	.143	.154	.166	.178	.190	.202	.214
.200		.050	.063	.075	.088	.100	.113	.125	.138	.150	.163	.175	.188	.200	.213	.225
.210		.053	.066	.079	.092	.105	.118	.131	.144	.158	.171	.184	.197	.210	.223	.236
.220		.055	.069	.083	.096	.110	.124	.138	.151	.165	.179	.193	.206	.220	.234	.248
.230		.058	.072	.086	.101	.115	.129	.144	.158	.173	.187	.201	.216	.230	.244	.259
.240		.060	.075	.090	.105	.120	.135	.150	.165	.180	.195	.210	.225	.240	.255	.270
.250	1/4	.063	.078	.094	.109	.125	.141	.156	.172	.188	.203	.219	.234	.250	.266	.281
.260		.065	.081	.098	.114	.130	.146	.163	.179	.195	.211	.228	.244	.260	.276	.293
.270		.068	.084	.101	.118	.135	.152	.169	.186	.203	.219	.236	.253	.270	.287	.304
.280		.070	.088	.105	.123	.140	.158	.175	.193	.210	.228	.245	.263	.280	.298	.315
.290		.073	.091	.109	.127	.145	.163	.181	.199	.218	.236	.254	.272	.290	.308	.326
.300		.075	.094	.113	.131	.150	.169	.188	.206	.225	.244	.263	.281	.300	.319	.338
.310		.078	.097	.116	.136	.155	.174	.194	.213	.233	.252	.271	.291	.310	.329	.349
.3125	5/16	.078	.098	.117	.137	.156	.176	.195	.215	.234	.254	.273	.293	.313	.332	.352
.320		.080	.100	.120	.140	.160	.180	.200	.220	.240	.260	.280	.300	.320	.340	.360
.330		.083	.103	.124	.144	.165	.186	.206	.227	.248	.268	.289	.309	.330	.351	.371
.340		.085	.106	.128	.149	.170	.191	.213	.234	.255	.276	.298	.319	.340	.361	.382
.350		.088	.109	.131	.153	.175	.197	.219	.241	.263	.284	.306	.328	.350	.372	.394
.360		.090	.113	.135	.158	.180	.203	.225	.248	.270	.293	.315	.338	.360	.383	.405
.370		.093	.116	.139	.162	.185	.208	.231	.254	.278	.301	.324	.347	.370	.393	.416
.375	3/8	.094	.117	.141	.164	.188	.211	.234	.258	.281	.305	.328	.352	.375	.398	.422
.380		.095	.119	.143	.166	.190	.214	.238	.261	.285	.309	.333	.356	.380	.404	.428
.390		.098	.122	.146	.171	.195	.219	.244	.268	.293	.317	.341	.366	.390	.414	.439
.400		.100	.125	.150	.175	.200	.225	.250	.275	.300	.325	.350	.375	.400	.425	.450
.410		.103	.128	.154	.179	.205	.231	.256	.282	.308	.333	.359	.384	.410	.436	.461
.420		.105	.131	.158	.184	.210	.236	.263	.289	.315	.341	.368	.394	.420	.446	.473
.430		.108	.134	.161	.188	.215	.242	.269	.296	.323	.349	.376	.403	.430	.457	.484
.4375	7/16	.109	.137	.164	.191	.219	.246	.273	.301	.328	.355	.383	.410	.438	.465	.492
.440		.110	.138	.165	.193	.220	.248	.275	.303	.330	.358	.385	.413	.440	.468	.495
.450		.113	.141	.169	.197	.225	.253	.281	.309	.338	.366	.394	.422	.450	.478	.506
.460		.115	.144	.173	.201	.230	.258	.286	.316	.345	.374	.403	.431	.460	.489	.518
.470		.118	.147	.176	.206	.235	.264	.294	.323	.353	.382	.411	.441	.470	.499	.528
.480		.120	.150	.180	.210	.240	.270	.300	.330	.360	.390	.420	.450	.480	.510	.540
.490		.123	.153	.184	.214	.245	.276	.306	.337	.368	.398	.429	.459	.490	.521	.551
.500	1/2	.125	.156	.188	.219	.250	.281	.313	.344	.375	.406	.438	.469	.500	.531	.562
.510		.128	.159	.191	.223	.255	.287	.319	.351	.383	.414	.446	.478	.510	.542	.574
.520		.130	.163	.195	.228	.260	.293	.325	.358	.390	.423	.455	.488	.520	.553	.585
.530		.133	.166	.199	.232	.265	.298	.331	.364	.398	.431	.464	.497	.530	.563	.596
.540		.135	.169	.203	.236	.270	.304	.338	.371	.405	.439	.473	.506	.540	.574	.608
.550		.138	.172	.206	.241	.275	.309	.344	.378	.413	.447	.481	.516	.550	.584	.619
.560		.140	.175	.210	.245	.280	.315	.350	.385	.420	.455	.490	.525	.560	.595	.630
.5625	9/16	.141	.176	.211	.246	.281	.316	.352	.387	.422	.457	.492	.527	.563	.598	.633
.570		.143	.178	.214	.249	.285	.321	.356	.392	.428	.463	.499	.534	.570	.606	.641
.580		.145	.181	.218	.254	.290	.326	.363	.399	.435	.471	.508	.544	.580	.616	.653
.590		.148	.184	.221	.258	.295	.332	.369	.406	.443	.479	.516	.553	.590	.627	.664
.600		.150	.188	.225	.263	.300	.338	.375	.413	.450	.488	.525	.563	.600	.638	.675
.610		.153	.191	.229	.267	.305	.343	.381	.419	.458	.496	.534	.572	.610	.648	.686
.620		.155	.194	.233	.271	.310	.349	.388	.426	.465	.504	.543	.581	.620	.659	.698
.625	5/8	.156	.195	.234	.273	.313	.352	.391	.430	.469	.508	.547	.586	.625	.664	.703
.630		.158	.197	.236	.276	.315	.354	.394	.433	.473	.512	.551	.591	.630	.669	.709
.640		.160	.200	.240	.280	.320	.360	.400	.440	.480	.520	.560	.600	.640	.680	.720
.650		.163	.203	.244	.284	.325	.366	.406	.447	.488	.528	.569	.609	.650	.691	.732
.660		.165	.206	.248	.289	.330	.371	.413	.454	.495	.536	.578	.619	.660	.701	.743
.670		.168	.209	.251	.293	.335	.377	.419	.461	.503	.544	.586	.628	.670	.712	.754
.680		.170	.213	.255	.298	.340	.383	.425	.468	.510	.553	.595	.638	.680	.723	.765
.6875	11/16	.172	.215	.258	.301	.344	.387	.430	.473	.516	.559	.602	.645	.688	.730	.773
.690		.173	.216	.259	.302	.345	.388	.431	.474	.518	.561	.604	.647	.690	.733	.776
.700		.175	.219	.263	.306	.350	.394	.438	.481	.525	.569	.613	.656	.700	.744	.788
.710		.178	.222	.266	.311	.355	.399	.444	.488	.533	.577	.621	.666	.710	.754	.799
.720		.180	.225	.270	.315	.360	.405	.450	.495	.540	.585	.630	.675	.720	.765	.810
.730		.183	.228	.274	.319	.365	.411	.456	.502	.548	.593	.639	.684	.730	.776	.821
.740		.185	.231	.278	.324	.370	.416	.463	.509	.555	.601	.648	.694	.740	.786	.833
.750	3/4	.188	.234	.281	.328	.375	.422	.469	.516	.563	.609	.656	.703	.750	.797	.844
.8125	13/16	.203	.254	.305	.355	.406	.457	.508	.559	.609	.660	.711	.762	.813	.863	.914
.875	7/8	.219	.273	.328	.383	.438	.492	.547	.602	.656	.711	.766	.820	.875	.930	.984
.9375	15/16	.234	.292	.352	.410	.469	.527	.586	.645	.703	.762	.820	.879	.938	.996	1.05
1.000	1"	.250	.313	.375	.438	.500	.563	.625	.688	.750	.813	.875	.938	1.00	1.06	1.13

The reduction of areas for holes or thicknesses of plates not listed, may be found by addition or multiplication. Thus for a 2 3/4" plate, multiply figure given for 1 1/16" plate by 4, or add figure given for 3/4" plate to twice that given for 1" plate.

DIMENSIONS AND WEIGHTS OF MACHINE BOLTS

DIMENSIONS

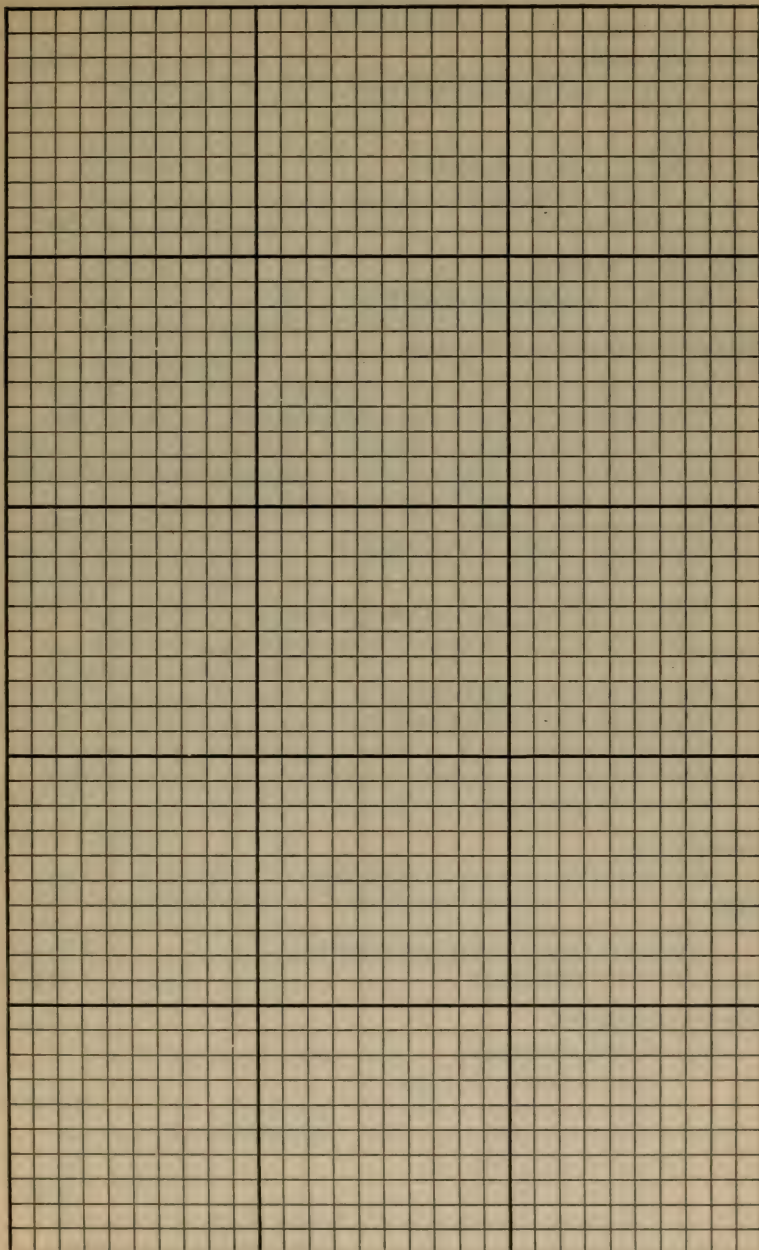


Diam. of Bolt	Bolt Head and Nut				Bolt Head Height	Nut Height	Thread Details										Diam. at Root of Thread	Area at Root of Thread
	Square		Hexagon				Length of Bolt								No. of Thrds per Inch			
	Diam. of Flats	Diam. of Corners	Diam. of Flats	Diam. of Corners			1" to 2"	2⅞ to 2½	2⅝ to 3"	3⅝ to 4"	4⅝ to 8"	8⅞ to 12"	12⅞ to 20"					
D	F	C	F	C	H	N	Length of Thread T											
¼	½	11/16	½	5/8	¼	¼	¾	¾	7/8	7/8	1	1	1	20	.185	.027		
⅜	11/8	1	11/8	1 13/16	⅜	⅜	¾	¾	7/8	7/8	1	1	1	16	.294	.068		
½	7/8	1 ¼	7/8	1	7/16	½	1	1	1	1¼	1¼	1½	1½	13	.400	.126		
5/8	1 1/16	1 ½	1 1/16	1 ¼	9/16	5/8	1¼	1¼	1¼	1¼	1½	1¾	2	11	.507	.202		
¾	1 ¼	1 13/16	1 ¼	1 7/16	¾	¾	1½	1½	1½	1½	1¾	2	2	10	.620	.302		
7/8	1 7/16	2 1/16	1 7/16	1 11/16	¾	7/8	1½	1¾	1¾	1¾	2	2¼	2¼	9	.731	.419		
1	1 5/8	2 5/16	1 5/8	1 7/8	13/16	1	...	1¾	1¾	1¾	2¼	2½	2½	8	.838	.551		
1 1/8	1 11/16	2 9/16	1 11/16	2 1/8	15/16	1 1/8	2¼	2¼	2½	3	3	7	.939	.693		
1 ¼	2	2 13/16	2	2 5/16	1	1 ¼	2½	2¾	3	3	7	1.064	.890		
1 ½	2 3/16	3 1/8	2 3/16	2 9/16	1 1/8	1 ½	3¼	3½	3½	6	6	1.158	1.054		
1 ⅝	2 3/8	3 3/8	2 3/8	2 ¾	1 3/16	1 ½	3¾	4	4	4	6	1.283	1.294		
1 ¾	2 9/16	3 5/8	2 9/16	3	1 5/16	1 5/8	4	4¼	4¼	5½	5½	1.389	1.515		
1 7/8	2 ¾	3 7/8	2 ¾	3 3/16	1 3/8	1 ¾	4½	4½	5	5	1.490	1.744		
2	2 15/16	4 3/16	2 15/16	3 7/16	1 ½	1 7/8	4¾	4¾	5	5	1.615	2.049		
2 ¼	3 1/8	4 7/16	3 1/8	3 5/8	1 9/16	2	5	5	4½	4½	1.711	2.300		
2 ½	3 1/2	4 15/16	3 1/2	4 1/16	1 ¾	2 ¼	5½	5½	4½	4½	1.961	3.021		
2 ¾	3 7/8	5 1/2	3 7/8	4 1/2	1 5/8	2 ½	6¼	6¼	4	4	2.175	3.716		
3	4 1/4	6	4 1/4	4 15/16	2 1/8	2 ¾	7	7	4	4	2.425	4.619		
3 ¼	4 5/8	6 9/16	4 5/8	5 3/8	2 5/16	3	7¾	7¾	3½	3½	2.629	5.428		
3 ½	5	7 1/16	5	5 13/16	2 ½	3 ¼	8½	8½	3½	3½	2.879	6.509		
3 ¾	5 5/8	7 5/8	5 3/8	6 1/4	2 11/16	3 ½	9½	9½	3¼	3¼	3.100	7.549		

WEIGHTS PER HUNDRED WITH NUTS

Length of Bolt	SQUARE HEADS AND NUTS										HEXAGON HEADS AND NUTS						
	Diameter of Bolt in Inches										Diameter of Bolt in Inches						
	1/4	5/16	3/8	7/16	1/2	5/8	3/4	7/8	1"		3/8	1/2	5/8	3/4	7/8	1"	
1	4	7	11	15	22	37	56	10	19	33	52
1 1/4	4	7	11	16	23	39	59	11	20	34	54
1 1/2	5	8	12	17	24	41	62	12	22	36	57
1 3/4	5	8	13	18	26	43	64	12	23	38	60
2	5	9	14	19	27	45	67	101	144	13	24	40	63	93	132	154	186
2 1/4	6	9	15	20	28	47	71	104	150	14	26	43	66	97	137	165	197
2 1/2	6	10	15	21	30	49	74	109	155	15	27	45	69	101	143	176	219
2 3/4	6	10	16	22	31	51	77	113	161	16	29	47	72	105	148	186	230
3	7	11	17	24	33	54	80	117	167	16	30	49	75	109	154	197	241
3 1/2	7	12	18	25	35	58	86	126	178	18	33	54	82	118	165	204	254
4	8	13	20	28	38	62	92	134	189	19	35	58	88	126	176	219	274
4 1/2	9	14	21	30	41	66	98	142	198	21	38	62	94	134	186	230	284
5	10	15	23	32	43	71	104	151	209	23	41	66	100	143	197	241	294
5 1/2	10	16	25	34	46	75	111	159	220	24	44	71	106	151	208	254	304
6	11	17	26	36	49	79	117	168	232	26	46	75	112	160	219	274	324
6 1/2	28	38	52	84	123	176	243	27	49	79	119	168	230	284	334
7	29	40	55	88	129	185	254	29	52	84	125	177	241	294	344
8	32	45	60	97	142	202	276	32	58	92	137	194	264	314	354
9	34	49	65	105	154	218	298	35	63	100	149	210	285	324	364
10	53	71	114	167	235	320	...	68	109	162	227	307	354	374
12	61	82	131	192	269	364	...	80	127	187	261	352	394	414
14	93	148	217	303	409	...	91	144	212	295	396	434	454
1" addition	1.4	2.2	3.1	4.3	5.6	8.7	12.5	17.0	22.3	3.1	5.6	8.7	12.5	17.0	22.3	27.3	32.3

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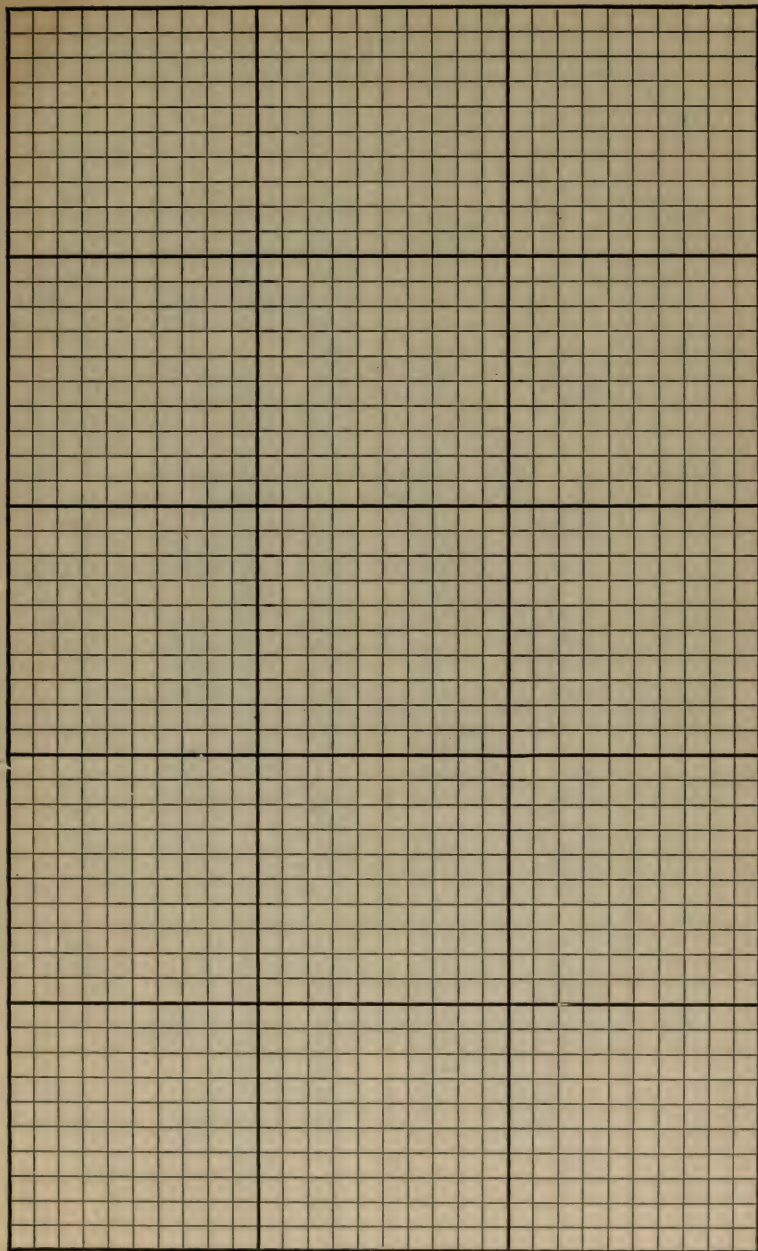
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DECIMALS OF A FOOT

FOR EACH $\frac{1}{16}$ OF AN INCH FROM $\frac{1}{16}$ TO 12 INCHES

Fraction	Decimal	Fraction	Decimal	Fraction	Decimal	Fraction	Decimal
$\frac{1}{16}$	0.0052	$3 \frac{1}{16}$	0.2552	$6 \frac{1}{16}$	0.5052	$9 \frac{1}{16}$	0.7552
$\frac{1}{8}$	0.0104	$3 \frac{1}{8}$	0.2604	$6 \frac{1}{8}$	0.5104	$9 \frac{1}{8}$	0.7604
$\frac{3}{16}$	0.0156	$3 \frac{3}{16}$	0.2656	$6 \frac{3}{16}$	0.5156	$9 \frac{3}{16}$	0.7656
$\frac{1}{4}$	0.0208	$3 \frac{1}{4}$	0.2708	$6 \frac{1}{4}$	0.5208	$9 \frac{1}{4}$	0.7708
$\frac{5}{16}$	0.0260	$3 \frac{5}{16}$	0.2760	$6 \frac{5}{16}$	0.5260	$9 \frac{5}{16}$	0.7760
$\frac{3}{8}$	0.0313	$3 \frac{3}{8}$	0.2813	$6 \frac{3}{8}$	0.5313	$9 \frac{3}{8}$	0.7813
$\frac{7}{16}$	0.0365	$3 \frac{7}{16}$	0.2865	$6 \frac{7}{16}$	0.5365	$9 \frac{7}{16}$	0.7865
$\frac{1}{2}$	0.0417	$3 \frac{1}{2}$	0.2917	$6 \frac{1}{2}$	0.5417	$9 \frac{1}{2}$	0.7917
$\frac{9}{16}$	0.0469	$3 \frac{9}{16}$	0.2969	$6 \frac{9}{16}$	0.5469	$9 \frac{9}{16}$	0.7969
$\frac{5}{8}$	0.0521	$3 \frac{5}{8}$	0.3021	$6 \frac{5}{8}$	0.5521	$9 \frac{5}{8}$	0.8021
$\frac{11}{16}$	0.0573	$3 \frac{11}{16}$	0.3073	$6 \frac{11}{16}$	0.5573	$9 \frac{11}{16}$	0.8073
$\frac{3}{4}$	0.0625	$3 \frac{3}{4}$	0.3125	$6 \frac{3}{4}$	0.5625	$9 \frac{3}{4}$	0.8125
$\frac{13}{16}$	0.0677	$3 \frac{13}{16}$	0.3177	$6 \frac{13}{16}$	0.5677	$9 \frac{13}{16}$	0.8177
$\frac{7}{8}$	0.0729	$3 \frac{7}{8}$	0.3229	$6 \frac{7}{8}$	0.5729	$9 \frac{7}{8}$	0.8229
$\frac{15}{16}$	0.0781	$3 \frac{15}{16}$	0.3281	$6 \frac{15}{16}$	0.5781	$9 \frac{15}{16}$	0.8281
1	0.0833	4	0.3333	7	0.5833	10	0.8333
$1 \frac{1}{16}$	0.0885	$4 \frac{1}{16}$	0.3385	$7 \frac{1}{16}$	0.5885	$10 \frac{1}{16}$	0.8385
$1 \frac{1}{8}$	0.0938	$4 \frac{1}{8}$	0.3438	$7 \frac{1}{8}$	0.5938	$10 \frac{1}{8}$	0.8438
$1 \frac{3}{16}$	0.0990	$4 \frac{3}{16}$	0.3490	$7 \frac{3}{16}$	0.5990	$10 \frac{3}{16}$	0.8490
$1 \frac{1}{4}$	0.1042	$4 \frac{1}{4}$	0.3542	$7 \frac{1}{4}$	0.6042	$10 \frac{1}{4}$	0.8542
$1 \frac{5}{16}$	0.1094	$4 \frac{5}{16}$	0.3594	$7 \frac{5}{16}$	0.6094	$10 \frac{5}{16}$	0.8594
$1 \frac{3}{8}$	0.1146	$4 \frac{3}{8}$	0.3646	$7 \frac{3}{8}$	0.6146	$10 \frac{3}{8}$	0.8646
$1 \frac{7}{16}$	0.1198	$4 \frac{7}{16}$	0.3698	$7 \frac{7}{16}$	0.6198	$10 \frac{7}{16}$	0.8698
$1 \frac{1}{2}$	0.1250	$4 \frac{1}{2}$	0.3750	$7 \frac{1}{2}$	0.6250	$10 \frac{1}{2}$	0.8750
$1 \frac{9}{16}$	0.1302	$4 \frac{9}{16}$	0.3802	$7 \frac{9}{16}$	0.6302	$10 \frac{9}{16}$	0.8802
$1 \frac{5}{8}$	0.1354	$4 \frac{5}{8}$	0.3854	$7 \frac{5}{8}$	0.6354	$10 \frac{5}{8}$	0.8854
$1 \frac{11}{16}$	0.1406	$4 \frac{11}{16}$	0.3906	$7 \frac{11}{16}$	0.6406	$10 \frac{11}{16}$	0.8906
$1 \frac{3}{4}$	0.1458	$4 \frac{3}{4}$	0.3958	$7 \frac{3}{4}$	0.6458	$10 \frac{3}{4}$	0.8958
$1 \frac{13}{16}$	0.1510	$4 \frac{13}{16}$	0.4010	$7 \frac{13}{16}$	0.6510	$10 \frac{13}{16}$	0.9010
$1 \frac{7}{8}$	0.1563	$4 \frac{7}{8}$	0.4063	$7 \frac{7}{8}$	0.6563	$10 \frac{7}{8}$	0.9063
$1 \frac{15}{16}$	0.1615	$4 \frac{15}{16}$	0.4115	$7 \frac{15}{16}$	0.6615	$10 \frac{15}{16}$	0.9115
2	0.1667	5	0.4167	8	0.6667	11	0.9167
$2 \frac{1}{16}$	0.1719	$5 \frac{1}{16}$	0.4219	$8 \frac{1}{16}$	0.6719	$11 \frac{1}{16}$	0.9219
$2 \frac{1}{8}$	0.1771	$5 \frac{1}{8}$	0.4271	$8 \frac{1}{8}$	0.6771	$11 \frac{1}{8}$	0.9271
$2 \frac{3}{16}$	0.1823	$5 \frac{3}{16}$	0.4323	$8 \frac{3}{16}$	0.6823	$11 \frac{3}{16}$	0.9323
$2 \frac{1}{4}$	0.1875	$5 \frac{1}{4}$	0.4375	$8 \frac{1}{4}$	0.6875	$11 \frac{1}{4}$	0.9375
$2 \frac{5}{16}$	0.1927	$5 \frac{5}{16}$	0.4427	$8 \frac{5}{16}$	0.6927	$11 \frac{5}{16}$	0.9427
$2 \frac{3}{8}$	0.1979	$5 \frac{3}{8}$	0.4479	$8 \frac{3}{8}$	0.6979	$11 \frac{3}{8}$	0.9479
$2 \frac{7}{16}$	0.2031	$5 \frac{7}{16}$	0.4531	$8 \frac{7}{16}$	0.7031	$11 \frac{7}{16}$	0.9531
$2 \frac{1}{2}$	0.2083	$5 \frac{1}{2}$	0.4583	$8 \frac{1}{2}$	0.7083	$11 \frac{1}{2}$	0.9583
$2 \frac{9}{16}$	0.2135	$5 \frac{9}{16}$	0.4635	$8 \frac{9}{16}$	0.7135	$11 \frac{9}{16}$	0.9635
$2 \frac{5}{8}$	0.2188	$5 \frac{5}{8}$	0.4688	$8 \frac{5}{8}$	0.7188	$11 \frac{5}{8}$	0.9688
$2 \frac{11}{16}$	0.2240	$5 \frac{11}{16}$	0.4740	$8 \frac{11}{16}$	0.7240	$11 \frac{11}{16}$	0.9740
$2 \frac{3}{4}$	0.2292	$5 \frac{3}{4}$	0.4792	$8 \frac{3}{4}$	0.7292	$11 \frac{3}{4}$	0.9792
$2 \frac{13}{16}$	0.2344	$5 \frac{13}{16}$	0.4844	$8 \frac{13}{16}$	0.7344	$11 \frac{13}{16}$	0.9844
$2 \frac{7}{8}$	0.2396	$5 \frac{7}{8}$	0.4896	$8 \frac{7}{8}$	0.7396	$11 \frac{7}{8}$	0.9896
$2 \frac{15}{16}$	0.2448	$5 \frac{15}{16}$	0.4948	$8 \frac{15}{16}$	0.7448	$11 \frac{15}{16}$	0.9948
3	0.2500	6	0.5000	9	0.7500	12	1.0000

DECIMALS OF AN INCH

FOR EACH $\frac{1}{64}$ TH.

Fractions	Decimals	Fractions	Decimals
$\frac{1}{64}$	0.015625	$\frac{33}{64}$	0.515625
$\frac{1}{32}$	0.03125	$\frac{17}{32}$	0.53125
$\frac{3}{64}$	0.046875	$\frac{35}{64}$	0.546875
$\frac{1}{16}$	0.0625	$\frac{9}{16}$	0.5625
$\frac{5}{64}$	0.078125	$\frac{37}{64}$	0.578125
$\frac{3}{32}$	0.09375	$\frac{19}{32}$	0.59375
$\frac{7}{64}$	0.109375	$\frac{39}{64}$	0.609375
$\frac{1}{8}$	0.125	$\frac{5}{8}$	0.625
$\frac{9}{64}$	0.140625	$\frac{41}{64}$	0.640625
$\frac{5}{32}$	0.15625	$\frac{21}{32}$	0.65625
$\frac{11}{64}$	0.171875	$\frac{43}{64}$	0.671875
$\frac{3}{16}$	0.1875	$\frac{11}{16}$	0.6875
$\frac{13}{64}$	0.203125	$\frac{45}{64}$	0.703125
$\frac{7}{32}$	0.21875	$\frac{23}{32}$	0.71875
$\frac{15}{64}$	0.234375	$\frac{47}{64}$	0.734375
$\frac{1}{4}$	0.250	$\frac{3}{4}$	0.750
$\frac{17}{64}$	0.265625	$\frac{49}{64}$	0.765625
$\frac{9}{32}$	0.28125	$\frac{25}{32}$	0.78125
$\frac{19}{64}$	0.296875	$\frac{51}{64}$	0.796875
$\frac{5}{16}$	0.3125	$\frac{13}{16}$	0.8125
$\frac{21}{64}$	0.328125	$\frac{53}{64}$	0.828125
$\frac{11}{32}$	0.34375	$\frac{27}{32}$	0.84375
$\frac{23}{64}$	0.359375	$\frac{55}{64}$	0.859375
$\frac{3}{8}$	0.375	$\frac{7}{8}$	0.875
$\frac{25}{64}$	0.390625	$\frac{57}{64}$	0.890625
$\frac{13}{32}$	0.40625	$\frac{29}{32}$	0.90625
$\frac{27}{64}$	0.421875	$\frac{59}{64}$	0.921875
$\frac{7}{16}$	0.4375	$\frac{15}{16}$	0.9375
$\frac{29}{64}$	0.453125	$\frac{61}{64}$	0.953125
$\frac{15}{32}$	0.46875	$\frac{31}{32}$	0.96875
$\frac{31}{64}$	0.484375	$\frac{63}{64}$	0.984375
$\frac{1}{2}$	0.500	1"	1.000

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